

Comune di Nole
Citta' Metropolitana di Torino

Progetto di ristrutturazione ed adeguamento
igienico funzionale ed impiantistico
dell'edificio comunale denominato ex scuole
di Vauda di Via Ponte Masino 1
I° Lotto

PROGETTO ESECUTIVO

Relazione di calcolo consolidamento edificio esistente

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DATA: Dicembre 2018

ELABORATO

E' vietata qualsiasi riproduzione non autorizzata.

S8



**VERIFICA STATICA E SISMICA DELL'EDIFICIO COMUNALE EX SCUOLE DI
VAUDA – VIA PONTE MASINO 1 - COMUNE DI NOLE (TO)
ANALISI DELLO STATO DI FATTO**

**Relazione di calcolo strutturale impostata e redatta secondo le modalità
previste nel D.M. 17 Gennaio 2018 cap. 10 “Redazione dei progetti
strutturali esecutivi e delle relazioni di calcolo”.**

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D.M. 17/01/18 cap. 10.2 Affidabilità dei codici utilizzati

<https://www.2si.it/it/prodotti/affidabilita/>

INTESTAZIONE E CONTENUTI DELLA RELAZIONE

Progetto

La seguente relazione sintetizza i risultati della verifica statica e sismica dell'edificio in oggetto, attualmente non in uso ma nel passato sede di una scuola comunale. Nell'ottica di una futura riutilizzazione con la medesima destinazione di uso scolastico, è stata eseguita una analisi dinamica lineare ai sensi delle Norme Tecniche per le Costruzioni (NTC 2018) di cui al D.M. 17/01/2018 per valutare la sicurezza sismica della struttura quale edificio ad uso scolastico nella situazione attuale (stato di fatto). Pertanto è stata data all'edificio una destinazione d'uso a classe III ai sensi del par. 2.4.2 e vita nominale 50 anni ai sensi del 2.4.1 delle NTC 2018. L'edificio è sotto vincolo della Soprintendenza ai Beni Architettonici del Piemonte.

La verifica oggetto di questa relazione riguarda solamente la parte di edificio originario in muratura portante, poiché l'ampliamento con telaio in c.a. e tamponamenti sarà oggetto di demolizione e ricostruzione. La parte originaria ha struttura portante in muratura con due diverse tessiture: in mattoni e malta cementizia di buona qualità per quanto riguarda l'ossatura portante, e con mattoni forati per le restanti parti (prevalentemente vano scale e parete di confine con ampliamento). I solai sono in laterocemento e la copertura con struttura lignea. In minima parte sono presenti anche travi a telaio in c.a.

Le strutture sono state oggetto di una campagna di prove su tutti i materiali, i cui risultati convergono con i valori medi delle tipologie murarie presenti nella tabella C8A.2.1. della Circolare di applicazione alle NTC 2008. L'estensione delle prove permette di quantificare il livello di conoscenza pari a LC2 (con fattore di confidenza = 1,2).

I risultati dell'analisi dinamica lineare evidenziano che anche solo all'1% dell'accelerazione attesa al suolo l'edificio in oggetto, nella sua parte strutturale originaria, non possiede le capacità dissipative e strutturali per resistere all'azione sismica.

Contenuti della relazione:

RELAZIONE DI CALCOLO STRUTTURALE

- Origine e Caratteristiche dei Codici di Calcolo

- Affidabilità dei codici utilizzati

- Validazione dei codici

- Tipo di analisi svolta

- Modalità di presentazione dei risultati

- Informazioni generali sull'elaborazione

- Giudizio motivato di accettabilità dei risultati

STAMPA DEI DATI DI INGRESSO

- Normative prese a riferimento

- Criteri adottati per le misure di sicurezza

- Criteri seguiti nella schematizzazione della struttura, dei vincoli e delle sconnessioni

- Interazione tra terreno e struttura

- Legami costitutivi adottati per la modellazione dei materiali e dei terreni

- Schematizzazione delle azioni, condizioni e combinazioni di carico

- Metodologie numeriche utilizzate per l'analisi strutturale

- Metodologie numeriche utilizzate per la progettazione e la verifica degli elementi strutturali

STAMPA DEI RISULTATI

Il Progettista:

Ing. Giovanni Data



17 December 2018

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RELAZIONE DI CALCOLO STRUTTURALE

Premessa

La presente relazione di calcolo strutturale, in conformità al §10.1 del DM 17/01/18, è comprensiva di una descrizione generale dell'opera e dei criteri generali di analisi e verifica. Segue inoltre le indicazioni fornite al §10.2 del DM stesso per quanto concerne analisi e verifiche svolte con l'ausilio di codici di calcolo.

Nella presente parte sono riportati i principali elementi di inquadramento del progetto esecutivo riguardante le strutture, in relazione agli strumenti urbanistici, al progetto architettonico, al progetto delle componenti tecnologiche in generale ed alle prestazioni attese dalla struttura.

Analisi storico-critica ed esito del rilievo geometrico-strutturale

Per edifici esistenti, in coerenza con il paragrafo 8.2 delle NTC-18, l'analisi storico-critica ed il rilievo geometrico-strutturale devono evidenziare i seguenti aspetti: (a) la costruzione riflette lo stato delle conoscenze al tempo della sua realizzazione; (b) possono essere insiti e non palesi difetti di impostazione e di realizzazione; (c) la costruzione può essere stata soggetta ad azioni, anche eccezionali, i cui effetti non siano completamente manifesti; (d) le strutture possono presentare degrado e/o modificazioni significative rispetto alla situazione originaria.

Analisi storico-critica

Per edifici esistenti, viene indicata la documentazione reperita e vengono esplicitate le informazioni desunte da ciascuno dei documenti esaminati per le finalità indicate al paragrafo 8.5.1 delle NTC-18.

Esito del rilievo geometrico-strutturale

Per edifici esistenti, vengono descritte le modalità con cui è stato effettuato il rilievo geometrico strutturale e gli esiti di quest'ultimo, anche con riferimenti espliciti e puntuali agli elaborati grafici che saranno riportati nella parte "4.1. Rilievo geometrico-strutturale". Il rilievo delle strutture deve essere eseguito e restituito secondo le modalità e con le finalità riportate nei paragrafi 8.5.2 e 8.7 delle NTC-18.

Descrizione generale dell'opera

La seguente relazione sintetizza i risultati della verifica statica e sismica dell'edificio in oggetto, attualmente non in uso ma nel passato sede di una scuola comunale. Nell'ottica di una futura riutilizzazione con la medesima destinazione di uso scolastico, è stata eseguita una analisi dinamica lineare ai sensi delle Norme Tecniche per le Costruzioni (NTC 2018) di cui al D.M. 17/01/2018 per valutare la sicurezza sismica della struttura quale edificio ad uso scolastico nella situazione attuale (stato di fatto). Pertanto è stata data all'edificio una destinazione d'uso a classe III ai sensi del par. 2.4.2 e vita nominale 50 anni ai sensi del 2.4.1 delle NTC 2018. L'edificio è sotto vincolo della Soprintendenza ai Beni Architettonici del Piemonte.

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I risultati dell'analisi dinamica lineare evidenziano che anche solo all'1% dell'accelerazione attesa al suolo l'edificio in oggetto, nella sua parte strutturale originaria, non possiede le capacità dissipative e strutturali per resistere all'azione sismica.

Descrizione generale dell'opera	
Fabbricato ad uso	Scuola
Ubicazione	Comune di NOLE (TO) (Regione PIEMONTE)
	Località NOLE (TO)
	Longitudine 7.572, Latitudine 45.244
Numero di piani	Fuori terra: 2
	Interrati: 1
	le dimensioni dell'opera in pianta sono racchiuse in un rettangolo di 11 x 12 m
Numero vani scale	1
Numero vani ascensore	0
Tipo di fondazione	Pareti in c.a.

Principali caratteristiche della struttura	
Struttura regolare in pianta	SI
Struttura regolare in altezza	SI
Classe di duttilità	BD
Travi: ricalate o in spessore	Ricalcate
Pilastrì	SI
Pilastrì in falso	NO
Tipo di fondazione	Pareti in c.a.
Condizioni per cui è necessario considerare	NO

la componente verticale del sisma	
-----------------------------------	--

Parametri della struttura			
Classe d'uso	Vita Vn [anni]	Coeff. Uso	Periodo Vr [anni]
III	50.0	1.5	75.0

Fattore di struttura
Ai sensi del par. 7.2.1. delle NTC 2018 l'edificio in oggetto può essere classificato come regolare sia in pianta che in altezza, e pertanto il fattore di struttura $q=3,4$.

Quadro normativo di riferimento adottato

Le norme ed i documenti assunti quale riferimento per la progettazione strutturale vengono indicati di seguito. Nel capitolo "normativa di riferimento" è comunque presente l'elenco completo delle normative disponibili.

Progetto-verifica degli elementi	
Progetto cemento armato	D.M. 09-01-1996
Progetto acciaio	D.M. 14-01-2008
Progetto legno	D.M. 14-01-2008
Progetto muratura	D.M. 20-11-1987
Azione sismica	
Norma applicata per l'azione sismica	D.M. 17-01-2018

Livelli di conoscenza e fattori di confidenza

Il livello di conoscenza, per edifici esistenti è LC2
Pertanto il fattore di confidenza è 1,2

Azioni di progetto sulla costruzione

Nei capitoli "modellazione delle azioni" e "schematizzazione dei casi di carico" sono indicate le azioni sulla costruzioni.

Nel prosieguo si indicano tipo di analisi strutturale condotta (statico,dinamico, lineare o non lineare) e il metodo adottato per la risoluzione del problema strutturale nonché le metodologie seguite per la verifica o per il progetto-verifica delle sezioni. Si riportano le combinazioni di carico adottate e, nel caso di calcoli non lineari, i percorsi di carico seguiti; le configurazioni studiate per la struttura in esame *sono risultate effettivamente esaustive per la progettazione-verifica*.

La verifica della sicurezza degli elementi strutturali avviene con i metodi della scienza delle costruzioni. L'analisi strutturale è condotta con il metodo degli spostamenti per la valutazione dello stato tensodeformativo indotto da carichi statici. L'analisi strutturale è condotta con il metodo dell'analisi modale e dello spettro di risposta in termini di accelerazione per la valutazione dello stato tensodeformativo indotto da carichi dinamici (tra cui quelli di tipo sismico).

L'analisi strutturale viene effettuata con il metodo degli elementi finiti. Il metodo sopraindicato si basa sulla schematizzazione della struttura in elementi connessi solo in corrispondenza di un numero prefissato di punti denominati nodi. I nodi sono definiti dalle tre coordinate cartesiane in un sistema di riferimento globale. Le incognite del problema (nell'ambito del metodo degli spostamenti) sono le componenti di spostamento dei nodi riferite al sistema di riferimento globale (traslazioni secondo X, Y, Z, rotazioni attorno X, Y, Z). La soluzione del problema si ottiene con un sistema di equazioni algebriche lineari i cui termini noti sono costituiti dai carichi agenti sulla struttura opportunamente concentrati ai nodi:

$$\mathbf{K} \cdot \mathbf{u} = \mathbf{F} \text{ dove } \begin{array}{l} \mathbf{K} = \text{matrice di rigidezza} \\ \mathbf{u} = \text{vettore spostamenti nodali} \\ \mathbf{F} = \text{vettore forze nodali} \end{array}$$

Dagli spostamenti ottenuti con la risoluzione del sistema vengono quindi dedotte le sollecitazioni e/o le tensioni di ogni elemento, riferite generalmente ad una terna locale all'elemento stesso.

Il sistema di riferimento utilizzato è costituito da una terna cartesiana destrorsa XYZ. Si assume l'asse Z verticale ed orientato verso l'alto.

Gli elementi utilizzati per la modellazione dello schema statico della struttura sono i seguenti:

Elemento tipo TRUSS	(biella-D2)
Elemento tipo BEAM	(trave-D2)
Elemento tipo MEMBRANE	(membrana-D3)
Elemento tipo PLATE	(piastra-guscio-D3)
Elemento tipo BOUNDARY	(molla)
Elemento tipo STIFFNESS	(matrice di rigidezza)
Elemento tipo BRICK	(elemento solido)
Elemento tipo SOLAIO	(macro elemento composto da più membrane)

Modello numerico

In questa parte viene descritto il modello numerico utilizzato (o i modelli numerici utilizzati) per l'analisi della struttura. La presentazione delle informazioni deve essere, coerentemente con le prescrizioni del paragrafo 10.2 e relativi sottoparagrafi delle NTC-18, tale da garantirne la leggibilità, la corretta interpretazione e la riproducibilità

Tipo di analisi strutturale	
Statica lineare	SI
Statica non lineare	NO
Sismica statica lineare	NO
Sismica dinamica lineare	SI
Sismica statica non lineare (prop. masse)	NO
Sismica statica non lineare (prop. modo)	NO
Sismica statica non lineare (triangolare)	NO
Non linearità geometriche (fattore P delta)	NO

Di seguito si indicano l'origine e le caratteristiche dei codici di calcolo utilizzati riportando titolo, produttore e distributore, versione, estremi della licenza d'uso:

Informazioni sul codice di calcolo	
Titolo:	PRO_SAP PROfessional Structural Analysis Program
Versione:	PROFESSIONAL (build 2018-07-183)
Produttore-Distributore:	2S.I. Software e Servizi per l'Ingegneria s.r.l., Ferrara
Dati utente finale:	In.Ar.Te. Torino S.r.l.
Codice Utente:	
Codice Licenza:	Licenza dsi4017

Un attento esame preliminare della documentazione a corredo del software **ha consentito di valutarne l'affidabilità e soprattutto l'idoneità al caso specifico**. La documentazione, fornita dal produttore e distributore del software, contiene una esauriente descrizione delle basi teoriche e degli algoritmi impiegati, l'individuazione dei campi d'impiego, nonché casi prova interamente risolti e commentati, corredati dei file di input necessari a riprodurre l'elaborazione:

Affidabilità dei codici utilizzati	
2S.I. ha verificato l'affidabilità e la robustezza del codice di calcolo attraverso un numero significativo di casi prova in cui i risultati dell'analisi numerica sono stati confrontati con soluzioni teoriche. E' possibile reperire la documentazione contenente alcuni dei più significativi casi trattati al seguente link: http://www.2si.it/Software/Affidabilità.htm	

Modellazione della geometria e proprietà meccaniche:	
nodi	3356
elementi D2 (per aste, travi, pilastri...)	352
elementi D3 (per pareti, platee, gusci...)	2953
elementi solaio	36
elementi solidi	0
Dimensione del modello strutturale [cm]:	
X min =	-636.36
Xmax =	528.64
Ymin =	-334.97
Ymax =	903.53
Zmin =	-315.00

Zmax =	1340.00
Strutture verticali:	
Elementi di tipo asta	NO
Pilastrì	SI
Pareti	SI
Setti (a comportamento membranale)	NO
Strutture non verticali:	
Elementi di tipo asta	SI
Travi	SI
Gusci	NO
Membrane	NO
Orizzontamenti:	
Solai con la proprietà piano rigido	SI
Solai senza la proprietà piano rigido	SI
Tipo di vincoli:	
Nodi vincolati rigidamente	SI
Nodi vincolati elasticamente	NO
Nodi con isolatori sismici	NO
Fondazioni puntuali (plinti/plinti su palo)	NO
Fondazioni di tipo trave	NO
Fondazioni di tipo platea	NO
Fondazioni con elementi solidi	NO

Modellazione delle azioni

Si veda il capitolo **“Schematizzazione dei casi di carico”** per le informazioni necessarie alla comprensione ed alla ricostruzione delle azioni applicate al modello numerico, coerentemente con quanto indicato nella parte *“2.6. Azioni di progetto sulla costruzione”*.

Combinazioni e/o percorsi di carico

Si veda il capitolo **“Definizione delle combinazioni”** in cui sono indicate le combinazioni di carico adottate e, nel caso di calcoli non lineari, i percorsi di carico seguiti.

Combinazioni dei casi di carico	
APPROCCIO PROGETTUALE	Approccio 2
Tensioni ammissibili	NO
SLU	SI
SLV (SLU con sisma)	SI
SLC	NO
SLD	SI
SLO	NO
SLU GEO A2 (per approccio 1)	NO
SLU EQU	NO
Combinazione caratteristica (rara)	NO
Combinazione frequente	NO
Combinazione quasi permanente (SLE)	NO
SLA (accidentale quale incendio)	NO

Principali risultati
I risultati devono costituire una sintesi completa ed efficace, presentata in modo da riassumere il comportamento della struttura, per ogni tipo di analisi svolta.
2.8.1. Risultati dell'analisi modale
Viene riportato il tipo di analisi modale condotta, restituiti i risultati della stessa e valutate le informazioni desumibili in merito al comportamento della struttura.

2.8.2. Deformate e sollecitazioni per condizioni di carico

Vengono riportati i principali risultati atti a descrivere il comportamento della struttura, in termini di stati di sollecitazione e di deformazione generalizzata, distinti per condizione elementare di carico o per combinazioni omogenee delle stesse.

2.8.3. Involuppo delle sollecitazioni maggiormente significative. L'analisi e la restituzione degli involuppi (nelle combinazioni considerate agli SLU e agli SLE) delle caratteristiche di sollecitazione devono essere finalizzate alla valutazione dello stato di sollecitazione nei diversi elementi della struttura.

2.8.4. Reazioni vincolari

Vengono riportate le reazioni dei vincoli nelle singole condizioni di carico e/o nelle combinazioni considerate.

2.8.5. Altri risultati significativi

Nella presente parte vengono riportati tutti gli altri risultati che il progettista ritiene di interesse per la descrizione e la comprensione del/i modello/i e del comportamento della struttura.

La presente relazione, oltre ad illustrare in modo esaustivo i dati in ingresso ed i risultati delle analisi in forma tabellare, riporta una serie di immagini:

per i dati in ingresso:

- modello solido della struttura
- numerazione di nodi e ed elementi
- configurazioni di carico statiche
- configurazioni di carico sismiche con baricentri delle masse e eccentricità

per le combinazioni più significative (statisticamente più gravose per la struttura):

- configurazioni deformate
- diagrammi e involuppi delle azioni interne
- mappe delle tensioni
- reazioni vincolari
- mappe delle pressioni sul terreno

per il progetto-verifica degli elementi:

- diagrammi di armatura
- percentuali di sfruttamento
- mappe delle verifiche più significative per i vari stati limite

Informazioni generali sull'elaborazione e giudizio motivato di accettabilità dei risultati.

Il programma prevede una serie di controlli automatici (check) che consentono l'individuazione di errori di modellazione. Al termine dell'analisi un controllo automatico identifica la presenza di spostamenti o rotazioni anormali. Si può pertanto asserire che l'elaborazione sia corretta e completa. I risultati delle elaborazioni sono stati sottoposti a controlli che ne comprovano l'attendibilità. Tale valutazione ha compreso il confronto con i risultati di semplici calcoli, eseguiti con metodi tradizionali e adottati, anche in fase di primo proporzionamento della struttura. Inoltre, sulla base di considerazioni riguardanti gli stati tensionali e deformativi determinati, si è valutata la validità delle scelte operate in sede di schematizzazione e di modellazione della struttura e delle azioni. Si allega al termine della presente relazione elenco sintetico dei controlli svolti (verifiche di equilibrio tra reazioni vincolari e carichi applicati, comparazioni tra i risultati delle analisi e quelli di valutazioni semplificate, etc.) .

Verifiche agli stati limite ultimi

Nel capitolo relativo alla progettazione degli elementi strutturali agli SLU vengono indicate, con riferimento alla normativa adottata, le modalità ed i criteri seguiti per valutare la sicurezza della struttura nei confronti delle possibili situazioni di crisi ed i risultati delle valutazioni svolte. In via generale, oltre alle verifiche di resistenza e di spostamento, devono essere prese in considerazione verifiche nei confronti dei fenomeni di instabilità, locale e globale, di fatica, di duttilità, di degrado.

Verifiche agli stati limite di esercizio

Nel capitolo relativo alla progettazione degli elementi strutturali agli SLU vengono indicate, con riferimento alla normativa adottata, le modalità seguite per valutare l'affidabilità della struttura nei confronti delle possibili situazioni di perdita di funzionalità (per eccessive deformazioni, fessurazioni, vibrazioni, etc.) ed i risultati delle valutazioni svolte.

RELAZIONE SUI MATERIALI

Il capitolo Materiali riporta informazioni esaustive relative all'elenco dei materiali impiegati e loro modalità di posa in opera e ai valori di calcolo.

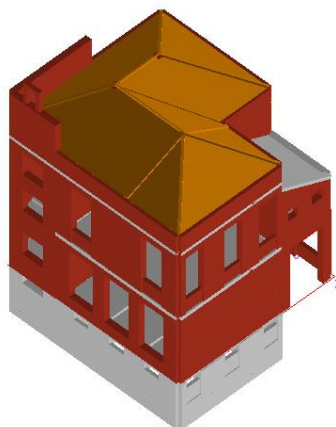
NORMATIVA DI RIFERIMENTO

1. D.Min. Infrastrutture Min. Interni e Prot. Civile 17 Gennaio 2018 e allegate "Norme tecniche per le costruzioni".
2. D.Min. Infrastrutture Min. Interni e Prot. Civile 14 Gennaio 2008 e allegate "Norme tecniche per le costruzioni".
3. D.Min. Infrastrutture e trasporti 14 Settembre 2005 e allegate "Norme tecniche per le costruzioni".
4. D.M. LL.PP. 9 Gennaio 1996 "Norme tecniche per il calcolo, l'esecuzione ed il collaudo delle strutture in cemento armato, normale e precompresso e per le strutture metalliche".
5. D.M. LL.PP. 16 Gennaio 1996 "Norme tecniche relative ai <<Criteri generali per la verifica di sicurezza delle costruzioni e dei carichi e sovraccarichi>>".
6. D.M. LL.PP. 16 Gennaio 1996 "Norme tecniche per le costruzioni in zone sismiche".
7. Circolare 4/07/96, n.156AA.GG./STC. istruzioni per l'applicazione delle "Norme tecniche relative ai <<Criteri generali per la verifica di sicurezza delle costruzioni e dei carichi e sovraccarichi>>" di cui al D.M. 16/01/96.
8. Circolare 10/04/97, n.65AA.GG. istruzioni per l'applicazione delle "Norme tecniche per le costruzioni in zone sismiche" di cui al D.M. 16/01/96.
9. D.M. LL.PP. 20 Novembre 1987 "Norme tecniche per la progettazione, esecuzione e collaudo degli edifici in muratura e per il loro consolidamento".
10. Circolare 4 Gennaio 1989 n. 30787 "Istruzioni in merito alle norme tecniche per la progettazione, esecuzione e collaudo degli edifici in muratura e per il loro consolidamento".
11. D.M. LL.PP. 11 Marzo 1988 "Norme tecniche riguardanti le indagini sui terreni e sulle rocce, la stabilità dei pendii naturali e delle scarpate, i criteri generali e le prescrizioni per la progettazione, l'esecuzione e il collaudo delle opere di sostegno delle terre e delle opere di fondazione".
12. D.M. LL.PP. 3 Dicembre 1987 "Norme tecniche per la progettazione, esecuzione e collaudo delle costruzioni prefabbricate".
13. UNI 9502 - Procedimento analitico per valutare la resistenza al fuoco degli elementi costruttivi di conglomerato cementizio armato, normale e precompresso - edizione maggio 2001
14. Ordinanza del Presidente del Consiglio dei Ministri n. 3274 del 20 marzo 2003 "Primi elementi in materia di criteri generali per la classificazione sismica del territorio nazionale e di normative tecniche per le costruzioni in zona sismica" e successive modificazioni e integrazioni.
15. UNI EN 1990:2006 13/04/2006 Eurocodice 0 - Criteri generali di progettazione strutturale.
16. UNI EN 1991-1-1:2004 01/08/2004 Eurocodice 1 - Azioni sulle strutture - Parte 1-1: Azioni in generale - Pesì per unità di volume, pesì propri e sovraccarichi per gli edifici.
17. UNI EN 1991-2:2005 01/03/2005 Eurocodice 1 - Azioni sulle strutture - Parte 2: Carichi da traffico sui ponti.
18. UNI EN 1991-1-3:2004 01/10/2004 Eurocodice 1 - Azioni sulle strutture - Parte 1-3: Azioni in generale - Carichi da neve.
19. UNI EN 1991-1-4:2005 01/07/2005 Eurocodice 1 - Azioni sulle strutture - Parte 1-4: Azioni in generale - Azioni del vento.
20. UNI EN 1991-1-5:2004 01/10/2004 Eurocodice 1 - Azioni sulle strutture - Parte 1-5: Azioni in generale - Azioni termiche.
21. UNI EN 1992-1-1:2005 24/11/2005 Eurocodice 2 - Progettazione delle strutture di calcestruzzo - Parte 1-1: Regole generali e regole per gli edifici.
22. UNI EN 1992-1-2:2005 01/04/2005 Eurocodice 2 - Progettazione delle strutture di calcestruzzo - Parte 1-2: Regole generali - Progettazione strutturale contro l'incendio.
23. UNI EN 1993-1-1:2005 01/08/2005 Eurocodice 3 - Progettazione delle strutture di acciaio - Parte 1-1: Regole generali e regole per gli edifici.
24. UNI EN 1993-1-8:2005 01/08/2005 Eurocodice 3 - Progettazione delle strutture di acciaio - Parte 1-8: Progettazione dei collegamenti.
25. UNI EN 1994-1-1:2005 01/03/2005 Eurocodice 4 - Progettazione delle strutture composte acciaio-calcestruzzo - Parte 1-1: Regole generali e regole per gli edifici.
26. UNI EN 1994-2:2006 12/01/2006 Eurocodice 4 - Progettazione delle strutture composte acciaio-calcestruzzo - Parte 2: Regole generali e regole per i ponti.
27. UNI EN 1995-1-1:2005 01/02/2005 Eurocodice 5 - Progettazione delle strutture di legno - Parte 1-1: Regole generali - Regole comuni e regole per gli edifici.
28. UNI EN 1995-2:2005 01/01/2005 Eurocodice 5 - Progettazione delle strutture di legno - Parte 2: Ponti.
29. UNI EN 1996-1-1:2006 26/01/2006 Eurocodice 6 - Progettazione delle strutture di muratura - Parte 1-1: Regole generali per strutture di muratura armata e non armata.
30. UNI EN 1996-3:2006 09/03/2006 Eurocodice 6 - Progettazione delle strutture di muratura - Parte 3: Metodi di calcolo semplificato per strutture di muratura non armata.
31. UNI EN 1997-1:2005 01/02/2005 Eurocodice 7 - Progettazione geotecnica - Parte 1: Regole generali.
32. UNI EN 1998-1:2005 01/03/2005 Eurocodice 8 - Progettazione delle strutture per la resistenza sismica - Parte 1: Regole generali, azioni sismiche e regole per gli edifici.
33. UNI EN 1998-3:2005 01/08/2005 Eurocodice 8 - Progettazione delle strutture per la resistenza sismica - Parte 3: Valutazione e adeguamento degli edifici.
34. UNI EN 1998-5:2005 01/01/2005 Eurocodice 8 - Progettazione delle strutture per la resistenza sismica - Parte 5: Fondazioni, strutture di contenimento ed aspetti geotecnici.

NOTA sul capitolo "normativa di riferimento": riporta l'elenco delle normative implementate nel software. Le norme utilizzate per la struttura oggetto della presente relazione sono indicate nel precedente capitolo "RELAZIONE DI CALCOLO STRUTTURALE" "ANALISI E VERIFICHE SVOLTE CON L'AUSILIO DI CODICI DI CALCOLO". Laddove nei capitoli successivi vengano richiamate norme antecedenti al DM 17.01.08 è dovuto o a progettazione simulata di edificio esistente.

In attesa della pubblicazione della circolare di istruzione per l'applicazione delle Norme Tecniche delle Costruzioni del 17 gennaio 2018 viene utilizzata la CIRCOLARE esplicativa n. 617 del 2 febbraio 2009, "Istruzioni per l'applicazione delle «Nuove norme tecniche per le costruzioni» di cui al decreto ministeriale 14 gennaio 2008".

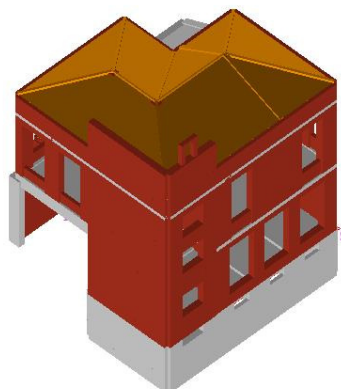
MODELLO



Scuola esistente Nole_50 anni 1%

vista 3D

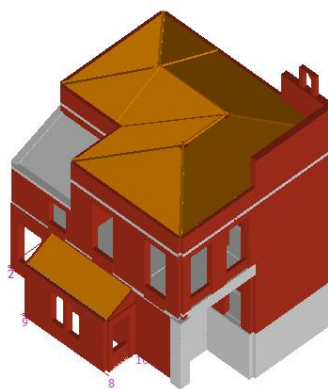
MODELLO



Scuola esistente Nole_50 anni 1%

vista 3D

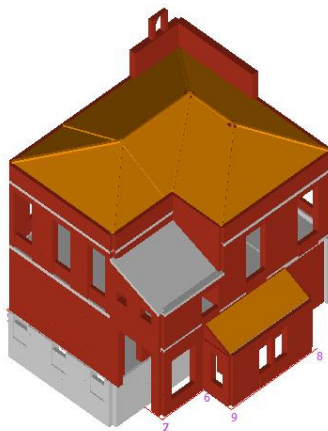
MODELLO



Scuola esistente Nole_50 anni 1%

vista 3D

MODELLO



Scuola esistente Nole_50 anni 1%

vista 3D

CARATTERISTICHE MATERIALI UTILIZZATI

LEGENDA TABELLA DATI MATERIALI

Il programma consente l'uso di materiali diversi. Sono previsti i seguenti tipi di materiale:

1	materiale tipo cemento armato
2	materiale tipo acciaio
3	materiale tipo muratura
4	materiale tipo legno
5	materiale tipo generico

I materiali utilizzati nella modellazione sono individuati da una sigla identificativa ed un codice numerico (gli elementi strutturali richiamano quest'ultimo nella propria descrizione). Per ogni materiale vengono riportati in tabella i seguenti dati:

Young	modulo di elasticità normale
Poisson	coefficiente di contrazione trasversale
G	modulo di elasticità tangenziale
Gamma	peso specifico
Alfa	coefficiente di dilatazione termica

I dati soprariportati vengono utilizzati per la modellazione dello schema statico e per la determinazione dei carichi inerziali e termici. In relazione al tipo di materiale vengono riportati inoltre:

1	cemento armato	Rck Fctm	resistenza caratteristica cubica resistenza media a trazione semplice
2	acciaio	Ft Fy Fd Fdt Sadm Sadmt	tensione di rottura a trazione tensione di snervamento resistenza di calcolo resistenza di calcolo per spess. t>40 mm tensione ammissibile tensione ammissibile per spess. t>40 mm
3	muratura	Resist. Fk Resist. Fvko	resistenza caratteristica a compressione resistenza caratteristica a taglio
4	legno	Resist. fc0k Resist. ft0k Resist. fmk Resist. fvk Modulo E0,05 Lamellare	Resistenza caratteristica (tensione amm. per REGLES) per compressione Resistenza caratteristica (tensione amm. per REGLES) per trazione Resistenza caratteristica (tensione amm. per REGLES) per flessione Resistenza caratteristica (tensione amm. per REGLES) per taglio Modulo elastico parallelo caratteristico lamellare o massiccio

Vengono inoltre riportate le tabelle contenenti il riassunto delle informazioni assegnate nei criteri di progetto in uso.

Con riferimento al **Documento di Affidabilità** "Test di validazione del software di calcolo PRO_SAP e dei moduli aggiuntivi PRO_SAP Modulo Geotecnico, PRO_CAD nodi acciaio e PRO_MST" - versione Maggio 2011, disponibile per il download sul sito www.2si.it, si segnalano i seguenti esempi applicativi:

Modellazione di strutture in c.a.

Test N°	Titolo
41	GERARCHIA DELLE RESISTENZE PER TRAVI IN C.A.
42	GERARCHIA DELLE RESISTENZE PER PILASTRI IN C.A.
43	VERIFICA ALLE T.A. DI STRUTTURE IN C.A.
44	VERIFICA AGLI SLU DI STRUTTURE IN C.A.
45	VERIFICA A PUNZONAMENTO ALLO SLU DI PIASTRE IN C.A.
46	VERIFICA A PUNZONAMENTO ALLO SLU DI TRAVI IN C.A.
47	PROGETTAZIONE A TAGLIO DI STRUTTURE IN C.A. SECONDO IL D.M. 9/1/96
48	PROGETTAZIONE A TAGLIO DI STRUTTURE IN C.A. SECONDO IL D.M. 14/1/2008
49	VERIFICA ALLO SLE (TENSIONI E FESSURAZIONE) DI STRUTTURE IN C.A.
50	VERIFICA ALLO SLE (DEFORMAZIONE) DI STRUTTURE IN C.A.
51	FATTORE DI STRUTTURA
52	SOVRARESISTENZE
53	DETTAGLI COSTRUTTIVI C.A.: LIMITI D'ARMATURA PILASTRI E NODI TRAVE-PILASTRO
54	PARETI IN C.A. SNELLE IN ZONA SISMICA
80	ANALISI PUSHOVER DI UN EDIFICIO IN C.A.
120	PROGETTO E VERIFICA DI TRAVI PREM

Modellazione di strutture in acciaio

Test N°	Titolo
55	VERIFICA DI STABILITA' DI ASTE COMPRESSE IN ACCIAIO – METODO OMEGA
56	LUCE LIBERA DI TRAVI E ASTE IN ACCIAIO
57	LUCE LIBERA DI COLONNE IN ACCIAIO
58	SVERGOLAMENTO DI TRAVI IN ACCIAIO
59	FATTORE DI STRUTTURA
60	ACCIAIO D.M.2008
61	ACCIAIO EC3
62	GERARCHIA RESISTENZE STRUTTURE IN ACCIAIO
63	STABILITA' DI ASTE COMPOSTE IN ACCIAIO
73	COLLEGAMENTI IN ACCIAIO: NODO TRAVE COLONNA FLANGIATO CON PRESENZA IRRIGIDIMENTI TRASVERSALI
74	COLLEGAMENTI IN ACCIAIO: NODO TRAVE COLONNA FLANGIATO CON PRESENZA DI UN PIATTO DI RINFORZO SALDATO ALL'ANIMA DELLA COLONNA
75	COLLEGAMENTI IN ACCIAIO: NODO TRAVE COLONNA FLANGIATO CON PRESENZA DI DUE PIATTI DI RINFORZO SALDATI ALL'ANIMA DELLA COLONNA
76	COLLEGAMENTI IN ACCIAIO: NODO TRAVE COLONNA FLANGIATO A DUE VIE SU ALI COLONNA
77	COLLEGAMENTI IN ACCIAIO: NODO TRAVE COLONNA FLANGIATO A UNA VIA CON DUE COMBINAZIONI DI CARICO
78	COLLEGAMENTI IN ACCIAIO: NODO TRAVE COLONNA FLANGIATO SU ANIMA SENZA RINFORZI A QUATTRO FILE DI BULLONI DI CUI UNA SU PIASTRA INFERIORE E UNA SU PIASTRA SUPERIORE
79	VERIFICA DELLA PIASTRA NODO TRAVE COLONNA
85	TELAIO ACCIAIO: CONTROVENTI CONCENTRICI

Modellazione di strutture in muratura

Test N°	Titolo
81	ANALISI PUSHOVER DI UNA STRUTTURA IN MURATURA
84	ANALISI ELASTO PLASTICA INCREMENTALE, PARETE IN MURATURA

86	VERIFICA NON SISMICA DELLE MURATURE (D.M. 87 TA)
87	VERIFICA NON SISMICA DELLE MURATURE (D.M. 2005 SL)
88	FATTORE DI STRUTTURA

Modellazione di strutture in legno

Test N°	Titolo
17	SOLAIO: MISTO LEGNO-CALCESTRUZZO
89	VERIFICA ALLO SLU DI STRUTTURE IN LEGNO SECONDO EC5
90	VERIFICA ALLO SLE DI STRUTTURE IN LEGNO SECONDO EC5
91	FATTORE DI STRUTTURA
92	VERIFICHE EC5
93	SNELLEZZE EC5
94	VERIFICA AL FUOCO DI STRUTTURE IN LEGNO SECONDO EC5
117	PROGETTO E VERIFICA DI GUSCI IN MATERIALE XLAM
118	PROGETTO E VERIFICA DI PARETI IN MATERIALE XLAM E RELATIVI COLLEGAMENTI
119	PROGETTO E VERIFICA DI SOLAI IN MATERIALE XLAM

Id	Tipo / Note		Young	Poisson	G	Gamma	Alfa
1	Calcestruzzo Classe C25/30	daN/cm2	daN/cm2	0.20	daN/cm2	daN/cm3	
	Rck	300.0	3.145e+05		1.310e+05	2.50e-03	1.00e-05
	fctm	25.6					
10	acciaio Fe360 - S235		2.100e+06	0.30	8.077e+05	7.80e-03	1.20e-05
	ft	3600.0					
	fy	2350.0					
	fd	2350.0					
	fdt	2100.0					
	sadm	1600.0					
	sadmt	1400.0					
13	Tamponatura 1100 daN/mc per elemento pannello		4.500e+04	0.0	1.800e+04	1.10e-03	1.00e-05
	Resist. fk	59.0					
	Resist. fvko	4.1					
31	Muratura in pietre a spacco con buona tessitura E = 1.740e+04		1.740e+04	0.0	5800.0	2.10e-03	1.00e-05
	Resist. fk	26.0					
	Resist. fvko	0.6					
34	mattoni pieni e malta di calce		3.375e+04	0.0	1.125e+04	1.80e-03	1.00e-05
	Resist. fk	72.0					
	Resist. fvko	2.2					
36	muratura E = 4.550e+04		4.550e+04	0.0	1.138e+04	1.50e-03	1.00e-05
	Resist. fk	65.0					
	Resist. fvko	3.5					
42	Legno massiccio C24		1.000e+05	0.0	6300.0	3.50e-04	0.0
	Modulo E0,05		6.727e+04				
	LamellareMateriale non massiccio e pertanto da considerare come lamellareNo						
	Resist. fc0k	210.0					
	Resist. ft0k	140.0					
	Resist. fmk	240.0					
	Resist. fvk	40.0					
54	Calcestruzzo C 8/10		2.533e+05	0.20	1.520e+05	2.50e-03	1.00e-05
	Rck	100.0					
	fctm	10.0					
55	mattoni pieni e malta di calce		3.375e+04	0.0	1.125e+04	1.80e-03	1.00e-05
	Resist. fk	72.0					
	Resist. fvko	2.2					
56	mattoni pieni e malta di calce		3.375e+04	0.0	1.125e+04	1.80e-03	1.00e-05
	Resist. fk	72.0					
	Resist. fvko	2.2					
57	muratura E = 1.024e+05		1.024e+05	0.0	2.559e+04	1.50e-03	1.00e-05
	Resist. fk	146.3					
	Resist. fvko	6.3					
58	mattoni pieni e malta di calce		3.375e+04	0.0	1.125e+04	1.80e-03	1.00e-05

Id	Tipo / Note		Young	Poisson	G	Gamma	Alfa
	Resist. fk	93.6					
	Resist. fvko	2.2					

Aste acc.	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Generalità						
Beta assegnato	0.80	0.80	0.80			
Verifica come controvento	No	No	No			
Usa condizioni I e II	Si	Si	Si			
Coefficiente gamma M0	1.05	1.05	1.05			
Coefficiente gamma M1	1.05	1.05	1.05			
Coefficiente gamma M2	1.25	1.25	1.25			

Pilastrici acc.	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Lunghezze libere						
Metodo di calcolo 2-2	Assegnato	Assegnato	Assegnato			
2-2 Beta assegnato	2.00	2.00	2.00			
2-2 Beta * L assegnato [cm]	0.0	0.0	0.0			
Metodo di calcolo 3-3	Assegnato	Assegnato	Assegnato			
3-3 Beta assegnato	2.00	2.00	2.00			
3-3 Beta * L assegnato [cm]	0.0	0.0	0.0			
1-1 Beta assegnato	1.00	1.00	1.00			
1-1 Beta * L assegnato [cm]	0.0	0.0	0.0			
Generalità						
Coefficiente gamma M0	1.05	1.05	1.05			
Coefficiente gamma M1	1.05	1.05	1.05			
Coefficiente gamma M2	1.25	1.25	1.25			
Effetti del 2 ordine	Si	Si	No			
Momenti equivalenti	Si	Si	Si			
Usa condizioni I e II	Si	Si	Si			

Travi acc.	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Lunghezze libere						
3-3 Beta * L automatico	Si	Si	Si			
3-3 Beta assegnato	1.00	1.00	1.00			
3-3 Beta assegnato [cm]	0.0	0.0	0.0			
2-2 Beta * L automatico	Si	Si	Si			
2-2 Beta assegnato	1.00	1.00	1.00			
2-2 Beta * L assegnato [cm]	0.0	0.0	0.0			
1-1 Beta * L automatico	Si	Si	Si			
1-1 Beta assegnato	1.00	1.00	1.00			
1-1 Beta * L assegnato [cm]	0.0	0.0	0.0			
Generalità						
Coefficiente gamma M0	1.05	1.05	1.05			
Coefficiente gamma M1	1.05	1.05	1.05			
Coefficiente gamma M2	1.25	1.25	1.25			
Luce di taglio per GR [cm]	1.00	1.00	1.00			
Usa condizioni I e II	Si	Si	Si			
Momenti equivalenti	Si	Si	Si			

Pareti c.a.	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Generalità						
Progetto armatura	Parete sismica	Parete sismica	Singolo elemento			
Armatura						
Inclinazione Av [gradi]	90.00	90.00	90.00			
Angolo Av-Ao [gradi]	90.00	90.00	90.00			
Minima tesa	0.25	0.25	0.25			
Massima tesa	4.00	4.00	4.00			
Maglia unica centrale	No	No	No			
Unico strato verticale	No	No	No			

Pareti c.a.	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Unico strato orizzontale	No	No	No			
Copriferro [cm]	2.00	2.00	2.00			
Maglia V						
diametro	10	10	10			
passo	25	25	25			
diametro aggiuntivi	12	12	12			
Maglia O						
diametro	8	8	8			
passo	25	25	25			
diametro aggiuntivi	8	8	8			
Stati limite ultimi						
Tensione fy [daN/cm2]	4500.00	4500.00	4300.00			
Tipo acciaio	tipo C	tipo C	tipo C			
Coefficiente gamma s	1.15	1.15	1.15			
Coefficiente gamma c	1.50	1.50	1.50			
Fattore di confidenza FC	0.0	0.0	0.0			
Verifiche con N costante	Si	Si	Si			
Tensioni ammissibili						
Tensione amm. cls [daN/cm2]	97.50	97.50	97.50			
Tensione amm. acciaio [daN/cm2]	2600.00	2600.00	2600.00			
Rapporto omogeneizzazione N	15.00	15.00	15.00			
Massimo rapporto area compressa/tesa	1.00	1.00	1.00			
Parete estesa debolmente armata						
Fattore amplificazione taglio V	1.50	1.50	1.50			
Hcrit. par. 7.4.4.5.1 [cm]	0.0	0.0	0.0			
Hcrit. par. 7.4.6.1.4 [cm]	0.0	0.0	0.0			
Diagramma involuppo taglio	Si	No	No			
Vincolo lati	nessun lato	nessun lato	nessun lato			
Verifica come fascia	No	No	No			
Diametro di estremità	0	0	0			
Zona confinata						
Minima tesa	1.00	1.00	1.00			
Massima tesa	4.00	4.00	4.00			
Distanza barre [cm]	2.00	2.00	2.00			
Interferro	2	2	2			
Armatura inclinata						
Area barre [cm2]	0.0	0.0	0.0			
Angolo orizzontale [gradi]	0.0	0.0	0.0			
Distanza di base [cm]	0.0	0.0	0.0			
Resistenza al fuoco						
3- intradosso	No	No	No			
3+ estradosso	No	No	No			
Tempo di esposizione R	15	15	120			

Gusci c.a.	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Armatura						
Inclinazione Ax [gradi]	0.0	0.0	0.0			
Angolo Ax-Ay [gradi]	90.00	90.00	90.00			
Minima tesa	0.31	0.31	0.33			
Massima tesa	0.78	0.78	0.81			
Maglia unica centrale	No	No	No			
Copriferro [cm]	2.00	2.00	2.00			
Maglia x						
diametro	10	10	10			
passo	20	20	20			
diametro aggiuntivi	12	12	12			
Maglia y						
diametro	10	10	10			
passo	20	20	20			
diametro aggiuntivi	12	12	12			
Stati limite ultimi						
Tensione fy [daN/cm2]	4500.00	4500.00	4300.00			
Tipo acciaio	tipo C	tipo C	tipo C			
Coefficiente gamma s	1.15	1.15	1.15			
Coefficiente gamma c	1.50	1.50	1.50			
Fattore di confidenza FC	0.0	0.0	0.0			
Verifiche con N costante	Si	Si	Si			
Applica SLU da DIN	No	No	No			
Tensioni ammissibili						
Tensione amm. cls [daN/cm2]	97.50	97.50	97.50			

Gusci c.a.	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Tensione amm. acciaio [daN/cm2]	2600.00	2600.00	2600.00			
Rapporto omogeneizzazione N	15.00	15.00	15.00			
Massimo rapporto area compressa/tesa	1.00	1.00	1.00			
Resistenza al fuoco						
3- intradosso	No	No	No			
3+ estradosso	No	No	No			
Tempo di esposizione R	15	15	120			

Travi c.a.	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Generalità						
Progetta a filo	No	No	No			
Af inf: da q*L*L /	0.0	0.0	0.0			
Armatura						
Minima tesa	0.31	0.31	0.33			
Minima compressa	0.31	0.31	0.33			
Massima tesa	0.78	0.78	0.81			
Da sezione	Si	Si	No			
Usa armatura teorica	No	No	No			
Stati limite ultimi						
Tensione fy [daN/cm2]	4500.00	4500.00	4300.00			
Tensione fy staffe [daN/cm2]	4500.00	4500.00	4300.00			
Tipo acciaio	tipo C	tipo C	tipo C			
Coefficiente gamma s	1.15	1.15	1.15			
Coefficiente gamma c	1.50	1.50	1.50			
Fattore di confidenza FC	0.0	0.0	0.0			
Verifiche con N costante	Si	Si	Si			
Fattore di ridistribuzione	0.0	0.0	0.0			
Modello per il confinamento						
Relazione tensio-deformativa	Mander	Mander	Mander			
Incrudimento acciaio	5.000e-03	5.000e-03	5.000e-03			
Fattore lambda	1.00	1.00	1.00			
epsilon max,s	4.000e-02	4.000e-02	4.000e-02			
epsilon cu2	4.500e-03	4.500e-03	4.500e-03			
epsilon c2	0.0	0.0	0.0			
epsilon cy	0.0	0.0	0.0			
Tensioni ammissibili						
Tensione amm. cls [daN/cm2]	97.50	97.50	97.50			
Tensione amm. acciaio [daN/cm2]	2600.00	2600.00	2600.00			
Rapporto omogeneizzazione N	15.00	15.00	15.00			
Massimo rapporto area compressa/tesa	1.00	1.00	1.00			
Staffe						
Diametro staffe	0.0	0.0	0.0			
Passo minimo [cm]	4.00	5.00	5.00			
Passo massimo [cm]	30.00	30.00	30.00			
Passo raffittito [cm]	15.00	15.00	15.00			
Lunghezza zona raffittita [cm]	50.00	50.00	50.00			
Ctg(Teta) Max	2.50	2.50	2.50			
Percentuale sagomati	0.0	0.0	0.0			
Luce di taglio per GR [cm]	1.00	1.00	1.00			
Adotta scorrimento medio	No	No	Si			
Torsione non essenziale inclusa	Si	Si	Si			

Pilastrì c.a.	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Generalità						
Progetto armatura	Privilegia lati	Privilegia lati	Disponi come da sezione			
Progetta a filo	No	No	No			
Effetti del 2 ordine	Si	Si	No			
Beta per 2-2	1.00	1.00	1.00			
Beta per 3-3	1.00	1.00	1.00			
Armatura						
Massima tesa	4.00	4.00	4.00			
Minima tesa	1.00	1.00	1.00			
Stati limite ultimi						
Tensione fy [daN/cm2]	4500.00	4500.00	4300.00			
Tensione fy staffe [daN/cm2]	4500.00	4500.00	4300.00			
Tipo acciaio	tipo C	tipo C	tipo C			

Pilastrì c.a.	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Coefficiente gamma s	1.15	1.15	1.15			
Coefficiente gamma c	1.50	1.50	1.50			
Fattore di confidenza FC	0.0	0.0	0.0			
Verifiche con N costante	Si	Si	Si			
Modello per il confinamento						
Relazione tensio-deformativa	Mander	Mander	Mander			
Incrudimento acciaio	5.000e-03	5.000e-03	5.000e-03			
Fattore lambda	1.00	1.00	1.00			
epsilon max.s	4.000e-02	4.000e-02	4.000e-02			
epsilon cu2	4.500e-03	4.500e-03	4.500e-03			
epsilon c2	0.0	0.0	0.0			
epsilon cy	0.0	0.0	0.0			
Tensioni ammissibili						
Tensione amm. cls [daN/cm2]	97.50	97.50	97.50			
Tensione amm. acciaio [daN/cm2]	2600.00	2600.00	2600.00			
Rapporto omogeneizzazione N	15.00	15.00	15.00			
Staffe						
Diametro staffe	0.0	0.0	0.0			
Passo minimo [cm]	5.00	5.00	5.00			
Passo massimo [cm]	25.00	25.00	25.00			
Passo raffittito [cm]	15.00	15.00	15.00			
Lunghezza zona raffittita [cm]	45.00	45.00	45.00			
Ctg(Teta) Max	2.50	2.50	2.50			
Luce di taglio per GR [cm]	1.00	1.00	1.00			
Massimizza gerarchia	Si	Si	Si			

Muratura	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Lunghezze libere						
Altezza interpiano [cm]	0.0	0.0	300.00			
Rho	0.85	0.85	1.00			
Snellezza limite	20.00	20.00	0.0			
Generalità						
Gamma non sismico	3.00	3.00	0.0			
Gamma sismico	2.00	2.00	0.0			
Fattore di confidenza FC	0.0	0.0	0.0			
Tolleranza azioni [daN/cm2]	0.0	0.0	0.0			
Media valori per quota	Si	Si	Si			
Media valori per elemento	Si	Si	No			
Verifica come fascia	No	No	Si			
Usa formula [7.8.3]	Si	Si	No			

Solai e pannelli	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Generalità						
Usa tensioni ammissibili	No	No	No			
Af inf: da traliccio	Si	Si	Si			
Consenti armatura a taglio	No	No	No			
Incrementa armatura longitudinale per taglio	Si	Si	Si			
Af inf: da q*L*L /	20.00	20.00	16.00			
Incremento fascia piena [cm]	5.00	5.00	5.00			
Armatura						
Minima tesa	0.15	0.15	0.15			
Massima tesa	3.00	3.00	3.00			
Minima compressa	0.0	0.0	0.0			
Af/h [cm]	7.000e-02	7.000e-02	7.000e-02			
Stati limite ultimi						
Tensione fy [daN/cm2]	4500.00	4500.00	4300.00			
Tipo acciaio	tipo C	tipo C	tipo C			
Coefficiente gamma s	1.15	1.15	1.15			
Coefficiente gamma c	1.50	1.50	1.50			
Fattore di ridistribuzione	0.0	0.0	0.0			
Tensioni ammissibili						
Tensione amm. cls [daN/cm2]	85.00	85.00	97.50			
Tensione amm. acciaio [daN/cm2]	2600.00	2600.00	2600.00			
Rapporto omogeneizzazione N	15.00	15.00	15.00			
Massimo rapporto area compressa/tesa	1.00	1.00	1.00			
Verifica freccia						

Solai e pannelli	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Infinita	250.00	500.00	500.00			
Istantanea	500.00	1000.00	1000.00			
Fattore viscosità	3.00	3.00	3.00			
Usa J non fessurato	No	No	No			
Elementi non strutturali						
Tamponatura antiespulsione	No	Si	Si			
Tamponatura con armatura	No	No	Si			
Fattore di struttura/comportamento	2.00	2.00	2.00			
Coefficiente gamma m	0.0	0.0	0.0			
Periodo Ta	0.0	0.0	0.0			
Altezza pannello	0.0	0.0	0.0			

Legno	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Lunghezze libere						
aste						
Beta assegnato	0.80	0.80	0.80			
travi						
3-3 Beta * L automatico	Si	Si	Si			
3-3 Beta assegnato	1.00	1.00	1.00			
3-3 Beta * L assegnato [cm]	0.0	0.0	0.0			
2-2 Beta * L automatico	Si	Si	Si			
2-2 Beta assegnato	1.00	1.00	1.00			
2-2 Beta * L assegnato [cm]	0.0	0.0	0.0			
1-1 Beta * L automatico	Si	Si	Si			
1-1 Beta assegnato	1.00	1.00	1.00			
1-1 Beta * L assegnato [cm]	0.0	0.0	0.0			
pilastrì						
Metodo di calcolo 3-3	Assegnato	Assegnato	Assegnato			
3-3 Beta assegnato	2.00	2.00	2.00			
3-3 Beta * L assegnato [cm]	0.0	0.0	0.0			
Metodo di calcolo 2-2	Assegnato	Assegnato	Assegnato			
2-2 Beta assegnato	2.00	2.00	2.00			
2-2 Beta * L assegnato [cm]	0.0	0.0	0.0			
1-1 Beta assegnato	1.00	1.00	1.00			
1-1 Beta * L assegnato [cm]	0.0	0.0	0.0			
Generalità						
Gamma non sismico	1.50	1.50	1.50			
Gamma sismico	1.50	1.50	1.50			
Fattore di confidenza FC	0.0	0.0	0.0			
Classificazione						
Classe di servizio	1 (bassa umidità)	1 (bassa umidità)	1 (bassa umidità)			
Per classe di servizio 1						
Kmod permanente	0.60	0.60	0.60			
Kmod lunga	0.70	0.70	0.70			
Kmod media	0.80	0.80	0.80			
Kmod breve	0.90	0.90	0.90			
Kmod istantanea	1.00	1.00	1.10			
Kdef	0.60	0.60	0.60			
Per classe di servizio 2						
Kmod permanente	0.60	0.60	0.60			
Kmod lunga	0.70	0.70	0.70			
Kmod media	0.80	0.80	0.80			
Kmod breve	0.90	0.90	0.90			
Kmod istantanea	1.00	1.00	1.10			
Kdef	0.80	0.80	0.80			
Per classe di servizio 3						
Kmod permanente	0.50	0.50	0.50			
Kmod lunga	0.55	0.55	0.55			
Kmod media	0.65	0.65	0.65			
Kmod breve	0.70	0.70	0.70			
Kmod istantanea	0.90	0.90	0.90			
Kdef	2.00	2.00	2.00			

XLAM	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Generalità						
L direzione 1 [*] [cm]	1.00	1.00	0.0			

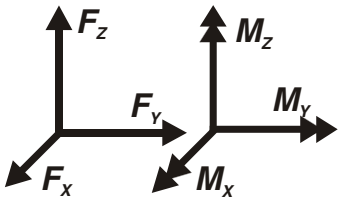
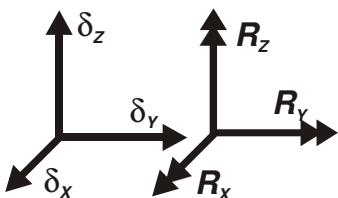
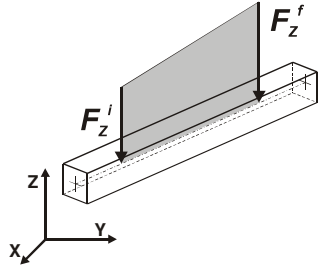
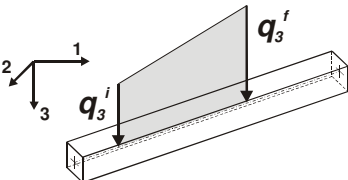
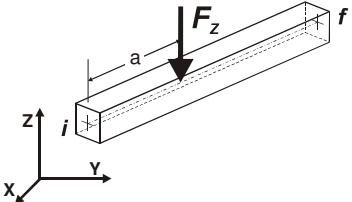
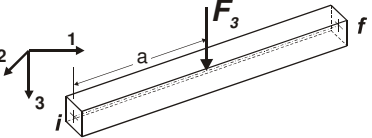
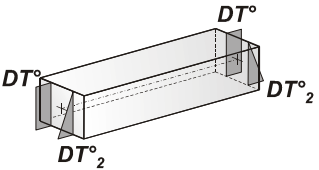
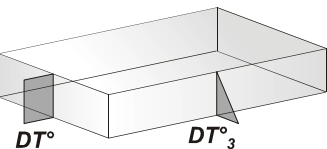
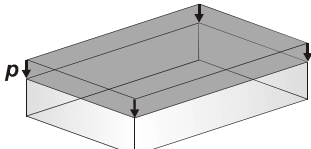
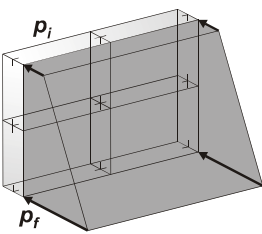
XLAM	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
L direzione 2 [cm]	0.0	0.0	0.0			
Verifica V da D.38	No	No	No			
Verifica M da M.5-45	No	No	No			
Media valori elementi	Si	Si	Si			
Connessioni pareti						
rvpk [daN/cm]	50.00	50.00	50.00			
rvtk [daN/cm]	50.00	50.00	50.00			
rvlk [daN/cm]	50.00	50.00	50.00			
RHk [daN]	5000.00	5000.00	5000.00			
dH [cm]	25.00	25.00	25.00			
fcH90k [daN/cm2]	20.00	20.00	20.00			
Pannelli solaio						
f ist<L/	500.00	500.00	500.00			
f inf<L/	350.00	350.00	350.00			
Verifica vibrazioni (EC5 7.3)	No	No	No			
E massetto collaborante [daN/cm2]	200000.00	200000.00	200000.00			
t massetto collaborante [cm]	4.00	4.00	4.00			
Smorzamento percentuale	0.0	0.0	0.0			
Resistenza al fuoco						
Spessore carbonizzazione [cm]	0.0	0.0	0.0			
3- intradosso	No	No	No			
3+ estradosso	No	No	No			

MODELLAZIONE DELLE AZIONI

LEGENDA TABELLA DATI AZIONI

Il programma consente l'uso di diverse tipologie di carico (azioni). Le azioni utilizzate nella modellazione sono individuate da una sigla identificativa ed un codice numerico (gli elementi strutturali richiamano quest'ultimo nella propria descrizione). Per ogni azione applicata alla struttura viene di riportato il codice, il tipo e la sigla identificativa. Le tabelle successive dettagliano i valori caratteristici di ogni azione in relazione al tipo. Le tabelle riportano infatti i seguenti dati in relazione al tipo:

1	carico concentrato nodale 6 dati (forza F_x , F_y , F_z , momento M_x , M_y , M_z)
2	spostamento nodale impresso 6 dati (spostamento T_x , T_y , T_z , rotazione R_x , R_y , R_z)
3	carico distribuito globale su elemento tipo trave 7 dati (f_x , f_y , f_z , m_x , m_y , m_z , ascissa di inizio carico) 7 dati (f_x , f_y , f_z , m_x , m_y , m_z , ascissa di fine carico)
4	carico distribuito locale su elemento tipo trave 7 dati (f_1 , f_2 , f_3 , m_1 , m_2 , m_3 , ascissa di inizio carico) 7 dati (f_1 , f_2 , f_3 , m_1 , m_2 , m_3 , ascissa di fine carico)
5	carico concentrato globale su elemento tipo trave 7 dati (F_x , F_y , F_z , M_x , M_y , M_z , ascissa di carico)
6	carico concentrato locale su elemento tipo trave 7 dati (F_1 , F_2 , F_3 , M_1 , M_2 , M_3 , ascissa di carico)
7	variazione termica applicata ad elemento tipo trave 7 dati (variazioni termiche: uniforme, media e differenza in altezza e larghezza al nodo iniziale e finale)
8	carico di pressione uniforme su elemento tipo piastra 1 dato (pressione)
9	carico di pressione variabile su elemento tipo piastra 4 dati (pressione, quota, pressione, quota)
10	variazione termica applicata ad elemento tipo piastra 2 dati (variazioni termiche: media e differenza nello spessore)
11	carico variabile generale su elementi tipo trave e piastra 1 dato descrizione della tipologia 4 dati per segmento (posizione, valore, posizione, valore) la tipologia precisa l'ascissa di definizione, la direzione del carico, la modalità di carico e la larghezza d'influenza per gli elementi tipo trave
12	gruppo di carichi con impronta su piastra 9 dati (numero di ripetizioni in direzione X e Y, valore di ciascun carico, posizione centrale del primo, dimensioni dell'impronta, interasse tra i carichi)

 <p>Carico nodale</p>	concentrato	 <p>Spostamento impresso</p>
 <p>Carico distribuito globale</p>		 <p>Carico distribuito locale</p>
 <p>Carico globale</p>	concentrato	 <p>Carico concentrato locale</p>
 <p>Carico termico 2D</p>		 <p>Carico termico 3D</p>
 <p>Carico uniforme</p>	pressione	 <p>Carico pressione variabile</p>

SCHEMATIZZAZIONE DEI CASI DI CARICO

LEGENDA TABELLA CASI DI CARICO

Il programma consente l'applicazione di diverse tipologie di casi di carico.

Sono previsti i seguenti 11 tipi di casi di carico:

	Sigla	Tipo	Descrizione
1	Ggk	A	caso di carico comprensivo del peso proprio struttura
2	Gk	NA	caso di carico con azioni permanenti
3	Qk	NA	caso di carico con azioni variabili
4	Gsk	A	caso di carico comprensivo dei carichi permanenti sui solai e sulle coperture
5	Qsk	A	caso di carico comprensivo dei carichi variabili sui solai
6	Qnk	A	caso di carico comprensivo dei carichi di neve sulle coperture
7	Qtk	SA	caso di carico comprensivo di una variazione termica agente sulla struttura
8	Qvk	NA	caso di carico comprensivo di azioni da vento sulla struttura
9	Esk	SA	caso di carico sismico con analisi statica equivalente
10	Edk	SA	caso di carico sismico con analisi dinamica
11	Etik	NA	caso di carico comprensivo di azioni derivanti dall' incremento di spinta delle terre in condizione sismica
12	Pk	NA	caso di carico comprensivo di azioni derivanti da coazioni, cedimenti e precompressioni

Sono di tipo automatico A (ossia non prevedono introduzione dati da parte dell'utente) i seguenti casi di carico: 1-Ggk; 4-Gsk; 5-Qsk; 6-Qnk.

Sono di tipo semi-automatico SA (ossia prevedono una minima introduzione dati da parte dell'utente) i seguenti casi di carico:

7-Qtk, in quanto richiede solo il valore della variazione termica;

9-Esk e 10-Edk, in quanto richiedono il valore dell'angolo di ingresso del sisma e l'individuazione dei casi di carico partecipanti alla definizione delle masse.

Sono di tipo non automatico NA ossia prevedono la diretta applicazione di carichi generici agli elementi strutturali (si veda il precedente punto Modellazione delle Azioni) i restanti casi di carico.

Nella tabella successiva vengono riportati i casi di carico agenti sulla struttura, con l'indicazione dei dati relativi al caso di carico stesso: Numero Tipo e Sigla identificativa, Valore di riferimento del caso di carico (se previsto).

In successione, per i casi di carico non automatici, viene riportato l'elenco di nodi ed elementi direttamente caricati con la sigla identificativa del carico.

Per i casi di carico di tipo sismico (9-Esk e 10-Edk), viene riportata la tabella di definizione delle masse: per ogni caso di carico partecipante alla definizione delle masse viene indicata la relativa aliquota (partecipazione) considerata. Si precisa che per i caso di carico 5-Qsk e 6-Qnk la partecipazione è prevista localmente per ogni elemento solaio o copertura presente nel modello (si confronti il valore Sksol nel capitolo relativo agli elementi solaio) e pertanto la loro partecipazione è di norma pari a uno.

CDC	Tipo	Sigla Id	Note
1	Ggk	CDC=Ggk (peso proprio della struttura)	
2	Gsk	CDC=G1sk (permanente solai-coperture)	
3	Gsk	CDC=G2sk (permanente solai-coperture n.c.d.)	
4	Gsk	CDC=G2pk (permanente pannelli n.c.d.)	
5	Qsk	CDC=Qsk (variabile solai)	
6	Qnk	CDC=Qnk (carico da neve)	
7	Edk	CDC=Ed (dinamico SLU) alfa=0.0 (ecc. +)	partecipazione:1.00 per 1 CDC=Ggk (peso proprio della struttura)
			partecipazione:1.00 per 2 CDC=G1sk (permanente solai-coperture)
			partecipazione:1.00 per 3 CDC=G2sk (permanente solai-coperture n.c.d.)
			partecipazione:1.00 per 4 CDC=G2pk (permanente pannelli n.c.d.)
			partecipazione:1.00 per 5 CDC=Qsk (variabile solai)
			partecipazione:1.00 per 6 CDC=Qnk (carico da neve)
8	Edk	CDC=Ed (dinamico SLU) alfa=0.0 (ecc. -)	come precedente CDC sismico
9	Edk	CDC=Ed (dinamico SLU) alfa=90.00 (ecc. +)	come precedente CDC sismico
10	Edk	CDC=Ed (dinamico SLU) alfa=90.00 (ecc. -)	come precedente CDC sismico
11	Edk	CDC=Ed (dinamico SLD) alfa=0.0 (ecc. +)	come precedente CDC sismico
12	Edk	CDC=Ed (dinamico SLD) alfa=0.0 (ecc. -)	come precedente CDC sismico
13	Edk	CDC=Ed (dinamico SLD) alfa=90.00 (ecc. +)	come precedente CDC sismico
14	Edk	CDC=Ed (dinamico SLD) alfa=90.00 (ecc. -)	come precedente CDC sismico

DEFINIZIONE DELLE COMBINAZIONI

LEGENDA TABELLA COMBINAZIONI DI CARICO

Il programma combina i diversi tipi di casi di carico (CDC) secondo le regole previste dalla normativa vigente. Le combinazioni previste sono destinate al controllo di sicurezza della struttura ed alla verifica degli spostamenti e delle sollecitazioni.

La prima tabella delle combinazioni riportata di seguito comprende le seguenti informazioni: Numero, Tipo, Sigla identificativa. Una seconda tabella riporta il peso nella combinazione assunto per ogni caso di carico.

Ai fini delle verifiche degli stati limite si definiscono le seguenti combinazioni delle azioni:

Combinazione fondamentale SLU

$\gamma_{G1} \cdot G_1 + \gamma_{G2} \cdot G_2 + \gamma_P \cdot P + \gamma_{Q1} \cdot Q_{k1} + \gamma_{Q2} \cdot \psi_{02} \cdot Q_{k2} + \gamma_{Q3} \cdot \psi_{03} \cdot Q_{k3} + \dots$

Combinazione caratteristica (rara) SLE

$G_1 + G_2 + P + Q_{k1} + \psi_{02} \cdot Q_{k2} + \psi_{03} \cdot Q_{k3} + \dots$

Combinazione frequente SLE

$G_1 + G_2 + P + \psi_{11} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \psi_{23} \cdot Q_{k3} + \dots$

Combinazione quasi permanente SLE

$G_1 + G_2 + P + \psi_{21} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \psi_{23} \cdot Q_{k3} + \dots$

Combinazione sismica, impiegata per gli stati limite ultimi e di esercizio connessi all'azione sismica E

$E + G_1 + G_2 + P + \psi_{21} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \dots$

Combinazione eccezionale, impiegata per gli stati limite connessi alle azioni eccezionali

$G_1 + G_2 + A_d + P + \psi_{21} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \dots$

Dove:

NTC 2018 Tabella 2.5.I

Destinazione d'uso/azione	ψ_0	ψ_1	ψ_2
Categoria A residenziali	0,70	0,50	0,30
Categoria B uffici	0,70	0,50	0,30
Categoria C ambienti suscettibili di affollamento	0,70	0,70	0,60
Categoria D ambienti ad uso commerciale	0,70	0,70	0,60
Categoria E biblioteche, archivi, magazzini,...	1,00	0,90	0,80
Categoria F Rimesse e parcheggi (autoveicoli ≤ 30 kN)	0,70	0,70	0,60
Categoria G Rimesse e parcheggi (autoveicoli > 30 kN)	0,70	0,50	0,30
Categoria H Coperture	0,00	0,00	0,00
Vento	0,60	0,20	0,00
Neve a quota ≤ 1000 m	0,50	0,20	0,00
Neve a quota > 1000 m	0,70	0,50	0,20
Variazioni Termiche	0,60	0,50	0,00

Nelle verifiche possono essere adottati in alternativa due diversi approcci progettuali:

- per l'approccio 1 si considerano due diverse combinazioni di gruppi di coefficienti di sicurezza parziali per le azioni, per i materiali e per la resistenza globale (combinazione 1 con coefficienti A1 e combinazione 2 con coefficienti A2),
- per l'approccio 2 si definisce un'unica combinazione per le azioni, per la resistenza dei materiali e per la resistenza globale (con coefficienti A1).

NTC 2018 Tabella 2.6.I

		Coefficiente γ_f	EQU	A1	A2
Carichi permanenti	Favorevoli	γ_{G1}	0,9	1,0	1,0
	Sfavorevoli		1,1	1,3	1,0
Carichi permanenti non strutturali (Non compiutamente definiti)	Favorevoli	γ_{G2}	0,8	0,8	0,8
	Sfavorevoli		1,5	1,5	1,3
Carichi variabili	Favorevoli	γ_{Qi}	0,0	0,0	0,0
	Sfavorevoli		1,5	1,5	1,3

Cmb	Tipo	Sigla Id	effetto P-delta
1	SLU	Comb. SLU A1 1	
2	SLU	Comb. SLU A1 2	
3	SLU	Comb. SLU A1 3	
4	SLU	Comb. SLU A1 4	
5	SLU	Comb. SLU A1 5	
6	SLU	Comb. SLU A1 6	
7	SLU	Comb. SLU A1 7	
8	SLU	Comb. SLU A1 8	

	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
2	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4	1.00	1.00	0.0	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
6	1.30	1.30	1.50	1.50	1.05	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
7	1.30	1.30	1.50	1.50	1.05	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
8	1.00	1.00	0.0	0.0	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
9	1.00	1.00	0.0	0.0	1.05	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
10	1.00	1.00	0.0	0.0	1.05	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
11	1.00	1.00	1.00	1.00	0.60	0.0	-1.00	0.0	-0.30	0.0	0.0	0.0	0.0	0.0
12	1.00	1.00	1.00	1.00	0.60	0.0	-1.00	0.0	0.30	0.0	0.0	0.0	0.0	0.0
13	1.00	1.00	1.00	1.00	0.60	0.0	1.00	0.0	-0.30	0.0	0.0	0.0	0.0	0.0
14	1.00	1.00	1.00	1.00	0.60	0.0	1.00	0.0	0.30	0.0	0.0	0.0	0.0	0.0
15	1.00	1.00	1.00	1.00	0.60	0.0	-1.00	0.0	0.0	-0.30	0.0	0.0	0.0	0.0
16	1.00	1.00	1.00	1.00	0.60	0.0	-1.00	0.0	0.0	0.30	0.0	0.0	0.0	0.0
17	1.00	1.00	1.00	1.00	0.60	0.0	1.00	0.0	0.0	-0.30	0.0	0.0	0.0	0.0
18	1.00	1.00	1.00	1.00	0.60	0.0	1.00	0.0	0.0	0.30	0.0	0.0	0.0	0.0
19	1.00	1.00	1.00	1.00	0.60	0.0	0.0	-1.00	-0.30	0.0	0.0	0.0	0.0	0.0
20	1.00	1.00	1.00	1.00	0.60	0.0	0.0	-1.00	0.30	0.0	0.0	0.0	0.0	0.0
21	1.00	1.00	1.00	1.00	0.60	0.0	0.0	1.00	-0.30	0.0	0.0	0.0	0.0	0.0
22	1.00	1.00	1.00	1.00	0.60	0.0	0.0	1.00	0.30	0.0	0.0	0.0	0.0	0.0
23	1.00	1.00	1.00	1.00	0.60	0.0	0.0	-1.00	0.0	-0.30	0.0	0.0	0.0	0.0
24	1.00	1.00	1.00	1.00	0.60	0.0	0.0	-1.00	0.0	0.30	0.0	0.0	0.0	0.0
25	1.00	1.00	1.00	1.00	0.60	0.0	0.0	1.00	0.0	-0.30	0.0	0.0	0.0	0.0
26	1.00	1.00	1.00	1.00	0.60	0.0	0.0	1.00	0.0	0.30	0.0	0.0	0.0	0.0
27	1.00	1.00	1.00	1.00	0.60	0.0	-0.30	0.0	-1.00	0.0	0.0	0.0	0.0	0.0
28	1.00	1.00	1.00	1.00	0.60	0.0	-0.30	0.0	1.00	0.0	0.0	0.0	0.0	0.0
29	1.00	1.00	1.00	1.00	0.60	0.0	0.30	0.0	-1.00	0.0	0.0	0.0	0.0	0.0
30	1.00	1.00	1.00	1.00	0.60	0.0	0.30	0.0	1.00	0.0	0.0	0.0	0.0	0.0
31	1.00	1.00	1.00	1.00	0.60	0.0	0.0	-0.30	-1.00	0.0	0.0	0.0	0.0	0.0
32	1.00	1.00	1.00	1.00	0.60	0.0	0.0	-0.30	1.00	0.0	0.0	0.0	0.0	0.0
33	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.30	-1.00	0.0	0.0	0.0	0.0	0.0
34	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.30	1.00	0.0	0.0	0.0	0.0	0.0
35	1.00	1.00	1.00	1.00	0.60	0.0	-0.30	0.0	0.0	-1.00	0.0	0.0	0.0	0.0
36	1.00	1.00	1.00	1.00	0.60	0.0	-0.30	0.0	0.0	1.00	0.0	0.0	0.0	0.0
37	1.00	1.00	1.00	1.00	0.60	0.0	0.30	0.0	0.0	-1.00	0.0	0.0	0.0	0.0
38	1.00	1.00	1.00	1.00	0.60	0.0	0.30	0.0	0.0	1.00	0.0	0.0	0.0	0.0
39	1.00	1.00	1.00	1.00	0.60	0.0	0.0	-0.30	0.0	-1.00	0.0	0.0	0.0	0.0
40	1.00	1.00	1.00	1.00	0.60	0.0	0.0	-0.30	0.0	1.00	0.0	0.0	0.0	0.0
41	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.30	0.0	-1.00	0.0	0.0	0.0	0.0
42	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.30	0.0	1.00	0.0	0.0	0.0	0.0
43	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	-0.30	0.0
44	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	0.30	0.0
45	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	1.00	0.0	-0.30	0.0
46	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	1.00	0.0	0.30	0.0
47	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	0.0	-0.30
48	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	0.0	0.30
49	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	1.00	0.0	0.0	-0.30
50	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	1.00	0.0	0.0	0.30
51	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	-0.30	0.0
52	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	0.30	0.0
53	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.0	1.00	-0.30	0.0
54	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.30	0.0
55	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	-0.30
56	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	0.30
57	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.0	-0.30
58	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.0	0.30
59	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	-1.00	0.0
60	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	1.00	0.0
61	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.30	0.0	-1.00	0.0
62	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.30	0.0	1.00	0.0
63	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.0	-0.30	-1.00	0.0
64	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.0	-0.30	1.00	0.0
65	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.0	0.30	-1.00	0.0
66	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.0	0.30	1.00	0.0
67	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	0.0	-1.00
68	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	0.0	1.00
69	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.30	0.0	0.0	-1.00
70	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.30	0.0	0.0	1.00
71	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	-1.00
72	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	1.00
73	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.0	0.30	0.0	-1.00
74	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.0	0.30	0.0	1.00

AZIONE SISMICA

VALUTAZIONE DELL' AZIONE SISMICA

L'azione sismica sulle costruzioni è valutata a partire dalla "pericolosità sismica di base", in condizioni ideali di sito di riferimento rigido con superficie topografica orizzontale.

Allo stato attuale, la pericolosità sismica su reticolo di riferimento nell'intervallo di riferimento è fornita dai dati pubblicati sul sito <http://esse1.mi.ingv.it/>. Per punti non coincidenti con il reticolo di riferimento e periodi di ritorno non contemplati direttamente si opera come indicato nell' allegato alle NTC (rispettivamente media pesata e interpolazione).

L' azione sismica viene definita in relazione ad un periodo di riferimento V_r che si ricava, per ciascun tipo di costruzione, moltiplicandone la vita nominale per il coefficiente d'uso (vedi tabella Parametri della struttura). Fissato il periodo di riferimento V_r e la probabilità di superamento P_{ver} associata a ciascuno degli stati limite considerati, si ottiene il periodo di ritorno T_r e i relativi parametri di pericolosità sismica (vedi tabella successiva):

a_g : accelerazione orizzontale massima del terreno;

F_o : valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale;

T^*c : periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale;

Parametri della struttura

Classe d'uso	Vita V_n [anni]	Coeff. Uso	Periodo V_r [anni]	Tipo di suolo	Categoria topografica
III	50.0	1.5	75.0	B	T1

Individuati su reticolo di riferimento i parametri di pericolosità sismica si valutano i parametri spettrali riportati in tabella:

S è il coefficiente che tiene conto della categoria di sottosuolo e delle condizioni topografiche mediante la relazione seguente $S = S_s \cdot S_t$ (3.2.3)

F_o è il fattore che quantifica l'amplificazione spettrale massima, su sito di riferimento rigido orizzontale

F_v è il fattore che quantifica l'amplificazione spettrale massima verticale, in termini di accelerazione orizzontale massima del terreno a_g su sito di riferimento rigido orizzontale

T_b è il periodo corrispondente all'inizio del tratto dello spettro ad accelerazione costante.

T_c è il periodo corrispondente all'inizio del tratto dello spettro a velocità costante.

T_d è il periodo corrispondente all'inizio del tratto dello spettro a spostamento costante.

Id nodo	Longitudine	Latitudine	Distanza
			Km
Loc.	7.572	45.244	
12903	7.528	45.237	3.520
12904	7.599	45.241	2.133
12682	7.594	45.291	5.484
12681	7.523	45.287	6.109

SL	P_{ver}	T_r	a_g	F_o	T^*c
		Anni	g		sec
SLO	92.0	30.0	0.024	2.570	0.180
SLD	92.0	30.0	0.024	2.570	0.180
SLV	92.0	30.0	0.024	2.570	0.180
SLC	92.0	30.0	0.024	2.570	0.180

SL	a_g	S	F_o	F_v	T_b	T_c	T_d
	g				sec	sec	sec
SLO	0.024	1.200	2.570	0.541	0.093	0.279	1.697
SLD	0.024	1.200	2.570	0.541	0.093	0.279	1.697
SLV	0.024	1.200	2.570	0.541	0.093	0.279	1.697
SLC	0.024	1.200	2.570	0.541	0.093	0.279	1.697

RISULTATI ANALISI SISMICHE

LEGENDA TABELLA ANALISI SISMICHE

Il programma consente l'analisi di diverse configurazioni sismiche.

Sono previsti, infatti, i seguenti casi di carico:

9. Esk caso di carico sismico con analisi statica equivalente

10. Edk caso di carico sismico con analisi dinamica

Ciascun caso di carico è caratterizzato da un angolo di ingresso e da una configurazione di masse determinante la forza sismica complessiva (si rimanda al capitolo relativo ai casi di carico per chiarimenti inerenti questo aspetto).

Nella colonna Note, in funzione della norma in uso sono riportati i parametri fondamentali che caratterizzano l'azione sismica: in particolare possono essere presenti i seguenti valori:

Angolo di ingresso	Angolo di ingresso dell'azione sismica orizzontale
Fattore di importanza	Fattore di importanza dell'edificio, in base alla categoria di appartenenza
Zona sismica	Zona sismica
Accelerazione ag	Accelerazione orizzontale massima sul suolo
Categoria suolo	Categoria di profilo stratigrafico del suolo di fondazione
Fattore q	Fattore di struttura/di comportamento. Dipendente dalla tipologia strutturale
Fattore di sito S	Fattore dipendente dalla stratigrafia e dal profilo topografico
Classe di duttilità CD	Classe di duttilità della struttura – "A" duttilità alta, "B" duttilità bassa
Fattore riduz. SLD	Fattore di riduzione dello spettro elastico per lo stato limite di danno
Periodo proprio T1	Periodo proprio di vibrazione della struttura
Coefficiente Lambda	Coefficiente dipendente dal periodo proprio T1 e dal numero di piani della struttura
Ordinata spettro Sd(T1)	Valore delle ordinate dello spettro di progetto per lo stato limite ultimo, componente orizzontale (verticale Svd)
Ordinata spettro Se(T1)	Valore delle ordinate dello spettro elastico ridotta del fattore SLD per lo stato limite di danno, componente orizzontale (verticale Sve)
Ordinata spettro S (Tb-Tc)	Valore dell' ordinata dello spettro in uso nel tratto costante
numero di modi considerati	Numero di modi di vibrare della struttura considerati nell'analisi dinamica

Per ciascun caso di carico sismico viene riportato l'insieme di dati sotto riportati (le masse sono espresse in unità di forza):

- a) analisi sismica statica equivalente:
 - quota, posizione del centro di applicazione e azione orizzontale risultante, posizione del baricentro delle rigidezze, rapporto r/L_s (per strutture a nucleo), indici di regolarità e/r secondo EC8 4.2.3.2
 - azione sismica complessiva
- b) analisi sismica dinamica con spettro di risposta:
 - quota, posizione del centro di massa e massa risultante, posizione del baricentro delle rigidezze, rapporto r/L_s (per strutture a nucleo) , indici di regolarità e/r secondo EC8 4.2.3.2
 - frequenza, periodo, accelerazione spettrale, massa eccitata nelle tre direzioni globali per tutti i modi
 - massa complessiva ed aliquota di massa complessiva eccitata.

Per ciascuna combinazione sismica definita SLD o SLO viene riportato il livello di deformazione η_T (dr) degli elementi strutturali verticali. Per semplicità di consultazione il livello è espresso anche in unità $1000 \cdot \eta_T/h$ da confrontare direttamente con i valori forniti nella norma (es. 5 per edifici con tamponamenti collegati rigidamente alla struttura, 10.0 per edifici con tamponamenti collegati elasticamente, 3 per edifici in muratura ordinaria, 4 per edifici in muratura armata).

Qualora si applichi il D.M. 96 (vedi NOTA sul capitolo "normativa di riferimento") l'analisi sismica dinamica può essere comprensiva di sollecitazione verticale contemporanea a quella orizzontale, nel qual caso è effettuata una sovrapposizione degli effetti in ragione della radice dei quadrati degli effetti stessi. Per ciascuna combinazione sismica - analisi effettuate con il D.M. 96 (vedi NOTA sul capitolo "normativa di riferimento") - viene riportato il livello di deformazione η_T , η_P e η_D degli elementi strutturali verticali. Per semplicità di consultazione il livello è espresso in unità $1000 \cdot \eta_T/h$ da confrontare direttamente con il valore 2 o 4 per la verifica.

Per gli edifici sismicamente isolati si riportano di seguito le verifiche condotte sui dispositivi di isolamento. Le verifiche sono effettuate secondo la circolare 619/2009 del C.S.LL.PP nelle combinazioni in SLC come previsto dal DM 17-01-2018. Per ogni combinazione è riportato il codice di verifica ed i valori utilizzati per la verifica: spostamento dE, area ridotta e dimensione A2, azione verticale, deformazioni di taglio dell'elastomero e tensioni nell'acciaio.

Qualora si applichi l'Ordinanza 3274 e s.m.i. le verifiche sono eseguite in accordo con l'allegato 10.A.

In particolare la tabella, per ogni combinazione di calcolo, riporta:

Nodo	Nodo di appoggio dell' isolatore
Cmb	Combinazione oggetto della verifica
Verif.	Codice di verifica ok – verifica positiva , NV – verifica negativa, ND – verifica non completata
dE	Spostamento relativo tra le due facce (amplificato del 20% per Ordinanza 3274 e smi) combinato con la regola del 30%
Ang fi	Angolo utilizzato per il calcolo dell' area ridotta Ar (per dispositivi circolari)
V	Azione verticale agente
Ar	Area ridotta efficace
Dim A2	Dimensione utile per il calcolo della deformazione per rotazione
Sig s	Tensione nell' inserto in acciaio

Gam c(a,s,t)	Deformazioni di taglio dell' elastomero
Vcr	Carico critico per instabilità

Affinché la verifica sia positiva deve essere:

- 1) $V > 0$
- 2) $\text{Sig s} < f_{yk}$
- 3) $\text{Gam t} < 5$
- 4) $\text{Gam s} < \text{Gam}^*$ (caratteristica dell' elastomero)
- 5) $\text{Gam s} < 2$
- 6) $V < 0.5 V_{cr}$

Con riferimento al **Documento di Affidabilità** "Test di validazione del software di calcolo PRO_SAP e dei moduli aggiuntivi PRO_SAP Modulo Geotecnico, PRO_CAD nodi acciaio e PRO_MST" - versione Maggio 2011, disponibile per il download sul sito www.2si.it, si segnalano i seguenti esempi applicativi:

Test N°	Titolo
23	DM 2008: SPETTRO
29	SISMICA 1000/H, SOMMA V, EFFETTO P-δ
30	ANALISI DI UN EDIFICIO CON ISOLATORI SISMICI
70	MASSE SISMICHE
75	PROGETTO DI ISOLATORI ELASTOMERICI
76	VERIFICA DI ISOLATORI ELASTOMERICI
77	VERIFICA DI ISOLATORI FRICTION PENDULUM

Calcolo dei fattori di comportamento secondo il D.M. 17/01/2018

La costruzione, esistente, è caratterizzata da regolarità sia in pianta sia in altezza ed è progettata in classe di duttilità media (CD"B").

Parametri fattore in direzione x e y

Sistema costruttivo: muratura

Definizione rapporto α_u/α_1 : valore come da normativa

Riferimento normativo α_u/α_1 : costruzioni di muratura ordinaria

Valore rapporto $\alpha_u/\alpha_1 = 1.700$

Fattore dissipativo $q_D = 2.000 \alpha_u/\alpha_1 = 3.400$

Fattori di comportamento utilizzati

	Dissipativi	Verifiche fragili
q SLU x	3.400	1.000
q SLU y	3.400	1.000
q SLU z	1.500	1.000

CDC	Tipo	Sigla Id	Note
7	Edk	CDC=Ed (dinamico SLU) alfa=0.0 (ecc. +)	
			verifica esistenti: fattore FC 1.200
			categoria suolo: B
			fattore di sito S = 1.200
			ordinata spettro (tratto Tb-Tc) = 0.022 g
			angolo di ingresso: 0.0
			eccentricità aggiuntiva: positiva
			periodo proprio T1: 0.168 sec.
			fattore q: 3.400
			fattore per spost. mu d: 4.986
			classe di duttilità CD: B
			numero di modi considerati: 220
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
cm	daN	cm	cm	cm	cm	cm	cm			
1340.00	96.19	-491.36	-334.97	0.0	0.0	-491.36	-334.97	0.155	0.0	0.0
1295.00	116.44	-491.36	-334.97	0.0	0.0	-491.36	-334.97	1.791	0.0	0.0
1250.00	101.25	-491.36	-334.97	0.0	0.0	-491.36	-334.97	1.791	0.0	0.0
1205.00	1203.52	-572.28	-173.84	0.0	-26.80	-635.82	-328.32	0.015	2.913	3.350
1195.00	7848.27	-175.90	173.40	0.0	-15.15	-313.36	198.69	0.654	1.046	0.168
1160.00	2326.05	-575.55	-168.23	0.0	-26.80	-635.82	-328.32	0.015	2.763	3.471
1115.00	2319.30	-575.63	-167.75	0.0	-26.80	-635.82	-328.32	0.015	2.759	3.482
1070.00	2319.30	-575.63	-167.75	0.0	-26.80	-635.82	-328.32	0.015	2.759	3.482
1025.00	1.465e+04	-128.29	99.57	0.0	-52.28	-544.32	97.18	0.605	1.184	0.002
985.00	1.083e+04	-102.23	128.80	0.0	-52.28	-542.11	167.56	0.726	1.143	0.047
945.00	1.083e+04	-102.21	128.80	0.0	-52.28	-542.11	167.56	0.726	1.143	0.047
905.00	6.437e+04	-130.89	142.36	0.0	-52.28	-458.71	212.95	0.530	0.997	0.097
855.00	1.642e+04	-128.78	145.90	0.0	-52.28	-485.70	259.69	0.343	1.348	0.177
830.00	1249.33	528.64	424.28	0.0	0.0	0.0	0.0	0.0	0.0	0.0
805.00	1.479e+04	-102.33	164.15	0.0	-52.28	-485.70	259.69	0.343	1.448	0.149
780.00	1249.33	528.64	538.78	0.0	0.0	0.0	0.0	0.0	0.0	0.0
755.00	1.526e+04	-82.93	181.97	0.0	-52.28	-481.74	260.08	0.362	1.467	0.118
728.69	1131.11	528.64	656.28	0.0	0.0	0.0	0.0	0.0	0.0	0.0
705.00	1.607e+04	-55.85	217.96	0.0	-52.28	-388.08	347.18	0.814	0.815	0.144
675.00	466.53	528.64	533.13	0.0	-12.20	0.0	0.0	0.0	0.0	0.0
655.00	1.415e+04	-110.23	162.68	0.0	-52.28	-485.60	338.86	0.413	1.292	0.286
605.00	1.443e+04	-81.71	180.98	0.0	-52.28	-388.24	376.21	0.787	0.765	0.213
555.00	1.494e+04	-58.92	172.30	0.0	-52.28	-381.08	258.88	0.824	0.785	0.088
535.00	462.89	-284.62	710.53	0.0	0.0	-295.19	710.53	0.049	0.058	0.0
505.00	1.668e+04	-63.27	192.44	0.0	-52.28	-380.93	345.75	0.857	0.759	0.170
455.00	1.393e+05	-26.77	231.20	0.0	-52.28	-366.53	489.83	0.922	0.783	0.375
404.44	1.848e+04	-42.92	230.40	0.0	-52.28	-385.70	570.64	0.732	0.887	0.542
378.89	7112.79	-473.91	-262.63	0.0	-6.20	-474.86	-329.87	2.180	0.006	0.456
353.89	2.196e+04	-32.62	456.21	0.0	-61.93	-355.57	632.92	0.678	0.799	0.423
303.33	1.928e+04	-91.51	295.05	0.0	-61.93	-445.29	639.78	0.388	1.157	0.686
252.78	2.190e+04	-176.89	242.77	0.0	-61.93	-448.92	647.41	0.369	0.913	0.816
202.22	1.592e+04	-73.92	284.63	0.0	-61.93	-448.92	647.41	0.369	1.258	0.731
151.67	1.601e+04	-65.56	283.49	0.0	-61.93	-448.94	620.41	0.408	1.223	0.654
122.00	7167.74	-473.02	-262.23	0.0	-6.20	-474.86	-329.87	2.180	0.012	0.459
101.11	1.343e+04	-59.25	403.57	0.0	-61.93	-371.53	681.11	0.575	0.839	0.682
88.00	511.85	445.72	710.53	0.0	0.0	459.84	710.53	0.039	0.268	0.0
80.00	1592.11	106.62	-334.97	0.0	0.0	101.38	-334.97	0.074	0.024	0.0
50.56	1.912e+04	-72.11	249.76	0.0	-61.93	-446.67	538.92	0.539	1.040	0.516

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
Risulta	5.461e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	4.057	0.246	0.022	683.51	0.1	8.018e+04	14.7	0.10	1.89e-05	0.0	0.0
2	4.203	0.238	0.022	3194.54	0.6	8.942e+04	16.4	0.07	1.34e-05	0.0	0.0
3	5.953	0.168	0.022	3.258e+05	59.7	5260.42	1.0	5.08	9.30e-04	0.0	0.0
4	6.890	0.145	0.022	87.98	1.61e-02	1.526e+05	27.9	3.74	6.85e-04	0.0	0.0
5	7.504	0.133	0.022	8103.68	1.5	606.23	0.1	2.52	4.62e-04	0.0	0.0
6	8.323	0.120	0.022	3.489e+04	6.4	1.213e+04	2.2	19.35	3.54e-03	0.0	0.0
7	8.540	0.117	0.022	2980.50	0.5	6.238e+04	11.4	29.25	5.36e-03	0.0	0.0
8	9.183	0.109	0.022	6471.64	1.2	703.74	0.1	62.78	1.15e-02	0.0	0.0
9	9.287	0.108	0.022	8493.51	1.6	1650.90	0.3	3.22	5.90e-04	0.0	0.0
10	9.876	0.101	0.022	397.25	7.28e-02	1269.15	0.2	7.58	1.39e-03	0.0	0.0
11	9.939	0.101	0.022	2.458e+04	4.5	2414.30	0.4	1.21	2.22e-04	0.0	0.0
12	10.445	0.096	0.022	3233.36	0.6	9698.97	1.8	21.03	3.85e-03	0.0	0.0
13	10.503	0.095	0.022	1225.94	0.2	75.83	1.39e-02	1.58	2.89e-04	0.0	0.0
14	10.845	0.092	0.022	5201.01	1.0	8853.37	1.6	0.01	2.32e-06	0.0	0.0
15	11.829	0.085	0.023	8057.19	1.5	321.47	5.89e-02	0.25	4.64e-05	0.0	0.0
16	12.334	0.081	0.023	283.23	5.19e-02	1.73	3.18e-04	7.11	1.30e-03	0.0	0.0
17	12.893	0.078	0.023	185.48	3.40e-02	5050.34	0.9	21.93	4.02e-03	0.0	0.0
18	13.024	0.077	0.023	6717.20	1.2	359.55	6.58e-02	36.62	6.71e-03	0.0	0.0
19	13.360	0.075	0.023	8097.79	1.5	1739.00	0.3	4.55	8.33e-04	0.0	0.0
20	13.772	0.073	0.024	1169.01	0.2	3967.50	0.7	2.50	4.58e-04	0.0	0.0
21	14.359	0.070	0.024	61.29	1.12e-02	2421.27	0.4	81.99	1.50e-02	0.0	0.0
22	14.543	0.069	0.024	8599.36	1.6	888.75	0.2	0.03	6.10e-06	0.0	0.0
23	14.762	0.068	0.024	2501.47	0.5	743.21	0.1	35.78	6.55e-03	0.0	0.0
24	15.113	0.066	0.024	750.85	0.1	4001.85	0.7	29.06	5.32e-03	0.0	0.0
25	15.667	0.064	0.024	2479.43	0.5	685.39	0.1	586.43	0.1	0.0	0.0
26	16.275	0.061	0.024	30.88	5.66e-03	6759.85	1.2	91.98	1.68e-02	0.0	0.0
27	16.346	0.061	0.024	1646.74	0.3	814.16	0.1	35.66	6.53e-03	0.0	0.0
28	16.574	0.060	0.025	992.38	0.2	1436.54	0.3	5.88	1.08e-03	0.0	0.0
29	17.021	0.059	0.025	8231.75	1.5	1654.23	0.3	526.05	9.63e-02	0.0	0.0
30	17.457	0.057	0.025	6398.67	1.2	2198.42	0.4	388.51	7.11e-02	0.0	0.0
31	17.542	0.057	0.025	2035.52	0.4	37.97	6.95e-03	411.90	7.54e-02	0.0	0.0
32	17.789	0.056	0.025	211.05	3.86e-02	2502.73	0.5	4219.43	0.8	0.0	0.0
33	18.042	0.055	0.025	2249.99	0.4	19.04	3.49e-03	1.00	1.83e-04	0.0	0.0
34	18.256	0.055	0.025	145.67	2.67e-02	1811.51	0.3	2.026e+04	3.7	0.0	0.0
35	19.173	0.052	0.025	1919.78	0.4	125.14	2.29e-02	454.28	8.32e-02	0.0	0.0
36	19.313	0.052	0.025	2.04	3.74e-04	178.33	3.27e-02	1.070e+04	2.0	0.0	0.0
37	19.822	0.050	0.025	75.23	1.38e-02	320.88	5.88e-02	3.356e+04	6.1	0.0	0.0
38	20.138	0.050	0.025	948.37	0.2	11.25	2.06e-03	9133.19	1.7	0.0	0.0
39	20.282	0.049	0.025	106.29	1.95e-02	113.15	2.07e-02	3857.05	0.7	0.0	0.0
40	20.608	0.049	0.025	270.98	4.96e-02	2123.07	0.4	6718.20	1.2	0.0	0.0
41	20.956	0.048	0.026	465.01	8.52e-02	6831.19	1.3	2.077e+04	3.8	0.0	0.0
42	21.194	0.047	0.026	696.26	0.1	43.11	7.89e-03	2.749e+04	5.0	0.0	0.0
43	21.430	0.047	0.026	130.92	2.40e-02	31.39	5.75e-03	1.228e+04	2.2	0.0	0.0
44	21.485	0.047	0.026	1535.09	0.3	3605.99	0.7	2533.07	0.5	0.0	0.0
45	21.857	0.046	0.026	0.41	7.56e-05	3563.48	0.7	4565.98	0.8	0.0	0.0
46	22.067	0.045	0.026	32.19	5.89e-03	684.78	0.1	767.94	0.1	0.0	0.0
47	22.144	0.045	0.026	21.62	3.96e-03	7105.67	1.3	2.437e+04	4.5	0.0	0.0
48	22.769	0.044	0.026	17.31	3.17e-03	6.99	1.28e-03	3.462e+04	6.3	0.0	0.0
49	22.889	0.044	0.026	397.49	7.28e-02	1256.68	0.2	4.824e+04	8.8	0.0	0.0
50	23.055	0.043	0.026	2528.93	0.5	3363.41	0.6	2.833e+04	5.2	0.0	0.0
51	23.709	0.042	0.026	765.43	0.1	4428.86	0.8	9608.87	1.8	0.0	0.0
52	23.999	0.042	0.026	866.27	0.2	694.27	0.1	33.96	6.22e-03	0.0	0.0
53	24.271	0.041	0.026	62.27	1.14e-02	177.72	3.25e-02	142.30	2.61e-02	0.0	0.0
54	24.282	0.041	0.026	246.65	4.52e-02	2296.04	0.4	199.16	3.65e-02	0.0	0.0
55	24.811	0.040	0.026	18.01	3.30e-03	1.51	2.76e-04	469.33	8.59e-02	0.0	0.0
56	24.886	0.040	0.026	247.95	4.54e-02	435.32	7.97e-02	526.82	9.65e-02	0.0	0.0
57	25.095	0.040	0.026	202.90	3.72e-02	270.76	4.96e-02	136.71	2.50e-02	0.0	0.0
58	25.382	0.039	0.026	1.89	3.46e-04	412.42	7.55e-02	301.76	5.53e-02	0.0	0.0
59	25.656	0.039	0.026	1.46	2.67e-04	576.40	0.1	3769.30	0.7	0.0	0.0
60	26.453	0.038	0.026	9.95	1.82e-03	258.01	4.73e-02	1.130e+04	2.1	0.0	0.0
61	26.532	0.038	0.026	238.71	4.37e-02	82.65	1.51e-02	2967.15	0.5	0.0	0.0
62	26.910	0.037	0.026	8.54	1.56e-03	320.49	5.87e-02	5594.76	1.0	0.0	0.0
63	27.101	0.037	0.026	198.13	3.63e-02	378.89	6.94e-02	1.767e+04	3.2	0.0	0.0
64	27.391	0.037	0.026	97.33	1.78e-02	157.19	2.88e-02	5064.58	0.9	0.0	0.0
65	27.556	0.036	0.026	0.31	5.64e-05	340.34	6.23e-02	6173.83	1.1	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	Z %	Energia	Energia x v
66	27.763	0.036	0.026	618.41	0.1	23.48	4.30e-03	854.23	0.2	0.0	0.0
67	27.903	0.036	0.026	25.92	4.75e-03	2064.14	0.4	222.08	4.07e-02	0.0	0.0
68	28.194	0.035	0.026	732.66	0.1	16.82	3.08e-03	3670.98	0.7	0.0	0.0
69	28.306	0.035	0.026	537.93	9.85e-02	588.53	0.1	753.18	0.1	0.0	0.0
70	28.700	0.035	0.026	1891.72	0.3	312.33	5.72e-02	7617.52	1.4	0.0	0.0
71	29.109	0.034	0.027	9.66	1.77e-03	536.69	9.83e-02	4761.66	0.9	0.0	0.0
72	29.848	0.034	0.027	2.28	4.17e-04	4.45	8.14e-04	3.98	7.28e-04	0.0	0.0
73	30.035	0.033	0.027	251.81	4.61e-02	1104.08	0.2	3363.43	0.6	0.0	0.0
74	30.124	0.033	0.027	3.11	5.69e-04	118.09	2.16e-02	31.16	5.71e-03	0.0	0.0
75	30.669	0.033	0.027	545.65	9.99e-02	84.82	1.55e-02	4695.12	0.9	0.0	0.0
76	30.901	0.032	0.027	3.64	6.67e-04	391.15	7.16e-02	217.05	3.97e-02	0.0	0.0
77	31.327	0.032	0.027	621.00	0.1	344.62	6.31e-02	1.303e+04	2.4	0.0	0.0
78	31.415	0.032	0.027	14.58	2.67e-03	289.36	5.30e-02	1119.66	0.2	0.0	0.0
79	31.774	0.031	0.027	91.84	1.68e-02	155.25	2.84e-02	4503.75	0.8	0.0	0.0
80	32.122	0.031	0.027	9.34	1.71e-03	561.20	0.1	1835.72	0.3	0.0	0.0
81	32.457	0.031	0.027	244.37	4.48e-02	61.02	1.12e-02	1254.85	0.2	0.0	0.0
82	32.683	0.031	0.027	941.30	0.2	476.39	8.72e-02	4687.72	0.9	0.0	0.0
83	32.740	0.031	0.027	70.69	1.29e-02	86.37	1.58e-02	2312.07	0.4	0.0	0.0
84	33.211	0.030	0.027	0.78	1.44e-04	78.21	1.43e-02	82.73	1.52e-02	0.0	0.0
85	33.308	0.030	0.027	13.57	2.48e-03	266.39	4.88e-02	0.62	1.13e-04	0.0	0.0
86	33.505	0.030	0.027	191.78	3.51e-02	69.20	1.27e-02	267.76	4.90e-02	0.0	0.0
87	33.846	0.030	0.027	2.84	5.20e-04	3.98e-03	0.0	5099.46	0.9	0.0	0.0
88	34.010	0.029	0.027	62.81	1.15e-02	340.34	6.23e-02	6127.96	1.1	0.0	0.0
89	34.644	0.029	0.027	461.68	8.45e-02	502.16	9.20e-02	2.02	3.70e-04	0.0	0.0
90	35.188	0.028	0.027	4.16	7.61e-04	489.33	8.96e-02	1872.03	0.3	0.0	0.0
91	35.384	0.028	0.027	3.49	6.39e-04	0.09	1.58e-05	4345.15	0.8	0.0	0.0
92	35.990	0.028	0.027	195.20	3.57e-02	27.53	5.04e-03	1639.55	0.3	0.0	0.0
93	36.087	0.028	0.027	2.18	3.99e-04	79.98	1.46e-02	5162.36	0.9	0.0	0.0
94	36.430	0.027	0.027	508.24	9.31e-02	272.34	4.99e-02	11.93	2.18e-03	0.0	0.0
95	36.521	0.027	0.027	160.11	2.93e-02	194.22	3.56e-02	1827.56	0.3	0.0	0.0
96	36.862	0.027	0.027	25.22	4.62e-03	41.20	7.55e-03	1396.28	0.3	0.0	0.0
97	37.051	0.027	0.027	299.84	5.49e-02	22.43	4.11e-03	80.48	1.47e-02	0.0	0.0
98	37.529	0.027	0.027	8.49e-04	0.0	1.02	1.87e-04	486.68	8.91e-02	0.0	0.0
99	37.619	0.027	0.027	30.27	5.54e-03	1.77	3.24e-04	417.95	7.65e-02	0.0	0.0
100	37.697	0.027	0.027	82.66	1.51e-02	33.15	6.07e-03	390.67	7.15e-02	0.0	0.0
101	37.840	0.026	0.027	0.22	4.07e-05	717.83	0.1	4919.19	0.9	0.0	0.0
102	38.326	0.026	0.027	13.53	2.48e-03	558.59	0.1	722.38	0.1	0.0	0.0
103	38.498	0.026	0.027	5.57	1.02e-03	4.73	8.67e-04	242.59	4.44e-02	0.0	0.0
104	38.751	0.026	0.027	272.30	4.99e-02	81.32	1.49e-02	438.39	8.03e-02	0.0	0.0
105	39.309	0.025	0.027	97.96	1.79e-02	143.95	2.64e-02	377.22	6.91e-02	0.0	0.0
106	39.353	0.025	0.027	7.87	1.44e-03	32.39	5.93e-03	84.51	1.55e-02	0.0	0.0
107	39.854	0.025	0.027	104.36	1.91e-02	202.57	3.71e-02	867.00	0.2	0.0	0.0
108	40.063	0.025	0.027	242.57	4.44e-02	1.68	3.08e-04	305.65	5.60e-02	0.0	0.0
109	40.283	0.025	0.027	762.45	0.1	6.24	1.14e-03	48.68	8.92e-03	0.0	0.0
110	40.458	0.025	0.027	269.54	4.94e-02	52.18	9.56e-03	70.08	1.28e-02	0.0	0.0
111	40.586	0.025	0.027	151.62	2.78e-02	561.40	0.1	284.63	5.21e-02	0.0	0.0
112	40.948	0.024	0.027	190.60	3.49e-02	223.20	4.09e-02	307.85	5.64e-02	0.0	0.0
113	41.035	0.024	0.027	101.70	1.86e-02	180.47	3.30e-02	349.23	6.40e-02	0.0	0.0
114	41.326	0.024	0.027	54.87	1.00e-02	0.14	2.52e-05	32.59	5.97e-03	0.0	0.0
115	41.683	0.024	0.027	41.08	7.52e-03	51.32	9.40e-03	147.04	2.69e-02	0.0	0.0
116	41.823	0.024	0.027	796.10	0.1	95.37	1.75e-02	16.47	3.02e-03	0.0	0.0
117	42.037	0.024	0.027	3.32	6.08e-04	48.80	8.94e-03	0.14	2.50e-05	0.0	0.0
118	42.106	0.024	0.027	41.08	7.52e-03	308.81	5.66e-02	157.11	2.88e-02	0.0	0.0
119	42.545	0.024	0.027	3.83	7.02e-04	20.43	3.74e-03	113.35	2.08e-02	0.0	0.0
120	42.803	0.023	0.027	420.21	7.70e-02	52.01	9.52e-03	234.94	4.30e-02	0.0	0.0
121	42.935	0.023	0.027	1826.06	0.3	95.75	1.75e-02	10.38	1.90e-03	0.0	0.0
122	43.126	0.023	0.027	88.71	1.62e-02	26.71	4.89e-03	25.88	4.74e-03	0.0	0.0
123	43.449	0.023	0.027	186.36	3.41e-02	78.34	1.43e-02	7.03	1.29e-03	0.0	0.0
124	43.721	0.023	0.027	28.73	5.26e-03	61.21	1.12e-02	112.65	2.06e-02	0.0	0.0
125	43.923	0.023	0.027	943.18	0.2	7.55	1.38e-03	548.23	0.1	0.0	0.0
126	44.149	0.023	0.027	253.03	4.63e-02	2.36	4.32e-04	67.78	1.24e-02	0.0	0.0
127	44.364	0.023	0.027	3.20	5.86e-04	44.61	8.17e-03	102.28	1.87e-02	0.0	0.0
128	44.603	0.022	0.027	0.66	1.21e-04	13.10	2.40e-03	434.44	7.96e-02	0.0	0.0
129	44.918	0.022	0.027	579.95	0.1	27.67	5.07e-03	142.28	2.61e-02	0.0	0.0
130	45.307	0.022	0.027	519.73	9.52e-02	50.03	9.16e-03	607.60	0.1	0.0	0.0
131	45.338	0.022	0.027	1015.75	0.2	12.09	2.21e-03	168.81	3.09e-02	0.0	0.0
132	45.691	0.022	0.027	12.41	2.27e-03	12.23	2.24e-03	362.17	6.63e-02	0.0	0.0
133	45.893	0.022	0.027	21.54	3.94e-03	0.05	8.27e-06	1.80	3.30e-04	0.0	0.0
134	46.212	0.022	0.028	35.39	6.48e-03	44.13	8.08e-03	527.11	9.65e-02	0.0	0.0
135	46.389	0.022	0.028	517.37	9.47e-02	195.41	3.58e-02	9.77	1.79e-03	0.0	0.0
136	46.631	0.021	0.028	80.15	1.47e-02	0.30	5.43e-05	53.10	9.72e-03	0.0	0.0
137	46.831	0.021	0.028	8.38	1.53e-03	25.95	4.75e-03	1.00	1.84e-04	0.0	0.0
138	47.070	0.021	0.028	0.08	1.43e-05	0.02	2.88e-06	280.94	5.14e-02	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	Z %	Energia	Energia x v
139	47.253	0.021	0.028	14.83	2.72e-03	12.17	2.23e-03	210.13	3.85e-02	0.0	0.0
140	47.585	0.021	0.028	3.86	7.07e-04	544.61	9.97e-02	428.84	7.85e-02	0.0	0.0
141	47.817	0.021	0.028	59.80	1.10e-02	112.84	2.07e-02	226.07	4.14e-02	0.0	0.0
142	48.018	0.021	0.028	0.84	1.54e-04	72.19	1.32e-02	3.20	5.85e-04	0.0	0.0
143	48.342	0.021	0.028	7.17	1.31e-03	1.84	3.36e-04	469.59	8.60e-02	0.0	0.0
144	48.698	0.021	0.028	13.31	2.44e-03	413.38	7.57e-02	7.79	1.43e-03	0.0	0.0
145	48.899	0.020	0.028	6.35	1.16e-03	208.32	3.81e-02	137.36	2.52e-02	0.0	0.0
146	49.143	0.020	0.028	504.84	9.25e-02	8.95	1.64e-03	720.94	0.1	0.0	0.0
147	49.509	0.020	0.028	57.98	1.06e-02	814.93	0.1	0.23	4.17e-05	0.0	0.0
148	49.824	0.020	0.028	374.05	6.85e-02	90.28	1.65e-02	8.76	1.60e-03	0.0	0.0
149	50.169	0.020	0.028	6.12e-03	1.12e-06	31.42	5.75e-03	265.76	4.87e-02	0.0	0.0
150	50.359	0.020	0.028	283.16	5.19e-02	67.81	1.24e-02	92.20	1.69e-02	0.0	0.0
151	50.566	0.020	0.028	403.86	7.40e-02	132.87	2.43e-02	0.31	5.62e-05	0.0	0.0
152	50.892	0.020	0.028	0.28	5.14e-05	215.17	3.94e-02	90.77	1.66e-02	0.0	0.0
153	51.063	0.020	0.028	4.54	8.32e-04	243.21	4.45e-02	157.72	2.89e-02	0.0	0.0
154	51.239	0.020	0.028	53.61	9.82e-03	0.03	5.59e-06	291.89	5.35e-02	0.0	0.0
155	51.291	0.019	0.028	1.66	3.05e-04	11.90	2.18e-03	4.14	7.58e-04	0.0	0.0
156	51.709	0.019	0.028	190.57	3.49e-02	74.14	1.36e-02	671.48	0.1	0.0	0.0
157	51.956	0.019	0.028	394.27	7.22e-02	1.11	2.04e-04	1.40	2.57e-04	0.0	0.0
158	52.391	0.019	0.028	19.50	3.57e-03	107.57	1.97e-02	249.24	4.56e-02	0.0	0.0
159	52.719	0.019	0.028	4.84	8.86e-04	0.55	1.00e-04	149.77	2.74e-02	0.0	0.0
160	52.824	0.019	0.028	92.68	1.70e-02	285.43	5.23e-02	351.97	6.45e-02	0.0	0.0
161	53.103	0.019	0.028	54.89	1.01e-02	37.33	6.84e-03	724.58	0.1	0.0	0.0
162	53.265	0.019	0.028	640.58	0.1	6.92	1.27e-03	103.56	1.90e-02	0.0	0.0
163	53.772	0.019	0.028	8.73	1.60e-03	457.16	8.37e-02	25.41	4.65e-03	0.0	0.0
164	54.029	0.019	0.028	53.07	9.72e-03	0.01	2.59e-06	138.97	2.55e-02	0.0	0.0
165	54.301	0.018	0.028	29.13	5.33e-03	132.27	2.42e-02	1.63	2.98e-04	0.0	0.0
166	54.477	0.018	0.028	0.67	1.23e-04	12.89	2.36e-03	31.46	5.76e-03	0.0	0.0
167	54.722	0.018	0.028	124.09	2.27e-02	0.04	8.02e-06	77.32	1.42e-02	0.0	0.0
168	54.902	0.018	0.028	41.73	7.64e-03	58.12	1.06e-02	150.04	2.75e-02	0.0	0.0
169	55.218	0.018	0.028	1.71	3.14e-04	10.67	1.95e-03	47.05	8.62e-03	0.0	0.0
170	55.299	0.018	0.028	29.31	5.37e-03	119.30	2.18e-02	98.69	1.81e-02	0.0	0.0
171	55.649	0.018	0.028	92.96	1.70e-02	300.56	5.50e-02	62.38	1.14e-02	0.0	0.0
172	55.860	0.018	0.028	2.34	4.29e-04	51.22	9.38e-03	37.13	6.80e-03	0.0	0.0
173	56.145	0.018	0.028	39.32	7.20e-03	287.53	5.27e-02	0.49	9.03e-05	0.0	0.0
174	56.442	0.018	0.028	16.35	2.99e-03	713.66	0.1	388.30	7.11e-02	0.0	0.0
175	56.768	0.018	0.028	505.12	9.25e-02	89.09	1.63e-02	428.15	7.84e-02	0.0	0.0
176	56.897	0.018	0.028	159.69	2.92e-02	15.39	2.82e-03	436.77	8.00e-02	0.0	0.0
177	57.001	0.018	0.028	165.19	3.03e-02	14.65	2.68e-03	147.23	2.70e-02	0.0	0.0
178	57.125	0.018	0.028	9.06	1.66e-03	61.66	1.13e-02	0.79	1.44e-04	0.0	0.0
179	57.292	0.017	0.028	17.23	3.16e-03	163.69	3.00e-02	30.77	5.64e-03	0.0	0.0
180	57.569	0.017	0.028	45.77	8.38e-03	61.02	1.12e-02	5.80	1.06e-03	0.0	0.0
181	57.854	0.017	0.028	666.77	0.1	56.09	1.03e-02	564.56	0.1	0.0	0.0
182	58.144	0.017	0.028	29.36	5.38e-03	352.45	6.45e-02	617.07	0.1	0.0	0.0
183	58.504	0.017	0.028	160.90	2.95e-02	51.11	9.36e-03	89.89	1.65e-02	0.0	0.0
184	58.660	0.017	0.028	0.77	1.40e-04	13.56	2.48e-03	41.85	7.66e-03	0.0	0.0
185	58.725	0.017	0.028	20.76	3.80e-03	4.20	7.69e-04	71.92	1.32e-02	0.0	0.0
186	58.910	0.017	0.028	444.41	8.14e-02	46.33	8.48e-03	351.76	6.44e-02	0.0	0.0
187	59.251	0.017	0.028	4.12	7.55e-04	6.18	1.13e-03	765.27	0.1	0.0	0.0
188	59.546	0.017	0.028	277.96	5.09e-02	93.27	1.71e-02	802.14	0.1	0.0	0.0
189	59.716	0.017	0.028	29.07	5.32e-03	94.74	1.74e-02	1173.84	0.2	0.0	0.0
190	59.879	0.017	0.028	0.56	1.02e-04	4.62	8.45e-04	6.19	1.13e-03	0.0	0.0
191	60.224	0.017	0.028	93.63	1.71e-02	2.06	3.77e-04	8.35	1.53e-03	0.0	0.0
192	60.267	0.017	0.028	2.64	4.84e-04	0.04	6.76e-06	763.60	0.1	0.0	0.0
193	60.480	0.017	0.028	126.66	2.32e-02	40.19	7.36e-03	140.68	2.58e-02	0.0	0.0
194	60.541	0.017	0.028	106.17	1.94e-02	78.65	1.44e-02	0.08	1.49e-05	0.0	0.0
195	60.816	0.016	0.028	31.53	5.77e-03	12.86	2.36e-03	141.64	2.59e-02	0.0	0.0
196	61.046	0.016	0.028	338.43	6.20e-02	0.03	5.51e-06	21.63	3.96e-03	0.0	0.0
197	61.151	0.016	0.028	26.92	4.93e-03	103.90	1.90e-02	35.99	6.59e-03	0.0	0.0
198	61.475	0.016	0.028	45.78	8.38e-03	38.14	6.98e-03	15.24	2.79e-03	0.0	0.0
199	61.573	0.016	0.028	0.05	8.83e-06	488.76	8.95e-02	396.30	7.26e-02	0.0	0.0
200	61.678	0.016	0.028	46.62	8.54e-03	9.71	1.78e-03	280.31	5.13e-02	0.0	0.0
201	61.784	0.016	0.028	0.22	3.98e-05	102.30	1.87e-02	1.32	2.41e-04	0.0	0.0
202	61.869	0.016	0.028	66.13	1.21e-02	5.94	1.09e-03	448.20	8.21e-02	0.0	0.0
203	62.323	0.016	0.028	0.07	1.33e-05	86.04	1.58e-02	163.83	3.00e-02	0.0	0.0
204	62.588	0.016	0.028	5.15	9.43e-04	22.84	4.18e-03	312.83	5.73e-02	0.0	0.0
205	62.737	0.016	0.028	176.37	3.23e-02	236.11	4.32e-02	701.92	0.1	0.0	0.0
206	62.905	0.016	0.028	1.07	1.96e-04	103.96	1.90e-02	98.29	1.80e-02	0.0	0.0
207	63.168	0.016	0.028	62.62	1.15e-02	218.24	4.00e-02	1.67	3.07e-04	0.0	0.0
208	63.357	0.016	0.028	7.50	1.37e-03	4.17	7.63e-04	253.75	4.65e-02	0.0	0.0
209	63.450	0.016	0.028	0.05	1.01e-05	12.51	2.29e-03	63.26	1.16e-02	0.0	0.0
210	63.670	0.016	0.028	3.29e-05	0.0	1.35	2.48e-04	64.21	1.18e-02	0.0	0.0
211	63.907	0.016	0.028	58.25	1.07e-02	408.33	7.48e-02	114.58	2.10e-02	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
212	64.104	0.016	0.028	27.14	4.97e-03	6.60	1.21e-03	85.52	1.57e-02	0.0	0.0
213	64.345	0.016	0.028	14.01	2.57e-03	14.24	2.61e-03	221.71	4.06e-02	0.0	0.0
214	64.492	0.016	0.028	110.69	2.03e-02	5.22	9.55e-04	84.09	1.54e-02	0.0	0.0
215	64.680	0.015	0.028	44.49	8.15e-03	18.42	3.37e-03	9.82	1.80e-03	0.0	0.0
216	65.005	0.015	0.028	71.23	1.30e-02	3.91e-03	0.0	97.17	1.78e-02	0.0	0.0
217	65.239	0.015	0.028	0.33	5.99e-05	707.36	0.1	307.24	5.63e-02	0.0	0.0
218	65.371	0.015	0.028	11.29	2.07e-03	2.21	4.04e-04	1647.02	0.3	0.0	0.0
219	65.528	0.015	0.028	57.10	1.05e-02	127.06	2.33e-02	479.42	8.78e-02	0.0	0.0
220	65.584	0.015	0.028	74.09	1.36e-02	105.79	1.94e-02	1295.90	0.2	0.0	0.0
Risulta In percentuale				5.244e+05 96.03		5.282e+05 96.74		4.768e+05 87.32			

CDC	Tipo	Sigla Id	Note
8	Edk	CDC=Ed (dinamico SLU) alfa=0.0 (ecc. -)	
			verifica esistenti: fattore FC 1.200
			categoria suolo: B
			fattore di sito S = 1.200
			ordinata spettro (tratto Tb-Tc) = 0.022 g
			angolo di ingresso:0.0
			eccentricità aggiuntiva: negativa
			periodo proprio T1: 0.159 sec.
			fattore q: 3.400
			fattore per spost. mu d: 5.217
			classe di duttilità CD: B
			numero di modi considerati:220
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
cm	daN	cm	cm	cm	cm	cm	cm			
1340.00	96.19	-491.36	-334.97	0.0	0.0	-491.36	-334.97	0.155	0.0	0.0
1295.00	116.44	-491.36	-334.97	0.0	0.0	-491.36	-334.97	1.791	0.0	0.0
1250.00	101.25	-491.36	-334.97	0.0	0.0	-491.36	-334.97	1.791	0.0	0.0
1205.00	1203.52	-572.28	-173.84	0.0	26.80	-635.82	-328.32	0.015	2.913	3.350
1195.00	7848.27	-175.90	173.40	0.0	15.15	-313.36	198.69	0.654	1.046	0.168
1160.00	2326.05	-575.55	-168.23	0.0	26.80	-635.82	-328.32	0.015	2.763	3.471
1115.00	2319.30	-575.63	-167.75	0.0	26.80	-635.82	-328.32	0.015	2.759	3.482
1070.00	2319.30	-575.63	-167.75	0.0	26.80	-635.82	-328.32	0.015	2.759	3.482
1025.00	1.465e+04	-128.29	99.57	0.0	52.28	-544.32	97.18	0.605	1.184	0.002
985.00	1.083e+04	-102.23	128.80	0.0	52.28	-542.11	167.56	0.726	1.143	0.047
945.00	1.083e+04	-102.21	128.80	0.0	52.28	-542.11	167.56	0.726	1.143	0.047
905.00	6.437e+04	-130.89	142.36	0.0	52.28	-458.71	212.95	0.530	0.997	0.097
855.00	1.642e+04	-128.78	145.90	0.0	52.28	-485.70	259.69	0.343	1.348	0.177
830.00	1249.33	528.64	424.28	0.0	0.0	0.0	0.0	0.0	0.0	0.0
805.00	1.479e+04	-102.33	164.15	0.0	52.28	-485.70	259.69	0.343	1.448	0.149
780.00	1249.33	528.64	538.78	0.0	0.0	0.0	0.0	0.0	0.0	0.0
755.00	1.526e+04	-82.93	181.97	0.0	52.28	-481.74	260.08	0.362	1.467	0.118
728.69	1131.11	528.64	656.28	0.0	0.0	0.0	0.0	0.0	0.0	0.0
705.00	1.607e+04	-55.85	217.96	0.0	52.28	-388.08	347.18	0.814	0.815	0.144
675.00	466.53	528.64	533.13	0.0	12.20	0.0	0.0	0.0	0.0	0.0
655.00	1.415e+04	-110.23	162.68	0.0	52.28	-485.60	338.86	0.413	1.292	0.286
605.00	1.443e+04	-81.71	180.98	0.0	52.28	-388.24	376.21	0.787	0.765	0.213
555.00	1.494e+04	-58.92	172.30	0.0	52.28	-381.08	258.88	0.824	0.785	0.088
535.00	462.89	-284.62	710.53	0.0	0.0	-295.19	710.53	0.049	0.058	0.0
505.00	1.668e+04	-63.27	192.44	0.0	52.28	-380.93	345.75	0.857	0.759	0.170
455.00	1.393e+05	-26.77	231.20	0.0	52.28	-366.53	489.83	0.922	0.783	0.375
404.44	1.848e+04	-42.92	230.40	0.0	52.28	-385.70	570.64	0.732	0.887	0.542
378.89	7112.79	-473.91	-262.63	0.0	6.20	-474.86	-329.87	2.180	0.006	0.456
353.89	2.196e+04	-32.62	456.21	0.0	61.93	-355.57	632.92	0.678	0.799	0.423
303.33	1.928e+04	-91.51	295.05	0.0	61.93	-445.29	639.78	0.388	1.157	0.686
252.78	2.190e+04	-176.89	242.77	0.0	61.93	-448.92	647.41	0.369	0.913	0.816
202.22	1.592e+04	-73.92	284.63	0.0	61.93	-448.92	647.41	0.369	1.258	0.731
151.67	1.601e+04	-65.56	283.49	0.0	61.93	-448.94	620.41	0.408	1.223	0.654
122.00	7167.74	-473.02	-262.23	0.0	6.20	-474.86	-329.87	2.180	0.012	0.459
101.11	1.343e+04	-59.25	403.57	0.0	61.93	-371.53	681.11	0.575	0.839	0.682
88.00	511.85	445.72	710.53	0.0	0.0	459.84	710.53	0.039	0.268	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
80.00	1592.11	106.62	-334.97	0.0	0.0	101.38	-334.97	0.074	0.024	0.0
50.56	1.912e+04	-72.11	249.76	0.0	61.93	-446.67	538.92	0.539	1.040	0.516
Risulta	5.461e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	4.060	0.246	0.022	574.71	0.1	8.608e+04	15.8	0.10	1.78e-05	0.0	0.0
2	4.217	0.237	0.022	1535.80	0.3	8.421e+04	15.4	0.06	1.09e-05	0.0	0.0
3	6.297	0.159	0.022	3.256e+05	59.6	5178.54	0.9	7.03	1.29e-03	0.0	0.0
4	6.890	0.145	0.022	535.87	9.81e-02	1.516e+05	27.8	4.18	7.65e-04	0.0	0.0
5	7.700	0.130	0.022	5397.59	1.0	260.12	4.76e-02	3.03	5.55e-04	0.0	0.0
6	8.255	0.121	0.022	4.776e+04	8.7	2.879e+04	5.3	37.83	6.93e-03	0.0	0.0
7	8.591	0.116	0.022	4.86	8.91e-04	4.472e+04	8.2	11.33	2.08e-03	0.0	0.0
8	9.027	0.111	0.022	5985.47	1.1	1801.10	0.3	10.22	1.87e-03	0.0	0.0
9	9.236	0.108	0.022	2731.05	0.5	912.40	0.2	46.55	8.52e-03	0.0	0.0
10	9.721	0.103	0.022	1.109e+04	2.0	309.24	5.66e-02	0.32	5.83e-05	0.0	0.0
11	9.832	0.102	0.022	1615.94	0.3	1035.16	0.2	1.89	3.46e-04	0.0	0.0
12	10.046	0.100	0.022	9162.05	1.7	2008.79	0.4	5.84	1.07e-03	0.0	0.0
13	10.469	0.096	0.022	2829.49	0.5	1.900e+04	3.5	4.94	9.06e-04	0.0	0.0
14	10.939	0.091	0.022	1.317e+04	2.4	120.06	2.20e-02	12.90	2.36e-03	0.0	0.0
15	11.184	0.089	0.022	731.74	0.1	260.52	4.77e-02	8.52	1.56e-03	0.0	0.0
16	12.038	0.083	0.023	5897.49	1.1	609.54	0.1	5.12	9.38e-04	0.0	0.0
17	12.741	0.078	0.023	744.75	0.1	6107.25	1.1	10.37	1.90e-03	0.0	0.0
18	12.925	0.077	0.023	8242.37	1.5	406.53	7.44e-02	33.34	6.11e-03	0.0	0.0
19	13.140	0.076	0.023	5937.30	1.1	159.07	2.91e-02	16.62	3.04e-03	0.0	0.0
20	13.640	0.073	0.024	1533.42	0.3	969.28	0.2	1.73	3.17e-04	0.0	0.0
21	14.061	0.071	0.024	956.84	0.2	7121.70	1.3	55.20	1.01e-02	0.0	0.0
22	14.507	0.069	0.024	496.43	9.09e-02	39.04	7.15e-03	121.65	2.23e-02	0.0	0.0
23	14.853	0.067	0.024	546.75	0.1	1899.80	0.3	1.19	2.18e-04	0.0	0.0
24	15.265	0.066	0.024	3890.17	0.7	226.07	4.14e-02	213.74	3.91e-02	0.0	0.0
25	15.545	0.064	0.024	4616.46	0.8	1598.78	0.3	54.37	9.96e-03	0.0	0.0
26	16.048	0.062	0.024	6.45	1.18e-03	4706.60	0.9	245.53	4.50e-02	0.0	0.0
27	16.252	0.062	0.024	762.13	0.1	5362.69	1.0	0.14	2.61e-05	0.0	0.0
28	16.437	0.061	0.025	2095.29	0.4	1394.31	0.3	197.28	3.61e-02	0.0	0.0
29	17.021	0.059	0.025	3125.19	0.6	5.46	1.00e-03	276.86	5.07e-02	0.0	0.0
30	17.221	0.058	0.025	5574.94	1.0	4106.98	0.8	124.52	2.28e-02	0.0	0.0
31	17.988	0.056	0.025	6593.90	1.2	1701.44	0.3	5920.68	1.1	0.0	0.0
32	18.060	0.055	0.025	124.47	2.28e-02	141.78	2.60e-02	0.13	2.42e-05	0.0	0.0
33	18.252	0.055	0.025	166.29	3.05e-02	1748.57	0.3	1.695e+04	3.1	0.0	0.0
34	18.860	0.053	0.025	217.74	3.99e-02	80.85	1.48e-02	311.51	5.70e-02	0.0	0.0
35	19.235	0.052	0.025	1523.61	0.3	185.45	3.40e-02	1.643e+04	3.0	0.0	0.0
36	19.325	0.052	0.025	7.62	1.40e-03	10.15	1.86e-03	3283.38	0.6	0.0	0.0
37	19.865	0.050	0.025	179.19	3.28e-02	320.98	5.88e-02	3.574e+04	6.5	0.0	0.0
38	19.953	0.050	0.025	562.63	0.1	543.16	9.95e-02	776.44	0.1	0.0	0.0
39	20.463	0.049	0.025	1565.64	0.3	3218.74	0.6	7458.55	1.4	0.0	0.0
40	20.651	0.048	0.025	1057.88	0.2	1549.42	0.3	6807.15	1.2	0.0	0.0
41	20.976	0.048	0.026	1.01	1.85e-04	642.44	0.1	20.01	3.67e-03	0.0	0.0
42	21.072	0.047	0.026	422.83	7.74e-02	2491.45	0.5	2.078e+04	3.8	0.0	0.0
43	21.133	0.047	0.026	4773.08	0.9	2.83e-04	0.0	2.446e+04	4.5	0.0	0.0
44	21.279	0.047	0.026	394.69	7.23e-02	132.99	2.44e-02	2580.82	0.5	0.0	0.0
45	21.392	0.047	0.026	4204.62	0.8	1250.02	0.2	63.72	1.17e-02	0.0	0.0
46	21.901	0.046	0.026	81.63	1.49e-02	908.06	0.2	1.722e+04	3.2	0.0	0.0
47	22.039	0.045	0.026	17.30	3.17e-03	7139.72	1.3	322.23	5.90e-02	0.0	0.0
48	22.124	0.045	0.026	3.09	5.65e-04	7154.73	1.3	1.797e+04	3.3	0.0	0.0
49	22.844	0.044	0.026	78.41	1.44e-02	126.45	2.32e-02	1.084e+05	19.8	0.0	0.0
50	23.228	0.043	0.026	5.29	9.69e-04	3751.25	0.7	1.085e+04	2.0	0.0	0.0
51	23.565	0.042	0.026	85.58	1.57e-02	5809.62	1.1	7406.51	1.4	0.0	0.0
52	23.819	0.042	0.026	252.52	4.62e-02	95.91	1.76e-02	954.74	0.2	0.0	0.0
53	24.252	0.041	0.026	1.94	3.56e-04	1819.37	0.3	770.89	0.1	0.0	0.0
54	24.290	0.041	0.026	0.09	1.57e-05	160.49	2.94e-02	28.55	5.23e-03	0.0	0.0
55	24.709	0.040	0.026	0.40	7.40e-05	25.88	4.74e-03	338.71	6.20e-02	0.0	0.0
56	24.917	0.040	0.026	147.36	2.70e-02	49.69	9.10e-03	12.62	2.31e-03	0.0	0.0
57	25.125	0.040	0.026	59.57	1.09e-02	203.97	3.74e-02	315.64	5.78e-02	0.0	0.0
58	25.775	0.039	0.026	45.17	8.27e-03	256.15	4.69e-02	500.28	9.16e-02	0.0	0.0
59	25.973	0.039	0.026	20.31	3.72e-03	689.35	0.1	1.017e+04	1.9	0.0	0.0
60	26.386	0.038	0.026	208.58	3.82e-02	87.66	1.61e-02	6938.85	1.3	0.0	0.0
61	26.674	0.037	0.026	180.79	3.31e-02	3.55	6.49e-04	6593.59	1.2	0.0	0.0
62	26.773	0.037	0.026	5.55	1.02e-03	43.31	7.93e-03	213.37	3.91e-02	0.0	0.0
63	27.116	0.037	0.026	766.66	0.1	811.75	0.1	55.64	1.02e-02	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	Z %	Energia	Energia x v
64	27.461	0.036	0.026	92.60	1.70e-02	2.26	4.14e-04	5038.50	0.9	0.0	0.0
65	27.515	0.036	0.026	3.44	6.30e-04	1376.54	0.3	2.582e+04	4.7	0.0	0.0
66	27.885	0.036	0.026	0.96	1.76e-04	1523.54	0.3	99.01	1.81e-02	0.0	0.0
67	28.203	0.035	0.026	101.25	1.85e-02	40.38	7.39e-03	337.41	6.18e-02	0.0	0.0
68	28.696	0.035	0.026	3.38	6.19e-04	7.08	1.30e-03	4818.41	0.9	0.0	0.0
69	29.132	0.034	0.027	837.21	0.2	13.75	2.52e-03	4441.29	0.8	0.0	0.0
70	29.468	0.034	0.027	1452.13	0.3	418.07	7.66e-02	189.74	3.47e-02	0.0	0.0
71	29.849	0.034	0.027	250.66	4.59e-02	2647.91	0.5	171.80	3.15e-02	0.0	0.0
72	29.979	0.033	0.027	683.69	0.1	7.44	1.36e-03	2099.27	0.4	0.0	0.0
73	30.132	0.033	0.027	37.27	6.83e-03	5.63	1.03e-03	89.74	1.64e-02	0.0	0.0
74	30.342	0.033	0.027	813.76	0.1	17.99	3.29e-03	5339.96	1.0	0.0	0.0
75	30.548	0.033	0.027	121.50	2.22e-02	2.97	5.44e-04	5452.43	1.0	0.0	0.0
76	31.117	0.032	0.027	509.91	9.34e-02	930.21	0.2	826.60	0.2	0.0	0.0
77	31.407	0.032	0.027	557.77	0.1	48.98	8.97e-03	7020.59	1.3	0.0	0.0
78	31.450	0.032	0.027	18.42	3.37e-03	13.50	2.47e-03	361.59	6.62e-02	0.0	0.0
79	31.714	0.032	0.027	1202.64	0.2	29.65	5.43e-03	9465.75	1.7	0.0	0.0
80	31.987	0.031	0.027	102.29	1.87e-02	64.31	1.18e-02	1871.89	0.3	0.0	0.0
81	32.225	0.031	0.027	35.44	6.49e-03	125.74	2.30e-02	272.44	4.99e-02	0.0	0.0
82	32.585	0.031	0.027	287.31	5.26e-02	4.46	8.16e-04	447.12	8.19e-02	0.0	0.0
83	32.775	0.031	0.027	128.02	2.34e-02	21.00	3.85e-03	1.046e+04	1.9	0.0	0.0
84	33.225	0.030	0.027	883.49	0.2	85.99	1.57e-02	1529.62	0.3	0.0	0.0
85	33.471	0.030	0.027	0.11	1.94e-05	783.60	0.1	956.44	0.2	0.0	0.0
86	33.823	0.030	0.027	1044.52	0.2	197.62	3.62e-02	5673.64	1.0	0.0	0.0
87	33.997	0.029	0.027	558.84	0.1	1.10	2.02e-04	1549.00	0.3	0.0	0.0
88	34.173	0.029	0.027	138.28	2.53e-02	662.17	0.1	2634.90	0.5	0.0	0.0
89	34.469	0.029	0.027	70.24	1.29e-02	127.83	2.34e-02	3274.31	0.6	0.0	0.0
90	34.883	0.029	0.027	24.85	4.55e-03	271.29	4.97e-02	1831.04	0.3	0.0	0.0
91	35.095	0.028	0.027	62.54	1.15e-02	81.32	1.49e-02	421.71	7.72e-02	0.0	0.0
92	35.330	0.028	0.027	148.61	2.72e-02	36.17	6.62e-03	984.87	0.2	0.0	0.0
93	36.034	0.028	0.027	124.37	2.28e-02	20.28	3.71e-03	468.91	8.59e-02	0.0	0.0
94	36.100	0.028	0.027	473.48	8.67e-02	152.68	2.80e-02	2.38	4.37e-04	0.0	0.0
95	36.294	0.028	0.027	10.48	1.92e-03	682.30	0.1	4.64	8.50e-04	0.0	0.0
96	36.978	0.027	0.027	42.63	7.81e-03	11.32	2.07e-03	4.60	8.43e-04	0.0	0.0
97	37.070	0.027	0.027	6.92	1.27e-03	44.77	8.20e-03	935.93	0.2	0.0	0.0
98	37.441	0.027	0.027	0.10	1.82e-05	13.88	2.54e-03	18.50	3.39e-03	0.0	0.0
99	37.509	0.027	0.027	248.63	4.55e-02	56.57	1.04e-02	1325.49	0.2	0.0	0.0
100	37.633	0.027	0.027	19.45	3.56e-03	50.98	9.34e-03	4071.35	0.7	0.0	0.0
101	37.836	0.026	0.027	14.46	2.65e-03	159.39	2.92e-02	1003.35	0.2	0.0	0.0
102	37.924	0.026	0.027	20.57	3.77e-03	52.32	9.58e-03	179.20	3.28e-02	0.0	0.0
103	38.310	0.026	0.027	49.33	9.03e-03	654.88	0.1	3051.53	0.6	0.0	0.0
104	38.556	0.026	0.027	105.96	1.94e-02	176.37	3.23e-02	508.67	9.32e-02	0.0	0.0
105	38.654	0.026	0.027	4.21	7.71e-04	79.65	1.46e-02	2506.84	0.5	0.0	0.0
106	39.061	0.026	0.027	2.48e-04	0.0	1.96	3.60e-04	215.70	3.95e-02	0.0	0.0
107	39.592	0.025	0.027	9.62	1.76e-03	24.18	4.43e-03	13.64	2.50e-03	0.0	0.0
108	39.922	0.025	0.027	286.11	5.24e-02	145.35	2.66e-02	744.73	0.1	0.0	0.0
109	40.004	0.025	0.027	233.54	4.28e-02	25.90	4.74e-03	218.79	4.01e-02	0.0	0.0
110	40.121	0.025	0.027	5.65	1.03e-03	34.71	6.36e-03	143.48	2.63e-02	0.0	0.0
111	40.270	0.025	0.027	8.75	1.60e-03	34.02	6.23e-03	5.05	9.24e-04	0.0	0.0
112	40.772	0.025	0.027	10.63	1.95e-03	158.01	2.89e-02	704.80	0.1	0.0	0.0
113	40.894	0.024	0.027	174.50	3.20e-02	147.30	2.70e-02	5.88	1.08e-03	0.0	0.0
114	40.968	0.024	0.027	64.36	1.18e-02	285.87	5.24e-02	575.29	0.1	0.0	0.0
115	41.359	0.024	0.027	32.32	5.92e-03	414.92	7.60e-02	263.98	4.83e-02	0.0	0.0
116	41.395	0.024	0.027	142.66	2.61e-02	442.89	8.11e-02	12.06	2.21e-03	0.0	0.0
117	41.499	0.024	0.027	37.78	6.92e-03	6.19	1.13e-03	181.73	3.33e-02	0.0	0.0
118	41.946	0.024	0.027	2.25	4.13e-04	30.76	5.63e-03	25.57	4.68e-03	0.0	0.0
119	42.360	0.024	0.027	55.24	1.01e-02	72.35	1.33e-02	10.77	1.97e-03	0.0	0.0
120	42.449	0.024	0.027	89.04	1.63e-02	29.14	5.34e-03	280.30	5.13e-02	0.0	0.0
121	42.867	0.023	0.027	2.75	5.04e-04	31.49	5.77e-03	26.21	4.80e-03	0.0	0.0
122	43.072	0.023	0.027	518.00	9.49e-02	73.17	1.34e-02	0.03	5.49e-06	0.0	0.0
123	43.400	0.023	0.027	73.57	1.35e-02	140.65	2.58e-02	663.22	0.1	0.0	0.0
124	43.494	0.023	0.027	90.11	1.65e-02	38.88	7.12e-03	559.69	0.1	0.0	0.0
125	43.749	0.023	0.027	8.88	1.63e-03	40.39	7.40e-03	60.63	1.11e-02	0.0	0.0
126	44.173	0.023	0.027	55.74	1.02e-02	1.16	2.13e-04	65.91	1.21e-02	0.0	0.0
127	44.528	0.022	0.027	99.50	1.82e-02	14.98	2.74e-03	528.69	9.68e-02	0.0	0.0
128	44.694	0.022	0.027	21.94	4.02e-03	103.04	1.89e-02	1211.57	0.2	0.0	0.0
129	45.096	0.022	0.027	195.43	3.58e-02	81.17	1.49e-02	33.90	6.21e-03	0.0	0.0
130	45.197	0.022	0.027	1.63	2.99e-04	34.06	6.24e-03	34.76	6.37e-03	0.0	0.0
131	45.757	0.022	0.027	127.86	2.34e-02	77.83	1.43e-02	316.59	5.80e-02	0.0	0.0
132	46.081	0.022	0.027	426.10	7.80e-02	152.96	2.80e-02	42.91	7.86e-03	0.0	0.0
133	46.217	0.022	0.028	497.43	9.11e-02	2.01	3.67e-04	230.87	4.23e-02	0.0	0.0
134	46.538	0.021	0.028	355.25	6.51e-02	4.04	7.39e-04	147.50	2.70e-02	0.0	0.0
135	46.838	0.021	0.028	762.69	0.1	75.39	1.38e-02	24.38	4.47e-03	0.0	0.0
136	46.917	0.021	0.028	72.48	1.33e-02	102.42	1.88e-02	210.76	3.86e-02	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	Z %	Energia	Energia x v
137	47.145	0.021	0.028	250.73	4.59e-02	3.35	6.14e-04	198.10	3.63e-02	0.0	0.0
138	47.579	0.021	0.028	745.69	0.1	0.07	1.34e-05	51.14	9.37e-03	0.0	0.0
139	47.802	0.021	0.028	1221.34	0.2	48.64	8.91e-03	19.26	3.53e-03	0.0	0.0
140	47.942	0.021	0.028	328.65	6.02e-02	286.31	5.24e-02	5.76	1.05e-03	0.0	0.0
141	48.103	0.021	0.028	31.25	5.72e-03	358.08	6.56e-02	29.88	5.47e-03	0.0	0.0
142	48.246	0.021	0.028	57.41	1.05e-02	337.88	6.19e-02	117.36	2.15e-02	0.0	0.0
143	48.311	0.021	0.028	0.30	5.56e-05	11.58	2.12e-03	0.19	3.51e-05	0.0	0.0
144	48.813	0.020	0.028	61.26	1.12e-02	1.98	3.62e-04	1.92	3.52e-04	0.0	0.0
145	48.834	0.020	0.028	321.53	5.89e-02	254.32	4.66e-02	262.71	4.81e-02	0.0	0.0
146	49.120	0.020	0.028	115.09	2.11e-02	380.08	6.96e-02	2.28	4.17e-04	0.0	0.0
147	49.532	0.020	0.028	19.87	3.64e-03	249.89	4.58e-02	6.05	1.11e-03	0.0	0.0
148	49.712	0.020	0.028	25.55	4.68e-03	110.56	2.02e-02	161.03	2.95e-02	0.0	0.0
149	50.071	0.020	0.028	85.86	1.57e-02	242.24	4.44e-02	3.08	5.64e-04	0.0	0.0
150	50.240	0.020	0.028	243.70	4.46e-02	50.58	9.26e-03	10.12	1.85e-03	0.0	0.0
151	50.584	0.020	0.028	82.58	1.51e-02	67.79	1.24e-02	228.97	4.19e-02	0.0	0.0
152	50.768	0.020	0.028	182.49	3.34e-02	67.94	1.24e-02	21.80	3.99e-03	0.0	0.0
153	50.927	0.020	0.028	1.64	3.01e-04	4.84	8.86e-04	55.37	1.01e-02	0.0	0.0
154	51.027	0.020	0.028	336.56	6.16e-02	57.01	1.04e-02	600.07	0.1	0.0	0.0
155	51.278	0.020	0.028	215.62	3.95e-02	38.95	7.13e-03	405.82	7.43e-02	0.0	0.0
156	51.502	0.019	0.028	0.82	1.51e-04	5.46	1.00e-03	324.81	5.95e-02	0.0	0.0
157	51.793	0.019	0.028	2.03	3.72e-04	105.04	1.92e-02	544.17	9.97e-02	0.0	0.0
158	52.142	0.019	0.028	1.64	3.00e-04	9.78	1.79e-03	79.16	1.45e-02	0.0	0.0
159	52.388	0.019	0.028	150.49	2.76e-02	3.99	7.31e-04	403.01	7.38e-02	0.0	0.0
160	52.805	0.019	0.028	221.46	4.06e-02	3.29	6.02e-04	275.11	5.04e-02	0.0	0.0
161	52.956	0.019	0.028	70.10	1.28e-02	564.53	0.1	899.23	0.2	0.0	0.0
162	53.154	0.019	0.028	61.36	1.12e-02	5.02e-03	0.0	20.40	3.74e-03	0.0	0.0
163	53.511	0.019	0.028	16.43	3.01e-03	389.80	7.14e-02	5.17	9.48e-04	0.0	0.0
164	53.713	0.019	0.028	5.62	1.03e-03	35.37	6.48e-03	161.08	2.95e-02	0.0	0.0
165	53.986	0.019	0.028	111.60	2.04e-02	105.79	1.94e-02	250.49	4.59e-02	0.0	0.0
166	54.484	0.018	0.028	2.67	4.89e-04	0.33	6.03e-05	69.71	1.28e-02	0.0	0.0
167	54.772	0.018	0.028	26.69	4.89e-03	1.92	3.51e-04	101.29	1.85e-02	0.0	0.0
168	55.016	0.018	0.028	15.78	2.89e-03	208.06	3.81e-02	70.62	1.29e-02	0.0	0.0
169	55.301	0.018	0.028	226.62	4.15e-02	80.75	1.48e-02	143.50	2.63e-02	0.0	0.0
170	55.379	0.018	0.028	54.47	9.98e-03	53.79	9.85e-03	41.65	7.63e-03	0.0	0.0
171	55.846	0.018	0.028	316.62	5.80e-02	62.30	1.14e-02	909.86	0.2	0.0	0.0
172	56.135	0.018	0.028	1.65	3.03e-04	888.90	0.2	98.46	1.80e-02	0.0	0.0
173	56.312	0.018	0.028	71.88	1.32e-02	182.96	3.35e-02	0.44	8.05e-05	0.0	0.0
174	56.521	0.018	0.028	320.74	5.87e-02	273.50	5.01e-02	72.75	1.33e-02	0.0	0.0
175	56.641	0.018	0.028	4.03	7.37e-04	1.08	1.97e-04	74.08	1.36e-02	0.0	0.0
176	57.043	0.018	0.028	246.02	4.51e-02	62.63	1.15e-02	607.37	0.1	0.0	0.0
177	57.089	0.018	0.028	0.54	9.84e-05	127.46	2.33e-02	1.73	3.17e-04	0.0	0.0
178	57.349	0.017	0.028	100.25	1.84e-02	187.29	3.43e-02	637.74	0.1	0.0	0.0
179	57.623	0.017	0.028	14.04	2.57e-03	34.86	6.38e-03	7.33	1.34e-03	0.0	0.0
180	57.963	0.017	0.028	15.92	2.92e-03	184.28	3.37e-02	861.60	0.2	0.0	0.0
181	57.998	0.017	0.028	18.33	3.36e-03	6.61	1.21e-03	119.86	2.20e-02	0.0	0.0
182	58.361	0.017	0.028	38.85	7.12e-03	15.85	2.90e-03	619.55	0.1	0.0	0.0
183	58.725	0.017	0.028	31.63	5.79e-03	12.39	2.27e-03	233.74	4.28e-02	0.0	0.0
184	58.822	0.017	0.028	129.28	2.37e-02	0.09	1.59e-05	33.20	6.08e-03	0.0	0.0
185	59.134	0.017	0.028	1.64	3.01e-04	3.30	6.05e-04	143.15	2.62e-02	0.0	0.0
186	59.318	0.017	0.028	2.97	5.44e-04	12.54	2.30e-03	86.88	1.59e-02	0.0	0.0
187	59.429	0.017	0.028	0.04	7.04e-06	60.03	1.10e-02	130.95	2.40e-02	0.0	0.0
188	59.714	0.017	0.028	28.28	5.18e-03	146.69	2.69e-02	375.14	6.87e-02	0.0	0.0
189	60.295	0.017	0.028	11.48	2.10e-03	90.86	1.66e-02	169.37	3.10e-02	0.0	0.0
190	60.403	0.017	0.028	21.95	4.02e-03	401.61	7.35e-02	33.70	6.17e-03	0.0	0.0
191	60.602	0.017	0.028	128.27	2.35e-02	160.83	2.95e-02	337.94	6.19e-02	0.0	0.0
192	60.793	0.016	0.028	4.96	9.07e-04	169.12	3.10e-02	62.00	1.14e-02	0.0	0.0
193	60.992	0.016	0.028	24.12	4.42e-03	38.53	7.06e-03	227.73	4.17e-02	0.0	0.0
194	61.077	0.016	0.028	96.51	1.77e-02	88.62	1.62e-02	15.32	2.81e-03	0.0	0.0
195	61.358	0.016	0.028	185.93	3.40e-02	102.37	1.87e-02	81.30	1.49e-02	0.0	0.0
196	61.741	0.016	0.028	49.79	9.12e-03	238.37	4.37e-02	34.88	6.39e-03	0.0	0.0
197	61.983	0.016	0.028	33.80	6.19e-03	89.15	1.63e-02	296.41	5.43e-02	0.0	0.0
198	62.268	0.016	0.028	16.26	2.98e-03	14.34	2.63e-03	1536.42	0.3	0.0	0.0
199	62.310	0.016	0.028	60.70	1.11e-02	36.23	6.63e-03	165.93	3.04e-02	0.0	0.0
200	62.544	0.016	0.028	3.04	5.58e-04	12.78	2.34e-03	2.34	4.29e-04	0.0	0.0
201	62.694	0.016	0.028	24.99	4.58e-03	21.24	3.89e-03	345.98	6.34e-02	0.0	0.0
202	62.888	0.016	0.028	50.07	9.17e-03	192.30	3.52e-02	0.15	2.77e-05	0.0	0.0
203	62.956	0.016	0.028	223.86	4.10e-02	3.36	6.16e-04	4.95	9.07e-04	0.0	0.0
204	63.091	0.016	0.028	5.78	1.06e-03	3.30	6.04e-04	0.99	1.82e-04	0.0	0.0
205	63.402	0.016	0.028	65.39	1.20e-02	187.00	3.42e-02	47.24	8.65e-03	0.0	0.0
206	63.529	0.016	0.028	0.12	2.15e-05	310.42	5.68e-02	371.75	6.81e-02	0.0	0.0
207	63.730	0.016	0.028	10.80	1.98e-03	33.41	6.12e-03	113.72	2.08e-02	0.0	0.0
208	63.846	0.016	0.028	0.24	4.36e-05	46.28	8.47e-03	234.80	4.30e-02	0.0	0.0
209	64.215	0.016	0.028	55.61	1.02e-02	37.59	6.88e-03	2.71	4.97e-04	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
210	64.321	0.016	0.028	144.83	2.65e-02	26.57	4.87e-03	164.96	3.02e-02	0.0	0.0
211	64.367	0.016	0.028	27.93	5.11e-03	194.48	3.56e-02	392.75	7.19e-02	0.0	0.0
212	64.706	0.015	0.028	5.97	1.09e-03	21.51	3.94e-03	384.03	7.03e-02	0.0	0.0
213	64.800	0.015	0.028	0.05	8.63e-06	127.60	2.34e-02	1.54	2.83e-04	0.0	0.0
214	64.928	0.015	0.028	9.78	1.79e-03	106.60	1.95e-02	8.97	1.64e-03	0.0	0.0
215	65.259	0.015	0.028	92.00	1.68e-02	29.63	5.43e-03	50.05	9.17e-03	0.0	0.0
216	65.546	0.015	0.028	4.63	8.48e-04	159.03	2.91e-02	1199.96	0.2	0.0	0.0
217	65.613	0.015	0.028	29.19	5.35e-03	45.77	8.38e-03	1466.01	0.3	0.0	0.0
218	65.664	0.015	0.028	1.59	2.91e-04	65.62	1.20e-02	3.17	5.80e-04	0.0	0.0
219	65.897	0.015	0.028	46.51	8.52e-03	5.97	1.09e-03	125.15	2.29e-02	0.0	0.0
220	66.037	0.015	0.028	77.66	1.42e-02	58.36	1.07e-02	830.46	0.2	0.0	0.0
Risulta				5.208e+05		5.282e+05		4.765e+05			
In percentuale				95.38		96.73		87.27			

CDC	Tipo	Sigla Id	Note
9	Edk	CDC=Ed (dinamico SLU) alfa=90.00 (ecc. +)	
			verifica esistenti: fattore FC 1.200
			categoria suolo: B
			fattore di sito S = 1.200
			ordinata spettro (tratto Tb-Tc) = 0.022 g
			angolo di ingresso:90.00
			eccentricità aggiuntiva: positiva
			periodo proprio T1: 0.149 sec.
			fattore q: 3.400
			fattore per spost. mu d: 5.501
			classe di duttilità CD: B
			numero di modi considerati:220
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
cm	daN	cm	cm	cm	cm	cm	cm			
1340.00	96.19	-491.36	-334.97	5.50	0.0	-491.36	-334.97	0.155	0.0	0.0
1295.00	116.44	-491.36	-334.97	5.50	0.0	-491.36	-334.97	1.791	0.0	0.0
1250.00	101.25	-491.36	-334.97	5.50	0.0	-491.36	-334.97	1.791	0.0	0.0
1205.00	1203.52	-572.28	-173.84	16.15	0.0	-635.82	-328.32	0.015	2.913	3.350
1195.00	7848.27	-175.90	173.40	23.73	0.0	-313.36	198.69	0.654	1.046	0.168
1160.00	2326.05	-575.55	-168.23	16.15	0.0	-635.82	-328.32	0.015	2.763	3.471
1115.00	2319.30	-575.63	-167.75	16.15	0.0	-635.82	-328.32	0.015	2.759	3.482
1070.00	2319.30	-575.63	-167.75	16.15	0.0	-635.82	-328.32	0.015	2.759	3.482
1025.00	1.465e+04	-128.29	99.57	58.25	0.0	-544.32	97.18	0.605	1.184	0.002
985.00	1.083e+04	-102.23	128.80	58.25	0.0	-542.11	167.56	0.726	1.143	0.047
945.00	1.083e+04	-102.21	128.80	58.25	0.0	-542.11	167.56	0.726	1.143	0.047
905.00	6.437e+04	-130.89	142.36	58.25	0.0	-458.71	212.95	0.530	0.997	0.097
855.00	1.642e+04	-128.78	145.90	58.25	0.0	-485.70	259.69	0.343	1.348	0.177
830.00	1249.33	528.64	424.28	0.0	0.0	0.0	0.0	0.0	0.0	0.0
805.00	1.479e+04	-102.33	164.15	58.25	0.0	-485.70	259.69	0.343	1.448	0.149
780.00	1249.33	528.64	538.78	0.0	0.0	0.0	0.0	0.0	0.0	0.0
755.00	1.526e+04	-82.93	181.97	58.25	0.0	-481.74	260.08	0.362	1.467	0.118
728.69	1131.11	528.64	656.28	0.0	0.0	0.0	0.0	0.0	0.0	0.0
705.00	1.607e+04	-55.85	217.96	58.25	0.0	-388.08	347.18	0.814	0.815	0.144
675.00	466.53	528.64	533.13	0.0	0.0	0.0	0.0	0.0	0.0	0.0
655.00	1.415e+04	-110.23	162.68	58.25	0.0	-485.60	338.86	0.413	1.292	0.286
605.00	1.443e+04	-81.71	180.98	58.25	0.0	-388.24	376.21	0.787	0.765	0.213
555.00	1.494e+04	-58.92	172.30	58.25	0.0	-381.08	258.88	0.824	0.785	0.088
535.00	462.89	-284.62	710.53	25.37	0.0	-295.19	710.53	0.049	0.058	0.0
505.00	1.668e+04	-63.27	192.44	58.25	0.0	-380.93	345.75	0.857	0.759	0.170
455.00	1.393e+05	-26.77	231.20	58.25	0.0	-366.53	489.83	0.922	0.783	0.375
404.44	1.848e+04	-42.92	230.40	58.25	0.0	-385.70	570.64	0.732	0.887	0.542
378.89	7112.79	-473.91	-262.63	16.15	0.0	-474.86	-329.87	2.180	0.006	0.456
353.89	2.196e+04	-32.62	456.21	58.25	0.0	-355.57	632.92	0.678	0.799	0.423
303.33	1.928e+04	-91.51	295.05	58.25	0.0	-445.29	639.78	0.388	1.157	0.686
252.78	2.190e+04	-176.89	242.77	58.25	0.0	-448.92	647.41	0.369	0.913	0.816
202.22	1.592e+04	-73.92	284.63	58.25	0.0	-448.92	647.41	0.369	1.258	0.731
151.67	1.601e+04	-65.56	283.49	58.25	0.0	-448.94	620.41	0.408	1.223	0.654
122.00	7167.74	-473.02	-262.23	16.15	0.0	-474.86	-329.87	2.180	0.012	0.459

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
101.11	1.343e+04	-59.25	403.57	58.25	0.0	-371.53	681.11	0.575	0.839	0.682
88.00	511.85	445.72	710.53	10.71	0.0	459.84	710.53	0.039	0.268	0.0
80.00	1592.11	106.62	-334.97	37.58	0.0	101.38	-334.97	0.074	0.024	0.0
50.56	1.912e+04	-72.11	249.76	58.25	0.0	-446.67	538.92	0.539	1.040	0.516
Risulta	5.461e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	3.930	0.254	0.022	496.54	9.09e-02	8.522e+04	15.6	0.08	1.55e-05	0.0	0.0
2	4.059	0.246	0.022	2033.34	0.4	9.361e+04	17.1	0.05	9.32e-06	0.0	0.0
3	6.124	0.163	0.022	3.185e+05	58.3	176.89	3.24e-02	6.85	1.25e-03	0.0	0.0
4	6.723	0.149	0.022	4922.38	0.9	1.329e+05	24.3	1.34	2.45e-04	0.0	0.0
5	7.492	0.133	0.022	7097.43	1.3	447.14	8.19e-02	3.13	5.74e-04	0.0	0.0
6	8.208	0.122	0.022	4.156e+04	7.6	1.483e+04	2.7	21.68	3.97e-03	0.0	0.0
7	8.419	0.119	0.022	110.20	2.02e-02	7.118e+04	13.0	16.48	3.02e-03	0.0	0.0
8	9.068	0.110	0.022	1.573e+04	2.9	2882.30	0.5	6.65	1.22e-03	0.0	0.0
9	9.091	0.110	0.022	1307.15	0.2	83.41	1.53e-02	64.73	1.19e-02	0.0	0.0
10	9.697	0.103	0.022	1.431e+04	2.6	0.02	2.77e-06	0.16	2.98e-05	0.0	0.0
11	9.828	0.102	0.022	5063.24	0.9	1106.31	0.2	9.24	1.69e-03	0.0	0.0
12	10.139	0.099	0.022	875.17	0.2	692.71	0.1	1.10	2.02e-04	0.0	0.0
13	10.541	0.095	0.022	8628.14	1.6	1.599e+04	2.9	22.28	4.08e-03	0.0	0.0
14	10.715	0.093	0.022	186.47	3.41e-02	4062.67	0.7	2.29	4.19e-04	0.0	0.0
15	11.356	0.088	0.022	7619.48	1.4	161.66	2.96e-02	0.03	6.17e-06	0.0	0.0
16	11.876	0.084	0.023	118.94	2.18e-02	163.30	2.99e-02	7.42	1.36e-03	0.0	0.0
17	12.646	0.079	0.023	3599.48	0.7	1037.10	0.2	3.61	6.61e-04	0.0	0.0
18	12.931	0.077	0.023	9618.77	1.8	4693.11	0.9	49.49	9.06e-03	0.0	0.0
19	13.070	0.077	0.023	6004.82	1.1	259.23	4.75e-02	10.59	1.94e-03	0.0	0.0
20	13.547	0.074	0.024	1580.19	0.3	7472.24	1.4	10.81	1.98e-03	0.0	0.0
21	14.069	0.071	0.024	3909.63	0.7	2408.86	0.4	82.69	1.51e-02	0.0	0.0
22	14.183	0.071	0.024	745.66	0.1	13.51	2.47e-03	58.44	1.07e-02	0.0	0.0
23	14.574	0.069	0.024	55.18	1.01e-02	4710.76	0.9	0.91	1.67e-04	0.0	0.0
24	15.001	0.067	0.024	4572.73	0.8	59.64	1.09e-02	8.21	1.50e-03	0.0	0.0
25	15.196	0.066	0.024	2275.74	0.4	924.58	0.2	344.62	6.31e-02	0.0	0.0
26	15.749	0.063	0.024	3.36	6.15e-04	8645.83	1.6	6.34	1.16e-03	0.0	0.0
27	16.365	0.061	0.024	5880.88	1.1	2529.07	0.5	4.58	8.38e-04	0.0	0.0
28	16.701	0.060	0.025	243.51	4.46e-02	3386.35	0.6	109.09	2.00e-02	0.0	0.0
29	16.938	0.059	0.025	4420.96	0.8	330.86	6.06e-02	433.65	7.94e-02	0.0	0.0
30	17.055	0.059	0.025	2104.32	0.4	2478.11	0.5	55.36	1.01e-02	0.0	0.0
31	17.579	0.057	0.025	1571.97	0.3	530.50	9.72e-02	356.07	6.52e-02	0.0	0.0
32	17.764	0.056	0.025	5019.44	0.9	228.10	4.18e-02	9408.47	1.7	0.0	0.0
33	17.895	0.056	0.025	2953.11	0.5	1523.37	0.3	864.32	0.2	0.0	0.0
34	18.441	0.054	0.025	953.80	0.2	296.87	5.44e-02	7528.20	1.4	0.0	0.0
35	19.238	0.052	0.025	1319.12	0.2	12.88	2.36e-03	9424.08	1.7	0.0	0.0
36	19.321	0.052	0.025	144.89	2.65e-02	93.78	1.72e-02	2.167e+04	4.0	0.0	0.0
37	19.367	0.052	0.025	31.49	5.77e-03	42.35	7.75e-03	1409.98	0.3	0.0	0.0
38	19.624	0.051	0.025	10.85	1.99e-03	482.25	8.83e-02	2.182e+04	4.0	0.0	0.0
39	20.174	0.050	0.025	1289.12	0.2	3880.30	0.7	7623.55	1.4	0.0	0.0
40	20.230	0.049	0.025	339.61	6.22e-02	119.93	2.20e-02	2299.89	0.4	0.0	0.0
41	20.615	0.049	0.025	18.13	3.32e-03	1421.40	0.3	5881.19	1.1	0.0	0.0
42	20.965	0.048	0.026	0.47	8.67e-05	325.19	5.96e-02	2243.23	0.4	0.0	0.0
43	21.207	0.047	0.026	687.61	0.1	280.69	5.14e-02	3.430e+04	6.3	0.0	0.0
44	21.347	0.047	0.026	24.38	4.46e-03	1132.99	0.2	1.788e+04	3.3	0.0	0.0
45	21.514	0.046	0.026	3812.61	0.7	6649.32	1.2	1088.54	0.2	0.0	0.0
46	21.832	0.046	0.026	1994.33	0.4	1589.25	0.3	1.611e+04	3.0	0.0	0.0
47	21.985	0.045	0.026	105.34	1.93e-02	1388.03	0.3	868.41	0.2	0.0	0.0
48	22.033	0.045	0.026	94.20	1.73e-02	313.79	5.75e-02	1985.69	0.4	0.0	0.0
49	22.495	0.044	0.026	942.35	0.2	5415.87	1.0	26.73	4.90e-03	0.0	0.0
50	22.720	0.044	0.026	641.85	0.1	741.82	0.1	1.263e+05	23.1	0.0	0.0
51	23.449	0.043	0.026	7.24	1.33e-03	255.77	4.68e-02	9718.61	1.8	0.0	0.0
52	23.589	0.042	0.026	59.75	1.09e-02	1037.60	0.2	1863.41	0.3	0.0	0.0
53	23.855	0.042	0.026	179.70	3.29e-02	5314.26	1.0	2865.08	0.5	0.0	0.0
54	24.241	0.041	0.026	185.24	3.39e-02	238.35	4.36e-02	1.96	3.59e-04	0.0	0.0
55	24.281	0.041	0.026	131.06	2.40e-02	1693.15	0.3	967.85	0.2	0.0	0.0
56	24.481	0.041	0.026	166.15	3.04e-02	3918.80	0.7	2337.21	0.4	0.0	0.0
57	25.018	0.040	0.026	3.01	5.52e-04	62.39	1.14e-02	0.60	1.10e-04	0.0	0.0
58	25.160	0.040	0.026	14.56	2.67e-03	5.18	9.48e-04	785.81	0.1	0.0	0.0
59	25.559	0.039	0.026	73.15	1.34e-02	10.48	1.92e-03	1.086e+04	2.0	0.0	0.0
60	25.877	0.039	0.026	2.56	4.69e-04	44.15	8.08e-03	1796.67	0.3	0.0	0.0
61	26.222	0.038	0.026	30.06	5.51e-03	0.16	2.98e-05	31.76	5.82e-03	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
62	26.608	0.038	0.026	161.74	2.96e-02	352.42	6.45e-02	4077.99	0.7	0.0	0.0
63	26.932	0.037	0.026	141.98	2.60e-02	2.59	4.74e-04	3820.47	0.7	0.0	0.0
64	27.476	0.036	0.026	152.51	2.79e-02	2535.16	0.5	1.248e+04	2.3	0.0	0.0
65	27.680	0.036	0.026	36.81	6.74e-03	260.77	4.78e-02	4378.99	0.8	0.0	0.0
66	27.723	0.036	0.026	58.36	1.07e-02	1470.51	0.3	4723.37	0.9	0.0	0.0
67	28.037	0.036	0.026	192.78	3.53e-02	152.53	2.79e-02	1.072e+04	2.0	0.0	0.0
68	28.372	0.035	0.026	9.11	1.67e-03	624.27	0.1	310.77	5.69e-02	0.0	0.0
69	28.712	0.035	0.026	169.90	3.11e-02	84.00	1.54e-02	97.79	1.79e-02	0.0	0.0
70	28.862	0.035	0.027	2827.38	0.5	186.31	3.41e-02	1258.26	0.2	0.0	0.0
71	29.045	0.034	0.027	1.65	3.02e-04	691.66	0.1	7961.01	1.5	0.0	0.0
72	29.559	0.034	0.027	646.97	0.1	26.01	4.76e-03	4006.96	0.7	0.0	0.0
73	29.791	0.034	0.027	94.94	1.74e-02	1633.40	0.3	1629.39	0.3	0.0	0.0
74	30.256	0.033	0.027	300.89	5.51e-02	690.41	0.1	6766.69	1.2	0.0	0.0
75	30.436	0.033	0.027	97.64	1.79e-02	853.10	0.2	2807.36	0.5	0.0	0.0
76	30.700	0.033	0.027	686.96	0.1	62.91	1.15e-02	5453.92	1.0	0.0	0.0
77	30.910	0.032	0.027	59.01	1.08e-02	766.79	0.1	1630.84	0.3	0.0	0.0
78	31.041	0.032	0.027	37.85	6.93e-03	7.69	1.41e-03	272.86	5.00e-02	0.0	0.0
79	31.500	0.032	0.027	309.09	5.66e-02	113.89	2.09e-02	4754.07	0.9	0.0	0.0
80	31.774	0.031	0.027	2.37	4.33e-04	27.39	5.02e-03	3031.34	0.6	0.0	0.0
81	31.971	0.031	0.027	592.73	0.1	0.61	1.11e-04	5195.71	1.0	0.0	0.0
82	32.010	0.031	0.027	520.02	9.52e-02	202.61	3.71e-02	1937.23	0.4	0.0	0.0
83	32.273	0.031	0.027	38.35	7.02e-03	6.54	1.20e-03	86.39	1.58e-02	0.0	0.0
84	32.383	0.031	0.027	90.44	1.66e-02	11.35	2.08e-03	2706.34	0.5	0.0	0.0
85	32.942	0.030	0.027	448.58	8.21e-02	362.89	6.65e-02	3954.27	0.7	0.0	0.0
86	33.424	0.030	0.027	382.49	7.00e-02	243.90	4.47e-02	4770.46	0.9	0.0	0.0
87	33.584	0.030	0.027	127.70	2.34e-02	2.87	5.25e-04	1713.66	0.3	0.0	0.0
88	33.878	0.030	0.027	353.16	6.47e-02	631.02	0.1	7.73	1.42e-03	0.0	0.0
89	34.114	0.029	0.027	268.17	4.91e-02	92.61	1.70e-02	3806.69	0.7	0.0	0.0
90	34.276	0.029	0.027	685.59	0.1	79.04	1.45e-02	679.40	0.1	0.0	0.0
91	34.590	0.029	0.027	253.20	4.64e-02	479.59	8.78e-02	1442.28	0.3	0.0	0.0
92	35.283	0.028	0.027	19.45	3.56e-03	0.19	3.51e-05	2339.35	0.4	0.0	0.0
93	35.585	0.028	0.027	173.03	3.17e-02	282.80	5.18e-02	4142.86	0.8	0.0	0.0
94	36.082	0.028	0.027	276.98	5.07e-02	255.39	4.68e-02	211.13	3.87e-02	0.0	0.0
95	36.715	0.027	0.027	12.54	2.30e-03	4.82	8.83e-04	5790.22	1.1	0.0	0.0
96	36.906	0.027	0.027	217.46	3.98e-02	2.17	3.97e-04	777.51	0.1	0.0	0.0
97	37.032	0.027	0.027	5.10	9.33e-04	7.63	1.40e-03	1.50	2.75e-04	0.0	0.0
98	37.363	0.027	0.027	16.87	3.09e-03	172.31	3.16e-02	314.94	5.77e-02	0.0	0.0
99	37.490	0.027	0.027	8.89	1.63e-03	337.95	6.19e-02	2982.46	0.5	0.0	0.0
100	37.781	0.026	0.027	172.14	3.15e-02	306.63	5.62e-02	648.19	0.1	0.0	0.0
101	38.112	0.026	0.027	139.45	2.55e-02	58.64	1.07e-02	2184.14	0.4	0.0	0.0
102	38.266	0.026	0.027	0.05	8.85e-06	106.25	1.95e-02	1548.89	0.3	0.0	0.0
103	38.626	0.026	0.027	181.99	3.33e-02	4.05	7.41e-04	0.36	6.63e-05	0.0	0.0
104	39.158	0.026	0.027	33.56	6.15e-03	140.36	2.57e-02	84.58	1.55e-02	0.0	0.0
105	39.396	0.025	0.027	0.62	1.14e-04	13.41	2.46e-03	137.37	2.52e-02	0.0	0.0
106	39.550	0.025	0.027	160.19	2.93e-02	282.39	5.17e-02	754.06	0.1	0.0	0.0
107	39.627	0.025	0.027	266.94	4.89e-02	33.43	6.12e-03	3.62	6.62e-04	0.0	0.0
108	39.982	0.025	0.027	621.95	0.1	41.30	7.56e-03	935.32	0.2	0.0	0.0
109	40.165	0.025	0.027	1.43	2.62e-04	14.48	2.65e-03	211.41	3.87e-02	0.0	0.0
110	40.286	0.025	0.027	16.66	3.05e-03	19.95	3.65e-03	38.09	6.98e-03	0.0	0.0
111	40.478	0.025	0.027	2.77	5.06e-04	200.58	3.67e-02	469.89	8.61e-02	0.0	0.0
112	40.776	0.025	0.027	170.31	3.12e-02	89.99	1.65e-02	279.78	5.12e-02	0.0	0.0
113	41.187	0.024	0.027	38.25	7.00e-03	5.10	9.35e-04	339.67	6.22e-02	0.0	0.0
114	41.243	0.024	0.027	251.44	4.60e-02	4.64	8.50e-04	28.78	5.27e-03	0.0	0.0
115	41.614	0.024	0.027	51.44	9.42e-03	190.01	3.48e-02	21.00	3.85e-03	0.0	0.0
116	42.043	0.024	0.027	3.66	6.70e-04	7.45	1.36e-03	199.20	3.65e-02	0.0	0.0
117	42.120	0.024	0.027	248.12	4.54e-02	76.56	1.40e-02	6.27	1.15e-03	0.0	0.0
118	42.396	0.024	0.027	5.11	9.36e-04	556.27	0.1	49.28	9.03e-03	0.0	0.0
119	42.668	0.023	0.027	222.00	4.07e-02	105.31	1.93e-02	143.98	2.64e-02	0.0	0.0
120	42.917	0.023	0.027	175.94	3.22e-02	64.85	1.19e-02	341.23	6.25e-02	0.0	0.0
121	43.165	0.023	0.027	321.75	5.89e-02	62.44	1.14e-02	274.14	5.02e-02	0.0	0.0
122	43.320	0.023	0.027	2.37	4.34e-04	116.20	2.13e-02	216.61	3.97e-02	0.0	0.0
123	43.601	0.023	0.027	46.36	8.49e-03	2.36	4.33e-04	353.49	6.47e-02	0.0	0.0
124	43.682	0.023	0.027	219.63	4.02e-02	231.82	4.25e-02	164.61	3.01e-02	0.0	0.0
125	43.973	0.023	0.027	1175.22	0.2	6.49	1.19e-03	220.22	4.03e-02	0.0	0.0
126	44.312	0.023	0.027	1329.67	0.2	3.21	5.87e-04	62.59	1.15e-02	0.0	0.0
127	44.478	0.022	0.027	6.39	1.17e-03	39.80	7.29e-03	51.52	9.43e-03	0.0	0.0
128	44.589	0.022	0.027	11.58	2.12e-03	21.36	3.91e-03	13.23	2.42e-03	0.0	0.0
129	44.856	0.022	0.027	253.56	4.64e-02	387.59	7.10e-02	131.66	2.41e-02	0.0	0.0
130	45.221	0.022	0.027	249.96	4.58e-02	84.29	1.54e-02	239.33	4.38e-02	0.0	0.0
131	45.503	0.022	0.027	213.94	3.92e-02	119.21	2.18e-02	542.67	9.94e-02	0.0	0.0
132	45.663	0.022	0.027	0.48	8.82e-05	40.23	7.37e-03	0.34	6.21e-05	0.0	0.0
133	45.782	0.022	0.027	440.22	8.06e-02	494.07	9.05e-02	6.95	1.27e-03	0.0	0.0
134	45.870	0.022	0.027	90.73	1.66e-02	38.34	7.02e-03	1643.39	0.3	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	Z %	Energia	Energia x v
135	46.214	0.022	0.028	944.84	0.2	8.27	1.51e-03	184.78	3.38e-02	0.0	0.0
136	46.564	0.021	0.028	143.54	2.63e-02	415.87	7.62e-02	64.19	1.18e-02	0.0	0.0
137	46.698	0.021	0.028	530.02	9.71e-02	0.02	3.08e-06	116.29	2.13e-02	0.0	0.0
138	46.968	0.021	0.028	8.84	1.62e-03	6.03	1.10e-03	34.31	6.28e-03	0.0	0.0
139	47.129	0.021	0.028	61.89	1.13e-02	31.89	5.84e-03	19.35	3.54e-03	0.0	0.0
140	47.576	0.021	0.028	348.56	6.38e-02	18.68	3.42e-03	11.77	2.15e-03	0.0	0.0
141	47.686	0.021	0.028	2.50	4.58e-04	131.64	2.41e-02	39.66	7.26e-03	0.0	0.0
142	48.005	0.021	0.028	132.29	2.42e-02	53.50	9.80e-03	0.04	7.89e-06	0.0	0.0
143	48.430	0.021	0.028	83.14	1.52e-02	64.23	1.18e-02	151.82	2.78e-02	0.0	0.0
144	48.752	0.021	0.028	617.62	0.1	70.31	1.29e-02	749.73	0.1	0.0	0.0
145	49.000	0.020	0.028	48.50	8.88e-03	150.21	2.75e-02	21.43	3.92e-03	0.0	0.0
146	49.235	0.020	0.028	0.71	1.31e-04	13.99	2.56e-03	0.02	3.15e-06	0.0	0.0
147	49.628	0.020	0.028	129.16	2.37e-02	24.61	4.51e-03	61.43	1.12e-02	0.0	0.0
148	49.898	0.020	0.028	128.09	2.35e-02	69.83	1.28e-02	26.11	4.78e-03	0.0	0.0
149	50.044	0.020	0.028	8.51	1.56e-03	535.35	9.80e-02	130.27	2.39e-02	0.0	0.0
150	50.116	0.020	0.028	3.02	5.52e-04	76.39	1.40e-02	101.00	1.85e-02	0.0	0.0
151	50.338	0.020	0.028	86.06	1.58e-02	363.52	6.66e-02	125.15	2.29e-02	0.0	0.0
152	50.603	0.020	0.028	27.87	5.10e-03	38.24	7.00e-03	22.97	4.21e-03	0.0	0.0
153	50.622	0.020	0.028	6.59	1.21e-03	1.13	2.06e-04	0.76	1.40e-04	0.0	0.0
154	50.904	0.020	0.028	49.55	9.07e-03	1.21	2.22e-04	267.23	4.89e-02	0.0	0.0
155	51.056	0.020	0.028	2.70	4.95e-04	494.63	9.06e-02	129.58	2.37e-02	0.0	0.0
156	51.188	0.020	0.028	33.57	6.15e-03	189.03	3.46e-02	242.94	4.45e-02	0.0	0.0
157	51.823	0.019	0.028	52.41	9.60e-03	137.29	2.51e-02	573.46	0.1	0.0	0.0
158	52.026	0.019	0.028	108.14	1.98e-02	0.66	1.21e-04	105.93	1.94e-02	0.0	0.0
159	52.351	0.019	0.028	874.49	0.2	551.93	0.1	44.07	8.07e-03	0.0	0.0
160	52.652	0.019	0.028	1.40	2.56e-04	177.90	3.26e-02	153.85	2.82e-02	0.0	0.0
161	52.682	0.019	0.028	164.28	3.01e-02	135.70	2.49e-02	1302.59	0.2	0.0	0.0
162	53.131	0.019	0.028	16.05	2.94e-03	159.52	2.92e-02	13.15	2.41e-03	0.0	0.0
163	53.320	0.019	0.028	58.30	1.07e-02	133.57	2.45e-02	226.14	4.14e-02	0.0	0.0
164	53.551	0.019	0.028	10.10	1.85e-03	235.03	4.30e-02	19.70	3.61e-03	0.0	0.0
165	53.626	0.019	0.028	1.25	2.29e-04	27.61	5.06e-03	89.08	1.63e-02	0.0	0.0
166	53.862	0.019	0.028	68.37	1.25e-02	24.63	4.51e-03	125.13	2.29e-02	0.0	0.0
167	53.986	0.019	0.028	14.44	2.64e-03	169.88	3.11e-02	82.37	1.51e-02	0.0	0.0
168	54.274	0.018	0.028	2.24	4.11e-04	11.41	2.09e-03	0.06	1.02e-05	0.0	0.0
169	54.600	0.018	0.028	0.27	5.03e-05	346.15	6.34e-02	8.22	1.50e-03	0.0	0.0
170	54.740	0.018	0.028	139.06	2.55e-02	53.30	9.76e-03	649.90	0.1	0.0	0.0
171	54.980	0.018	0.028	178.29	3.26e-02	403.41	7.39e-02	12.54	2.30e-03	0.0	0.0
172	55.123	0.018	0.028	19.28	3.53e-03	287.54	5.27e-02	6.99	1.28e-03	0.0	0.0
173	55.466	0.018	0.028	321.48	5.89e-02	54.98	1.01e-02	7.86	1.44e-03	0.0	0.0
174	55.896	0.018	0.028	0.47	8.70e-05	145.13	2.66e-02	34.83	6.38e-03	0.0	0.0
175	56.098	0.018	0.028	27.44	5.03e-03	52.46	9.61e-03	591.60	0.1	0.0	0.0
176	56.308	0.018	0.028	1.05	1.93e-04	194.30	3.56e-02	115.85	2.12e-02	0.0	0.0
177	56.539	0.018	0.028	69.98	1.28e-02	33.36	6.11e-03	4.82	8.83e-04	0.0	0.0
178	57.053	0.018	0.028	172.55	3.16e-02	15.98	2.93e-03	129.92	2.38e-02	0.0	0.0
179	57.190	0.017	0.028	2.92	5.35e-04	8.31	1.52e-03	203.03	3.72e-02	0.0	0.0
180	57.254	0.017	0.028	8.96	1.64e-03	12.46	2.28e-03	2.55	4.67e-04	0.0	0.0
181	57.542	0.017	0.028	35.31	6.47e-03	307.93	5.64e-02	38.84	7.11e-03	0.0	0.0
182	57.700	0.017	0.028	21.20	3.88e-03	32.57	5.97e-03	0.15	2.83e-05	0.0	0.0
183	57.902	0.017	0.028	74.78	1.37e-02	105.34	1.93e-02	5.42e-04	0.0	0.0	0.0
184	58.307	0.017	0.028	142.64	2.61e-02	49.39	9.04e-03	1670.41	0.3	0.0	0.0
185	58.690	0.017	0.028	0.79	1.44e-04	2.72	4.98e-04	73.59	1.35e-02	0.0	0.0
186	58.964	0.017	0.028	66.82	1.22e-02	19.74	3.61e-03	26.63	4.88e-03	0.0	0.0
187	59.222	0.017	0.028	6.25e-03	1.14e-06	3.24	5.93e-04	180.23	3.30e-02	0.0	0.0
188	59.273	0.017	0.028	68.76	1.26e-02	44.12	8.08e-03	271.71	4.98e-02	0.0	0.0
189	59.456	0.017	0.028	71.98	1.32e-02	13.92	2.55e-03	1820.55	0.3	0.0	0.0
190	59.612	0.017	0.028	14.17	2.60e-03	131.84	2.41e-02	148.52	2.72e-02	0.0	0.0
191	59.928	0.017	0.028	196.00	3.59e-02	0.01	2.52e-06	16.72	3.06e-03	0.0	0.0
192	60.212	0.017	0.028	6.60	1.21e-03	263.82	4.83e-02	258.44	4.73e-02	0.0	0.0
193	60.534	0.017	0.028	15.49	2.84e-03	2.21	4.05e-04	64.25	1.18e-02	0.0	0.0
194	60.789	0.016	0.028	95.44	1.75e-02	1.28	2.34e-04	103.97	1.90e-02	0.0	0.0
195	61.018	0.016	0.028	56.29	1.03e-02	68.53	1.26e-02	0.03	4.91e-06	0.0	0.0
196	61.138	0.016	0.028	396.81	7.27e-02	111.93	2.05e-02	211.20	3.87e-02	0.0	0.0
197	61.289	0.016	0.028	25.53	4.68e-03	7.75	1.42e-03	1191.83	0.2	0.0	0.0
198	61.633	0.016	0.028	4.71	8.63e-04	61.85	1.13e-02	1407.80	0.3	0.0	0.0
199	61.759	0.016	0.028	115.83	2.12e-02	229.46	4.20e-02	41.05	7.52e-03	0.0	0.0
200	62.011	0.016	0.028	0.79	1.45e-04	8.11	1.49e-03	48.89	8.95e-03	0.0	0.0
201	62.168	0.016	0.028	71.50	1.31e-02	94.47	1.73e-02	3.65	6.68e-04	0.0	0.0
202	62.256	0.016	0.028	8.87	1.62e-03	18.29	3.35e-03	0.56	1.03e-04	0.0	0.0
203	62.589	0.016	0.028	0.06	1.03e-05	88.37	1.62e-02	145.19	2.66e-02	0.0	0.0
204	62.678	0.016	0.028	86.11	1.58e-02	18.37	3.36e-03	17.47	3.20e-03	0.0	0.0
205	62.837	0.016	0.028	78.77	1.44e-02	32.62	5.97e-03	113.39	2.08e-02	0.0	0.0
206	62.920	0.016	0.028	2.76	5.06e-04	13.73	2.51e-03	63.67	1.17e-02	0.0	0.0
207	63.069	0.016	0.028	27.88	5.11e-03	346.79	6.35e-02	85.95	1.57e-02	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
208	63.312	0.016	0.028	39.06	7.15e-03	1.34	2.45e-04	66.79	1.22e-02	0.0	0.0
209	63.423	0.016	0.028	99.83	1.83e-02	0.94	1.73e-04	128.18	2.35e-02	0.0	0.0
210	63.617	0.016	0.028	12.69	2.32e-03	22.74	4.17e-03	98.58	1.81e-02	0.0	0.0
211	63.852	0.016	0.028	62.38	1.14e-02	12.41	2.27e-03	10.68	1.95e-03	0.0	0.0
212	64.057	0.016	0.028	27.72	5.08e-03	88.99	1.63e-02	22.05	4.04e-03	0.0	0.0
213	64.072	0.016	0.028	62.25	1.14e-02	49.29	9.03e-03	46.85	8.58e-03	0.0	0.0
214	64.196	0.016	0.028	174.20	3.19e-02	36.41	6.67e-03	3.17	5.80e-04	0.0	0.0
215	64.555	0.015	0.028	371.13	6.80e-02	2.26	4.14e-04	108.51	1.99e-02	0.0	0.0
216	64.774	0.015	0.028	24.66	4.52e-03	7.87	1.44e-03	362.30	6.63e-02	0.0	0.0
217	65.011	0.015	0.028	49.88	9.13e-03	172.87	3.17e-02	735.15	0.1	0.0	0.0
218	65.403	0.015	0.028	228.29	4.18e-02	4.38	8.02e-04	478.82	8.77e-02	0.0	0.0
219	65.608	0.015	0.028	63.89	1.17e-02	0.31	5.72e-05	904.74	0.2	0.0	0.0
220	66.051	0.015	0.028	237.04	4.34e-02	88.34	1.62e-02	616.15	0.1	0.0	0.0
Risulta In percentuale				5.229e+05 95.76		5.278e+05 96.66		4.756e+05 87.10			

CDC	Tipo	Sigla Id	Note
10	Edk	CDC=Ed (dinamico SLU) alfa=90.00 (ecc. -)	
			verifica esistenti: fattore FC 1.200
			categoria suolo: B
			fattore di sito S = 1.200
			ordinata spettro (tratto Tb-Tc) = 0.022 g
			angolo di ingresso:90.00
			eccentricità aggiuntiva: negativa
			periodo proprio T1: 0.142 sec.
			fattore q: 3.400
			fattore per spost. mu d: 5.705
			classe di duttilità CD: B
			numero di modi considerati:220
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
cm	daN	cm	cm	cm	cm	cm	cm			
1340.00	96.19	-491.36	-334.97	-5.50	0.0	-491.36	-334.97	0.155	0.0	0.0
1295.00	116.44	-491.36	-334.97	-5.50	0.0	-491.36	-334.97	1.791	0.0	0.0
1250.00	101.25	-491.36	-334.97	-5.50	0.0	-491.36	-334.97	1.791	0.0	0.0
1205.00	1203.52	-572.28	-173.84	-16.15	0.0	-635.82	-328.32	0.015	2.913	3.350
1195.00	7848.27	-175.90	173.40	-23.73	0.0	-313.36	198.69	0.654	1.046	0.168
1160.00	2326.05	-575.55	-168.23	-16.15	0.0	-635.82	-328.32	0.015	2.763	3.471
1115.00	2319.30	-575.63	-167.75	-16.15	0.0	-635.82	-328.32	0.015	2.759	3.482
1070.00	2319.30	-575.63	-167.75	-16.15	0.0	-635.82	-328.32	0.015	2.759	3.482
1025.00	1.465e+04	-128.29	99.57	-58.25	0.0	-544.32	97.18	0.605	1.184	0.002
985.00	1.083e+04	-102.23	128.80	-58.25	0.0	-542.11	167.56	0.726	1.143	0.047
945.00	1.083e+04	-102.21	128.80	-58.25	0.0	-542.11	167.56	0.726	1.143	0.047
905.00	6.437e+04	-130.89	142.36	-58.25	0.0	-458.71	212.95	0.530	0.997	0.097
855.00	1.642e+04	-128.78	145.90	-58.25	0.0	-485.70	259.69	0.343	1.348	0.177
830.00	1249.33	528.64	424.28	0.0	0.0	0.0	0.0	0.0	0.0	0.0
805.00	1.479e+04	-102.33	164.15	-58.25	0.0	-485.70	259.69	0.343	1.448	0.149
780.00	1249.33	528.64	538.78	0.0	0.0	0.0	0.0	0.0	0.0	0.0
755.00	1.526e+04	-82.93	181.97	-58.25	0.0	-481.74	260.08	0.362	1.467	0.118
728.69	1131.11	528.64	656.28	0.0	0.0	0.0	0.0	0.0	0.0	0.0
705.00	1.607e+04	-55.85	217.96	-58.25	0.0	-388.08	347.18	0.814	0.815	0.144
675.00	466.53	528.64	533.13	0.0	0.0	0.0	0.0	0.0	0.0	0.0
655.00	1.415e+04	-110.23	162.68	-58.25	0.0	-485.60	338.86	0.413	1.292	0.286
605.00	1.443e+04	-81.71	180.98	-58.25	0.0	-388.24	376.21	0.787	0.765	0.213
555.00	1.494e+04	-58.92	172.30	-58.25	0.0	-381.08	258.88	0.824	0.785	0.088
535.00	462.89	-284.62	710.53	-25.37	0.0	-295.19	710.53	0.049	0.058	0.0
505.00	1.668e+04	-63.27	192.44	-58.25	0.0	-380.93	345.75	0.857	0.759	0.170
455.00	1.393e+05	-26.77	231.20	-58.25	0.0	-366.53	489.83	0.922	0.783	0.375
404.44	1.848e+04	-42.92	230.40	-58.25	0.0	-385.70	570.64	0.732	0.887	0.542
378.89	7112.79	-473.91	-262.63	-16.15	0.0	-474.86	-329.87	2.180	0.006	0.456
353.89	2.196e+04	-32.62	456.21	-58.25	0.0	-355.57	632.92	0.678	0.799	0.423
303.33	1.928e+04	-91.51	295.05	-58.25	0.0	-445.29	639.78	0.388	1.157	0.686
252.78	2.190e+04	-176.89	242.77	-58.25	0.0	-448.92	647.41	0.369	0.913	0.816
202.22	1.592e+04	-73.92	284.63	-58.25	0.0	-448.92	647.41	0.369	1.258	0.731

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
151.67	1.601e+04	-65.56	283.49	-58.25	0.0	-448.94	620.41	0.408	1.223	0.654
122.00	7167.74	-473.02	-262.23	-16.15	0.0	-474.86	-329.87	2.180	0.012	0.459
101.11	1.343e+04	-59.25	403.57	-58.25	0.0	-371.53	681.11	0.575	0.839	0.682
88.00	511.85	445.72	710.53	-10.71	0.0	459.84	710.53	0.039	0.268	0.0
80.00	1592.11	106.62	-334.97	-37.58	0.0	101.38	-334.97	0.074	0.024	0.0
50.56	1.912e+04	-72.11	249.76	-58.25	0.0	-446.67	538.92	0.539	1.040	0.516
Risulta	5.461e+05									

Modo	Frequenza	Periodo	Acc. Spetttrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	4.195	0.238	0.022	774.14	0.1	8.205e+04	15.0	0.12	2.14e-05	0.0	0.0
2	4.376	0.229	0.022	2488.22	0.5	8.018e+04	14.7	0.09	1.61e-05	0.0	0.0
3	6.123	0.163	0.022	3.182e+05	58.3	1.496e+04	2.7	4.83	8.84e-04	0.0	0.0
4	7.026	0.142	0.022	8019.33	1.5	1.732e+05	31.7	8.19	1.50e-03	0.0	0.0
5	7.743	0.129	0.022	8784.12	1.6	2.97	5.45e-04	3.45	6.31e-04	0.0	0.0
6	8.420	0.119	0.022	4.832e+04	8.8	2.357e+04	4.3	41.99	7.69e-03	0.0	0.0
7	8.701	0.115	0.022	143.40	2.63e-02	2.565e+04	4.7	13.89	2.54e-03	0.0	0.0
8	9.197	0.109	0.022	3801.24	0.7	7212.28	1.3	20.64	3.78e-03	0.0	0.0
9	9.402	0.106	0.022	6040.17	1.1	1377.73	0.3	33.90	6.21e-03	0.0	0.0
10	9.878	0.101	0.022	3586.10	0.7	3440.92	0.6	3.13	5.74e-04	0.0	0.0
11	9.967	0.100	0.022	5823.70	1.1	21.35	3.91e-03	1.04	1.91e-04	0.0	0.0
12	10.401	0.096	0.022	9627.06	1.8	776.94	0.1	0.63	1.16e-04	0.0	0.0
13	10.634	0.094	0.022	2819.20	0.5	1.696e+04	3.1	5.00	9.15e-04	0.0	0.0
14	10.910	0.092	0.022	3719.33	0.7	40.64	7.44e-03	17.77	3.25e-03	0.0	0.0
15	11.493	0.087	0.023	1.109e+04	2.0	169.80	3.11e-02	1.37	2.51e-04	0.0	0.0
16	12.542	0.080	0.023	6996.57	1.3	193.83	3.55e-02	4.65	8.52e-04	0.0	0.0
17	12.905	0.077	0.023	1193.13	0.2	7034.82	1.3	33.62	6.16e-03	0.0	0.0
18	13.020	0.077	0.023	1353.09	0.2	1047.40	0.2	17.28	3.17e-03	0.0	0.0
19	13.522	0.074	0.023	7743.48	1.4	18.97	3.47e-03	4.59	8.40e-04	0.0	0.0
20	13.877	0.072	0.024	1379.72	0.3	782.61	0.1	5.05	9.25e-04	0.0	0.0
21	14.455	0.069	0.024	504.71	9.24e-02	4786.68	0.9	86.23	1.58e-02	0.0	0.0
22	14.789	0.068	0.024	856.43	0.2	427.15	7.82e-02	20.87	3.82e-03	0.0	0.0
23	15.040	0.066	0.024	4046.55	0.7	372.69	6.83e-02	19.05	3.49e-03	0.0	0.0
24	15.515	0.064	0.024	5514.93	1.0	40.71	7.46e-03	219.49	4.02e-02	0.0	0.0
25	15.687	0.064	0.024	832.29	0.2	6417.61	1.2	111.59	2.04e-02	0.0	0.0
26	15.997	0.063	0.024	0.58	1.06e-04	290.35	5.32e-02	19.05	3.49e-03	0.0	0.0
27	16.537	0.060	0.025	56.99	1.04e-02	1651.93	0.3	633.64	0.1	0.0	0.0
28	16.919	0.059	0.025	3232.23	0.6	19.41	3.55e-03	362.79	6.64e-02	0.0	0.0
29	17.041	0.059	0.025	2257.99	0.4	4508.02	0.8	3.64	6.66e-04	0.0	0.0
30	17.476	0.057	0.025	1.185e+04	2.2	980.18	0.2	2161.88	0.4	0.0	0.0
31	18.101	0.055	0.025	155.84	2.85e-02	3448.83	0.6	1691.34	0.3	0.0	0.0
32	18.252	0.055	0.025	1037.93	0.2	45.50	8.33e-03	4146.03	0.8	0.0	0.0
33	18.451	0.054	0.025	651.05	0.1	2839.31	0.5	1.674e+04	3.1	0.0	0.0
34	18.664	0.054	0.025	22.14	4.06e-03	4.56	8.35e-04	1.166e+04	2.1	0.0	0.0
35	19.271	0.052	0.025	1270.02	0.2	8.17	1.50e-03	6444.83	1.2	0.0	0.0
36	19.370	0.052	0.025	1157.10	0.2	119.41	2.19e-02	1259.67	0.2	0.0	0.0
37	20.016	0.050	0.025	83.63	1.53e-02	3028.54	0.6	4271.63	0.8	0.0	0.0
38	20.348	0.049	0.025	55.28	1.01e-02	54.13	9.91e-03	3.104e+04	5.7	0.0	0.0
39	20.582	0.049	0.025	823.12	0.2	667.71	0.1	3.265e+04	6.0	0.0	0.0
40	20.939	0.048	0.026	519.01	9.50e-02	9219.42	1.7	6786.46	1.2	0.0	0.0
41	21.103	0.047	0.026	212.08	3.88e-02	2837.82	0.5	2.221e+04	4.1	0.0	0.0
42	21.262	0.047	0.026	2545.21	0.5	1511.71	0.3	3127.15	0.6	0.0	0.0
43	21.604	0.046	0.026	557.56	0.1	119.65	2.19e-02	859.94	0.2	0.0	0.0
44	21.827	0.046	0.026	3819.16	0.7	3.59	6.57e-04	1.420e+04	2.6	0.0	0.0
45	21.901	0.046	0.026	57.84	1.06e-02	20.58	3.77e-03	3135.01	0.6	0.0	0.0
46	22.099	0.045	0.026	239.50	4.39e-02	1700.21	0.3	354.76	6.50e-02	0.0	0.0
47	22.208	0.045	0.026	74.71	1.37e-02	5185.83	0.9	2.048e+04	3.8	0.0	0.0
48	22.351	0.045	0.026	258.74	4.74e-02	8070.36	1.5	1094.67	0.2	0.0	0.0
49	22.946	0.044	0.026	342.99	6.28e-02	576.03	0.1	1.062e+05	19.4	0.0	0.0
50	23.367	0.043	0.026	337.26	6.18e-02	2255.79	0.4	197.26	3.61e-02	0.0	0.0
51	23.411	0.043	0.026	881.60	0.2	1418.54	0.3	1.039e+04	1.9	0.0	0.0
52	24.085	0.042	0.026	65.68	1.20e-02	1237.95	0.2	526.00	9.63e-02	0.0	0.0
53	24.227	0.041	0.026	196.89	3.61e-02	11.84	2.17e-03	1167.37	0.2	0.0	0.0
54	24.396	0.041	0.026	296.23	5.42e-02	64.66	1.18e-02	721.59	0.1	0.0	0.0
55	25.214	0.040	0.026	0.07	1.19e-05	27.10	4.96e-03	55.58	1.02e-02	0.0	0.0
56	25.559	0.039	0.026	218.80	4.01e-02	24.62	4.51e-03	1022.08	0.2	0.0	0.0
57	25.999	0.038	0.026	0.80	1.47e-04	171.53	3.14e-02	876.78	0.2	0.0	0.0
58	26.196	0.038	0.026	15.78	2.89e-03	267.65	4.90e-02	4340.65	0.8	0.0	0.0
59	26.447	0.038	0.026	50.77	9.30e-03	1293.13	0.2	1.157e+04	2.1	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	Z %	Energia	Energia x v
60	26.763	0.037	0.026	84.47	1.55e-02	83.67	1.53e-02	2.808e+04	5.1	0.0	0.0
61	26.950	0.037	0.026	172.80	3.16e-02	58.43	1.07e-02	40.84	7.48e-03	0.0	0.0
62	27.402	0.036	0.026	31.33	5.74e-03	942.31	0.2	2177.84	0.4	0.0	0.0
63	27.566	0.036	0.026	0.66	1.21e-04	251.87	4.61e-02	15.65	2.87e-03	0.0	0.0
64	27.652	0.036	0.026	250.87	4.59e-02	51.87	9.50e-03	6009.69	1.1	0.0	0.0
65	27.913	0.036	0.026	194.80	3.57e-02	698.78	0.1	7327.08	1.3	0.0	0.0
66	28.109	0.036	0.026	146.59	2.68e-02	802.73	0.1	1201.68	0.2	0.0	0.0
67	28.489	0.035	0.026	279.50	5.12e-02	3.22	5.89e-04	264.82	4.85e-02	0.0	0.0
68	28.676	0.035	0.026	21.58	3.95e-03	88.23	1.62e-02	194.18	3.56e-02	0.0	0.0
69	28.929	0.035	0.027	2264.83	0.4	147.31	2.70e-02	2574.16	0.5	0.0	0.0
70	28.975	0.035	0.027	200.11	3.66e-02	20.15	3.69e-03	778.57	0.1	0.0	0.0
71	29.149	0.034	0.027	84.42	1.55e-02	325.13	5.95e-02	1616.06	0.3	0.0	0.0
72	29.422	0.034	0.027	259.73	4.76e-02	421.92	7.73e-02	1262.31	0.2	0.0	0.0
73	29.967	0.033	0.027	25.42	4.65e-03	920.27	0.2	420.94	7.71e-02	0.0	0.0
74	30.421	0.033	0.027	122.78	2.25e-02	10.26	1.88e-03	4993.72	0.9	0.0	0.0
75	31.023	0.032	0.027	128.52	2.35e-02	3.38	6.18e-04	3621.44	0.7	0.0	0.0
76	31.502	0.032	0.027	90.97	1.67e-02	574.52	0.1	2702.12	0.5	0.0	0.0
77	31.556	0.032	0.027	1387.64	0.3	13.45	2.46e-03	973.89	0.2	0.0	0.0
78	31.804	0.031	0.027	378.82	6.94e-02	4.44	8.13e-04	2.420e+04	4.4	0.0	0.0
79	32.161	0.031	0.027	55.86	1.02e-02	59.90	1.10e-02	258.99	4.74e-02	0.0	0.0
80	32.313	0.031	0.027	377.27	6.91e-02	522.67	9.57e-02	137.21	2.51e-02	0.0	0.0
81	32.617	0.031	0.027	848.93	0.2	234.98	4.30e-02	0.02	3.57e-06	0.0	0.0
82	32.862	0.030	0.027	149.95	2.75e-02	493.64	9.04e-02	314.18	5.75e-02	0.0	0.0
83	32.902	0.030	0.027	21.49	3.94e-03	34.74	6.36e-03	1888.32	0.3	0.0	0.0
84	33.466	0.030	0.027	564.30	0.1	176.45	3.23e-02	3403.53	0.6	0.0	0.0
85	33.771	0.030	0.027	154.39	2.83e-02	145.63	2.67e-02	2230.61	0.4	0.0	0.0
86	33.901	0.029	0.027	6.94	1.27e-03	85.23	1.56e-02	2986.10	0.5	0.0	0.0
87	34.089	0.029	0.027	150.96	2.76e-02	107.15	1.96e-02	1545.99	0.3	0.0	0.0
88	34.424	0.029	0.027	263.18	4.82e-02	10.58	1.94e-03	4449.73	0.8	0.0	0.0
89	34.578	0.029	0.027	30.46	5.58e-03	2.33	4.26e-04	2044.97	0.4	0.0	0.0
90	34.857	0.029	0.027	9.86	1.81e-03	282.59	5.18e-02	142.40	2.61e-02	0.0	0.0
91	35.264	0.028	0.027	36.46	6.68e-03	539.45	9.88e-02	830.11	0.2	0.0	0.0
92	35.582	0.028	0.027	840.78	0.2	179.00	3.28e-02	3976.40	0.7	0.0	0.0
93	35.911	0.028	0.027	69.98	1.28e-02	1721.01	0.3	151.40	2.77e-02	0.0	0.0
94	36.152	0.028	0.027	317.94	5.82e-02	2.49	4.56e-04	98.29	1.80e-02	0.0	0.0
95	36.240	0.028	0.027	6.73	1.23e-03	475.72	8.71e-02	418.00	7.65e-02	0.0	0.0
96	37.163	0.027	0.027	0.04	6.88e-06	45.08	8.26e-03	5451.31	1.0	0.0	0.0
97	37.267	0.027	0.027	45.45	8.32e-03	73.94	1.35e-02	4.01	7.33e-04	0.0	0.0
98	37.641	0.027	0.027	12.33	2.26e-03	17.16	3.14e-03	3.69	6.76e-04	0.0	0.0
99	37.772	0.026	0.027	69.46	1.27e-02	289.51	5.30e-02	797.99	0.1	0.0	0.0
100	37.855	0.026	0.027	3.19	5.83e-04	454.75	8.33e-02	3398.39	0.6	0.0	0.0
101	38.121	0.026	0.027	15.47	2.83e-03	2.45	4.48e-04	3045.53	0.6	0.0	0.0
102	38.615	0.026	0.027	623.36	0.1	68.00	1.25e-02	19.43	3.56e-03	0.0	0.0
103	38.742	0.026	0.027	138.16	2.53e-02	140.64	2.58e-02	165.33	3.03e-02	0.0	0.0
104	39.072	0.026	0.027	6.66	1.22e-03	2.75	5.03e-04	12.36	2.26e-03	0.0	0.0
105	39.181	0.026	0.027	194.01	3.55e-02	221.22	4.05e-02	374.33	6.86e-02	0.0	0.0
106	39.412	0.025	0.027	256.21	4.69e-02	3.29	6.02e-04	451.66	8.27e-02	0.0	0.0
107	39.583	0.025	0.027	161.36	2.96e-02	435.88	7.98e-02	20.87	3.82e-03	0.0	0.0
108	39.955	0.025	0.027	6.85	1.26e-03	53.60	9.82e-03	38.69	7.09e-03	0.0	0.0
109	40.019	0.025	0.027	91.51	1.68e-02	308.23	5.64e-02	11.36	2.08e-03	0.0	0.0
110	40.258	0.025	0.027	150.85	2.76e-02	41.75	7.65e-03	1032.63	0.2	0.0	0.0
111	40.412	0.025	0.027	3.86	7.06e-04	91.58	1.68e-02	178.22	3.26e-02	0.0	0.0
112	40.612	0.025	0.027	40.83	7.48e-03	141.42	2.59e-02	561.27	0.1	0.0	0.0
113	41.128	0.024	0.027	7.94	1.45e-03	117.06	2.14e-02	412.46	7.55e-02	0.0	0.0
114	41.556	0.024	0.027	12.68	2.32e-03	0.02	3.44e-06	119.77	2.19e-02	0.0	0.0
115	41.710	0.024	0.027	32.17	5.89e-03	288.18	5.28e-02	12.74	2.33e-03	0.0	0.0
116	41.923	0.024	0.027	8.50	1.56e-03	6.72	1.23e-03	24.90	4.56e-03	0.0	0.0
117	42.123	0.024	0.027	33.87	6.20e-03	6.72	1.23e-03	1.38	2.54e-04	0.0	0.0
118	42.221	0.024	0.027	7.87	1.44e-03	1.36	2.48e-04	136.68	2.50e-02	0.0	0.0
119	42.844	0.023	0.027	655.15	0.1	16.42	3.01e-03	112.10	2.05e-02	0.0	0.0
120	42.996	0.023	0.027	141.22	2.59e-02	10.98	2.01e-03	77.16	1.41e-02	0.0	0.0
121	43.220	0.023	0.027	273.39	5.01e-02	49.26	9.02e-03	484.47	8.87e-02	0.0	0.0
122	43.616	0.023	0.027	13.17	2.41e-03	32.94	6.03e-03	532.67	9.75e-02	0.0	0.0
123	43.702	0.023	0.027	125.02	2.29e-02	65.57	1.20e-02	31.25	5.72e-03	0.0	0.0
124	43.972	0.023	0.027	4.49	8.21e-04	0.87	1.59e-04	7.68	1.41e-03	0.0	0.0
125	44.233	0.023	0.027	70.09	1.28e-02	55.19	1.01e-02	0.32	5.84e-05	0.0	0.0
126	44.519	0.022	0.027	185.18	3.39e-02	106.44	1.95e-02	177.02	3.24e-02	0.0	0.0
127	44.808	0.022	0.027	237.21	4.34e-02	6.34	1.16e-03	127.60	2.34e-02	0.0	0.0
128	45.067	0.022	0.027	205.21	3.76e-02	25.62	4.69e-03	351.96	6.45e-02	0.0	0.0
129	45.096	0.022	0.027	13.17	2.41e-03	16.67	3.05e-03	271.14	4.97e-02	0.0	0.0
130	45.301	0.022	0.027	2101.37	0.4	41.03	7.51e-03	890.80	0.2	0.0	0.0
131	45.701	0.022	0.027	2120.21	0.4	180.44	3.30e-02	791.96	0.1	0.0	0.0
132	45.941	0.022	0.027	42.32	7.75e-03	0.79	1.44e-04	36.12	6.61e-03	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	Z %	Energia	Energia x v
133	46.181	0.022	0.028	324.57	5.94e-02	8.20e-03	1.50e-06	50.61	9.27e-03	0.0	0.0
134	46.281	0.022	0.028	28.68	5.25e-03	250.32	4.58e-02	23.68	4.34e-03	0.0	0.0
135	46.517	0.021	0.028	18.94	3.47e-03	8.43	1.54e-03	145.11	2.66e-02	0.0	0.0
136	46.627	0.021	0.028	115.76	2.12e-02	2.30	4.21e-04	113.59	2.08e-02	0.0	0.0
137	46.732	0.021	0.028	627.71	0.1	129.83	2.38e-02	98.69	1.81e-02	0.0	0.0
138	46.906	0.021	0.028	43.99	8.06e-03	164.65	3.02e-02	69.55	1.27e-02	0.0	0.0
139	47.176	0.021	0.028	10.75	1.97e-03	20.53	3.76e-03	319.67	5.85e-02	0.0	0.0
140	47.815	0.021	0.028	27.49	5.04e-03	0.24	4.48e-05	113.13	2.07e-02	0.0	0.0
141	48.516	0.021	0.028	29.70	5.44e-03	502.06	9.19e-02	0.34	6.24e-05	0.0	0.0
142	48.670	0.021	0.028	5.91	1.08e-03	627.92	0.1	494.77	9.06e-02	0.0	0.0
143	48.914	0.020	0.028	101.78	1.86e-02	130.83	2.40e-02	5.14	9.41e-04	0.0	0.0
144	49.047	0.020	0.028	301.41	5.52e-02	8.34	1.53e-03	535.63	9.81e-02	0.0	0.0
145	49.303	0.020	0.028	47.57	8.71e-03	25.51	4.67e-03	161.22	2.95e-02	0.0	0.0
146	49.591	0.020	0.028	43.07	7.89e-03	32.03	5.87e-03	14.47	2.65e-03	0.0	0.0
147	49.738	0.020	0.028	9.46	1.73e-03	40.11	7.34e-03	80.21	1.47e-02	0.0	0.0
148	50.030	0.020	0.028	1.91	3.50e-04	136.26	2.50e-02	673.87	0.1	0.0	0.0
149	50.123	0.020	0.028	288.57	5.28e-02	220.84	4.04e-02	15.27	2.80e-03	0.0	0.0
150	50.450	0.020	0.028	23.93	4.38e-03	42.04	7.70e-03	46.02	8.43e-03	0.0	0.0
151	50.593	0.020	0.028	4.91e-04	0.0	403.95	7.40e-02	14.61	2.68e-03	0.0	0.0
152	50.787	0.020	0.028	29.73	5.44e-03	74.83	1.37e-02	42.08	7.71e-03	0.0	0.0
153	51.100	0.020	0.028	123.75	2.27e-02	24.63	4.51e-03	25.96	4.75e-03	0.0	0.0
154	51.241	0.020	0.028	334.07	6.12e-02	37.69	6.90e-03	64.86	1.19e-02	0.0	0.0
155	51.503	0.019	0.028	140.54	2.57e-02	0.30	5.47e-05	7.30	1.34e-03	0.0	0.0
156	51.984	0.019	0.028	18.41	3.37e-03	4.03	7.39e-04	60.34	1.10e-02	0.0	0.0
157	52.287	0.019	0.028	0.34	6.19e-05	128.99	2.36e-02	75.71	1.39e-02	0.0	0.0
158	52.523	0.019	0.028	203.83	3.73e-02	49.57	9.08e-03	729.97	0.1	0.0	0.0
159	52.738	0.019	0.028	301.06	5.51e-02	12.21	2.24e-03	659.11	0.1	0.0	0.0
160	53.324	0.019	0.028	171.27	3.14e-02	3.27	5.99e-04	10.67	1.95e-03	0.0	0.0
161	53.530	0.019	0.028	24.91	4.56e-03	238.64	4.37e-02	414.09	7.58e-02	0.0	0.0
162	53.700	0.019	0.028	35.33	6.47e-03	159.59	2.92e-02	83.99	1.54e-02	0.0	0.0
163	53.820	0.019	0.028	11.09	2.03e-03	259.97	4.76e-02	164.29	3.01e-02	0.0	0.0
164	53.899	0.019	0.028	53.31	9.76e-03	191.02	3.50e-02	50.70	9.29e-03	0.0	0.0
165	54.153	0.018	0.028	43.22	7.92e-03	40.11	7.35e-03	103.69	1.90e-02	0.0	0.0
166	54.476	0.018	0.028	167.45	3.07e-02	77.84	1.43e-02	253.77	4.65e-02	0.0	0.0
167	54.957	0.018	0.028	341.42	6.25e-02	63.46	1.16e-02	292.05	5.35e-02	0.0	0.0
168	54.979	0.018	0.028	61.98	1.14e-02	86.25	1.58e-02	33.61	6.16e-03	0.0	0.0
169	55.429	0.018	0.028	3.35	6.14e-04	150.51	2.76e-02	72.57	1.33e-02	0.0	0.0
170	55.872	0.018	0.028	78.62	1.44e-02	54.93	1.01e-02	38.40	7.03e-03	0.0	0.0
171	56.018	0.018	0.028	72.73	1.33e-02	65.71	1.20e-02	34.87	6.39e-03	0.0	0.0
172	56.333	0.018	0.028	31.84	5.83e-03	252.59	4.63e-02	920.19	0.2	0.0	0.0
173	56.777	0.018	0.028	173.48	3.18e-02	0.13	2.30e-05	3.37	6.18e-04	0.0	0.0
174	56.816	0.018	0.028	4.88	8.94e-04	30.89	5.66e-03	235.95	4.32e-02	0.0	0.0
175	57.023	0.018	0.028	101.85	1.87e-02	19.27	3.53e-03	684.35	0.1	0.0	0.0
176	57.221	0.017	0.028	0.03	4.83e-06	27.39	5.02e-03	0.79	1.45e-04	0.0	0.0
177	57.530	0.017	0.028	31.03	5.68e-03	0.64	1.16e-04	6.55	1.20e-03	0.0	0.0
178	57.851	0.017	0.028	1.13	2.07e-04	381.52	6.99e-02	95.14	1.74e-02	0.0	0.0
179	58.067	0.017	0.028	70.49	1.29e-02	93.87	1.72e-02	1097.90	0.2	0.0	0.0
180	58.347	0.017	0.028	10.73	1.96e-03	209.61	3.84e-02	323.36	5.92e-02	0.0	0.0
181	58.585	0.017	0.028	27.37	5.01e-03	95.44	1.75e-02	188.62	3.45e-02	0.0	0.0
182	58.687	0.017	0.028	2.19	4.00e-04	0.08	1.38e-05	527.30	9.66e-02	0.0	0.0
183	58.870	0.017	0.028	45.26	8.29e-03	410.49	7.52e-02	245.04	4.49e-02	0.0	0.0
184	59.279	0.017	0.028	16.51	3.02e-03	231.17	4.23e-02	132.89	2.43e-02	0.0	0.0
185	59.311	0.017	0.028	70.32	1.29e-02	253.12	4.64e-02	1.97	3.61e-04	0.0	0.0
186	59.597	0.017	0.028	26.73	4.89e-03	27.62	5.06e-03	385.53	7.06e-02	0.0	0.0
187	59.832	0.017	0.028	42.20	7.73e-03	18.78	3.44e-03	86.90	1.59e-02	0.0	0.0
188	60.166	0.017	0.028	336.24	6.16e-02	74.68	1.37e-02	75.78	1.39e-02	0.0	0.0
189	60.390	0.017	0.028	331.00	6.06e-02	52.86	9.68e-03	556.22	0.1	0.0	0.0
190	60.664	0.016	0.028	10.90	2.00e-03	118.30	2.17e-02	710.63	0.1	0.0	0.0
191	60.695	0.016	0.028	147.13	2.69e-02	40.14	7.35e-03	9.21	1.69e-03	0.0	0.0
192	61.025	0.016	0.028	20.58	3.77e-03	434.89	7.96e-02	183.49	3.36e-02	0.0	0.0
193	61.386	0.016	0.028	129.48	2.37e-02	174.33	3.19e-02	50.66	9.28e-03	0.0	0.0
194	61.523	0.016	0.028	120.99	2.22e-02	147.13	2.69e-02	432.27	7.92e-02	0.0	0.0
195	61.726	0.016	0.028	72.99	1.34e-02	0.91	1.68e-04	0.24	4.31e-05	0.0	0.0
196	61.856	0.016	0.028	0.16	2.85e-05	3.67	6.73e-04	92.79	1.70e-02	0.0	0.0
197	62.039	0.016	0.028	3.08	5.64e-04	0.91	1.67e-04	197.09	3.61e-02	0.0	0.0
198	62.130	0.016	0.028	173.22	3.17e-02	20.82	3.81e-03	163.81	3.00e-02	0.0	0.0
199	62.430	0.016	0.028	9.38	1.72e-03	1.95	3.58e-04	113.95	2.09e-02	0.0	0.0
200	62.522	0.016	0.028	48.33	8.85e-03	6.02	1.10e-03	99.11	1.81e-02	0.0	0.0
201	62.709	0.016	0.028	32.77	6.00e-03	0.05	8.53e-06	455.68	8.35e-02	0.0	0.0
202	62.820	0.016	0.028	53.36	9.77e-03	16.29	2.98e-03	146.07	2.67e-02	0.0	0.0
203	62.960	0.016	0.028	11.41	2.09e-03	13.29	2.43e-03	2.40	4.40e-04	0.0	0.0
204	63.074	0.016	0.028	5.67	1.04e-03	41.30	7.56e-03	10.09	1.85e-03	0.0	0.0
205	63.138	0.016	0.028	111.69	2.05e-02	303.97	5.57e-02	163.62	3.00e-02	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
206	63.206	0.016	0.028	35.72	6.54e-03	118.47	2.17e-02	133.56	2.45e-02	0.0	0.0
207	63.491	0.016	0.028	2.56	4.70e-04	26.33	4.82e-03	219.98	4.03e-02	0.0	0.0
208	63.712	0.016	0.028	0.55	1.01e-04	156.66	2.87e-02	48.52	8.89e-03	0.0	0.0
209	63.993	0.016	0.028	46.35	8.49e-03	168.85	3.09e-02	361.75	6.62e-02	0.0	0.0
210	64.215	0.016	0.028	352.54	6.46e-02	817.07	0.1	292.94	5.36e-02	0.0	0.0
211	64.420	0.016	0.028	115.85	2.12e-02	46.71	8.55e-03	26.72	4.89e-03	0.0	0.0
212	64.480	0.016	0.028	38.07	6.97e-03	149.34	2.73e-02	1301.78	0.2	0.0	0.0
213	64.699	0.015	0.028	73.76	1.35e-02	316.69	5.80e-02	170.17	3.12e-02	0.0	0.0
214	64.791	0.015	0.028	0.03	4.92e-06	3.38	6.19e-04	8.03	1.47e-03	0.0	0.0
215	64.980	0.015	0.028	127.39	2.33e-02	21.69	3.97e-03	48.32	8.85e-03	0.0	0.0
216	65.200	0.015	0.028	34.45	6.31e-03	19.40	3.55e-03	1008.32	0.2	0.0	0.0
217	65.492	0.015	0.028	194.30	3.56e-02	9.87	1.81e-03	106.67	1.95e-02	0.0	0.0
218	65.700	0.015	0.028	0.22	4.09e-05	319.03	5.84e-02	1333.22	0.2	0.0	0.0
219	65.924	0.015	0.028	4.94	9.05e-04	226.38	4.15e-02	87.40	1.60e-02	0.0	0.0
220	66.340	0.015	0.028	490.58	8.98e-02	98.83	1.81e-02	15.38	2.82e-03	0.0	0.0
Risulta				5.232e+05		5.288e+05		4.763e+05			
In percentuale				95.82		96.84		87.23			

CDC	Tipo	Sigla Id	Note
11	Edk	CDC=Ed (dinamico SLD) alfa=0.0 (ecc. +)	
			verifica esistenti: fattore FC 1.200
			categoria suolo: B
			fattore di sito S = 1.200
			ordinata spettro (tratto Tb-Tc) = 0.075 g
			angolo di ingresso:0.0
			eccentricità aggiuntiva: positiva
			periodo proprio T1: 0.168 sec.
			numero di modi considerati:220
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
cm	daN	cm	cm	cm	cm	cm	cm			
1340.00	96.19	-491.36	-334.97	0.0	0.0	-491.36	-334.97	0.155	0.0	0.0
1295.00	116.44	-491.36	-334.97	0.0	0.0	-491.36	-334.97	1.791	0.0	0.0
1250.00	101.25	-491.36	-334.97	0.0	0.0	-491.36	-334.97	1.791	0.0	0.0
1205.00	1203.52	-572.28	-173.84	0.0	-26.80	-635.82	-328.32	0.015	2.913	3.350
1195.00	7848.27	-175.90	173.40	0.0	-15.15	-313.36	198.69	0.654	1.046	0.168
1160.00	2326.05	-575.55	-168.23	0.0	-26.80	-635.82	-328.32	0.015	2.763	3.471
1115.00	2319.30	-575.63	-167.75	0.0	-26.80	-635.82	-328.32	0.015	2.759	3.482
1070.00	2319.30	-575.63	-167.75	0.0	-26.80	-635.82	-328.32	0.015	2.759	3.482
1025.00	1.465e+04	-128.29	99.57	0.0	-52.28	-544.32	97.18	0.605	1.184	0.002
985.00	1.083e+04	-102.23	128.80	0.0	-52.28	-542.11	167.56	0.726	1.143	0.047
945.00	1.083e+04	-102.21	128.80	0.0	-52.28	-542.11	167.56	0.726	1.143	0.047
905.00	6.437e+04	-130.89	142.36	0.0	-52.28	-458.71	212.95	0.530	0.997	0.097
855.00	1.642e+04	-128.78	145.90	0.0	-52.28	-485.70	259.69	0.343	1.348	0.177
830.00	1249.33	528.64	424.28	0.0	0.0	0.0	0.0	0.0	0.0	0.0
805.00	1.479e+04	-102.33	164.15	0.0	-52.28	-485.70	259.69	0.343	1.448	0.149
780.00	1249.33	528.64	538.78	0.0	0.0	0.0	0.0	0.0	0.0	0.0
755.00	1.526e+04	-82.93	181.97	0.0	-52.28	-481.74	260.08	0.362	1.467	0.118
728.69	1131.11	528.64	656.28	0.0	0.0	0.0	0.0	0.0	0.0	0.0
705.00	1.607e+04	-55.85	217.96	0.0	-52.28	-388.08	347.18	0.814	0.815	0.144
675.00	466.53	528.64	533.13	0.0	-12.20	0.0	0.0	0.0	0.0	0.0
655.00	1.415e+04	-110.23	162.68	0.0	-52.28	-485.60	338.86	0.413	1.292	0.286
605.00	1.443e+04	-81.71	180.98	0.0	-52.28	-388.24	376.21	0.787	0.765	0.213
555.00	1.494e+04	-58.92	172.30	0.0	-52.28	-381.08	258.88	0.824	0.785	0.088
535.00	462.89	-284.62	710.53	0.0	0.0	-295.19	710.53	0.049	0.058	0.0
505.00	1.668e+04	-63.27	192.44	0.0	-52.28	-380.93	345.75	0.857	0.759	0.170
455.00	1.393e+05	-26.77	231.20	0.0	-52.28	-366.53	489.83	0.922	0.783	0.375
404.44	1.848e+04	-42.92	230.40	0.0	-52.28	-385.70	570.64	0.732	0.887	0.542
378.89	7112.79	-473.91	-262.63	0.0	-6.20	-474.86	-329.87	2.180	0.006	0.456
353.89	2.196e+04	-32.62	456.21	0.0	-61.93	-355.57	632.92	0.678	0.799	0.423
303.33	1.928e+04	-91.51	295.05	0.0	-61.93	-445.29	639.78	0.388	1.157	0.686
252.78	2.190e+04	-176.89	242.77	0.0	-61.93	-448.92	647.41	0.369	0.913	0.816
202.22	1.592e+04	-73.92	284.63	0.0	-61.93	-448.92	647.41	0.369	1.258	0.731
151.67	1.601e+04	-65.56	283.49	0.0	-61.93	-448.94	620.41	0.408	1.223	0.654

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
122.00	7167.74	-473.02	-262.23	0.0	-6.20	-474.86	-329.87	2.180	0.012	0.459
101.11	1.343e+04	-59.25	403.57	0.0	-61.93	-371.53	681.11	0.575	0.839	0.682
88.00	511.85	445.72	710.53	0.0	0.0	459.84	710.53	0.039	0.268	0.0
80.00	1592.11	106.62	-334.97	0.0	0.0	101.38	-334.97	0.074	0.024	0.0
50.56	1.912e+04	-72.11	249.76	0.0	-61.93	-446.67	538.92	0.539	1.040	0.516
Risulta	5.461e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	4.057	0.246	0.075	683.51	0.1	8.018e+04	14.7	0.10	1.89e-05	0.0	0.0
2	4.203	0.238	0.075	3194.54	0.6	8.942e+04	16.4	0.07	1.34e-05	0.0	0.0
3	5.953	0.168	0.075	3.258e+05	59.7	5260.42	1.0	5.08	9.30e-04	0.0	0.0
4	6.890	0.145	0.075	87.98	1.61e-02	1.526e+05	27.9	3.74	6.85e-04	0.0	0.0
5	7.504	0.133	0.075	8103.68	1.5	606.23	0.1	2.52	4.62e-04	0.0	0.0
6	8.323	0.120	0.075	3.489e+04	6.4	1.213e+04	2.2	19.35	3.54e-03	0.0	0.0
7	8.540	0.117	0.075	2980.50	0.5	6.238e+04	11.4	29.25	5.36e-03	0.0	0.0
8	9.183	0.109	0.075	6471.64	1.2	703.74	0.1	62.78	1.15e-02	0.0	0.0
9	9.287	0.108	0.075	8493.51	1.6	1650.90	0.3	3.22	5.90e-04	0.0	0.0
10	9.876	0.101	0.075	397.25	7.28e-02	1269.15	0.2	7.58	1.39e-03	0.0	0.0
11	9.939	0.101	0.075	2.458e+04	4.5	2414.30	0.4	1.21	2.22e-04	0.0	0.0
12	10.445	0.096	0.075	3233.36	0.6	9698.97	1.8	21.03	3.85e-03	0.0	0.0
13	10.503	0.095	0.075	1225.94	0.2	75.83	1.39e-02	1.58	2.89e-04	0.0	0.0
14	10.845	0.092	0.075	5201.01	1.0	8853.37	1.6	0.01	2.32e-06	0.0	0.0
15	11.829	0.085	0.071	8057.19	1.5	321.47	5.89e-02	0.25	4.64e-05	0.0	0.0
16	12.334	0.081	0.069	283.23	5.19e-02	1.73	3.18e-04	7.11	1.30e-03	0.0	0.0
17	12.893	0.078	0.067	185.48	3.40e-02	5050.34	0.9	21.93	4.02e-03	0.0	0.0
18	13.024	0.077	0.067	6717.20	1.2	359.55	6.58e-02	36.62	6.71e-03	0.0	0.0
19	13.360	0.075	0.066	8097.79	1.5	1739.00	0.3	4.55	8.33e-04	0.0	0.0
20	13.772	0.073	0.065	1169.01	0.2	3967.50	0.7	2.50	4.58e-04	0.0	0.0
21	14.359	0.070	0.063	61.29	1.12e-02	2421.27	0.4	81.99	1.50e-02	0.0	0.0
22	14.543	0.069	0.063	8599.36	1.6	888.75	0.2	0.03	6.10e-06	0.0	0.0
23	14.762	0.068	0.063	2501.47	0.5	743.21	0.1	35.78	6.55e-03	0.0	0.0
24	15.113	0.066	0.062	750.85	0.1	4001.85	0.7	29.06	5.32e-03	0.0	0.0
25	15.667	0.064	0.061	2479.43	0.5	685.39	0.1	586.43	0.1	0.0	0.0
26	16.275	0.061	0.059	30.88	5.66e-03	6759.85	1.2	91.98	1.68e-02	0.0	0.0
27	16.346	0.061	0.059	1646.74	0.3	814.16	0.1	35.66	6.53e-03	0.0	0.0
28	16.574	0.060	0.059	992.38	0.2	1436.54	0.3	5.88	1.08e-03	0.0	0.0
29	17.021	0.059	0.058	8231.75	1.5	1654.23	0.3	526.05	9.63e-02	0.0	0.0
30	17.457	0.057	0.057	6398.67	1.2	2198.42	0.4	388.51	7.11e-02	0.0	0.0
31	17.542	0.057	0.057	2035.52	0.4	37.97	6.95e-03	411.90	7.54e-02	0.0	0.0
32	17.789	0.056	0.057	211.05	3.86e-02	2502.73	0.5	4219.43	0.8	0.0	0.0
33	18.042	0.055	0.056	2249.99	0.4	19.04	3.49e-03	1.00	1.83e-04	0.0	0.0
34	18.256	0.055	0.056	145.67	2.67e-02	1811.51	0.3	2.026e+04	3.7	0.0	0.0
35	19.173	0.052	0.055	1919.78	0.4	125.14	2.29e-02	454.28	8.32e-02	0.0	0.0
36	19.313	0.052	0.055	2.04	3.74e-04	178.33	3.27e-02	1.070e+04	2.0	0.0	0.0
37	19.822	0.050	0.054	75.23	1.38e-02	320.88	5.88e-02	3.356e+04	6.1	0.0	0.0
38	20.138	0.050	0.054	948.37	0.2	11.25	2.06e-03	9133.19	1.7	0.0	0.0
39	20.282	0.049	0.053	106.29	1.95e-02	113.15	2.07e-02	3857.05	0.7	0.0	0.0
40	20.608	0.049	0.053	270.98	4.96e-02	2123.07	0.4	6718.20	1.2	0.0	0.0
41	20.956	0.048	0.053	465.01	8.52e-02	6831.19	1.3	2.077e+04	3.8	0.0	0.0
42	21.194	0.047	0.052	696.26	0.1	43.11	7.89e-03	2.749e+04	5.0	0.0	0.0
43	21.430	0.047	0.052	130.92	2.40e-02	31.39	5.75e-03	1.228e+04	2.2	0.0	0.0
44	21.485	0.047	0.052	1535.09	0.3	3605.99	0.7	2533.07	0.5	0.0	0.0
45	21.857	0.046	0.052	0.41	7.56e-05	3563.48	0.7	4565.98	0.8	0.0	0.0
46	22.067	0.045	0.051	32.19	5.89e-03	684.78	0.1	767.94	0.1	0.0	0.0
47	22.144	0.045	0.051	21.62	3.96e-03	7105.67	1.3	2.437e+04	4.5	0.0	0.0
48	22.769	0.044	0.051	17.31	3.17e-03	6.99	1.28e-03	3.462e+04	6.3	0.0	0.0
49	22.889	0.044	0.051	397.49	7.28e-02	1256.68	0.2	4.824e+04	8.8	0.0	0.0
50	23.055	0.043	0.051	2528.93	0.5	3363.41	0.6	2.833e+04	5.2	0.0	0.0
51	23.709	0.042	0.050	765.43	0.1	4428.86	0.8	9608.87	1.8	0.0	0.0
52	23.999	0.042	0.050	866.27	0.2	694.27	0.1	33.96	6.22e-03	0.0	0.0
53	24.271	0.041	0.049	62.27	1.14e-02	177.72	3.25e-02	142.30	2.61e-02	0.0	0.0
54	24.282	0.041	0.049	246.65	4.52e-02	2296.04	0.4	199.16	3.65e-02	0.0	0.0
55	24.811	0.040	0.049	18.01	3.30e-03	1.51	2.76e-04	469.33	8.59e-02	0.0	0.0
56	24.886	0.040	0.049	247.95	4.54e-02	435.32	7.97e-02	526.82	9.65e-02	0.0	0.0
57	25.095	0.040	0.049	202.90	3.72e-02	270.76	4.96e-02	136.71	2.50e-02	0.0	0.0
58	25.382	0.039	0.049	1.89	3.46e-04	412.42	7.55e-02	301.76	5.53e-02	0.0	0.0
59	25.656	0.039	0.048	1.46	2.67e-04	576.40	0.1	3769.30	0.7	0.0	0.0
60	26.453	0.038	0.048	9.95	1.82e-03	258.01	4.73e-02	1.130e+04	2.1	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	Z %	Energia	Energia x v
61	26.532	0.038	0.048	238.71	4.37e-02	82.65	1.51e-02	2967.15	0.5	0.0	0.0
62	26.910	0.037	0.047	8.54	1.56e-03	320.49	5.87e-02	5594.76	1.0	0.0	0.0
63	27.101	0.037	0.047	198.13	3.63e-02	378.89	6.94e-02	1.767e+04	3.2	0.0	0.0
64	27.391	0.037	0.047	97.33	1.78e-02	157.19	2.88e-02	5064.58	0.9	0.0	0.0
65	27.556	0.036	0.047	0.31	5.64e-05	340.34	6.23e-02	6173.83	1.1	0.0	0.0
66	27.763	0.036	0.047	618.41	0.1	23.48	4.30e-03	854.23	0.2	0.0	0.0
67	27.903	0.036	0.047	25.92	4.75e-03	2064.14	0.4	222.08	4.07e-02	0.0	0.0
68	28.194	0.035	0.047	732.66	0.1	16.82	3.08e-03	3670.98	0.7	0.0	0.0
69	28.306	0.035	0.047	537.93	9.85e-02	588.53	0.1	753.18	0.1	0.0	0.0
70	28.700	0.035	0.046	1891.72	0.3	312.33	5.72e-02	7617.52	1.4	0.0	0.0
71	29.109	0.034	0.046	9.66	1.77e-03	536.69	9.83e-02	4761.66	0.9	0.0	0.0
72	29.848	0.034	0.046	2.28	4.17e-04	4.45	8.14e-04	3.98	7.28e-04	0.0	0.0
73	30.035	0.033	0.046	251.81	4.61e-02	1104.08	0.2	3363.43	0.6	0.0	0.0
74	30.124	0.033	0.046	3.11	5.69e-04	118.09	2.16e-02	31.16	5.71e-03	0.0	0.0
75	30.669	0.033	0.045	545.65	9.99e-02	84.82	1.55e-02	4695.12	0.9	0.0	0.0
76	30.901	0.032	0.045	3.64	6.67e-04	391.15	7.16e-02	217.05	3.97e-02	0.0	0.0
77	31.327	0.032	0.045	621.00	0.1	344.62	6.31e-02	1.303e+04	2.4	0.0	0.0
78	31.415	0.032	0.045	14.58	2.67e-03	289.36	5.30e-02	1119.66	0.2	0.0	0.0
79	31.774	0.031	0.045	91.84	1.68e-02	155.25	2.84e-02	4503.75	0.8	0.0	0.0
80	32.122	0.031	0.044	9.34	1.71e-03	561.20	0.1	1835.72	0.3	0.0	0.0
81	32.457	0.031	0.044	244.37	4.48e-02	61.02	1.12e-02	1254.85	0.2	0.0	0.0
82	32.683	0.031	0.044	941.30	0.2	476.39	8.72e-02	4687.72	0.9	0.0	0.0
83	32.740	0.031	0.044	70.69	1.29e-02	86.37	1.58e-02	2312.07	0.4	0.0	0.0
84	33.211	0.030	0.044	0.78	1.44e-04	78.21	1.43e-02	82.73	1.52e-02	0.0	0.0
85	33.308	0.030	0.044	13.57	2.48e-03	266.39	4.88e-02	0.62	1.13e-04	0.0	0.0
86	33.505	0.030	0.044	191.78	3.51e-02	69.20	1.27e-02	267.76	4.90e-02	0.0	0.0
87	33.846	0.030	0.044	2.84	5.20e-04	3.98e-03	0.0	5099.46	0.9	0.0	0.0
88	34.010	0.029	0.044	62.81	1.15e-02	340.34	6.23e-02	6127.96	1.1	0.0	0.0
89	34.644	0.029	0.043	461.68	8.45e-02	502.16	9.20e-02	2.02	3.70e-04	0.0	0.0
90	35.188	0.028	0.043	4.16	7.61e-04	489.33	8.96e-02	1872.03	0.3	0.0	0.0
91	35.384	0.028	0.043	3.49	6.39e-04	0.09	1.58e-05	4345.15	0.8	0.0	0.0
92	35.990	0.028	0.043	195.20	3.57e-02	27.53	5.04e-03	1639.55	0.3	0.0	0.0
93	36.087	0.028	0.043	2.18	3.99e-04	79.98	1.46e-02	5162.36	0.9	0.0	0.0
94	36.430	0.027	0.043	508.24	9.31e-02	272.34	4.99e-02	11.93	2.18e-03	0.0	0.0
95	36.521	0.027	0.043	160.11	2.93e-02	194.22	3.56e-02	1827.56	0.3	0.0	0.0
96	36.862	0.027	0.043	25.22	4.62e-03	41.20	7.55e-03	1396.28	0.3	0.0	0.0
97	37.051	0.027	0.042	299.84	5.49e-02	22.43	4.11e-03	80.48	1.47e-02	0.0	0.0
98	37.529	0.027	0.042	8.49e-04	0.0	1.02	1.87e-04	486.68	8.91e-02	0.0	0.0
99	37.619	0.027	0.042	30.27	5.54e-03	1.77	3.24e-04	417.95	7.65e-02	0.0	0.0
100	37.697	0.027	0.042	82.66	1.51e-02	33.15	6.07e-03	390.67	7.15e-02	0.0	0.0
101	37.840	0.026	0.042	0.22	4.07e-05	717.83	0.1	4919.19	0.9	0.0	0.0
102	38.326	0.026	0.042	13.53	2.48e-03	558.59	0.1	722.38	0.1	0.0	0.0
103	38.498	0.026	0.042	5.57	1.02e-03	4.73	8.67e-04	242.59	4.44e-02	0.0	0.0
104	38.751	0.026	0.042	272.30	4.99e-02	81.32	1.49e-02	438.39	8.03e-02	0.0	0.0
105	39.309	0.025	0.042	97.96	1.79e-02	143.95	2.64e-02	377.22	6.91e-02	0.0	0.0
106	39.353	0.025	0.042	7.87	1.44e-03	32.39	5.93e-03	84.51	1.55e-02	0.0	0.0
107	39.854	0.025	0.042	104.36	1.91e-02	202.57	3.71e-02	867.00	0.2	0.0	0.0
108	40.063	0.025	0.041	242.57	4.44e-02	1.68	3.08e-04	305.65	5.60e-02	0.0	0.0
109	40.283	0.025	0.041	762.45	0.1	6.24	1.14e-03	48.68	8.92e-03	0.0	0.0
110	40.458	0.025	0.041	269.54	4.94e-02	52.18	9.56e-03	70.08	1.28e-02	0.0	0.0
111	40.586	0.025	0.041	151.62	2.78e-02	561.40	0.1	284.63	5.21e-02	0.0	0.0
112	40.948	0.024	0.041	190.60	3.49e-02	223.20	4.09e-02	307.85	5.64e-02	0.0	0.0
113	41.035	0.024	0.041	101.70	1.86e-02	180.47	3.30e-02	349.23	6.40e-02	0.0	0.0
114	41.326	0.024	0.041	54.87	1.00e-02	0.14	2.52e-05	32.59	5.97e-03	0.0	0.0
115	41.683	0.024	0.041	41.08	7.52e-03	51.32	9.40e-03	147.04	2.69e-02	0.0	0.0
116	41.823	0.024	0.041	796.10	0.1	95.37	1.75e-02	16.47	3.02e-03	0.0	0.0
117	42.037	0.024	0.041	3.32	6.08e-04	48.80	8.94e-03	0.14	2.50e-05	0.0	0.0
118	42.106	0.024	0.041	41.08	7.52e-03	308.81	5.66e-02	157.11	2.88e-02	0.0	0.0
119	42.545	0.024	0.041	3.83	7.02e-04	20.43	3.74e-03	113.35	2.08e-02	0.0	0.0
120	42.803	0.023	0.041	420.21	7.70e-02	52.01	9.52e-03	234.94	4.30e-02	0.0	0.0
121	42.935	0.023	0.041	1826.06	0.3	95.75	1.75e-02	10.38	1.90e-03	0.0	0.0
122	43.126	0.023	0.041	88.71	1.62e-02	26.71	4.89e-03	25.88	4.74e-03	0.0	0.0
123	43.449	0.023	0.040	186.36	3.41e-02	78.34	1.43e-02	7.03	1.29e-03	0.0	0.0
124	43.721	0.023	0.040	28.73	5.26e-03	61.21	1.12e-02	112.65	2.06e-02	0.0	0.0
125	43.923	0.023	0.040	943.18	0.2	7.55	1.38e-03	548.23	0.1	0.0	0.0
126	44.149	0.023	0.040	253.03	4.63e-02	2.36	4.32e-04	67.78	1.24e-02	0.0	0.0
127	44.364	0.023	0.040	3.20	5.86e-04	44.61	8.17e-03	102.28	1.87e-02	0.0	0.0
128	44.603	0.022	0.040	0.66	1.21e-04	13.10	2.40e-03	434.44	7.96e-02	0.0	0.0
129	44.918	0.022	0.040	579.95	0.1	27.67	5.07e-03	142.28	2.61e-02	0.0	0.0
130	45.307	0.022	0.040	519.73	9.52e-02	50.03	9.16e-03	607.60	0.1	0.0	0.0
131	45.338	0.022	0.040	1015.75	0.2	12.09	2.21e-03	168.81	3.09e-02	0.0	0.0
132	45.691	0.022	0.040	12.41	2.27e-03	12.23	2.24e-03	362.17	6.63e-02	0.0	0.0
133	45.893	0.022	0.040	21.54	3.94e-03	0.05	8.27e-06	1.80	3.30e-04	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	Z %	Energia	Energia x v
134	46.212	0.022	0.040	35.39	6.48e-03	44.13	8.08e-03	527.11	9.65e-02	0.0	0.0
135	46.389	0.022	0.040	517.37	9.47e-02	195.41	3.58e-02	9.77	1.79e-03	0.0	0.0
136	46.631	0.021	0.040	80.15	1.47e-02	0.30	5.43e-05	53.10	9.72e-03	0.0	0.0
137	46.831	0.021	0.040	8.38	1.53e-03	25.95	4.75e-03	1.00	1.84e-04	0.0	0.0
138	47.070	0.021	0.040	0.08	1.43e-05	0.02	2.88e-06	280.94	5.14e-02	0.0	0.0
139	47.253	0.021	0.040	14.83	2.72e-03	12.17	2.23e-03	210.13	3.85e-02	0.0	0.0
140	47.585	0.021	0.040	3.86	7.07e-04	544.61	9.97e-02	428.84	7.85e-02	0.0	0.0
141	47.817	0.021	0.039	59.80	1.10e-02	112.84	2.07e-02	226.07	4.14e-02	0.0	0.0
142	48.018	0.021	0.039	0.84	1.54e-04	72.19	1.32e-02	3.20	5.85e-04	0.0	0.0
143	48.342	0.021	0.039	7.17	1.31e-03	1.84	3.36e-04	469.59	8.60e-02	0.0	0.0
144	48.698	0.021	0.039	13.31	2.44e-03	413.38	7.57e-02	7.79	1.43e-03	0.0	0.0
145	48.899	0.020	0.039	6.35	1.16e-03	208.32	3.81e-02	137.36	2.52e-02	0.0	0.0
146	49.143	0.020	0.039	504.84	9.25e-02	8.95	1.64e-03	720.94	0.1	0.0	0.0
147	49.509	0.020	0.039	57.98	1.06e-02	814.93	0.1	0.23	4.17e-05	0.0	0.0
148	49.824	0.020	0.039	374.05	6.85e-02	90.28	1.65e-02	8.76	1.60e-03	0.0	0.0
149	50.169	0.020	0.039	6.12e-03	1.12e-06	31.42	5.75e-03	265.76	4.87e-02	0.0	0.0
150	50.359	0.020	0.039	283.16	5.19e-02	67.81	1.24e-02	92.20	1.69e-02	0.0	0.0
151	50.566	0.020	0.039	403.86	7.40e-02	132.87	2.43e-02	0.31	5.62e-05	0.0	0.0
152	50.892	0.020	0.039	0.28	5.14e-05	215.17	3.94e-02	90.77	1.66e-02	0.0	0.0
153	51.063	0.020	0.039	4.54	8.32e-04	243.21	4.45e-02	157.72	2.89e-02	0.0	0.0
154	51.239	0.020	0.039	53.61	9.82e-03	0.03	5.59e-06	291.89	5.35e-02	0.0	0.0
155	51.291	0.019	0.039	1.66	3.05e-04	11.90	2.18e-03	4.14	7.58e-04	0.0	0.0
156	51.709	0.019	0.039	190.57	3.49e-02	74.14	1.36e-02	671.48	0.1	0.0	0.0
157	51.956	0.019	0.039	394.27	7.22e-02	1.11	2.04e-04	1.40	2.57e-04	0.0	0.0
158	52.391	0.019	0.039	19.50	3.57e-03	107.57	1.97e-02	249.24	4.56e-02	0.0	0.0
159	52.719	0.019	0.038	4.84	8.86e-04	0.55	1.00e-04	149.77	2.74e-02	0.0	0.0
160	52.824	0.019	0.038	92.68	1.70e-02	285.43	5.23e-02	351.97	6.45e-02	0.0	0.0
161	53.103	0.019	0.038	54.89	1.01e-02	37.33	6.84e-03	724.58	0.1	0.0	0.0
162	53.265	0.019	0.038	640.58	0.1	6.92	1.27e-03	103.56	1.90e-02	0.0	0.0
163	53.772	0.019	0.038	8.73	1.60e-03	457.16	8.37e-02	25.41	4.65e-03	0.0	0.0
164	54.029	0.019	0.038	53.07	9.72e-03	0.01	2.59e-06	138.97	2.55e-02	0.0	0.0
165	54.301	0.018	0.038	29.13	5.33e-03	132.27	2.42e-02	1.63	2.98e-04	0.0	0.0
166	54.477	0.018	0.038	0.67	1.23e-04	12.89	2.36e-03	31.46	5.76e-03	0.0	0.0
167	54.722	0.018	0.038	124.09	2.27e-02	0.04	8.02e-06	77.32	1.42e-02	0.0	0.0
168	54.902	0.018	0.038	41.73	7.64e-03	58.12	1.06e-02	150.04	2.75e-02	0.0	0.0
169	55.218	0.018	0.038	1.71	3.14e-04	10.67	1.95e-03	47.05	8.62e-03	0.0	0.0
170	55.299	0.018	0.038	29.31	5.37e-03	119.30	2.18e-02	98.69	1.81e-02	0.0	0.0
171	55.649	0.018	0.038	92.96	1.70e-02	300.56	5.50e-02	62.38	1.14e-02	0.0	0.0
172	55.860	0.018	0.038	2.34	4.29e-04	51.22	9.38e-03	37.13	6.80e-03	0.0	0.0
173	56.145	0.018	0.038	39.32	7.20e-03	287.53	5.27e-02	0.49	9.03e-05	0.0	0.0
174	56.442	0.018	0.038	16.35	2.99e-03	713.66	0.1	388.30	7.11e-02	0.0	0.0
175	56.768	0.018	0.038	505.12	9.25e-02	89.09	1.63e-02	428.15	7.84e-02	0.0	0.0
176	56.897	0.018	0.038	159.69	2.92e-02	15.39	2.82e-03	436.77	8.00e-02	0.0	0.0
177	57.001	0.018	0.038	165.19	3.03e-02	14.65	2.68e-03	147.23	2.70e-02	0.0	0.0
178	57.125	0.018	0.038	9.06	1.66e-03	61.66	1.13e-02	0.79	1.44e-04	0.0	0.0
179	57.292	0.017	0.038	17.23	3.16e-03	163.69	3.00e-02	30.77	5.64e-03	0.0	0.0
180	57.569	0.017	0.038	45.77	8.38e-03	61.02	1.12e-02	5.80	1.06e-03	0.0	0.0
181	57.854	0.017	0.038	666.77	0.1	56.09	1.03e-02	564.56	0.1	0.0	0.0
182	58.144	0.017	0.038	29.36	5.38e-03	352.45	6.45e-02	617.07	0.1	0.0	0.0
183	58.504	0.017	0.038	160.90	2.95e-02	51.11	9.36e-03	89.89	1.65e-02	0.0	0.0
184	58.660	0.017	0.038	0.77	1.40e-04	13.56	2.48e-03	41.85	7.66e-03	0.0	0.0
185	58.725	0.017	0.038	20.76	3.80e-03	4.20	7.69e-04	71.92	1.32e-02	0.0	0.0
186	58.910	0.017	0.038	444.41	8.14e-02	46.33	8.48e-03	351.76	6.44e-02	0.0	0.0
187	59.251	0.017	0.037	4.12	7.55e-04	6.18	1.13e-03	765.27	0.1	0.0	0.0
188	59.546	0.017	0.037	277.96	5.09e-02	93.27	1.71e-02	802.14	0.1	0.0	0.0
189	59.716	0.017	0.037	29.07	5.32e-03	94.74	1.74e-02	1173.84	0.2	0.0	0.0
190	59.879	0.017	0.037	0.56	1.02e-04	4.62	8.45e-04	6.19	1.13e-03	0.0	0.0
191	60.224	0.017	0.037	93.63	1.71e-02	2.06	3.77e-04	8.35	1.53e-03	0.0	0.0
192	60.267	0.017	0.037	2.64	4.84e-04	0.04	6.76e-06	763.60	0.1	0.0	0.0
193	60.480	0.017	0.037	126.66	2.32e-02	40.19	7.36e-03	140.68	2.58e-02	0.0	0.0
194	60.541	0.017	0.037	106.17	1.94e-02	78.65	1.44e-02	0.08	1.49e-05	0.0	0.0
195	60.816	0.016	0.037	31.53	5.77e-03	12.86	2.36e-03	141.64	2.59e-02	0.0	0.0
196	61.046	0.016	0.037	338.43	6.20e-02	0.03	5.51e-06	21.63	3.96e-03	0.0	0.0
197	61.151	0.016	0.037	26.92	4.93e-03	103.90	1.90e-02	35.99	6.59e-03	0.0	0.0
198	61.475	0.016	0.037	45.78	8.38e-03	38.14	6.98e-03	15.24	2.79e-03	0.0	0.0
199	61.573	0.016	0.037	0.05	8.83e-06	488.76	8.95e-02	396.30	7.26e-02	0.0	0.0
200	61.678	0.016	0.037	46.62	8.54e-03	9.71	1.78e-03	280.31	5.13e-02	0.0	0.0
201	61.784	0.016	0.037	0.22	3.98e-05	102.30	1.87e-02	1.32	2.41e-04	0.0	0.0
202	61.869	0.016	0.037	66.13	1.21e-02	5.94	1.09e-03	448.20	8.21e-02	0.0	0.0
203	62.323	0.016	0.037	0.07	1.33e-05	86.04	1.58e-02	163.83	3.00e-02	0.0	0.0
204	62.588	0.016	0.037	5.15	9.43e-04	22.84	4.18e-03	312.83	5.73e-02	0.0	0.0
205	62.737	0.016	0.037	176.37	3.23e-02	236.11	4.32e-02	701.92	0.1	0.0	0.0
206	62.905	0.016	0.037	1.07	1.96e-04	103.96	1.90e-02	98.29	1.80e-02	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
207	63.168	0.016	0.037	62.62	1.15e-02	218.24	4.00e-02	1.67	3.07e-04	0.0	0.0
208	63.357	0.016	0.037	7.50	1.37e-03	4.17	7.63e-04	253.75	4.65e-02	0.0	0.0
209	63.450	0.016	0.037	0.05	1.01e-05	12.51	2.29e-03	63.26	1.16e-02	0.0	0.0
210	63.670	0.016	0.037	3.29e-05	0.0	1.35	2.48e-04	64.21	1.18e-02	0.0	0.0
211	63.907	0.016	0.037	58.25	1.07e-02	408.33	7.48e-02	114.58	2.10e-02	0.0	0.0
212	64.104	0.016	0.037	27.14	4.97e-03	6.60	1.21e-03	85.52	1.57e-02	0.0	0.0
213	64.345	0.016	0.037	14.01	2.57e-03	14.24	2.61e-03	221.71	4.06e-02	0.0	0.0
214	64.492	0.016	0.037	110.69	2.03e-02	5.22	9.55e-04	84.09	1.54e-02	0.0	0.0
215	64.680	0.015	0.037	44.49	8.15e-03	18.42	3.37e-03	9.82	1.80e-03	0.0	0.0
216	65.005	0.015	0.037	71.23	1.30e-02	3.91e-03	0.0	97.17	1.78e-02	0.0	0.0
217	65.239	0.015	0.037	0.33	5.99e-05	707.36	0.1	307.24	5.63e-02	0.0	0.0
218	65.371	0.015	0.037	11.29	2.07e-03	2.21	4.04e-04	1647.02	0.3	0.0	0.0
219	65.528	0.015	0.037	57.10	1.05e-02	127.06	2.33e-02	479.42	8.78e-02	0.0	0.0
220	65.584	0.015	0.037	74.09	1.36e-02	105.79	1.94e-02	1295.90	0.2	0.0	0.0
Risulta				5.244e+05		5.282e+05		4.768e+05			
In percentuale				96.03		96.74		87.32			

CDC	Tipo	Sigla Id	Note
12	Edk	CDC=Ed (dinamico SLD) alfa=0.0 (ecc. -)	
			verifica esistenti: fattore FC 1.200
			categoria suolo: B
			fattore di sito S = 1.200
			ordinata spettro (tratto Tb-Tc) = 0.075 g
			angolo di ingresso:0.0
			eccentricità aggiuntiva: negativa
			periodo proprio T1: 0.159 sec.
			numero di modi considerati:220
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
cm	daN	cm	cm	cm	cm	cm	cm			
1340.00	96.19	-491.36	-334.97	0.0	0.0	-491.36	-334.97	0.155	0.0	0.0
1295.00	116.44	-491.36	-334.97	0.0	0.0	-491.36	-334.97	1.791	0.0	0.0
1250.00	101.25	-491.36	-334.97	0.0	0.0	-491.36	-334.97	1.791	0.0	0.0
1205.00	1203.52	-572.28	-173.84	0.0	26.80	-635.82	-328.32	0.015	2.913	3.350
1195.00	7848.27	-175.90	173.40	0.0	15.15	-313.36	198.69	0.654	1.046	0.168
1160.00	2326.05	-575.55	-168.23	0.0	26.80	-635.82	-328.32	0.015	2.763	3.471
1115.00	2319.30	-575.63	-167.75	0.0	26.80	-635.82	-328.32	0.015	2.759	3.482
1070.00	2319.30	-575.63	-167.75	0.0	26.80	-635.82	-328.32	0.015	2.759	3.482
1025.00	1.465e+04	-128.29	99.57	0.0	52.28	-544.32	97.18	0.605	1.184	0.002
985.00	1.083e+04	-102.23	128.80	0.0	52.28	-542.11	167.56	0.726	1.143	0.047
945.00	1.083e+04	-102.21	128.80	0.0	52.28	-542.11	167.56	0.726	1.143	0.047
905.00	6.437e+04	-130.89	142.36	0.0	52.28	-458.71	212.95	0.530	0.997	0.097
855.00	1.642e+04	-128.78	145.90	0.0	52.28	-485.70	259.69	0.343	1.348	0.177
830.00	1249.33	528.64	424.28	0.0	0.0	0.0	0.0	0.0	0.0	0.0
805.00	1.479e+04	-102.33	164.15	0.0	52.28	-485.70	259.69	0.343	1.448	0.149
780.00	1249.33	528.64	538.78	0.0	0.0	0.0	0.0	0.0	0.0	0.0
755.00	1.526e+04	-82.93	181.97	0.0	52.28	-481.74	260.08	0.362	1.467	0.118
728.69	1131.11	528.64	656.28	0.0	0.0	0.0	0.0	0.0	0.0	0.0
705.00	1.607e+04	-55.85	217.96	0.0	52.28	-388.08	347.18	0.814	0.815	0.144
675.00	466.53	528.64	533.13	0.0	12.20	0.0	0.0	0.0	0.0	0.0
655.00	1.415e+04	-110.23	162.68	0.0	52.28	-485.60	338.86	0.413	1.292	0.286
605.00	1.443e+04	-81.71	180.98	0.0	52.28	-388.24	376.21	0.787	0.765	0.213
555.00	1.494e+04	-58.92	172.30	0.0	52.28	-381.08	258.88	0.824	0.785	0.088
535.00	462.89	-284.62	710.53	0.0	0.0	-295.19	710.53	0.049	0.058	0.0
505.00	1.668e+04	-63.27	192.44	0.0	52.28	-380.93	345.75	0.857	0.759	0.170
455.00	1.393e+05	-26.77	231.20	0.0	52.28	-366.53	489.83	0.922	0.783	0.375
404.44	1.848e+04	-42.92	230.40	0.0	52.28	-385.70	570.64	0.732	0.887	0.542
378.89	7112.79	-473.91	-262.63	0.0	6.20	-474.86	-329.87	2.180	0.006	0.456
353.89	2.196e+04	-32.62	456.21	0.0	61.93	-355.57	632.92	0.678	0.799	0.423
303.33	1.928e+04	-91.51	295.05	0.0	61.93	-445.29	639.78	0.388	1.157	0.686
252.78	2.190e+04	-176.89	242.77	0.0	61.93	-448.92	647.41	0.369	0.913	0.816
202.22	1.592e+04	-73.92	284.63	0.0	61.93	-448.92	647.41	0.369	1.258	0.731
151.67	1.601e+04	-65.56	283.49	0.0	61.93	-448.94	620.41	0.408	1.223	0.654
122.00	7167.74	-473.02	-262.23	0.0	6.20	-474.86	-329.87	2.180	0.012	0.459

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
101.11	1.343e+04	-59.25	403.57	0.0	61.93	-371.53	681.11	0.575	0.839	0.682
88.00	511.85	445.72	710.53	0.0	0.0	459.84	710.53	0.039	0.268	0.0
80.00	1592.11	106.62	-334.97	0.0	0.0	101.38	-334.97	0.074	0.024	0.0
50.56	1.912e+04	-72.11	249.76	0.0	61.93	-446.67	538.92	0.539	1.040	0.516
Risulta	5.461e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	4.060	0.246	0.075	574.71	0.1	8.608e+04	15.8	0.10	1.78e-05	0.0	0.0
2	4.217	0.237	0.075	1535.80	0.3	8.421e+04	15.4	0.06	1.09e-05	0.0	0.0
3	6.297	0.159	0.075	3.256e+05	59.6	5178.54	0.9	7.03	1.29e-03	0.0	0.0
4	6.890	0.145	0.075	535.87	9.81e-02	1.516e+05	27.8	4.18	7.65e-04	0.0	0.0
5	7.700	0.130	0.075	5397.59	1.0	260.12	4.76e-02	3.03	5.55e-04	0.0	0.0
6	8.255	0.121	0.075	4.776e+04	8.7	2.879e+04	5.3	37.83	6.93e-03	0.0	0.0
7	8.591	0.116	0.075	4.86	8.91e-04	4.472e+04	8.2	11.33	2.08e-03	0.0	0.0
8	9.027	0.111	0.075	5985.47	1.1	1801.10	0.3	10.22	1.87e-03	0.0	0.0
9	9.236	0.108	0.075	2731.05	0.5	912.40	0.2	46.55	8.52e-03	0.0	0.0
10	9.721	0.103	0.075	1.109e+04	2.0	309.24	5.66e-02	0.32	5.83e-05	0.0	0.0
11	9.832	0.102	0.075	1615.94	0.3	1035.16	0.2	1.89	3.46e-04	0.0	0.0
12	10.046	0.100	0.075	9162.05	1.7	2008.79	0.4	5.84	1.07e-03	0.0	0.0
13	10.469	0.096	0.075	2829.49	0.5	1.900e+04	3.5	4.94	9.06e-04	0.0	0.0
14	10.939	0.091	0.074	1.317e+04	2.4	120.06	2.20e-02	12.90	2.36e-03	0.0	0.0
15	11.184	0.089	0.073	731.74	0.1	260.52	4.77e-02	8.52	1.56e-03	0.0	0.0
16	12.038	0.083	0.070	5897.49	1.1	609.54	0.1	5.12	9.38e-04	0.0	0.0
17	12.741	0.078	0.068	744.75	0.1	6107.25	1.1	10.37	1.90e-03	0.0	0.0
18	12.925	0.077	0.067	8242.37	1.5	406.53	7.44e-02	33.34	6.11e-03	0.0	0.0
19	13.140	0.076	0.067	5937.30	1.1	159.07	2.91e-02	16.62	3.04e-03	0.0	0.0
20	13.640	0.073	0.065	1533.42	0.3	969.28	0.2	1.73	3.17e-04	0.0	0.0
21	14.061	0.071	0.064	956.84	0.2	7121.70	1.3	55.20	1.01e-02	0.0	0.0
22	14.507	0.069	0.063	496.43	9.09e-02	39.04	7.15e-03	121.65	2.23e-02	0.0	0.0
23	14.853	0.067	0.062	546.75	0.1	1899.80	0.3	1.19	2.18e-04	0.0	0.0
24	15.265	0.066	0.061	3890.17	0.7	226.07	4.14e-02	213.74	3.91e-02	0.0	0.0
25	15.545	0.064	0.061	4616.46	0.8	1598.78	0.3	54.37	9.96e-03	0.0	0.0
26	16.048	0.062	0.060	6.45	1.18e-03	4706.60	0.9	245.53	4.50e-02	0.0	0.0
27	16.252	0.062	0.059	762.13	0.1	5362.69	1.0	0.14	2.61e-05	0.0	0.0
28	16.437	0.061	0.059	2095.29	0.4	1394.31	0.3	197.28	3.61e-02	0.0	0.0
29	17.021	0.059	0.058	3125.19	0.6	5.46	1.00e-03	276.86	5.07e-02	0.0	0.0
30	17.221	0.058	0.058	5574.94	1.0	4106.98	0.8	124.52	2.28e-02	0.0	0.0
31	17.988	0.056	0.057	6593.90	1.2	1701.44	0.3	5920.68	1.1	0.0	0.0
32	18.060	0.055	0.056	124.47	2.28e-02	141.78	2.60e-02	0.13	2.42e-05	0.0	0.0
33	18.252	0.055	0.056	166.29	3.05e-02	1748.57	0.3	1.695e+04	3.1	0.0	0.0
34	18.860	0.053	0.055	217.74	3.99e-02	80.85	1.48e-02	311.51	5.70e-02	0.0	0.0
35	19.235	0.052	0.055	1523.61	0.3	185.45	3.40e-02	1.643e+04	3.0	0.0	0.0
36	19.325	0.052	0.055	7.62	1.40e-03	10.15	1.86e-03	3283.38	0.6	0.0	0.0
37	19.865	0.050	0.054	179.19	3.28e-02	320.98	5.88e-02	3.574e+04	6.5	0.0	0.0
38	19.953	0.050	0.054	562.63	0.1	543.16	9.95e-02	776.44	0.1	0.0	0.0
39	20.463	0.049	0.053	1565.64	0.3	3218.74	0.6	7458.55	1.4	0.0	0.0
40	20.651	0.048	0.053	1057.88	0.2	1549.42	0.3	6807.15	1.2	0.0	0.0
41	20.976	0.048	0.053	1.01	1.85e-04	642.44	0.1	20.01	3.67e-03	0.0	0.0
42	21.072	0.047	0.053	422.83	7.74e-02	2491.45	0.5	2.078e+04	3.8	0.0	0.0
43	21.133	0.047	0.052	4773.08	0.9	2.83e-04	0.0	2.446e+04	4.5	0.0	0.0
44	21.279	0.047	0.052	394.69	7.23e-02	132.99	2.44e-02	2580.82	0.5	0.0	0.0
45	21.392	0.047	0.052	4204.62	0.8	1250.02	0.2	63.72	1.17e-02	0.0	0.0
46	21.901	0.046	0.052	81.63	1.49e-02	908.06	0.2	1.722e+04	3.2	0.0	0.0
47	22.039	0.045	0.051	17.30	3.17e-03	7139.72	1.3	322.23	5.90e-02	0.0	0.0
48	22.124	0.045	0.051	3.09	5.65e-04	7154.73	1.3	1.797e+04	3.3	0.0	0.0
49	22.844	0.044	0.051	78.41	1.44e-02	126.45	2.32e-02	1.084e+05	19.8	0.0	0.0
50	23.228	0.043	0.050	5.29	9.69e-04	3751.25	0.7	1.085e+04	2.0	0.0	0.0
51	23.565	0.042	0.050	85.58	1.57e-02	5809.62	1.1	7406.51	1.4	0.0	0.0
52	23.819	0.042	0.050	252.52	4.62e-02	95.91	1.76e-02	954.74	0.2	0.0	0.0
53	24.252	0.041	0.049	1.94	3.56e-04	1819.37	0.3	770.89	0.1	0.0	0.0
54	24.290	0.041	0.049	0.09	1.57e-05	160.49	2.94e-02	28.55	5.23e-03	0.0	0.0
55	24.709	0.040	0.049	0.40	7.40e-05	25.88	4.74e-03	338.71	6.20e-02	0.0	0.0
56	24.917	0.040	0.049	147.36	2.70e-02	49.69	9.10e-03	12.62	2.31e-03	0.0	0.0
57	25.125	0.040	0.049	59.57	1.09e-02	203.97	3.74e-02	315.64	5.78e-02	0.0	0.0
58	25.775	0.039	0.048	45.17	8.27e-03	256.15	4.69e-02	500.28	9.16e-02	0.0	0.0
59	25.973	0.039	0.048	20.31	3.72e-03	689.35	0.1	1.017e+04	1.9	0.0	0.0
60	26.386	0.038	0.048	208.58	3.82e-02	87.66	1.61e-02	6938.85	1.3	0.0	0.0
61	26.674	0.037	0.048	180.79	3.31e-02	3.55	6.49e-04	6593.59	1.2	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	Z %	Energia	Energia x v
62	26.773	0.037	0.048	5.55	1.02e-03	43.31	7.93e-03	213.37	3.91e-02	0.0	0.0
63	27.116	0.037	0.047	766.66	0.1	811.75	0.1	55.64	1.02e-02	0.0	0.0
64	27.461	0.036	0.047	92.60	1.70e-02	2.26	4.14e-04	5038.50	0.9	0.0	0.0
65	27.515	0.036	0.047	3.44	6.30e-04	1376.54	0.3	2.582e+04	4.7	0.0	0.0
66	27.885	0.036	0.047	0.96	1.76e-04	1523.54	0.3	99.01	1.81e-02	0.0	0.0
67	28.203	0.035	0.047	101.25	1.85e-02	40.38	7.39e-03	337.41	6.18e-02	0.0	0.0
68	28.696	0.035	0.046	3.38	6.19e-04	7.08	1.30e-03	4818.41	0.9	0.0	0.0
69	29.132	0.034	0.046	837.21	0.2	13.75	2.52e-03	4441.29	0.8	0.0	0.0
70	29.468	0.034	0.046	1452.13	0.3	418.07	7.66e-02	189.74	3.47e-02	0.0	0.0
71	29.849	0.034	0.046	250.66	4.59e-02	2647.91	0.5	171.80	3.15e-02	0.0	0.0
72	29.979	0.033	0.046	683.69	0.1	7.44	1.36e-03	2099.27	0.4	0.0	0.0
73	30.132	0.033	0.045	37.27	6.83e-03	5.63	1.03e-03	89.74	1.64e-02	0.0	0.0
74	30.342	0.033	0.045	813.76	0.1	17.99	3.29e-03	5339.96	1.0	0.0	0.0
75	30.548	0.033	0.045	121.50	2.22e-02	2.97	5.44e-04	5452.43	1.0	0.0	0.0
76	31.117	0.032	0.045	509.91	9.34e-02	930.21	0.2	826.60	0.2	0.0	0.0
77	31.407	0.032	0.045	557.77	0.1	48.98	8.97e-03	7020.59	1.3	0.0	0.0
78	31.450	0.032	0.045	18.42	3.37e-03	13.50	2.47e-03	361.59	6.62e-02	0.0	0.0
79	31.714	0.032	0.045	1202.64	0.2	29.65	5.43e-03	9465.75	1.7	0.0	0.0
80	31.987	0.031	0.045	102.29	1.87e-02	64.31	1.18e-02	1871.89	0.3	0.0	0.0
81	32.225	0.031	0.044	35.44	6.49e-03	125.74	2.30e-02	272.44	4.99e-02	0.0	0.0
82	32.585	0.031	0.044	287.31	5.26e-02	4.46	8.16e-04	447.12	8.19e-02	0.0	0.0
83	32.775	0.031	0.044	128.02	2.34e-02	21.00	3.85e-03	1.046e+04	1.9	0.0	0.0
84	33.225	0.030	0.044	883.49	0.2	85.99	1.57e-02	1529.62	0.3	0.0	0.0
85	33.471	0.030	0.044	0.11	1.94e-05	783.60	0.1	956.44	0.2	0.0	0.0
86	33.823	0.030	0.044	1044.52	0.2	197.62	3.62e-02	5673.64	1.0	0.0	0.0
87	33.997	0.029	0.044	558.84	0.1	1.10	2.02e-04	1549.00	0.3	0.0	0.0
88	34.173	0.029	0.044	138.28	2.53e-02	662.17	0.1	2634.90	0.5	0.0	0.0
89	34.469	0.029	0.043	70.24	1.29e-02	127.83	2.34e-02	3274.31	0.6	0.0	0.0
90	34.883	0.029	0.043	24.85	4.55e-03	271.29	4.97e-02	1831.04	0.3	0.0	0.0
91	35.095	0.028	0.043	62.54	1.15e-02	81.32	1.49e-02	421.71	7.72e-02	0.0	0.0
92	35.330	0.028	0.043	148.61	2.72e-02	36.17	6.62e-03	984.87	0.2	0.0	0.0
93	36.034	0.028	0.043	124.37	2.28e-02	20.28	3.71e-03	468.91	8.59e-02	0.0	0.0
94	36.100	0.028	0.043	473.48	8.67e-02	152.68	2.80e-02	2.38	4.37e-04	0.0	0.0
95	36.294	0.028	0.043	10.48	1.92e-03	682.30	0.1	4.64	8.50e-04	0.0	0.0
96	36.978	0.027	0.042	42.63	7.81e-03	11.32	2.07e-03	4.60	8.43e-04	0.0	0.0
97	37.070	0.027	0.042	6.92	1.27e-03	44.77	8.20e-03	935.93	0.2	0.0	0.0
98	37.441	0.027	0.042	0.10	1.82e-05	13.88	2.54e-03	18.50	3.39e-03	0.0	0.0
99	37.509	0.027	0.042	248.63	4.55e-02	56.57	1.04e-02	1325.49	0.2	0.0	0.0
100	37.633	0.027	0.042	19.45	3.56e-03	50.98	9.34e-03	4071.35	0.7	0.0	0.0
101	37.836	0.026	0.042	14.46	2.65e-03	159.39	2.92e-02	1003.35	0.2	0.0	0.0
102	37.924	0.026	0.042	20.57	3.77e-03	52.32	9.58e-03	179.20	3.28e-02	0.0	0.0
103	38.310	0.026	0.042	49.33	9.03e-03	654.88	0.1	3051.53	0.6	0.0	0.0
104	38.556	0.026	0.042	105.96	1.94e-02	176.37	3.23e-02	508.67	9.32e-02	0.0	0.0
105	38.654	0.026	0.042	4.21	7.71e-04	79.65	1.46e-02	2506.84	0.5	0.0	0.0
106	39.061	0.026	0.042	2.48e-04	0.0	1.96	3.60e-04	215.70	3.95e-02	0.0	0.0
107	39.592	0.025	0.042	9.62	1.76e-03	24.18	4.43e-03	13.64	2.50e-03	0.0	0.0
108	39.922	0.025	0.041	286.11	5.24e-02	145.35	2.66e-02	744.73	0.1	0.0	0.0
109	40.004	0.025	0.041	233.54	4.28e-02	25.90	4.74e-03	218.79	4.01e-02	0.0	0.0
110	40.121	0.025	0.041	5.65	1.03e-03	34.71	6.36e-03	143.48	2.63e-02	0.0	0.0
111	40.270	0.025	0.041	8.75	1.60e-03	34.02	6.23e-03	5.05	9.24e-04	0.0	0.0
112	40.772	0.025	0.041	10.63	1.95e-03	158.01	2.89e-02	704.80	0.1	0.0	0.0
113	40.894	0.024	0.041	174.50	3.20e-02	147.30	2.70e-02	5.88	1.08e-03	0.0	0.0
114	40.968	0.024	0.041	64.36	1.18e-02	285.87	5.24e-02	575.29	0.1	0.0	0.0
115	41.359	0.024	0.041	32.32	5.92e-03	414.92	7.60e-02	263.98	4.83e-02	0.0	0.0
116	41.395	0.024	0.041	142.66	2.61e-02	442.89	8.11e-02	12.06	2.21e-03	0.0	0.0
117	41.499	0.024	0.041	37.78	6.92e-03	6.19	1.13e-03	181.73	3.33e-02	0.0	0.0
118	41.946	0.024	0.041	2.25	4.13e-04	30.76	5.63e-03	25.57	4.68e-03	0.0	0.0
119	42.360	0.024	0.041	55.24	1.01e-02	72.35	1.33e-02	10.77	1.97e-03	0.0	0.0
120	42.449	0.024	0.041	89.04	1.63e-02	29.14	5.34e-03	280.30	5.13e-02	0.0	0.0
121	42.867	0.023	0.041	2.75	5.04e-04	31.49	5.77e-03	26.21	4.80e-03	0.0	0.0
122	43.072	0.023	0.041	518.00	9.49e-02	73.17	1.34e-02	0.03	5.49e-06	0.0	0.0
123	43.400	0.023	0.041	73.57	1.35e-02	140.65	2.58e-02	663.22	0.1	0.0	0.0
124	43.494	0.023	0.040	90.11	1.65e-02	38.88	7.12e-03	559.69	0.1	0.0	0.0
125	43.749	0.023	0.040	8.88	1.63e-03	40.39	7.40e-03	60.63	1.11e-02	0.0	0.0
126	44.173	0.023	0.040	55.74	1.02e-02	1.16	2.13e-04	65.91	1.21e-02	0.0	0.0
127	44.528	0.022	0.040	99.50	1.82e-02	14.98	2.74e-03	528.69	9.68e-02	0.0	0.0
128	44.694	0.022	0.040	21.94	4.02e-03	103.04	1.89e-02	1211.57	0.2	0.0	0.0
129	45.096	0.022	0.040	195.43	3.58e-02	81.17	1.49e-02	33.90	6.21e-03	0.0	0.0
130	45.197	0.022	0.040	1.63	2.99e-04	34.06	6.24e-03	34.76	6.37e-03	0.0	0.0
131	45.757	0.022	0.040	127.86	2.34e-02	77.83	1.43e-02	316.59	5.80e-02	0.0	0.0
132	46.081	0.022	0.040	426.10	7.80e-02	152.96	2.80e-02	42.91	7.86e-03	0.0	0.0
133	46.217	0.022	0.040	497.43	9.11e-02	2.01	3.67e-04	230.87	4.23e-02	0.0	0.0
134	46.538	0.021	0.040	355.25	6.51e-02	4.04	7.39e-04	147.50	2.70e-02	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	Z %	Energia	Energia x v
135	46.838	0.021	0.040	762.69	0.1	75.39	1.38e-02	24.38	4.47e-03	0.0	0.0
136	46.917	0.021	0.040	72.48	1.33e-02	102.42	1.88e-02	210.76	3.86e-02	0.0	0.0
137	47.145	0.021	0.040	250.73	4.59e-02	3.35	6.14e-04	198.10	3.63e-02	0.0	0.0
138	47.579	0.021	0.040	745.69	0.1	0.07	1.34e-05	51.14	9.37e-03	0.0	0.0
139	47.802	0.021	0.039	1221.34	0.2	48.64	8.91e-03	19.26	3.53e-03	0.0	0.0
140	47.942	0.021	0.039	328.65	6.02e-02	286.31	5.24e-02	5.76	1.05e-03	0.0	0.0
141	48.103	0.021	0.039	31.25	5.72e-03	358.08	6.56e-02	29.88	5.47e-03	0.0	0.0
142	48.246	0.021	0.039	57.41	1.05e-02	337.88	6.19e-02	117.36	2.15e-02	0.0	0.0
143	48.311	0.021	0.039	0.30	5.56e-05	11.58	2.12e-03	0.19	3.51e-05	0.0	0.0
144	48.813	0.020	0.039	61.26	1.12e-02	1.98	3.62e-04	1.92	3.52e-04	0.0	0.0
145	48.834	0.020	0.039	321.53	5.89e-02	254.32	4.66e-02	262.71	4.81e-02	0.0	0.0
146	49.120	0.020	0.039	115.09	2.11e-02	380.08	6.96e-02	2.28	4.17e-04	0.0	0.0
147	49.532	0.020	0.039	19.87	3.64e-03	249.89	4.58e-02	6.05	1.11e-03	0.0	0.0
148	49.712	0.020	0.039	25.55	4.68e-03	110.56	2.02e-02	161.03	2.95e-02	0.0	0.0
149	50.071	0.020	0.039	85.86	1.57e-02	242.24	4.44e-02	3.08	5.64e-04	0.0	0.0
150	50.240	0.020	0.039	243.70	4.46e-02	50.58	9.26e-03	10.12	1.85e-03	0.0	0.0
151	50.584	0.020	0.039	82.58	1.51e-02	67.79	1.24e-02	228.97	4.19e-02	0.0	0.0
152	50.768	0.020	0.039	182.49	3.34e-02	67.94	1.24e-02	21.80	3.99e-03	0.0	0.0
153	50.927	0.020	0.039	1.64	3.01e-04	4.84	8.86e-04	55.37	1.01e-02	0.0	0.0
154	51.027	0.020	0.039	336.56	6.16e-02	57.01	1.04e-02	600.07	0.1	0.0	0.0
155	51.278	0.020	0.039	215.62	3.95e-02	38.95	7.13e-03	405.82	7.43e-02	0.0	0.0
156	51.502	0.019	0.039	0.82	1.51e-04	5.46	1.00e-03	324.81	5.95e-02	0.0	0.0
157	51.793	0.019	0.039	2.03	3.72e-04	105.04	1.92e-02	544.17	9.97e-02	0.0	0.0
158	52.142	0.019	0.039	1.64	3.00e-04	9.78	1.79e-03	79.16	1.45e-02	0.0	0.0
159	52.388	0.019	0.039	150.49	2.76e-02	3.99	7.31e-04	403.01	7.38e-02	0.0	0.0
160	52.805	0.019	0.038	221.46	4.06e-02	3.29	6.02e-04	275.11	5.04e-02	0.0	0.0
161	52.956	0.019	0.038	70.10	1.28e-02	564.53	0.1	899.23	0.2	0.0	0.0
162	53.154	0.019	0.038	61.36	1.12e-02	5.02e-03	0.0	20.40	3.74e-03	0.0	0.0
163	53.511	0.019	0.038	16.43	3.01e-03	389.80	7.14e-02	5.17	9.48e-04	0.0	0.0
164	53.713	0.019	0.038	5.62	1.03e-03	35.37	6.48e-03	161.08	2.95e-02	0.0	0.0
165	53.986	0.019	0.038	111.60	2.04e-02	105.79	1.94e-02	250.49	4.59e-02	0.0	0.0
166	54.484	0.018	0.038	2.67	4.89e-04	0.33	6.03e-05	69.71	1.28e-02	0.0	0.0
167	54.772	0.018	0.038	26.69	4.89e-03	1.92	3.51e-04	101.29	1.85e-02	0.0	0.0
168	55.016	0.018	0.038	15.78	2.89e-03	208.06	3.81e-02	70.62	1.29e-02	0.0	0.0
169	55.301	0.018	0.038	226.62	4.15e-02	80.75	1.48e-02	143.50	2.63e-02	0.0	0.0
170	55.379	0.018	0.038	54.47	9.98e-03	53.79	9.85e-03	41.65	7.63e-03	0.0	0.0
171	55.846	0.018	0.038	316.62	5.80e-02	62.30	1.14e-02	909.86	0.2	0.0	0.0
172	56.135	0.018	0.038	1.65	3.03e-04	888.90	0.2	98.46	1.80e-02	0.0	0.0
173	56.312	0.018	0.038	71.88	1.32e-02	182.96	3.35e-02	0.44	8.05e-05	0.0	0.0
174	56.521	0.018	0.038	320.74	5.87e-02	273.50	5.01e-02	72.75	1.33e-02	0.0	0.0
175	56.641	0.018	0.038	4.03	7.37e-04	1.08	1.97e-04	74.08	1.36e-02	0.0	0.0
176	57.043	0.018	0.038	246.02	4.51e-02	62.63	1.15e-02	607.37	0.1	0.0	0.0
177	57.089	0.018	0.038	0.54	9.84e-05	127.46	2.33e-02	1.73	3.17e-04	0.0	0.0
178	57.349	0.017	0.038	100.25	1.84e-02	187.29	3.43e-02	637.74	0.1	0.0	0.0
179	57.623	0.017	0.038	14.04	2.57e-03	34.86	6.38e-03	7.33	1.34e-03	0.0	0.0
180	57.963	0.017	0.038	15.92	2.92e-03	184.28	3.37e-02	861.60	0.2	0.0	0.0
181	57.998	0.017	0.038	18.33	3.36e-03	6.61	1.21e-03	119.86	2.20e-02	0.0	0.0
182	58.361	0.017	0.038	38.85	7.12e-03	15.85	2.90e-03	619.55	0.1	0.0	0.0
183	58.725	0.017	0.038	31.63	5.79e-03	12.39	2.27e-03	233.74	4.28e-02	0.0	0.0
184	58.822	0.017	0.038	129.28	2.37e-02	0.09	1.59e-05	33.20	6.08e-03	0.0	0.0
185	59.134	0.017	0.037	1.64	3.01e-04	3.30	6.05e-04	143.15	2.62e-02	0.0	0.0
186	59.318	0.017	0.037	2.97	5.44e-04	12.54	2.30e-03	86.88	1.59e-02	0.0	0.0
187	59.429	0.017	0.037	0.04	7.04e-06	60.03	1.10e-02	130.95	2.40e-02	0.0	0.0
188	59.714	0.017	0.037	28.28	5.18e-03	146.69	2.69e-02	375.14	6.87e-02	0.0	0.0
189	60.295	0.017	0.037	11.48	2.10e-03	90.86	1.66e-02	169.37	3.10e-02	0.0	0.0
190	60.403	0.017	0.037	21.95	4.02e-03	401.61	7.35e-02	33.70	6.17e-03	0.0	0.0
191	60.602	0.017	0.037	128.27	2.35e-02	160.83	2.95e-02	337.94	6.19e-02	0.0	0.0
192	60.793	0.016	0.037	4.96	9.07e-04	169.12	3.10e-02	62.00	1.14e-02	0.0	0.0
193	60.992	0.016	0.037	24.12	4.42e-03	38.53	7.06e-03	227.73	4.17e-02	0.0	0.0
194	61.077	0.016	0.037	96.51	1.77e-02	88.62	1.62e-02	15.32	2.81e-03	0.0	0.0
195	61.358	0.016	0.037	185.93	3.40e-02	102.37	1.87e-02	81.30	1.49e-02	0.0	0.0
196	61.741	0.016	0.037	49.79	9.12e-03	238.37	4.37e-02	34.88	6.39e-03	0.0	0.0
197	61.983	0.016	0.037	33.80	6.19e-03	89.15	1.63e-02	296.41	5.43e-02	0.0	0.0
198	62.268	0.016	0.037	16.26	2.98e-03	14.34	2.63e-03	1536.42	0.3	0.0	0.0
199	62.310	0.016	0.037	60.70	1.11e-02	36.23	6.63e-03	165.93	3.04e-02	0.0	0.0
200	62.544	0.016	0.037	3.04	5.58e-04	12.78	2.34e-03	2.34	4.29e-04	0.0	0.0
201	62.694	0.016	0.037	24.99	4.58e-03	21.24	3.89e-03	345.98	6.34e-02	0.0	0.0
202	62.888	0.016	0.037	50.07	9.17e-03	192.30	3.52e-02	0.15	2.77e-05	0.0	0.0
203	62.956	0.016	0.037	223.86	4.10e-02	3.36	6.16e-04	4.95	9.07e-04	0.0	0.0
204	63.091	0.016	0.037	5.78	1.06e-03	3.30	6.04e-04	0.99	1.82e-04	0.0	0.0
205	63.402	0.016	0.037	65.39	1.20e-02	187.00	3.42e-02	47.24	8.65e-03	0.0	0.0
206	63.529	0.016	0.037	0.12	2.15e-05	310.42	5.68e-02	371.75	6.81e-02	0.0	0.0
207	63.730	0.016	0.037	10.80	1.98e-03	33.41	6.12e-03	113.72	2.08e-02	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
208	63.846	0.016	0.037	0.24	4.36e-05	46.28	8.47e-03	234.80	4.30e-02	0.0	0.0
209	64.215	0.016	0.037	55.61	1.02e-02	37.59	6.88e-03	2.71	4.97e-04	0.0	0.0
210	64.321	0.016	0.037	144.83	2.65e-02	26.57	4.87e-03	164.96	3.02e-02	0.0	0.0
211	64.367	0.016	0.037	27.93	5.11e-03	194.48	3.56e-02	392.75	7.19e-02	0.0	0.0
212	64.706	0.015	0.037	5.97	1.09e-03	21.51	3.94e-03	384.03	7.03e-02	0.0	0.0
213	64.800	0.015	0.037	0.05	8.63e-06	127.60	2.34e-02	1.54	2.83e-04	0.0	0.0
214	64.928	0.015	0.037	9.78	1.79e-03	106.60	1.95e-02	8.97	1.64e-03	0.0	0.0
215	65.259	0.015	0.037	92.00	1.68e-02	29.63	5.43e-03	50.05	9.17e-03	0.0	0.0
216	65.546	0.015	0.037	4.63	8.48e-04	159.03	2.91e-02	1199.96	0.2	0.0	0.0
217	65.613	0.015	0.037	29.19	5.35e-03	45.77	8.38e-03	1466.01	0.3	0.0	0.0
218	65.664	0.015	0.037	1.59	2.91e-04	65.62	1.20e-02	3.17	5.80e-04	0.0	0.0
219	65.897	0.015	0.037	46.51	8.52e-03	5.97	1.09e-03	125.15	2.29e-02	0.0	0.0
220	66.037	0.015	0.037	77.66	1.42e-02	58.36	1.07e-02	830.46	0.2	0.0	0.0
Risulta In percentuale				5.208e+05 95.38		5.282e+05 96.73		4.765e+05 87.27			

CDC	Tipo	Sigla Id	Note
13	Edk	CDC=Ed (dinamico SLD) alfa=90.00 (ecc. +)	
			verifica esistenti: fattore FC 1.200
			categoria suolo: B
			fattore di sito S = 1.200
			ordinata spettro (tratto Tb-Tc) = 0.075 g
			angolo di ingresso:90.00
			eccentricità aggiuntiva: positiva
			periodo proprio T1: 0.149 sec.
			numero di modi considerati:220
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
cm	daN	cm	cm	cm	cm	cm	cm			
1340.00	96.19	-491.36	-334.97	5.50	0.0	-491.36	-334.97	0.155	0.0	0.0
1295.00	116.44	-491.36	-334.97	5.50	0.0	-491.36	-334.97	1.791	0.0	0.0
1250.00	101.25	-491.36	-334.97	5.50	0.0	-491.36	-334.97	1.791	0.0	0.0
1205.00	1203.52	-572.28	-173.84	16.15	0.0	-635.82	-328.32	0.015	2.913	3.350
1195.00	7848.27	-175.90	173.40	23.73	0.0	-313.36	198.69	0.654	1.046	0.168
1160.00	2326.05	-575.55	-168.23	16.15	0.0	-635.82	-328.32	0.015	2.763	3.471
1115.00	2319.30	-575.63	-167.75	16.15	0.0	-635.82	-328.32	0.015	2.759	3.482
1070.00	2319.30	-575.63	-167.75	16.15	0.0	-635.82	-328.32	0.015	2.759	3.482
1025.00	1.465e+04	-128.29	99.57	58.25	0.0	-544.32	97.18	0.605	1.184	0.002
985.00	1.083e+04	-102.23	128.80	58.25	0.0	-542.11	167.56	0.726	1.143	0.047
945.00	1.083e+04	-102.21	128.80	58.25	0.0	-542.11	167.56	0.726	1.143	0.047
905.00	6.437e+04	-130.89	142.36	58.25	0.0	-458.71	212.95	0.530	0.997	0.097
855.00	1.642e+04	-128.78	145.90	58.25	0.0	-485.70	259.69	0.343	1.348	0.177
830.00	1249.33	528.64	424.28	0.0	0.0	0.0	0.0	0.0	0.0	0.0
805.00	1.479e+04	-102.33	164.15	58.25	0.0	-485.70	259.69	0.343	1.448	0.149
780.00	1249.33	528.64	538.78	0.0	0.0	0.0	0.0	0.0	0.0	0.0
755.00	1.526e+04	-82.93	181.97	58.25	0.0	-481.74	260.08	0.362	1.467	0.118
728.69	1131.11	528.64	656.28	0.0	0.0	0.0	0.0	0.0	0.0	0.0
705.00	1.607e+04	-55.85	217.96	58.25	0.0	-388.08	347.18	0.814	0.815	0.144
675.00	466.53	528.64	533.13	0.0	0.0	0.0	0.0	0.0	0.0	0.0
655.00	1.415e+04	-110.23	162.68	58.25	0.0	-485.60	338.86	0.413	1.292	0.286
605.00	1.443e+04	-81.71	180.98	58.25	0.0	-388.24	376.21	0.787	0.765	0.213
555.00	1.494e+04	-58.92	172.30	58.25	0.0	-381.08	258.88	0.824	0.785	0.088
535.00	462.89	-284.62	710.53	25.37	0.0	-295.19	710.53	0.049	0.058	0.0
505.00	1.668e+04	-63.27	192.44	58.25	0.0	-380.93	345.75	0.857	0.759	0.170
455.00	1.393e+05	-26.77	231.20	58.25	0.0	-366.53	489.83	0.922	0.783	0.375
404.44	1.848e+04	-42.92	230.40	58.25	0.0	-385.70	570.64	0.732	0.887	0.542
378.89	7112.79	-473.91	-262.63	16.15	0.0	-474.86	-329.87	2.180	0.006	0.456
353.89	2.196e+04	-32.62	456.21	58.25	0.0	-355.57	632.92	0.678	0.799	0.423
303.33	1.928e+04	-91.51	295.05	58.25	0.0	-445.29	639.78	0.388	1.157	0.686
252.78	2.190e+04	-176.89	242.77	58.25	0.0	-448.92	647.41	0.369	0.913	0.816
202.22	1.592e+04	-73.92	284.63	58.25	0.0	-448.92	647.41	0.369	1.258	0.731
151.67	1.601e+04	-65.56	283.49	58.25	0.0	-448.94	620.41	0.408	1.223	0.654
122.00	7167.74	-473.02	-262.23	16.15	0.0	-474.86	-329.87	2.180	0.012	0.459
101.11	1.343e+04	-59.25	403.57	58.25	0.0	-371.53	681.11	0.575	0.839	0.682

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
88.00	511.85	445.72	710.53	10.71	0.0	459.84	710.53	0.039	0.268	0.0
80.00	1592.11	106.62	-334.97	37.58	0.0	101.38	-334.97	0.074	0.024	0.0
50.56	1.912e+04	-72.11	249.76	58.25	0.0	-446.67	538.92	0.539	1.040	0.516
Risulta	5.461e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	3.930	0.254	0.075	496.54	9.09e-02	8.522e+04	15.6	0.08	1.55e-05	0.0	0.0
2	4.059	0.246	0.075	2033.34	0.4	9.361e+04	17.1	0.05	9.32e-06	0.0	0.0
3	6.124	0.163	0.075	3.185e+05	58.3	176.89	3.24e-02	6.85	1.25e-03	0.0	0.0
4	6.723	0.149	0.075	4922.38	0.9	1.329e+05	24.3	1.34	2.45e-04	0.0	0.0
5	7.492	0.133	0.075	7097.43	1.3	447.14	8.19e-02	3.13	5.74e-04	0.0	0.0
6	8.208	0.122	0.075	4.156e+04	7.6	1.483e+04	2.7	21.68	3.97e-03	0.0	0.0
7	8.419	0.119	0.075	110.20	2.02e-02	7.118e+04	13.0	16.48	3.02e-03	0.0	0.0
8	9.068	0.110	0.075	1.573e+04	2.9	2882.30	0.5	6.65	1.22e-03	0.0	0.0
9	9.091	0.110	0.075	1307.15	0.2	83.41	1.53e-02	64.73	1.19e-02	0.0	0.0
10	9.697	0.103	0.075	1.431e+04	2.6	0.02	2.77e-06	0.16	2.98e-05	0.0	0.0
11	9.828	0.102	0.075	5063.24	0.9	1106.31	0.2	9.24	1.69e-03	0.0	0.0
12	10.139	0.099	0.075	875.17	0.2	692.71	0.1	1.10	2.02e-04	0.0	0.0
13	10.541	0.095	0.075	8628.14	1.6	1.599e+04	2.9	22.28	4.08e-03	0.0	0.0
14	10.715	0.093	0.075	186.47	3.41e-02	4062.67	0.7	2.29	4.19e-04	0.0	0.0
15	11.356	0.088	0.073	7619.48	1.4	161.66	2.96e-02	0.03	6.17e-06	0.0	0.0
16	11.876	0.084	0.071	118.94	2.18e-02	163.30	2.99e-02	7.42	1.36e-03	0.0	0.0
17	12.646	0.079	0.068	3599.48	0.7	1037.10	0.2	3.61	6.61e-04	0.0	0.0
18	12.931	0.077	0.067	9618.77	1.8	4693.11	0.9	49.49	9.06e-03	0.0	0.0
19	13.070	0.077	0.067	6004.82	1.1	259.23	4.75e-02	10.59	1.94e-03	0.0	0.0
20	13.547	0.074	0.065	1580.19	0.3	7472.24	1.4	10.81	1.98e-03	0.0	0.0
21	14.069	0.071	0.064	3909.63	0.7	2408.86	0.4	82.69	1.51e-02	0.0	0.0
22	14.183	0.071	0.064	745.66	0.1	13.51	2.47e-03	58.44	1.07e-02	0.0	0.0
23	14.574	0.069	0.063	55.18	1.01e-02	4710.76	0.9	0.91	1.67e-04	0.0	0.0
24	15.001	0.067	0.062	4572.73	0.8	59.64	1.09e-02	8.21	1.50e-03	0.0	0.0
25	15.196	0.066	0.062	2275.74	0.4	924.58	0.2	344.62	6.31e-02	0.0	0.0
26	15.749	0.063	0.060	3.36	6.15e-04	8645.83	1.6	6.34	1.16e-03	0.0	0.0
27	16.365	0.061	0.059	5880.88	1.1	2529.07	0.5	4.58	8.38e-04	0.0	0.0
28	16.701	0.060	0.059	243.51	4.46e-02	3386.35	0.6	109.09	2.00e-02	0.0	0.0
29	16.938	0.059	0.058	4420.96	0.8	330.86	6.06e-02	433.65	7.94e-02	0.0	0.0
30	17.055	0.059	0.058	2104.32	0.4	2478.11	0.5	55.36	1.01e-02	0.0	0.0
31	17.579	0.057	0.057	1571.97	0.3	530.50	9.72e-02	356.07	6.52e-02	0.0	0.0
32	17.764	0.056	0.057	5019.44	0.9	228.10	4.18e-02	9408.47	1.7	0.0	0.0
33	17.895	0.056	0.057	2953.11	0.5	1523.37	0.3	864.32	0.2	0.0	0.0
34	18.441	0.054	0.056	953.80	0.2	296.87	5.44e-02	7528.20	1.4	0.0	0.0
35	19.238	0.052	0.055	1319.12	0.2	12.88	2.36e-03	9424.08	1.7	0.0	0.0
36	19.321	0.052	0.055	144.89	2.65e-02	93.78	1.72e-02	2.167e+04	4.0	0.0	0.0
37	19.367	0.052	0.055	31.49	5.77e-03	42.35	7.75e-03	1409.98	0.3	0.0	0.0
38	19.624	0.051	0.054	10.85	1.99e-03	482.25	8.83e-02	2.182e+04	4.0	0.0	0.0
39	20.174	0.050	0.054	1289.12	0.2	3880.30	0.7	7623.55	1.4	0.0	0.0
40	20.230	0.049	0.053	339.61	6.22e-02	119.93	2.20e-02	2299.89	0.4	0.0	0.0
41	20.615	0.049	0.053	18.13	3.32e-03	1421.40	0.3	5881.19	1.1	0.0	0.0
42	20.965	0.048	0.053	0.47	8.67e-05	325.19	5.96e-02	2243.23	0.4	0.0	0.0
43	21.207	0.047	0.052	687.61	0.1	280.69	5.14e-02	3.430e+04	6.3	0.0	0.0
44	21.347	0.047	0.052	24.38	4.46e-03	1132.99	0.2	1.788e+04	3.3	0.0	0.0
45	21.514	0.046	0.052	3812.61	0.7	6649.32	1.2	1088.54	0.2	0.0	0.0
46	21.832	0.046	0.052	1994.33	0.4	1589.25	0.3	1.611e+04	3.0	0.0	0.0
47	21.985	0.045	0.052	105.34	1.93e-02	1388.03	0.3	868.41	0.2	0.0	0.0
48	22.033	0.045	0.052	94.20	1.73e-02	313.79	5.75e-02	1985.69	0.4	0.0	0.0
49	22.495	0.044	0.051	942.35	0.2	5415.87	1.0	26.73	4.90e-03	0.0	0.0
50	22.720	0.044	0.051	641.85	0.1	741.82	0.1	1.263e+05	23.1	0.0	0.0
51	23.449	0.043	0.050	7.24	1.33e-03	255.77	4.68e-02	9718.61	1.8	0.0	0.0
52	23.589	0.042	0.050	59.75	1.09e-02	1037.60	0.2	1863.41	0.3	0.0	0.0
53	23.855	0.042	0.050	179.70	3.29e-02	5314.26	1.0	2865.08	0.5	0.0	0.0
54	24.241	0.041	0.049	185.24	3.39e-02	238.35	4.36e-02	1.96	3.59e-04	0.0	0.0
55	24.281	0.041	0.049	131.06	2.40e-02	1693.15	0.3	967.85	0.2	0.0	0.0
56	24.481	0.041	0.049	166.15	3.04e-02	3918.80	0.7	2337.21	0.4	0.0	0.0
57	25.018	0.040	0.049	3.01	5.52e-04	62.39	1.14e-02	0.60	1.10e-04	0.0	0.0
58	25.160	0.040	0.049	14.56	2.67e-03	5.18	9.48e-04	785.81	0.1	0.0	0.0
59	25.559	0.039	0.048	73.15	1.34e-02	10.48	1.92e-03	1.086e+04	2.0	0.0	0.0
60	25.877	0.039	0.048	2.56	4.69e-04	44.15	8.08e-03	1796.67	0.3	0.0	0.0
61	26.222	0.038	0.048	30.06	5.51e-03	0.16	2.98e-05	31.76	5.82e-03	0.0	0.0
62	26.608	0.038	0.048	161.74	2.96e-02	352.42	6.45e-02	4077.99	0.7	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
63	26.932	0.037	0.047	141.98	2.60e-02	2.59	4.74e-04	3820.47	0.7	0.0	0.0
64	27.476	0.036	0.047	152.51	2.79e-02	2535.16	0.5	1.248e+04	2.3	0.0	0.0
65	27.680	0.036	0.047	36.81	6.74e-03	260.77	4.78e-02	4378.99	0.8	0.0	0.0
66	27.723	0.036	0.047	58.36	1.07e-02	1470.51	0.3	4723.37	0.9	0.0	0.0
67	28.037	0.036	0.047	192.78	3.53e-02	152.53	2.79e-02	1.072e+04	2.0	0.0	0.0
68	28.372	0.035	0.047	9.11	1.67e-03	624.27	0.1	310.77	5.69e-02	0.0	0.0
69	28.712	0.035	0.046	169.90	3.11e-02	84.00	1.54e-02	97.79	1.79e-02	0.0	0.0
70	28.862	0.035	0.046	2827.38	0.5	186.31	3.41e-02	1258.26	0.2	0.0	0.0
71	29.045	0.034	0.046	1.65	3.02e-04	691.66	0.1	7961.01	1.5	0.0	0.0
72	29.559	0.034	0.046	646.97	0.1	26.01	4.76e-03	4006.96	0.7	0.0	0.0
73	29.791	0.034	0.046	94.94	1.74e-02	1633.40	0.3	1629.39	0.3	0.0	0.0
74	30.256	0.033	0.045	300.89	5.51e-02	690.41	0.1	6766.69	1.2	0.0	0.0
75	30.436	0.033	0.045	97.64	1.79e-02	853.10	0.2	2807.36	0.5	0.0	0.0
76	30.700	0.033	0.045	686.96	0.1	62.91	1.15e-02	5453.92	1.0	0.0	0.0
77	30.910	0.032	0.045	59.01	1.08e-02	766.79	0.1	1630.84	0.3	0.0	0.0
78	31.041	0.032	0.045	37.85	6.93e-03	7.69	1.41e-03	272.86	5.00e-02	0.0	0.0
79	31.500	0.032	0.045	309.09	5.66e-02	113.89	2.09e-02	4754.07	0.9	0.0	0.0
80	31.774	0.031	0.045	2.37	4.33e-04	27.39	5.02e-03	3031.34	0.6	0.0	0.0
81	31.971	0.031	0.045	592.73	0.1	0.61	1.11e-04	5195.71	1.0	0.0	0.0
82	32.010	0.031	0.045	520.02	9.52e-02	202.61	3.71e-02	1937.23	0.4	0.0	0.0
83	32.273	0.031	0.044	38.35	7.02e-03	6.54	1.20e-03	86.39	1.58e-02	0.0	0.0
84	32.383	0.031	0.044	90.44	1.66e-02	11.35	2.08e-03	2706.34	0.5	0.0	0.0
85	32.942	0.030	0.044	448.58	8.21e-02	362.89	6.65e-02	3954.27	0.7	0.0	0.0
86	33.424	0.030	0.044	382.49	7.00e-02	243.90	4.47e-02	4770.46	0.9	0.0	0.0
87	33.584	0.030	0.044	127.70	2.34e-02	2.87	5.25e-04	1713.66	0.3	0.0	0.0
88	33.878	0.030	0.044	353.16	6.47e-02	631.02	0.1	7.73	1.42e-03	0.0	0.0
89	34.114	0.029	0.044	268.17	4.91e-02	92.61	1.70e-02	3806.69	0.7	0.0	0.0
90	34.276	0.029	0.044	685.59	0.1	79.04	1.45e-02	679.40	0.1	0.0	0.0
91	34.590	0.029	0.043	253.20	4.64e-02	479.59	8.78e-02	1442.28	0.3	0.0	0.0
92	35.283	0.028	0.043	19.45	3.56e-03	0.19	3.51e-05	2339.35	0.4	0.0	0.0
93	35.585	0.028	0.043	173.03	3.17e-02	282.80	5.18e-02	4142.86	0.8	0.0	0.0
94	36.082	0.028	0.043	276.98	5.07e-02	255.39	4.68e-02	211.13	3.87e-02	0.0	0.0
95	36.715	0.027	0.043	12.54	2.30e-03	4.82	8.83e-04	5790.22	1.1	0.0	0.0
96	36.906	0.027	0.042	217.46	3.98e-02	2.17	3.97e-04	777.51	0.1	0.0	0.0
97	37.032	0.027	0.042	5.10	9.33e-04	7.63	1.40e-03	1.50	2.75e-04	0.0	0.0
98	37.363	0.027	0.042	16.87	3.09e-03	172.31	3.16e-02	314.94	5.77e-02	0.0	0.0
99	37.490	0.027	0.042	8.89	1.63e-03	337.95	6.19e-02	2982.46	0.5	0.0	0.0
100	37.781	0.026	0.042	172.14	3.15e-02	306.63	5.62e-02	648.19	0.1	0.0	0.0
101	38.112	0.026	0.042	139.45	2.55e-02	58.64	1.07e-02	2184.14	0.4	0.0	0.0
102	38.266	0.026	0.042	0.05	8.85e-06	106.25	1.95e-02	1548.89	0.3	0.0	0.0
103	38.626	0.026	0.042	181.99	3.33e-02	4.05	7.41e-04	0.36	6.63e-05	0.0	0.0
104	39.158	0.026	0.042	33.56	6.15e-03	140.36	2.57e-02	84.58	1.55e-02	0.0	0.0
105	39.396	0.025	0.042	0.62	1.14e-04	13.41	2.46e-03	137.37	2.52e-02	0.0	0.0
106	39.550	0.025	0.042	160.19	2.93e-02	282.39	5.17e-02	754.06	0.1	0.0	0.0
107	39.627	0.025	0.042	266.94	4.89e-02	33.43	6.12e-03	3.62	6.62e-04	0.0	0.0
108	39.982	0.025	0.041	621.95	0.1	41.30	7.56e-03	935.32	0.2	0.0	0.0
109	40.165	0.025	0.041	1.43	2.62e-04	14.48	2.65e-03	211.41	3.87e-02	0.0	0.0
110	40.286	0.025	0.041	16.66	3.05e-03	19.95	3.65e-03	38.09	6.98e-03	0.0	0.0
111	40.478	0.025	0.041	2.77	5.06e-04	200.58	3.67e-02	469.89	8.61e-02	0.0	0.0
112	40.776	0.025	0.041	170.31	3.12e-02	89.99	1.65e-02	279.78	5.12e-02	0.0	0.0
113	41.187	0.024	0.041	38.25	7.00e-03	5.10	9.35e-04	339.67	6.22e-02	0.0	0.0
114	41.243	0.024	0.041	251.44	4.60e-02	4.64	8.50e-04	28.78	5.27e-03	0.0	0.0
115	41.614	0.024	0.041	51.44	9.42e-03	190.01	3.48e-02	21.00	3.85e-03	0.0	0.0
116	42.043	0.024	0.041	3.66	6.70e-04	7.45	1.36e-03	199.20	3.65e-02	0.0	0.0
117	42.120	0.024	0.041	248.12	4.54e-02	76.56	1.40e-02	6.27	1.15e-03	0.0	0.0
118	42.396	0.024	0.041	5.11	9.36e-04	556.27	0.1	49.28	9.03e-03	0.0	0.0
119	42.668	0.023	0.041	222.00	4.07e-02	105.31	1.93e-02	143.98	2.64e-02	0.0	0.0
120	42.917	0.023	0.041	175.94	3.22e-02	64.85	1.19e-02	341.23	6.25e-02	0.0	0.0
121	43.165	0.023	0.041	321.75	5.89e-02	62.44	1.14e-02	274.14	5.02e-02	0.0	0.0
122	43.320	0.023	0.041	2.37	4.34e-04	116.20	2.13e-02	216.61	3.97e-02	0.0	0.0
123	43.601	0.023	0.040	46.36	8.49e-03	2.36	4.33e-04	353.49	6.47e-02	0.0	0.0
124	43.682	0.023	0.040	219.63	4.02e-02	231.82	4.25e-02	164.61	3.01e-02	0.0	0.0
125	43.973	0.023	0.040	1175.22	0.2	6.49	1.19e-03	220.22	4.03e-02	0.0	0.0
126	44.312	0.023	0.040	1329.67	0.2	3.21	5.87e-04	62.59	1.15e-02	0.0	0.0
127	44.478	0.022	0.040	6.39	1.17e-03	39.80	7.29e-03	51.52	9.43e-03	0.0	0.0
128	44.589	0.022	0.040	11.58	2.12e-03	21.36	3.91e-03	13.23	2.42e-03	0.0	0.0
129	44.856	0.022	0.040	253.56	4.64e-02	387.59	7.10e-02	131.66	2.41e-02	0.0	0.0
130	45.221	0.022	0.040	249.96	4.58e-02	84.29	1.54e-02	239.33	4.38e-02	0.0	0.0
131	45.503	0.022	0.040	213.94	3.92e-02	119.21	2.18e-02	542.67	9.94e-02	0.0	0.0
132	45.663	0.022	0.040	0.48	8.82e-05	40.23	7.37e-03	0.34	6.21e-05	0.0	0.0
133	45.782	0.022	0.040	440.22	8.06e-02	494.07	9.05e-02	6.95	1.27e-03	0.0	0.0
134	45.870	0.022	0.040	90.73	1.66e-02	38.34	7.02e-03	1643.39	0.3	0.0	0.0
135	46.214	0.022	0.040	944.84	0.2	8.27	1.51e-03	184.78	3.38e-02	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
136	46.564	0.021	0.040	143.54	2.63e-02	415.87	7.62e-02	64.19	1.18e-02	0.0	0.0
137	46.698	0.021	0.040	530.02	9.71e-02	0.02	3.08e-06	116.29	2.13e-02	0.0	0.0
138	46.968	0.021	0.040	8.84	1.62e-03	6.03	1.10e-03	34.31	6.28e-03	0.0	0.0
139	47.129	0.021	0.040	61.89	1.13e-02	31.89	5.84e-03	19.35	3.54e-03	0.0	0.0
140	47.576	0.021	0.040	348.56	6.38e-02	18.68	3.42e-03	11.77	2.15e-03	0.0	0.0
141	47.686	0.021	0.039	2.50	4.58e-04	131.64	2.41e-02	39.66	7.26e-03	0.0	0.0
142	48.005	0.021	0.039	132.29	2.42e-02	53.50	9.80e-03	0.04	7.89e-06	0.0	0.0
143	48.430	0.021	0.039	83.14	1.52e-02	64.23	1.18e-02	151.82	2.78e-02	0.0	0.0
144	48.752	0.021	0.039	617.62	0.1	70.31	1.29e-02	749.73	0.1	0.0	0.0
145	49.000	0.020	0.039	48.50	8.88e-03	150.21	2.75e-02	21.43	3.92e-03	0.0	0.0
146	49.235	0.020	0.039	0.71	1.31e-04	13.99	2.56e-03	0.02	3.15e-06	0.0	0.0
147	49.628	0.020	0.039	129.16	2.37e-02	24.61	4.51e-03	61.43	1.12e-02	0.0	0.0
148	49.898	0.020	0.039	128.09	2.35e-02	69.83	1.28e-02	26.11	4.78e-03	0.0	0.0
149	50.044	0.020	0.039	8.51	1.56e-03	535.35	9.80e-02	130.27	2.39e-02	0.0	0.0
150	50.116	0.020	0.039	3.02	5.52e-04	76.39	1.40e-02	101.00	1.85e-02	0.0	0.0
151	50.338	0.020	0.039	86.06	1.58e-02	363.52	6.66e-02	125.15	2.29e-02	0.0	0.0
152	50.603	0.020	0.039	27.87	5.10e-03	38.24	7.00e-03	22.97	4.21e-03	0.0	0.0
153	50.622	0.020	0.039	6.59	1.21e-03	1.13	2.06e-04	0.76	1.40e-04	0.0	0.0
154	50.904	0.020	0.039	49.55	9.07e-03	1.21	2.22e-04	267.23	4.89e-02	0.0	0.0
155	51.056	0.020	0.039	2.70	4.95e-04	494.63	9.06e-02	129.58	2.37e-02	0.0	0.0
156	51.188	0.020	0.039	33.57	6.15e-03	189.03	3.46e-02	242.94	4.45e-02	0.0	0.0
157	51.823	0.019	0.039	52.41	9.60e-03	137.29	2.51e-02	573.46	0.1	0.0	0.0
158	52.026	0.019	0.039	108.14	1.98e-02	0.66	1.21e-04	105.93	1.94e-02	0.0	0.0
159	52.351	0.019	0.039	874.49	0.2	551.93	0.1	44.07	8.07e-03	0.0	0.0
160	52.652	0.019	0.039	1.40	2.56e-04	177.90	3.26e-02	153.85	2.82e-02	0.0	0.0
161	52.682	0.019	0.039	164.28	3.01e-02	135.70	2.49e-02	1302.59	0.2	0.0	0.0
162	53.131	0.019	0.038	16.05	2.94e-03	159.52	2.92e-02	13.15	2.41e-03	0.0	0.0
163	53.320	0.019	0.038	58.30	1.07e-02	133.57	2.45e-02	226.14	4.14e-02	0.0	0.0
164	53.551	0.019	0.038	10.10	1.85e-03	235.03	4.30e-02	19.70	3.61e-03	0.0	0.0
165	53.626	0.019	0.038	1.25	2.29e-04	27.61	5.06e-03	89.08	1.63e-02	0.0	0.0
166	53.862	0.019	0.038	68.37	1.25e-02	24.63	4.51e-03	125.13	2.29e-02	0.0	0.0
167	53.986	0.019	0.038	14.44	2.64e-03	169.88	3.11e-02	82.37	1.51e-02	0.0	0.0
168	54.274	0.018	0.038	2.24	4.11e-04	11.41	2.09e-03	0.06	1.02e-05	0.0	0.0
169	54.600	0.018	0.038	0.27	5.03e-05	346.15	6.34e-02	8.22	1.50e-03	0.0	0.0
170	54.740	0.018	0.038	139.06	2.55e-02	53.30	9.76e-03	649.90	0.1	0.0	0.0
171	54.980	0.018	0.038	178.29	3.26e-02	403.41	7.39e-02	12.54	2.30e-03	0.0	0.0
172	55.123	0.018	0.038	19.28	3.53e-03	287.54	5.27e-02	6.99	1.28e-03	0.0	0.0
173	55.466	0.018	0.038	321.48	5.89e-02	54.98	1.01e-02	7.86	1.44e-03	0.0	0.0
174	55.896	0.018	0.038	0.47	8.70e-05	145.13	2.66e-02	34.83	6.38e-03	0.0	0.0
175	56.098	0.018	0.038	27.44	5.03e-03	52.46	9.61e-03	591.60	0.1	0.0	0.0
176	56.308	0.018	0.038	1.05	1.93e-04	194.30	3.56e-02	115.85	2.12e-02	0.0	0.0
177	56.539	0.018	0.038	69.98	1.28e-02	33.36	6.11e-03	4.82	8.83e-04	0.0	0.0
178	57.053	0.018	0.038	172.55	3.16e-02	15.98	2.93e-03	129.92	2.38e-02	0.0	0.0
179	57.190	0.017	0.038	2.92	5.35e-04	8.31	1.52e-03	203.03	3.72e-02	0.0	0.0
180	57.254	0.017	0.038	8.96	1.64e-03	12.46	2.28e-03	2.55	4.67e-04	0.0	0.0
181	57.542	0.017	0.038	35.31	6.47e-03	307.93	5.64e-02	38.84	7.11e-03	0.0	0.0
182	57.700	0.017	0.038	21.20	3.88e-03	32.57	5.97e-03	0.15	2.83e-05	0.0	0.0
183	57.902	0.017	0.038	74.78	1.37e-02	105.34	1.93e-02	5.42e-04	0.0	0.0	0.0
184	58.307	0.017	0.038	142.64	2.61e-02	49.39	9.04e-03	1670.41	0.3	0.0	0.0
185	58.690	0.017	0.038	0.79	1.44e-04	2.72	4.98e-04	73.59	1.35e-02	0.0	0.0
186	58.964	0.017	0.038	66.82	1.22e-02	19.74	3.61e-03	26.63	4.88e-03	0.0	0.0
187	59.222	0.017	0.037	6.25e-03	1.14e-06	3.24	5.93e-04	180.23	3.30e-02	0.0	0.0
188	59.273	0.017	0.037	68.76	1.26e-02	44.12	8.08e-03	271.71	4.98e-02	0.0	0.0
189	59.456	0.017	0.037	71.98	1.32e-02	13.92	2.55e-03	1820.55	0.3	0.0	0.0
190	59.612	0.017	0.037	14.17	2.60e-03	131.84	2.41e-02	148.52	2.72e-02	0.0	0.0
191	59.928	0.017	0.037	196.00	3.59e-02	0.01	2.52e-06	16.72	3.06e-03	0.0	0.0
192	60.212	0.017	0.037	6.60	1.21e-03	263.82	4.83e-02	258.44	4.73e-02	0.0	0.0
193	60.534	0.017	0.037	15.49	2.84e-03	2.21	4.05e-04	64.25	1.18e-02	0.0	0.0
194	60.789	0.016	0.037	95.44	1.75e-02	1.28	2.34e-04	103.97	1.90e-02	0.0	0.0
195	61.018	0.016	0.037	56.29	1.03e-02	68.53	1.26e-02	0.03	4.91e-06	0.0	0.0
196	61.138	0.016	0.037	396.81	7.27e-02	111.93	2.05e-02	211.20	3.87e-02	0.0	0.0
197	61.289	0.016	0.037	25.53	4.68e-03	7.75	1.42e-03	1191.83	0.2	0.0	0.0
198	61.633	0.016	0.037	4.71	8.63e-04	61.85	1.13e-02	1407.80	0.3	0.0	0.0
199	61.759	0.016	0.037	115.83	2.12e-02	229.46	4.20e-02	41.05	7.52e-03	0.0	0.0
200	62.011	0.016	0.037	0.79	1.45e-04	8.11	1.49e-03	48.89	8.95e-03	0.0	0.0
201	62.168	0.016	0.037	71.50	1.31e-02	94.47	1.73e-02	3.65	6.68e-04	0.0	0.0
202	62.256	0.016	0.037	8.87	1.62e-03	18.29	3.35e-03	0.56	1.03e-04	0.0	0.0
203	62.589	0.016	0.037	0.06	1.03e-05	88.37	1.62e-02	145.19	2.66e-02	0.0	0.0
204	62.678	0.016	0.037	86.11	1.58e-02	18.37	3.36e-03	17.47	3.20e-03	0.0	0.0
205	62.837	0.016	0.037	78.77	1.44e-02	32.62	5.97e-03	113.39	2.08e-02	0.0	0.0
206	62.920	0.016	0.037	2.76	5.06e-04	13.73	2.51e-03	63.67	1.17e-02	0.0	0.0
207	63.069	0.016	0.037	27.88	5.11e-03	346.79	6.35e-02	85.95	1.57e-02	0.0	0.0
208	63.312	0.016	0.037	39.06	7.15e-03	1.34	2.45e-04	66.79	1.22e-02	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
209	63.423	0.016	0.037	99.83	1.83e-02	0.94	1.73e-04	128.18	2.35e-02	0.0	0.0
210	63.617	0.016	0.037	12.69	2.32e-03	22.74	4.17e-03	98.58	1.81e-02	0.0	0.0
211	63.852	0.016	0.037	62.38	1.14e-02	12.41	2.27e-03	10.68	1.95e-03	0.0	0.0
212	64.057	0.016	0.037	27.72	5.08e-03	88.99	1.63e-02	22.05	4.04e-03	0.0	0.0
213	64.072	0.016	0.037	62.25	1.14e-02	49.29	9.03e-03	46.85	8.58e-03	0.0	0.0
214	64.196	0.016	0.037	174.20	3.19e-02	36.41	6.67e-03	3.17	5.80e-04	0.0	0.0
215	64.555	0.015	0.037	371.13	6.80e-02	2.26	4.14e-04	108.51	1.99e-02	0.0	0.0
216	64.774	0.015	0.037	24.66	4.52e-03	7.87	1.44e-03	362.30	6.63e-02	0.0	0.0
217	65.011	0.015	0.037	49.88	9.13e-03	172.87	3.17e-02	735.15	0.1	0.0	0.0
218	65.403	0.015	0.037	228.29	4.18e-02	4.38	8.02e-04	478.82	8.77e-02	0.0	0.0
219	65.608	0.015	0.037	63.89	1.17e-02	0.31	5.72e-05	904.74	0.2	0.0	0.0
220	66.051	0.015	0.037	237.04	4.34e-02	88.34	1.62e-02	616.15	0.1	0.0	0.0
Risulta				5.229e+05		5.278e+05		4.756e+05			
In percentuale				95.76		96.66		87.10			

CDC	Tipo	Sigla Id	Note
14	Edk	CDC=Ed (dinamico SLD) alfa=90.00 (ecc. -)	
			verifica esistenti: fattore FC 1.200
			categoria suolo: B
			fattore di sito S = 1.200
			ordinata spettro (tratto Tb-Tc) = 0.075 g
			angolo di ingresso:90.00
			eccentricità aggiuntiva: negativa
			periodo proprio T1: 0.142 sec.
			numero di modi considerati:220
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
cm	daN	cm	cm	cm	cm	cm	cm			
1340.00	96.19	-491.36	-334.97	-5.50	0.0	-491.36	-334.97	0.155	0.0	0.0
1295.00	116.44	-491.36	-334.97	-5.50	0.0	-491.36	-334.97	1.791	0.0	0.0
1250.00	101.25	-491.36	-334.97	-5.50	0.0	-491.36	-334.97	1.791	0.0	0.0
1205.00	1203.52	-572.28	-173.84	-16.15	0.0	-635.82	-328.32	0.015	2.913	3.350
1195.00	7848.27	-175.90	173.40	-23.73	0.0	-313.36	198.69	0.654	1.046	0.168
1160.00	2326.05	-575.55	-168.23	-16.15	0.0	-635.82	-328.32	0.015	2.763	3.471
1115.00	2319.30	-575.63	-167.75	-16.15	0.0	-635.82	-328.32	0.015	2.759	3.482
1070.00	2319.30	-575.63	-167.75	-16.15	0.0	-635.82	-328.32	0.015	2.759	3.482
1025.00	1.465e+04	-128.29	99.57	-58.25	0.0	-544.32	97.18	0.605	1.184	0.002
985.00	1.083e+04	-102.23	128.80	-58.25	0.0	-542.11	167.56	0.726	1.143	0.047
945.00	1.083e+04	-102.21	128.80	-58.25	0.0	-542.11	167.56	0.726	1.143	0.047
905.00	6.437e+04	-130.89	142.36	-58.25	0.0	-458.71	212.95	0.530	0.997	0.097
855.00	1.642e+04	-128.78	145.90	-58.25	0.0	-485.70	259.69	0.343	1.348	0.177
830.00	1249.33	528.64	424.28	0.0	0.0	0.0	0.0	0.0	0.0	0.0
805.00	1.479e+04	-102.33	164.15	-58.25	0.0	-485.70	259.69	0.343	1.448	0.149
780.00	1249.33	528.64	538.78	0.0	0.0	0.0	0.0	0.0	0.0	0.0
755.00	1.526e+04	-82.93	181.97	-58.25	0.0	-481.74	260.08	0.362	1.467	0.118
728.69	1131.11	528.64	656.28	0.0	0.0	0.0	0.0	0.0	0.0	0.0
705.00	1.607e+04	-55.85	217.96	-58.25	0.0	-388.08	347.18	0.814	0.815	0.144
675.00	466.53	528.64	533.13	0.0	0.0	0.0	0.0	0.0	0.0	0.0
655.00	1.415e+04	-110.23	162.68	-58.25	0.0	-485.60	338.86	0.413	1.292	0.286
605.00	1.443e+04	-81.71	180.98	-58.25	0.0	-388.24	376.21	0.787	0.765	0.213
555.00	1.494e+04	-58.92	172.30	-58.25	0.0	-381.08	258.88	0.824	0.785	0.088
535.00	462.89	-284.62	710.53	-25.37	0.0	-295.19	710.53	0.049	0.058	0.0
505.00	1.668e+04	-63.27	192.44	-58.25	0.0	-380.93	345.75	0.857	0.759	0.170
455.00	1.393e+05	-26.77	231.20	-58.25	0.0	-366.53	489.83	0.922	0.783	0.375
404.44	1.848e+04	-42.92	230.40	-58.25	0.0	-385.70	570.64	0.732	0.887	0.542
378.89	7112.79	-473.91	-262.63	-16.15	0.0	-474.86	-329.87	2.180	0.006	0.456
353.89	2.196e+04	-32.62	456.21	-58.25	0.0	-355.57	632.92	0.678	0.799	0.423
303.33	1.928e+04	-91.51	295.05	-58.25	0.0	-445.29	639.78	0.388	1.157	0.686
252.78	2.190e+04	-176.89	242.77	-58.25	0.0	-448.92	647.41	0.369	0.913	0.816
202.22	1.592e+04	-73.92	284.63	-58.25	0.0	-448.92	647.41	0.369	1.258	0.731
151.67	1.601e+04	-65.56	283.49	-58.25	0.0	-448.94	620.41	0.408	1.223	0.654
122.00	7167.74	-473.02	-262.23	-16.15	0.0	-474.86	-329.87	2.180	0.012	0.459
101.11	1.343e+04	-59.25	403.57	-58.25	0.0	-371.53	681.11	0.575	0.839	0.682
88.00	511.85	445.72	710.53	-10.71	0.0	459.84	710.53	0.039	0.268	0.0

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
80.00	1592.11	106.62	-334.97	-37.58	0.0	101.38	-334.97	0.074	0.024	0.0
50.56	1.912e+04	-72.11	249.76	-58.25	0.0	-446.67	538.92	0.539	1.040	0.516
Risulta	5.461e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	4.195	0.238	0.075	774.14	0.1	8.205e+04	15.0	0.12	2.14e-05	0.0	0.0
2	4.376	0.229	0.075	2488.22	0.5	8.018e+04	14.7	0.09	1.61e-05	0.0	0.0
3	6.123	0.163	0.075	3.182e+05	58.3	1.496e+04	2.7	4.83	8.84e-04	0.0	0.0
4	7.026	0.142	0.075	8019.33	1.5	1.732e+05	31.7	8.19	1.50e-03	0.0	0.0
5	7.743	0.129	0.075	8784.12	1.6	2.97	5.45e-04	3.45	6.31e-04	0.0	0.0
6	8.420	0.119	0.075	4.832e+04	8.8	2.357e+04	4.3	41.99	7.69e-03	0.0	0.0
7	8.701	0.115	0.075	143.40	2.63e-02	2.565e+04	4.7	13.89	2.54e-03	0.0	0.0
8	9.197	0.109	0.075	3801.24	0.7	7212.28	1.3	20.64	3.78e-03	0.0	0.0
9	9.402	0.106	0.075	6040.17	1.1	1377.73	0.3	33.90	6.21e-03	0.0	0.0
10	9.878	0.101	0.075	3586.10	0.7	3440.92	0.6	3.13	5.74e-04	0.0	0.0
11	9.967	0.100	0.075	5823.70	1.1	21.35	3.91e-03	1.04	1.91e-04	0.0	0.0
12	10.401	0.096	0.075	9627.06	1.8	776.94	0.1	0.63	1.16e-04	0.0	0.0
13	10.634	0.094	0.075	2819.20	0.5	1.696e+04	3.1	5.00	9.15e-04	0.0	0.0
14	10.910	0.092	0.074	3719.33	0.7	40.64	7.44e-03	17.77	3.25e-03	0.0	0.0
15	11.493	0.087	0.072	1.109e+04	2.0	169.80	3.11e-02	1.37	2.51e-04	0.0	0.0
16	12.542	0.080	0.068	6996.57	1.3	193.83	3.55e-02	4.65	8.52e-04	0.0	0.0
17	12.905	0.077	0.067	1193.13	0.2	7034.82	1.3	33.62	6.16e-03	0.0	0.0
18	13.020	0.077	0.067	1353.09	0.2	1047.40	0.2	17.28	3.17e-03	0.0	0.0
19	13.522	0.074	0.066	7743.48	1.4	18.97	3.47e-03	4.59	8.40e-04	0.0	0.0
20	13.877	0.072	0.065	1379.72	0.3	782.61	0.1	5.05	9.25e-04	0.0	0.0
21	14.455	0.069	0.063	504.71	9.24e-02	4786.68	0.9	86.23	1.58e-02	0.0	0.0
22	14.789	0.068	0.062	856.43	0.2	427.15	7.82e-02	20.87	3.82e-03	0.0	0.0
23	15.040	0.066	0.062	4046.55	0.7	372.69	6.83e-02	19.05	3.49e-03	0.0	0.0
24	15.515	0.064	0.061	5514.93	1.0	40.71	7.46e-03	219.49	4.02e-02	0.0	0.0
25	15.687	0.064	0.061	832.29	0.2	6417.61	1.2	111.59	2.04e-02	0.0	0.0
26	15.997	0.063	0.060	0.58	1.06e-04	290.35	5.32e-02	19.05	3.49e-03	0.0	0.0
27	16.537	0.060	0.059	56.99	1.04e-02	1651.93	0.3	633.64	0.1	0.0	0.0
28	16.919	0.059	0.058	3232.23	0.6	19.41	3.55e-03	362.79	6.64e-02	0.0	0.0
29	17.041	0.059	0.058	2257.99	0.4	4508.02	0.8	3.64	6.66e-04	0.0	0.0
30	17.476	0.057	0.057	1.185e+04	2.2	980.18	0.2	2161.88	0.4	0.0	0.0
31	18.101	0.055	0.056	155.84	2.85e-02	3448.83	0.6	1691.34	0.3	0.0	0.0
32	18.252	0.055	0.056	1037.93	0.2	45.50	8.33e-03	4146.03	0.8	0.0	0.0
33	18.451	0.054	0.056	651.05	0.1	2839.31	0.5	1.674e+04	3.1	0.0	0.0
34	18.664	0.054	0.056	22.14	4.06e-03	4.56	8.35e-04	1.166e+04	2.1	0.0	0.0
35	19.271	0.052	0.055	1270.02	0.2	8.17	1.50e-03	6444.83	1.2	0.0	0.0
36	19.370	0.052	0.055	1157.10	0.2	119.41	2.19e-02	1259.67	0.2	0.0	0.0
37	20.016	0.050	0.054	83.63	1.53e-02	3028.54	0.6	4271.63	0.8	0.0	0.0
38	20.348	0.049	0.053	55.28	1.01e-02	54.13	9.91e-03	3.104e+04	5.7	0.0	0.0
39	20.582	0.049	0.053	823.12	0.2	667.71	0.1	3.265e+04	6.0	0.0	0.0
40	20.939	0.048	0.053	519.01	9.50e-02	9219.42	1.7	6786.46	1.2	0.0	0.0
41	21.103	0.047	0.052	212.08	3.88e-02	2837.82	0.5	2.221e+04	4.1	0.0	0.0
42	21.262	0.047	0.052	2545.21	0.5	1511.71	0.3	3127.15	0.6	0.0	0.0
43	21.604	0.046	0.052	557.56	0.1	119.65	2.19e-02	859.94	0.2	0.0	0.0
44	21.827	0.046	0.052	3819.16	0.7	3.59	6.57e-04	1.420e+04	2.6	0.0	0.0
45	21.901	0.046	0.052	57.84	1.06e-02	20.58	3.77e-03	3135.01	0.6	0.0	0.0
46	22.099	0.045	0.051	239.50	4.39e-02	1700.21	0.3	354.76	6.50e-02	0.0	0.0
47	22.208	0.045	0.051	74.71	1.37e-02	5185.83	0.9	2.048e+04	3.8	0.0	0.0
48	22.351	0.045	0.051	258.74	4.74e-02	8070.36	1.5	1094.67	0.2	0.0	0.0
49	22.946	0.044	0.051	342.99	6.28e-02	576.03	0.1	1.062e+05	19.4	0.0	0.0
50	23.367	0.043	0.050	337.26	6.18e-02	2255.79	0.4	197.26	3.61e-02	0.0	0.0
51	23.411	0.043	0.050	881.60	0.2	1418.54	0.3	1.039e+04	1.9	0.0	0.0
52	24.085	0.042	0.050	65.68	1.20e-02	1237.95	0.2	526.00	9.63e-02	0.0	0.0
53	24.227	0.041	0.049	196.89	3.61e-02	11.84	2.17e-03	1167.37	0.2	0.0	0.0
54	24.396	0.041	0.049	296.23	5.42e-02	64.66	1.18e-02	721.59	0.1	0.0	0.0
55	25.214	0.040	0.049	0.07	1.19e-05	27.10	4.96e-03	55.58	1.02e-02	0.0	0.0
56	25.559	0.039	0.048	218.80	4.01e-02	24.62	4.51e-03	1022.08	0.2	0.0	0.0
57	25.999	0.038	0.048	0.80	1.47e-04	171.53	3.14e-02	876.78	0.2	0.0	0.0
58	26.196	0.038	0.048	15.78	2.89e-03	267.65	4.90e-02	4340.65	0.8	0.0	0.0
59	26.447	0.038	0.048	50.77	9.30e-03	1293.13	0.2	1.157e+04	2.1	0.0	0.0
60	26.763	0.037	0.048	84.47	1.55e-02	83.67	1.53e-02	2.808e+04	5.1	0.0	0.0
61	26.950	0.037	0.047	172.80	3.16e-02	58.43	1.07e-02	40.84	7.48e-03	0.0	0.0
62	27.402	0.036	0.047	31.33	5.74e-03	942.31	0.2	2177.84	0.4	0.0	0.0
63	27.566	0.036	0.047	0.66	1.21e-04	251.87	4.61e-02	15.65	2.87e-03	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	Z %	Energia	Energia x v
64	27.652	0.036	0.047	250.87	4.59e-02	51.87	9.50e-03	6009.69	1.1	0.0	0.0
65	27.913	0.036	0.047	194.80	3.57e-02	698.78	0.1	7327.08	1.3	0.0	0.0
66	28.109	0.036	0.047	146.59	2.68e-02	802.73	0.1	1201.68	0.2	0.0	0.0
67	28.489	0.035	0.046	279.50	5.12e-02	3.22	5.89e-04	264.82	4.85e-02	0.0	0.0
68	28.676	0.035	0.046	21.58	3.95e-03	88.23	1.62e-02	194.18	3.56e-02	0.0	0.0
69	28.929	0.035	0.046	2264.83	0.4	147.31	2.70e-02	2574.16	0.5	0.0	0.0
70	28.975	0.035	0.046	200.11	3.66e-02	20.15	3.69e-03	778.57	0.1	0.0	0.0
71	29.149	0.034	0.046	84.42	1.55e-02	325.13	5.95e-02	1616.06	0.3	0.0	0.0
72	29.422	0.034	0.046	259.73	4.76e-02	421.92	7.73e-02	1262.31	0.2	0.0	0.0
73	29.967	0.033	0.046	25.42	4.65e-03	920.27	0.2	420.94	7.71e-02	0.0	0.0
74	30.421	0.033	0.045	122.78	2.25e-02	10.26	1.88e-03	4993.72	0.9	0.0	0.0
75	31.023	0.032	0.045	128.52	2.35e-02	3.38	6.18e-04	3621.44	0.7	0.0	0.0
76	31.502	0.032	0.045	90.97	1.67e-02	574.52	0.1	2702.12	0.5	0.0	0.0
77	31.556	0.032	0.045	1387.64	0.3	13.45	2.46e-03	973.89	0.2	0.0	0.0
78	31.804	0.031	0.045	378.82	6.94e-02	4.44	8.13e-04	2.420e+04	4.4	0.0	0.0
79	32.161	0.031	0.044	55.86	1.02e-02	59.90	1.10e-02	258.99	4.74e-02	0.0	0.0
80	32.313	0.031	0.044	377.27	6.91e-02	522.67	9.57e-02	137.21	2.51e-02	0.0	0.0
81	32.617	0.031	0.044	848.93	0.2	234.98	4.30e-02	0.02	3.57e-02	0.0	0.0
82	32.862	0.030	0.044	149.95	2.75e-02	493.64	9.04e-02	314.18	5.75e-02	0.0	0.0
83	32.902	0.030	0.044	21.49	3.94e-03	34.74	6.36e-03	1888.32	0.3	0.0	0.0
84	33.466	0.030	0.044	564.30	0.1	176.45	3.23e-02	3403.53	0.6	0.0	0.0
85	33.771	0.030	0.044	154.39	2.83e-02	145.63	2.67e-02	2230.61	0.4	0.0	0.0
86	33.901	0.029	0.044	6.94	1.27e-03	85.23	1.56e-02	2986.10	0.5	0.0	0.0
87	34.089	0.029	0.044	150.96	2.76e-02	107.15	1.96e-02	1545.99	0.3	0.0	0.0
88	34.424	0.029	0.043	263.18	4.82e-02	10.58	1.94e-03	4449.73	0.8	0.0	0.0
89	34.578	0.029	0.043	30.46	5.58e-03	2.33	4.26e-04	2044.97	0.4	0.0	0.0
90	34.857	0.029	0.043	9.86	1.81e-03	282.59	5.18e-02	142.40	2.61e-02	0.0	0.0
91	35.264	0.028	0.043	36.46	6.68e-03	539.45	9.88e-02	830.11	0.2	0.0	0.0
92	35.582	0.028	0.043	840.78	0.2	179.00	3.28e-02	3976.40	0.7	0.0	0.0
93	35.911	0.028	0.043	69.98	1.28e-02	1721.01	0.3	151.40	2.77e-02	0.0	0.0
94	36.152	0.028	0.043	317.94	5.82e-02	2.49	4.56e-04	98.29	1.80e-02	0.0	0.0
95	36.240	0.028	0.043	6.73	1.23e-03	475.72	8.71e-02	418.00	7.65e-02	0.0	0.0
96	37.163	0.027	0.042	0.04	6.88e-06	45.08	8.26e-03	5451.31	1.0	0.0	0.0
97	37.267	0.027	0.042	45.45	8.32e-03	73.94	1.35e-02	4.01	7.33e-04	0.0	0.0
98	37.641	0.027	0.042	12.33	2.26e-03	17.16	3.14e-03	3.69	6.76e-04	0.0	0.0
99	37.772	0.026	0.042	69.46	1.27e-02	289.51	5.30e-02	797.99	0.1	0.0	0.0
100	37.855	0.026	0.042	3.19	5.83e-04	454.75	8.33e-02	3398.39	0.6	0.0	0.0
101	38.121	0.026	0.042	15.47	2.83e-03	2.45	4.48e-04	3045.53	0.6	0.0	0.0
102	38.615	0.026	0.042	623.36	0.1	68.00	1.25e-02	19.43	3.56e-03	0.0	0.0
103	38.742	0.026	0.042	138.16	2.53e-02	140.64	2.58e-02	165.33	3.03e-02	0.0	0.0
104	39.072	0.026	0.042	6.66	1.22e-03	2.75	5.03e-04	12.36	2.26e-03	0.0	0.0
105	39.181	0.026	0.042	194.01	3.55e-02	221.22	4.05e-02	374.33	6.86e-02	0.0	0.0
106	39.412	0.025	0.042	256.21	4.69e-02	3.29	6.02e-04	451.66	8.27e-02	0.0	0.0
107	39.583	0.025	0.042	161.36	2.96e-02	435.88	7.98e-02	20.87	3.82e-03	0.0	0.0
108	39.955	0.025	0.041	6.85	1.26e-03	53.60	9.82e-03	38.69	7.09e-03	0.0	0.0
109	40.019	0.025	0.041	91.51	1.68e-02	308.23	5.64e-02	11.36	2.08e-03	0.0	0.0
110	40.258	0.025	0.041	150.85	2.76e-02	41.75	7.65e-03	1032.63	0.2	0.0	0.0
111	40.412	0.025	0.041	3.86	7.06e-04	91.58	1.68e-02	178.22	3.26e-02	0.0	0.0
112	40.612	0.025	0.041	40.83	7.48e-03	141.42	2.59e-02	561.27	0.1	0.0	0.0
113	41.128	0.024	0.041	7.94	1.45e-03	117.06	2.14e-02	412.46	7.55e-02	0.0	0.0
114	41.556	0.024	0.041	12.68	2.32e-03	0.02	3.44e-06	119.77	2.19e-02	0.0	0.0
115	41.710	0.024	0.041	32.17	5.89e-03	288.18	5.28e-02	12.74	2.33e-03	0.0	0.0
116	41.923	0.024	0.041	8.50	1.56e-03	6.72	1.23e-03	24.90	4.56e-03	0.0	0.0
117	42.123	0.024	0.041	33.87	6.20e-03	6.72	1.23e-03	1.38	2.54e-04	0.0	0.0
118	42.221	0.024	0.041	7.87	1.44e-03	1.36	2.48e-04	136.68	2.50e-02	0.0	0.0
119	42.844	0.023	0.041	655.15	0.1	16.42	3.01e-03	112.10	2.05e-02	0.0	0.0
120	42.996	0.023	0.041	141.22	2.59e-02	10.98	2.01e-03	77.16	1.41e-02	0.0	0.0
121	43.220	0.023	0.041	273.39	5.01e-02	49.26	9.02e-03	484.47	8.87e-02	0.0	0.0
122	43.616	0.023	0.040	13.17	2.41e-03	32.94	6.03e-03	532.67	9.75e-02	0.0	0.0
123	43.702	0.023	0.040	125.02	2.29e-02	65.57	1.20e-02	31.25	5.72e-03	0.0	0.0
124	43.972	0.023	0.040	4.49	8.21e-04	0.87	1.59e-04	7.68	1.41e-03	0.0	0.0
125	44.233	0.023	0.040	70.09	1.28e-02	55.19	1.01e-02	0.32	5.84e-05	0.0	0.0
126	44.519	0.022	0.040	185.18	3.39e-02	106.44	1.95e-02	177.02	3.24e-02	0.0	0.0
127	44.808	0.022	0.040	237.21	4.34e-02	6.34	1.16e-03	127.60	2.34e-02	0.0	0.0
128	45.067	0.022	0.040	205.21	3.76e-02	25.62	4.69e-03	351.96	6.45e-02	0.0	0.0
129	45.096	0.022	0.040	13.17	2.41e-03	16.67	3.05e-03	271.14	4.97e-02	0.0	0.0
130	45.301	0.022	0.040	2101.37	0.4	41.03	7.51e-03	890.80	0.2	0.0	0.0
131	45.701	0.022	0.040	2120.21	0.4	180.44	3.30e-02	791.96	0.1	0.0	0.0
132	45.941	0.022	0.040	42.32	7.75e-03	0.79	1.44e-04	36.12	6.61e-03	0.0	0.0
133	46.181	0.022	0.040	324.57	5.94e-02	8.20e-03	1.50e-06	50.61	9.27e-03	0.0	0.0
134	46.281	0.022	0.040	28.68	5.25e-03	250.32	4.58e-02	23.68	4.34e-03	0.0	0.0
135	46.517	0.021	0.040	18.94	3.47e-03	8.43	1.54e-03	145.11	2.66e-02	0.0	0.0
136	46.627	0.021	0.040	115.76	2.12e-02	2.30	4.21e-04	113.59	2.08e-02	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	Z %	Energia	Energia x v
137	46.732	0.021	0.040	627.71	0.1	129.83	2.38e-02	98.69	1.81e-02	0.0	0.0
138	46.906	0.021	0.040	43.99	8.06e-03	164.65	3.02e-02	69.55	1.27e-02	0.0	0.0
139	47.176	0.021	0.040	10.75	1.97e-03	20.53	3.76e-03	319.67	5.85e-02	0.0	0.0
140	47.815	0.021	0.039	27.49	5.04e-03	0.24	4.48e-05	113.13	2.07e-02	0.0	0.0
141	48.516	0.021	0.039	29.70	5.44e-03	502.06	9.19e-02	0.34	6.24e-05	0.0	0.0
142	48.670	0.021	0.039	5.91	1.08e-03	627.92	0.1	494.77	9.06e-02	0.0	0.0
143	48.914	0.020	0.039	101.78	1.86e-02	130.83	2.40e-02	5.14	9.41e-04	0.0	0.0
144	49.047	0.020	0.039	301.41	5.52e-02	8.34	1.53e-03	535.63	9.81e-02	0.0	0.0
145	49.303	0.020	0.039	47.57	8.71e-03	25.51	4.67e-03	161.22	2.95e-02	0.0	0.0
146	49.591	0.020	0.039	43.07	7.89e-03	32.03	5.87e-03	14.47	2.65e-03	0.0	0.0
147	49.738	0.020	0.039	9.46	1.73e-03	40.11	7.34e-03	80.21	1.47e-02	0.0	0.0
148	50.030	0.020	0.039	1.91	3.50e-04	136.26	2.50e-02	673.87	0.1	0.0	0.0
149	50.123	0.020	0.039	288.57	5.28e-02	220.84	4.04e-02	15.27	2.80e-03	0.0	0.0
150	50.450	0.020	0.039	23.93	4.38e-03	42.04	7.70e-03	46.02	8.43e-03	0.0	0.0
151	50.593	0.020	0.039	4.91e-04	0.0	403.95	7.40e-02	14.61	2.68e-03	0.0	0.0
152	50.787	0.020	0.039	29.73	5.44e-03	74.83	1.37e-02	42.08	7.71e-03	0.0	0.0
153	51.100	0.020	0.039	123.75	2.27e-02	24.63	4.51e-03	25.96	4.75e-03	0.0	0.0
154	51.241	0.020	0.039	334.07	6.12e-02	37.69	6.90e-03	64.86	1.19e-02	0.0	0.0
155	51.503	0.019	0.039	140.54	2.57e-02	0.30	5.47e-05	7.30	1.34e-03	0.0	0.0
156	51.984	0.019	0.039	18.41	3.37e-03	4.03	7.39e-04	60.34	1.10e-02	0.0	0.0
157	52.287	0.019	0.039	0.34	6.19e-05	128.99	2.36e-02	75.71	1.39e-02	0.0	0.0
158	52.523	0.019	0.039	203.83	3.73e-02	49.57	9.08e-03	729.97	0.1	0.0	0.0
159	52.738	0.019	0.038	301.06	5.51e-02	12.21	2.24e-03	659.11	0.1	0.0	0.0
160	53.324	0.019	0.038	171.27	3.14e-02	3.27	5.99e-04	10.67	1.95e-03	0.0	0.0
161	53.530	0.019	0.038	24.91	4.56e-03	238.64	4.37e-02	414.09	7.58e-02	0.0	0.0
162	53.700	0.019	0.038	35.33	6.47e-03	159.59	2.92e-02	83.99	1.54e-02	0.0	0.0
163	53.820	0.019	0.038	11.09	2.03e-03	259.97	4.76e-02	164.29	3.01e-02	0.0	0.0
164	53.899	0.019	0.038	53.31	9.76e-03	191.02	3.50e-02	50.70	9.29e-03	0.0	0.0
165	54.153	0.018	0.038	43.22	7.92e-03	40.11	7.35e-03	103.69	1.90e-02	0.0	0.0
166	54.476	0.018	0.038	167.45	3.07e-02	77.84	1.43e-02	253.77	4.65e-02	0.0	0.0
167	54.957	0.018	0.038	341.42	6.25e-02	63.46	1.16e-02	292.05	5.35e-02	0.0	0.0
168	54.979	0.018	0.038	61.98	1.14e-02	86.25	1.58e-02	33.61	6.16e-03	0.0	0.0
169	55.429	0.018	0.038	3.35	6.14e-04	150.51	2.76e-02	72.57	1.33e-02	0.0	0.0
170	55.872	0.018	0.038	78.62	1.44e-02	54.93	1.01e-02	38.40	7.03e-03	0.0	0.0
171	56.018	0.018	0.038	72.73	1.33e-02	65.71	1.20e-02	34.87	6.39e-03	0.0	0.0
172	56.333	0.018	0.038	31.84	5.83e-03	252.59	4.63e-02	920.19	0.2	0.0	0.0
173	56.777	0.018	0.038	173.48	3.18e-02	0.13	2.30e-05	3.37	6.18e-04	0.0	0.0
174	56.816	0.018	0.038	4.88	8.94e-04	30.89	5.66e-03	235.95	4.32e-02	0.0	0.0
175	57.023	0.018	0.038	101.85	1.87e-02	19.27	3.53e-03	684.35	0.1	0.0	0.0
176	57.221	0.017	0.038	0.03	4.83e-06	27.39	5.02e-03	0.79	1.45e-04	0.0	0.0
177	57.530	0.017	0.038	31.03	5.68e-03	0.64	1.16e-04	6.55	1.20e-03	0.0	0.0
178	57.851	0.017	0.038	1.13	2.07e-04	381.52	6.99e-02	95.14	1.74e-02	0.0	0.0
179	58.067	0.017	0.038	70.49	1.29e-02	93.87	1.72e-02	1097.90	0.2	0.0	0.0
180	58.347	0.017	0.038	10.73	1.96e-03	209.61	3.84e-02	323.36	5.92e-02	0.0	0.0
181	58.585	0.017	0.038	27.37	5.01e-03	95.44	1.75e-02	188.62	3.45e-02	0.0	0.0
182	58.687	0.017	0.038	2.19	4.00e-04	0.08	1.38e-05	527.30	9.66e-02	0.0	0.0
183	58.870	0.017	0.038	45.26	8.29e-03	410.49	7.52e-02	245.04	4.49e-02	0.0	0.0
184	59.279	0.017	0.037	16.51	3.02e-03	231.17	4.23e-02	132.89	2.43e-02	0.0	0.0
185	59.311	0.017	0.037	70.32	1.29e-02	253.12	4.64e-02	1.97	3.61e-04	0.0	0.0
186	59.597	0.017	0.037	26.73	4.89e-03	27.62	5.06e-03	385.53	7.06e-02	0.0	0.0
187	59.832	0.017	0.037	42.20	7.73e-03	18.78	3.44e-03	86.90	1.59e-02	0.0	0.0
188	60.166	0.017	0.037	336.24	6.16e-02	74.68	1.37e-02	75.78	1.39e-02	0.0	0.0
189	60.390	0.017	0.037	331.00	6.06e-02	52.86	9.68e-03	556.22	0.1	0.0	0.0
190	60.664	0.016	0.037	10.90	2.00e-03	118.30	2.17e-02	710.63	0.1	0.0	0.0
191	60.695	0.016	0.037	147.13	2.69e-02	40.14	7.35e-03	9.21	1.69e-03	0.0	0.0
192	61.025	0.016	0.037	20.58	3.77e-03	434.89	7.96e-02	183.49	3.36e-02	0.0	0.0
193	61.386	0.016	0.037	129.48	2.37e-02	174.33	3.19e-02	50.66	9.28e-03	0.0	0.0
194	61.523	0.016	0.037	120.99	2.22e-02	147.13	2.69e-02	432.27	7.92e-02	0.0	0.0
195	61.726	0.016	0.037	72.99	1.34e-02	0.91	1.68e-04	0.24	4.31e-05	0.0	0.0
196	61.856	0.016	0.037	0.16	2.85e-05	3.67	6.73e-04	92.79	1.70e-02	0.0	0.0
197	62.039	0.016	0.037	3.08	5.64e-04	0.91	1.67e-04	197.09	3.61e-02	0.0	0.0
198	62.130	0.016	0.037	173.22	3.17e-02	20.82	3.81e-03	163.81	3.00e-02	0.0	0.0
199	62.430	0.016	0.037	9.38	1.72e-03	1.95	3.58e-04	113.95	2.09e-02	0.0	0.0
200	62.522	0.016	0.037	48.33	8.85e-03	6.02	1.10e-03	99.11	1.81e-02	0.0	0.0
201	62.709	0.016	0.037	32.77	6.00e-03	0.05	8.53e-06	455.68	8.35e-02	0.0	0.0
202	62.820	0.016	0.037	53.36	9.77e-03	16.29	2.98e-03	146.07	2.67e-02	0.0	0.0
203	62.960	0.016	0.037	11.41	2.09e-03	13.29	2.43e-03	2.40	4.40e-04	0.0	0.0
204	63.074	0.016	0.037	5.67	1.04e-03	41.30	7.56e-03	10.09	1.85e-03	0.0	0.0
205	63.138	0.016	0.037	111.69	2.05e-02	303.97	5.57e-02	163.62	3.00e-02	0.0	0.0
206	63.206	0.016	0.037	35.72	6.54e-03	118.47	2.17e-02	133.56	2.45e-02	0.0	0.0
207	63.491	0.016	0.037	2.56	4.70e-04	26.33	4.82e-03	219.98	4.03e-02	0.0	0.0
208	63.712	0.016	0.037	0.55	1.01e-04	156.66	2.87e-02	48.52	8.89e-03	0.0	0.0
209	63.993	0.016	0.037	46.35	8.49e-03	168.85	3.09e-02	361.75	6.62e-02	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
210	64.215	0.016	0.037	352.54	6.46e-02	817.07	0.1	292.94	5.36e-02	0.0	0.0
211	64.420	0.016	0.037	115.85	2.12e-02	46.71	8.55e-03	26.72	4.89e-03	0.0	0.0
212	64.480	0.016	0.037	38.07	6.97e-03	149.34	2.73e-02	1301.78	0.2	0.0	0.0
213	64.699	0.015	0.037	73.76	1.35e-02	316.69	5.80e-02	170.17	3.12e-02	0.0	0.0
214	64.791	0.015	0.037	0.03	4.92e-06	3.38	6.19e-04	8.03	1.47e-03	0.0	0.0
215	64.980	0.015	0.037	127.39	2.33e-02	21.69	3.97e-03	48.32	8.85e-03	0.0	0.0
216	65.200	0.015	0.037	34.45	6.31e-03	19.40	3.55e-03	1008.32	0.2	0.0	0.0
217	65.492	0.015	0.037	194.30	3.56e-02	9.87	1.81e-03	106.67	1.95e-02	0.0	0.0
218	65.700	0.015	0.037	0.22	4.09e-05	319.03	5.84e-02	1333.22	0.2	0.0	0.0
219	65.924	0.015	0.037	4.94	9.05e-04	226.38	4.15e-02	87.40	1.60e-02	0.0	0.0
220	66.340	0.015	0.037	490.58	8.98e-02	98.83	1.81e-02	15.38	2.82e-03	0.0	0.0
Risulta				5.232e+05		5.288e+05		4.763e+05			
In percentuale				95.82		96.84		87.23			

Cmb	Pilas. 1000 etaT/h	etaT cm	inter. h cm	Pilas. 1000 etaT/h	etaT cm	inter. h cm	Pilas. 1000 etaT/h	etaT cm	inter. h cm
43	295	0.052.46e-03	50.6	296	0.083.94e-03	50.6	297	0.062.86e-03	50.6
	298	0.168.09e-03	50.6	338	0.052.67e-03	50.6	339	0.052.45e-03	50.6
	340	0.042.05e-03	50.6	341	0.031.61e-03	50.6	342	0.031.60e-03	50.6
	343	0.09 0.03	290.0	344	0.013.82e-03	290.0			
44	295	0.042.17e-03	50.6	296	0.094.50e-03	50.6	297	0.126.23e-03	50.6
	298	0.168.27e-03	50.6	338	0.031.77e-03	50.6	339	0.031.65e-03	50.6
	340	0.031.51e-03	50.6	341	0.031.56e-03	50.6	342	0.042.09e-03	50.6
	343	0.08 0.02	290.0	344	0.037.45e-03	290.0			
45	295	0.031.49e-03	50.6	296	0.031.44e-03	50.6	297	0.084.16e-03	50.6
	298	0.157.43e-03	50.6	338	0.157.53e-03	50.6	339	0.147.11e-03	50.6
	340	0.126.28e-03	50.6	341	0.105.04e-03	50.6	342	0.073.42e-03	50.6
	343	0.06 0.02	290.0	344	0.12 0.04	290.0			
46	295	0.028.60e-04	50.6	296	0.041.89e-03	50.6	297	0.094.51e-03	50.6
	298	0.157.57e-03	50.6	338	0.136.37e-03	50.6	339	0.125.97e-03	50.6
	340	0.105.20e-03	50.6	341	0.084.05e-03	50.6	342	0.052.55e-03	50.6
	343	0.012.90e-03	290.0	344	0.08 0.02	290.0			
47	295	0.052.55e-03	50.6	296	0.083.98e-03	50.6	297	0.052.42e-03	50.6
	298	0.168.12e-03	50.6	338	0.062.91e-03	50.6	339	0.052.70e-03	50.6
	340	0.052.31e-03	50.6	341	0.041.87e-03	50.6	342	0.041.80e-03	50.6
	343	0.10 0.03	290.0	344	0.013.60e-03	290.0			
48	295	0.041.85e-03	50.6	296	0.094.48e-03	50.6	297	0.126.21e-03	50.6
	298	0.168.24e-03	50.6	338	0.031.49e-03	50.6	339	0.031.38e-03	50.6
	340	0.021.24e-03	50.6	341	0.031.37e-03	50.6	342	0.041.99e-03	50.6
	343	0.08 0.02	290.0	344	0.038.60e-03	290.0			
49	295	0.031.46e-03	50.6	296	0.031.27e-03	50.6	297	0.084.08e-03	50.6
	298	0.157.39e-03	50.6	338	0.157.65e-03	50.6	339	0.147.23e-03	50.6
	340	0.136.38e-03	50.6	341	0.105.13e-03	50.6	342	0.073.48e-03	50.6
	343	0.07 0.02	290.0	344	0.13 0.04	290.0			
50	295	0.021.00e-03	50.6	296	0.042.04e-03	50.6	297	0.094.58e-03	50.6
	298	0.157.61e-03	50.6	338	0.126.26e-03	50.6	339	0.125.87e-03	50.6
	340	0.105.11e-03	50.6	341	0.083.98e-03	50.6	342	0.052.52e-03	50.6
	343	0.025.17e-03	290.0	344	0.07 0.02	290.0			
51	295	0.052.42e-03	50.6	296	0.083.84e-03	50.6	297	0.083.93e-03	50.6
	298	0.168.06e-03	50.6	338	0.063.12e-03	50.6	339	0.062.90e-03	50.6
	340	0.052.47e-03	50.6	341	0.041.96e-03	50.6	342	0.031.76e-03	50.6
	343	0.11 0.03	290.0	344	0.025.20e-03	290.0			
52	295	0.063.02e-03	50.6	296	0.052.49e-03	50.6	297	0.126.15e-03	50.6
	298	0.168.24e-03	50.6	338	0.042.20e-03	50.6	339	0.042.06e-03	50.6
	340	0.041.85e-03	50.6	341	0.031.75e-03	50.6	342	0.042.10e-03	50.6
	343	0.09 0.03	290.0	344	0.026.16e-03	290.0			
53	295	0.031.41e-03	50.6	296	0.031.72e-03	50.6	297	0.094.35e-03	50.6
	298	0.157.54e-03	50.6	338	0.147.18e-03	50.6	339	0.136.76e-03	50.6
	340	0.125.95e-03	50.6	341	0.094.75e-03	50.6	342	0.063.18e-03	50.6
	343	0.05 0.01	290.0	344	0.12 0.03	290.0			
54	295	0.029.21e-04	50.6	296	0.042.16e-03	50.6	297	0.094.69e-03	50.6
	298	0.157.67e-03	50.6	338	0.126.01e-03	50.6	339	0.115.63e-03	50.6
	340	0.104.88e-03	50.6	341	0.073.76e-03	50.6	342	0.052.33e-03	50.6
	343	0.038.03e-03	290.0	344	0.07 0.02	290.0			
55	295	0.052.54e-03	50.6	296	0.083.90e-03	50.6	297	0.115.68e-03	50.6
	298	0.168.10e-03	50.6	338	0.073.36e-03	50.6	339	0.063.14e-03	50.6
	340	0.052.73e-03	50.6	341	0.042.22e-03	50.6	342	0.041.98e-03	50.6
	343	0.12 0.04	290.0	344	0.037.55e-03	290.0			
56	295	0.062.95e-03	50.6	296	0.073.41e-03	50.6	297	0.126.12e-03	50.6
	298	0.168.21e-03	50.6	338	0.041.93e-03	50.6	339	0.041.79e-03	50.6

	340	0.031.58e-03	50.6	341	0.031.52e-03	50.6	342	0.041.96e-03	50.6
	343	0.08 0.02	290.0	344	0.037.29e-03	290.0			
57	295	0.031.33e-03	50.6	296	0.031.55e-03	50.6	297	0.084.26e-03	50.6
	298	0.157.49e-03	50.6	338	0.147.29e-03	50.6	339	0.146.87e-03	50.6
	340	0.126.05e-03	50.6	341	0.104.82e-03	50.6	342	0.063.22e-03	50.6
	343	0.06 0.02	290.0	344	0.12 0.04	290.0			
58	295	0.021.12e-03	50.6	296	0.052.32e-03	50.6	297	0.094.77e-03	50.6
	298	0.157.72e-03	50.6	338	0.125.92e-03	50.6	339	0.115.54e-03	50.6
	340	0.094.80e-03	50.6	341	0.073.71e-03	50.6	342	0.052.33e-03	50.6
	343	0.04 0.01	290.0	344	0.07 0.02	290.0			
59	295	0.016.70e-04	50.6	296	0.042.18e-03	50.6	297	0.094.66e-03	50.6
	298	0.157.56e-03	50.6	338	0.115.54e-03	50.6	339	0.105.18e-03	50.6
	340	0.094.46e-03	50.6	341	0.073.39e-03	50.6	342	0.042.00e-03	50.6
	343	0.14 0.04	290.0	344	0.11 0.03	290.0			
60	295	0.052.55e-03	50.6	296	0.052.39e-03	50.6	297	0.125.96e-03	50.6
	298	0.168.13e-03	50.6	338	0.031.75e-03	50.6	339	0.031.53e-03	50.6
	340	0.021.13e-03	50.6	341	0.028.46e-04	50.6	342	0.031.38e-03	50.6
	343	0.09 0.03	290.0	344	0.04 0.01	290.0			
61	295	0.021.04e-03	50.6	296	0.031.36e-03	50.6	297	0.084.16e-03	50.6
	298	0.157.37e-03	50.6	338	0.147.06e-03	50.6	339	0.136.65e-03	50.6
	340	0.125.84e-03	50.6	341	0.094.64e-03	50.6	342	0.063.03e-03	50.6
	343	0.08 0.02	290.0	344	0.14 0.04	290.0			
62	295	0.031.44e-03	50.6	296	0.063.27e-03	50.6	297	0.104.93e-03	50.6
	298	0.167.90e-03	50.6	338	0.063.16e-03	50.6	339	0.062.85e-03	50.6
	340	0.042.25e-03	50.6	341	0.031.34e-03	50.6	342	5.10e-032.58e-04	50.6
	343	0.08 0.02	290.0	344	0.013.62e-03	290.0			
63	295	0.017.47e-04	50.6	296	0.042.14e-03	50.6	297	0.094.63e-03	50.6
	298	0.157.54e-03	50.6	338	0.115.66e-03	50.6	339	0.105.30e-03	50.6
	340	0.094.58e-03	50.6	341	0.073.51e-03	50.6	342	0.042.11e-03	50.6
	343	0.15 0.04	290.0	344	0.10 0.03	290.0			
64	295	0.052.51e-03	50.6	296	0.031.57e-03	50.6	297	0.125.93e-03	50.6
	298	0.168.11e-03	50.6	338	0.041.88e-03	50.6	339	0.031.66e-03	50.6
	340	0.021.26e-03	50.6	341	0.029.22e-04	50.6	342	0.031.36e-03	50.6
	343	0.09 0.02	290.0	344	0.04 0.01	290.0			
65	295	0.029.63e-04	50.6	296	0.031.43e-03	50.6	297	0.084.21e-03	50.6
	298	0.157.40e-03	50.6	338	0.146.95e-03	50.6	339	0.136.54e-03	50.6
	340	0.115.74e-03	50.6	341	0.094.54e-03	50.6	342	0.062.95e-03	50.6
	343	0.07 0.02	290.0	344	0.14 0.04	290.0			
66	295	0.031.51e-03	50.6	296	0.063.28e-03	50.6	297	0.073.46e-03	50.6
	298	0.167.92e-03	50.6	338	0.063.05e-03	50.6	339	0.052.74e-03	50.6
	340	0.042.13e-03	50.6	341	0.021.23e-03	50.6	342	3.35e-031.70e-04	50.6
	343	0.08 0.02	290.0	344	0.013.97e-03	290.0			
67	295	0.031.46e-03	50.6	296	0.052.34e-03	50.6	297	0.094.69e-03	50.6
	298	0.157.60e-03	50.6	338	0.126.13e-03	50.6	339	0.115.76e-03	50.6
	340	0.105.04e-03	50.6	341	0.083.98e-03	50.6	342	0.052.64e-03	50.6
	343	0.18 0.05	290.0	344	0.12 0.03	290.0			
68	295	0.021.22e-03	50.6	296	0.084.18e-03	50.6	297	0.126.00e-03	50.6
	298	0.168.11e-03	50.6	338	0.021.16e-03	50.6	339	0.029.03e-04	50.6
	340	7.81e-033.95e-04	50.6	341	7.22e-033.65e-04	50.6	342	0.031.38e-03	50.6
	343	0.12 0.04	290.0	344	0.06 0.02	290.0			
69	295	0.031.49e-03	50.6	296	0.031.33e-03	50.6	297	0.084.08e-03	50.6
	298	0.157.34e-03	50.6	338	0.157.56e-03	50.6	339	0.147.14e-03	50.6
	340	0.126.31e-03	50.6	341	0.105.08e-03	50.6	342	0.073.44e-03	50.6
	343	0.10 0.03	290.0	344	0.15 0.04	290.0			
70	295	0.031.76e-03	50.6	296	0.073.49e-03	50.6	297	0.031.59e-03	50.6
	298	0.167.95e-03	50.6	338	0.062.80e-03	50.6	339	0.052.50e-03	50.6
	340	0.041.93e-03	50.6	341	0.021.11e-03	50.6	342	0.015.78e-04	50.6
	343	0.10 0.03	290.0	344	0.037.90e-03	290.0			
71	295	0.031.54e-03	50.6	296	0.052.33e-03	50.6	297	0.094.67e-03	50.6
	298	0.157.59e-03	50.6	338	0.126.25e-03	50.6	339	0.125.89e-03	50.6
	340	0.105.17e-03	50.6	341	0.084.10e-03	50.6	342	0.052.75e-03	50.6
	343	0.18 0.05	290.0	344	0.12 0.03	290.0			
72	295	0.015.48e-04	50.6	296	0.084.13e-03	50.6	297	0.125.96e-03	50.6
	298	0.168.09e-03	50.6	338	0.031.27e-03	50.6	339	0.021.01e-03	50.6
	340	1.00e-025.05e-04	50.6	341	5.74e-032.90e-04	50.6	342	0.021.25e-03	50.6
	343	0.12 0.03	290.0	344	0.05 0.02	290.0			
73	295	0.031.39e-03	50.6	296	0.031.36e-03	50.6	297	0.084.11e-03	50.6
	298	0.157.36e-03	50.6	338	0.157.44e-03	50.6	339	0.147.02e-03	50.6
	340	0.126.20e-03	50.6	341	0.104.97e-03	50.6	342	0.073.34e-03	50.6
	343	0.09 0.03	290.0	344	0.15 0.04	290.0			
74	295	0.041.85e-03	50.6	296	0.073.56e-03	50.6	297	0.063.07e-03	50.6
	298	0.167.98e-03	50.6	338	0.052.71e-03	50.6	339	0.052.41e-03	50.6
	340	0.041.85e-03	50.6	341	0.021.06e-03	50.6	342	0.016.77e-04	50.6
	343	0.11 0.03	290.0	344	0.038.27e-03	290.0			

Cmb

1000 etaT/h
0.18

VERIFICHE ELEMENTI MURATURA

LEGENDA TABELLA VERIFICHE ELEMENTI MURATURA

In tabella vengono riportati per ogni elemento il numero dello stesso ed il codice di verifica.

Le verifiche sono state condotte secondo il DM.LL.PP. 20 Novembre 1987.

In particolare sono previste le seguenti verifiche:

- 2.2.1 Muri soggetti a carichi verticali
- 2.4.1 Verifiche di sicurezza con il metodo delle tensioni ammissibili
 - 2.4.1.1 Verifica dei muri soggetti a carichi verticali
 - 2.4.1.2 Verifica dei muri soggetti a forze orizzontali agenti nel piano del muro
 - 2.4.1.2.1 Verifica a pressoflessione
 - 2.4.1.2.2 Verifica a taglio
- 2.4.2 Verifiche di sicurezza con il metodo semiprobabilistico agli stati limite
 - 2.4.2.2 Verifica dei muri soggetti a carichi verticali
 - 2.4.2.3 Verifica dei muri soggetti a forze orizzontali agenti nel piano del muro
 - 2.4.2.3.1 Verifica a pressoflessione
 - 2.4.2.3.2 Verifica a taglio

Con riferimento ai punti succitati le verifiche vengono così tabellate:

Setto/Fascia/Elem.	numero del macroelemento (D3) o elemento (D2) considerato	
Mat.	Materiale	
s=,m=	Indice della sezione e del materiale assegnati all' elemento (per D2)	
Spessore	spessore dell'elemento	
Stato	ok T	elemento verificato (tensioni ammissibili)
	ok L	elemento verificato (stati limite ultimi)
	NV T	elemento non verificato (tensioni ammissibili)
	NV L	elemento non verificato (stati limite ultimi)

Nodo/Pos.	numero del nodo appartenente al setto / posizione relativa al nodo I per D2		
h0/t	valore della snellezza		
Ecc/t (M)	massimo valore del rapporto e1/t o e2/t		
6 Eb/B (M)	massimo valore dell'eccentricità Eb dei carichi verticali misurata nel piano mediano amplificata del fattore 6/B		
Fi	fattore fi per la riduzione della resistenza in funzione di h0 ed EccM; utilizzato nella verifica V.N-Mo		
Fi t	fattore fi per la riduzione della resistenza in funzione di e2 e h0; utilizzato nella verifica V.N-Mp		
Fi b	fattore fi per la riduzione della resistenza in funzione di 6Eb/B; utilizzato nella verifica V.N-Mp		
Beta	fattore di parzializzazione della sezione per la verifica a taglio		
V.N-Mo	rapporto tra la tensione (sforzo normale) e la tensione ammissibile (sforzo normale ultimo) in relazione alla verifica 2.4.1.1. (2.4.2.2)		
V.N-Mp	rapporto tra la tensione (sforzo normale) e la tensione ammissibile (sforzo normale ultimo) in relazione alla verifica 2.4.1.2.1 (2.4.2.3.1)		
Ver. V	rapporto tra la tensione tangenziale (sforzo tagliante) e la tensione tangenziale ammissibile (sforzo tagliante ultimo) in relazione alla verifica 2.4.1.2.2 (2.4.2.3.2)		
Rif. cmb	Combinazioni in cui si hanno i massimi valori dei rapporti V. N-Mo	V. N-Mp	Ver. V

Affinché l'elemento sia verificato deve essere:

h0/t	non superiore a 20
Ecc/t (M)	non superiore a 0.33
6 Eb/B (M)	non superiore a 1.33 con il metodo delle tensioni ammissibili
6 Eb/B (M)	non superiore a 2.00 con il metodo agli stati limite
V.N-Mo, V.N-Mp, Ver. V	non superiore a 1

Le verifiche sismiche condotte secondo le norme tecniche allegate all' ordinanza PCM 3274 prevedono gli ulteriori controlli:

- 8.2.2.1 Pressoflessione nel piano
- 8.2.2.2 Taglio (edifici nuovi)
- 11.5.8.1 Taglio (edifici esistenti)
- 8.2.2.3 Pressoflessione fuori piano

Con riferimento ai punti succitati le verifiche vengono così tabellate:

Nodo/Pos.	numero del nodo appartenente al setto / posizione relativa al nodo I per D2		
P / A	tensione verticale media (in uso nella verifica 8.2.2.1 e 11.5.8.1)		
P / Ac	tensione verticale media nella parte compressa (in uso nella verifica 8.2.2.2)		
P / A .3	tensione verticale corrispondente allo sforzo normale unitario da equilibrare con 0.85 fd (in uso nella verifica 8.2.2.3)		
Mu	valore del momento corrispondente al collasso per pressoflessione (in uso nella verifica 8.2.2.1)		
lc	dimensione della parte compressa della parete (in uso nella verifica 8.2.2.2)		
b (h/l)	rapporto dimensionale (altezza/base) (in uso nella verifica 11.5.8.1)		
tc	dimensione (al massimo pari allo spessore) reagente (in uso nella verifica 8.2.2.3)		
V. 8.2.2.1	massimo valore del rapporto tra il momento di progetto ed il momento ultimo calcolato in presenza dello sforzo normale di progetto		
V. 8.2.2.2	massimo valore del rapporto tra la forza orizzontale di progetto e la forza orizzontale Vt corrispondente al collasso per taglio (edifici nuovi)		

V. 11.5.8.1	massimo valore del rapporto tra la forza orizzontale di progetto e la forza orizzontale V_t corrispondente al collasso per taglio (edifici esistenti)
V. 8.2.2.3	massimo valore del rapporto tra il momento di progetto ed il momento ultimo calcolato in presenza dello sforzo normale di progetto
Rif. cmb	Combinazioni in cui si hanno i massimi valori dei rapporti V. 8.2.2.1, V. 8.2.2.2, V. 8.2.2.3

Affinché l'elemento sia verificato deve essere:

h_0/t	non superiore a 12 (10)
V.8.2.2.1(2,3) V.11.5.8.1	non superiore a 1

Le verifiche condotte per gli elementi trave in muratura sono così tabellate:

Ver. V	rapporto tra il taglio di progetto e il minore dei tagli resistenti V_p e V_t in relazione alla verifica 5.4.6.2.5
Ver. M	rapporto tra il momento di progetto e il momento ultimo M_u in relazione alla verifica 5.4.6.2.5
V_t	taglio resistente, funzione della resistenza della muratura al taglio in assenza di compressione
V_p	taglio resistente in funzione del momento resistente M_u
M_u	momento resistente, funzione della resistenza della muratura alla compressione in direzione orizzontale

Elem. cmb	Note	Pos.	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l) cm	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif.
343	ok L	0.0	1.78	1.78	1.78	5.288e+04	40.00	2.80	0.23	0.02	0.41	39,39,39
	s=14,m=34	290.0	1.25	1.25	1.24	3.816e+04	40.00	1.95	1.69e-03	0.02	7.91e-04	39,39,39
344	ok L	0.0	1.65	1.65	1.59	7.736e+04	50.00	2.49	0.12	0.01	0.06	37,37,37
	s=15,m=34	290.0	1.13	1.13	1.14	5.401e+04	50.00	1.78	3.47e-04	0.01	7.89e-04	29,37,29
Elem.			P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
						3.816e+04	40.00	1.78				
			1.78	1.78	1.78	7.736e+04	50.00	2.80	0.23	0.02	0.41	

Setto	Mat.	Spessore	Stato
		cm	
2	mattoni pieni e malta di calce	8.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
13	0.82	0.82	0.83	1.559e+05	220.98	0.26	0.12	0.05	0.0	36,36,39
14	0.86	0.86	0.86	4.231e+04	112.95	0.27	0.05	0.13	0.0	36,36,39
672	0.83	0.86	0.87	1.710e+05	142.41	0.27	0.12	0.13	0.0	36,36,39
673	0.83	0.83	0.83	1.710e+05	230.80	0.26	0.12	0.05	0.0	36,36,39
674	0.87	0.86	0.87	9.878e+04	142.41	0.27	0.04	0.13	0.0	36,36,39
675	0.82	0.87	0.85	1.981e+05	171.88	0.27	0.13	0.12	0.0	36,36,39
676	0.82	0.83	0.82	1.981e+05	240.63	0.26	0.13	0.04	0.0	36,36,39
677	0.85	0.87	0.85	1.338e+05	171.88	0.27	0.08	0.12	0.0	36,36,39
678	0.81	0.82	0.81	1.403e+05	220.98	0.25	0.12	0.05	0.0	36,36,39
686	0.82	0.85	0.85	1.981e+05	201.34	0.27	0.13	0.11	0.0	36,36,39
687	0.82	0.82	0.82	1.981e+05	250.45	0.26	0.13	0.03	0.0	36,36,39
688	0.86	0.86	0.84	4.231e+04	112.95	0.26	0.05	0.13	0.0	36,36,39
691	0.85	0.85	0.85	1.745e+05	201.34	0.27	0.08	0.11	0.0	36,36,39
692	0.82	0.85	0.85	2.161e+05	230.80	0.27	0.11	0.08	0.0	36,36,39
697	0.82	0.86	0.86	1.559e+05	112.95	0.27	0.12	0.13	0.0	36,36,39
1286	0.82	0.82	0.82	2.161e+05	260.27	0.26	0.11	0.02	0.0	36,36,39
1287	0.83	0.85	0.85	2.104e+05	230.80	0.27	0.10	0.08	0.0	36,36,39
1406	0.81	0.81	0.81	1.403e+05	211.16	0.25	0.12	0.04	0.0	36,36,39
1415	0.81	0.84	0.84	1.403e+05	111.31	0.26	0.12	0.13	0.0	36,36,39
1416	0.81	0.86	0.84	1.403e+05	112.95	0.26	0.12	0.13	0.0	36,36,39
1952	0.83	0.83	0.83	2.315e+05	255.36	0.26	0.11	0.03	0.0	36,36,39
1953	0.84	0.84	0.84	4.021e+04	111.31	0.26	0.02	0.13	0.0	36,36,39
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				4.021e+04	111.31	0.25				
	0.87	0.87	0.87	2.315e+05	260.27	0.27	0.13	0.13	0.0	

Setto	Mat.	Spessore	Stato
		cm	
3	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
1459	1.57	1.60	1.65	2.262e+05	87.50	2.58	0.21	0.27	0.08	17,22,27
1492	1.57	1.60	1.65	2.262e+05	87.50	2.58	0.21	0.27	0.08	17,22,27
1576	1.57	1.60	1.65	2.262e+05	87.50	2.58	0.21	0.27	0.08	17,22,27
1913	1.39	1.60	1.65	2.018e+05	87.50	2.58	0.34	0.27	0.08	29,22,27
1914	1.29	1.35	1.36	1.878e+05	87.22	2.14	0.36	0.41	0.12	27,11,30
1915	1.29	1.36	1.36	1.878e+05	87.50	2.14	0.36	0.53	0.12	27,11,30
1916	1.31	1.36	1.38	1.908e+05	87.50	2.17	0.24	0.53	0.11	31,11,28
1917	1.55	1.47	1.44	2.235e+05	87.50	2.26	0.08	0.50	0.05	12,11,34
1918	1.64	1.56	1.61	2.346e+05	87.50	2.53	0.22	0.49	0.08	15,11,27
1919	1.58	1.64	1.55	2.266e+05	87.50	2.43	0.31	0.48	0.13	15,11,27
1920	1.29	1.58	1.55	1.882e+05	87.50	2.43	0.33	0.41	0.13	15,11,27
1921	1.29	1.27	1.26	1.882e+05	87.50	1.97	0.33	0.21	0.12	15,31,35
1922	1.39	1.60	1.65	2.018e+05	87.50	2.58	0.34	0.27	0.08	29,22,27
1923	1.29	1.35	1.36	1.878e+05	87.22	2.14	0.36	0.41	0.12	27,11,30
1924	1.29	1.36	1.36	1.878e+05	87.50	2.14	0.36	0.53	0.12	27,11,30
1925	1.31	1.36	1.38	1.908e+05	87.50	2.17	0.24	0.53	0.11	31,11,28
1926	1.55	1.47	1.44	2.235e+05	87.50	2.26	0.08	0.50	0.05	12,11,34
1927	1.64	1.56	1.61	2.346e+05	87.50	2.53	0.22	0.49	0.08	15,11,27
1928	1.58	1.64	1.55	2.266e+05	87.50	2.43	0.31	0.48	0.13	15,11,27
1929	1.29	1.58	1.55	1.882e+05	87.50	2.43	0.33	0.41	0.13	15,11,27
1930	1.29	1.27	1.26	1.882e+05	87.50	1.97	0.33	0.21	0.12	15,31,35
1931	1.39	1.60	1.65	2.018e+05	87.50	2.58	0.34	0.27	0.08	29,22,27
1932	1.29	1.35	1.36	1.878e+05	87.22	2.14	0.36	0.41	0.12	27,11,30
1933	1.29	1.36	1.36	1.878e+05	87.50	2.14	0.36	0.53	0.12	27,11,30
1934	1.31	1.36	1.38	1.908e+05	87.50	2.17	0.24	0.53	0.11	31,11,28
1935	1.55	1.47	1.44	2.235e+05	87.50	2.26	0.08	0.50	0.05	12,11,34
1936	1.64	1.56	1.61	2.346e+05	87.50	2.53	0.22	0.49	0.08	15,11,27
1937	1.58	1.64	1.55	2.266e+05	87.50	2.43	0.31	0.48	0.13	15,11,27
1938	1.29	1.58	1.55	1.882e+05	87.50	2.43	0.33	0.41	0.13	15,11,27
1939	1.29	1.27	1.26	1.882e+05	87.50	1.97	0.33	0.21	0.12	15,31,35

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				1.878e+05	87.22	1.97			
	1.64	1.64	1.65	2.346e+05	87.50	2.58	0.36	0.53	0.13

Setto	Mat.	Spessore	Stato
		cm	
6	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
36	2.75	2.59	2.86	1.389e+07	536.00	4.97	0.06	0.08	0.02	37,16,14
37	2.75	2.59	2.86	1.389e+07	536.00	4.97	0.06	0.08	0.02	37,16,14
77	2.75	2.59	2.86	1.389e+07	536.00	4.97	0.06	0.08	0.02	37,16,14
84	2.75	2.59	2.86	1.389e+07	536.00	4.97	0.06	0.08	0.02	37,16,14
91	2.75	2.59	2.86	1.389e+07	536.00	4.97	0.06	0.08	0.02	37,16,14
98	2.75	2.59	2.86	1.389e+07	536.00	4.97	0.06	0.08	0.02	37,16,14
105	2.75	2.59	2.86	1.389e+07	536.00	4.97	0.06	0.08	0.02	37,16,14
112	2.75	2.59	2.86	1.389e+07	536.00	4.97	0.06	0.08	0.02	37,16,14
119	2.75	2.59	2.86	1.389e+07	536.00	4.97	0.06	0.08	0.02	37,16,14
126	2.75	2.59	2.86	1.389e+07	536.00	4.97	0.06	0.08	0.02	37,16,14
133	2.75	2.59	2.86	1.389e+07	536.00	4.97	0.06	0.08	0.02	37,16,14
1103	2.72	2.59	2.56	1.379e+07	536.00	4.45	0.07	0.08	0.04	37,16,11
1105	2.61	2.57	2.56	1.328e+07	536.00	4.45	0.10	0.08	0.04	37,16,11
1107	2.50	2.38	2.46	1.282e+07	536.00	4.27	0.11	0.08	0.03	37,16,11
1109	2.50	2.31	2.39	1.282e+07	536.00	4.16	0.11	0.09	0.03	37,16,40
1111	2.41	2.19	2.39	1.242e+07	536.00	4.16	0.10	0.09	0.03	37,16,40
1113	2.26	2.13	2.33	1.170e+07	455.60	4.06	0.10	0.10	0.02	37,16,14
1115	2.21	2.13	2.13	8.305e+06	455.60	3.69	0.10	0.10	0.01	37,16,11
1169	2.66	2.59	2.51	1.351e+07	536.00	4.36	0.08	0.08	0.03	37,16,11
1170	2.66	2.59	2.51	1.351e+07	536.00	4.36	0.08	0.08	0.03	37,16,11
1171	2.54	2.52	2.51	1.300e+07	536.00	4.36	0.10	0.07	0.03	37,16,11
1172	2.54	2.52	2.51	1.300e+07	536.00	4.36	0.10	0.07	0.03	37,16,11
1173	2.50	2.38	2.42	1.282e+07	536.00	4.20	0.11	0.08	0.01	37,16,16
1174	2.50	2.38	2.42	1.282e+07	536.00	4.20	0.11	0.08	0.01	37,16,16
1175	2.50	2.31	2.39	1.282e+07	536.00	4.16	0.11	0.09	0.03	37,16,40
1176	2.50	2.31	2.39	1.282e+07	536.00	4.16	0.11	0.09	0.03	37,16,40

1177	2.41	2.19	2.39	1.242e+07	536.00	4.16	0.10	0.09	0.03	37,16,40
1178	2.41	2.19	2.39	1.242e+07	536.00	4.16	0.10	0.09	0.03	37,16,40
1179	2.26	2.19	2.33	1.170e+07	536.00	4.06	0.10	0.09	0.02	37,16,14
1180	2.26	2.19	2.33	1.170e+07	536.00	4.06	0.10	0.09	0.02	37,16,14
1187	2.66	2.59	2.54	1.351e+07	536.00	4.41	0.08	0.08	0.03	37,16,11
1188	2.54	2.55	2.54	1.300e+07	536.00	4.41	0.10	0.07	0.03	37,16,11
1189	2.50	2.38	2.44	1.282e+07	536.00	4.24	0.11	0.08	0.02	37,16,16
1190	2.50	2.31	2.39	1.282e+07	536.00	4.16	0.11	0.09	0.03	37,16,40
1191	2.41	2.19	2.39	1.242e+07	536.00	4.16	0.10	0.09	0.03	37,16,40
1192	2.26	2.19	2.33	1.170e+07	536.00	4.06	0.10	0.09	0.02	37,16,14
1196	2.69	2.59	2.56	1.365e+07	536.00	4.45	0.07	0.08	0.04	37,16,11
1197	2.57	2.57	2.56	1.314e+07	536.00	4.45	0.10	0.08	0.04	37,16,11
1198	2.50	2.38	2.46	1.282e+07	536.00	4.27	0.11	0.08	0.03	37,16,11
1199	2.50	2.31	2.39	1.282e+07	536.00	4.16	0.11	0.09	0.03	37,16,40
1200	2.41	2.19	2.39	1.242e+07	536.00	4.16	0.10	0.09	0.03	37,16,40
1201	2.26	2.13	2.33	1.170e+07	455.60	4.06	0.10	0.10	0.02	37,16,14
1202	2.21	2.13	2.13	8.305e+06	455.60	3.69	0.10	0.10	0.01	37,16,11
1205	2.72	2.59	2.56	1.379e+07	536.00	4.45	0.07	0.08	0.04	37,16,11
1206	2.61	2.57	2.56	1.328e+07	536.00	4.45	0.10	0.08	0.04	37,16,11
1207	2.50	2.38	2.46	1.282e+07	536.00	4.27	0.11	0.08	0.03	37,16,11
1208	2.50	2.31	2.39	1.282e+07	536.00	4.16	0.11	0.09	0.03	37,16,40
1209	2.41	2.19	2.39	1.242e+07	536.00	4.16	0.10	0.09	0.03	37,16,40
1210	2.26	2.13	2.33	1.170e+07	455.60	4.06	0.10	0.10	0.02	37,16,14
1211	2.21	2.13	2.13	8.305e+06	455.60	3.69	0.10	0.10	0.01	37,16,11
1214	2.72	2.59	2.56	1.379e+07	536.00	4.45	0.07	0.08	0.04	37,16,11
1215	2.61	2.57	2.56	1.328e+07	536.00	4.45	0.10	0.08	0.04	37,16,11
1216	2.50	2.38	2.46	1.282e+07	536.00	4.27	0.11	0.08	0.03	37,16,11
1217	2.50	2.31	2.39	1.282e+07	536.00	4.16	0.11	0.09	0.03	37,16,40
1218	2.41	2.19	2.39	1.242e+07	536.00	4.16	0.10	0.09	0.03	37,16,40
1219	2.26	2.13	2.33	1.170e+07	455.60	4.06	0.10	0.10	0.02	37,16,14
1220	2.21	2.13	2.13	8.305e+06	455.60	3.69	0.10	0.10	0.01	37,16,11
1223	2.72	2.59	2.56	1.379e+07	536.00	4.45	0.07	0.08	0.04	37,16,11
1224	2.61	2.57	2.56	1.328e+07	536.00	4.45	0.10	0.08	0.04	37,16,11
1225	2.50	2.38	2.46	1.282e+07	536.00	4.27	0.11	0.08	0.03	37,16,11
1226	2.50	2.31	2.39	1.282e+07	536.00	4.16	0.11	0.09	0.03	37,16,40
1227	2.41	2.19	2.39	1.242e+07	536.00	4.16	0.10	0.09	0.03	37,16,40
1228	2.26	2.13	2.33	1.170e+07	455.60	4.06	0.10	0.10	0.02	37,16,14
1229	2.21	2.13	2.13	8.305e+06	455.60	3.69	0.10	0.10	0.01	37,16,11
1232	2.72	2.59	2.56	1.379e+07	536.00	4.45	0.07	0.08	0.04	37,16,11
1233	2.61	2.57	2.56	1.328e+07	536.00	4.45	0.10	0.08	0.04	37,16,11
1234	2.50	2.38	2.46	1.282e+07	536.00	4.27	0.11	0.08	0.03	37,16,11
1235	2.50	2.31	2.39	1.282e+07	536.00	4.16	0.11	0.09	0.03	37,16,40
1236	2.41	2.19	2.39	1.242e+07	536.00	4.16	0.10	0.09	0.03	37,16,40
1237	2.26	2.13	2.33	1.170e+07	455.60	4.06	0.10	0.10	0.02	37,16,14
1238	2.21	2.13	2.13	8.305e+06	455.60	3.69	0.10	0.10	0.01	37,16,11
1241	2.72	2.59	2.56	1.379e+07	536.00	4.45	0.07	0.08	0.04	37,16,11
1242	2.61	2.57	2.56	1.328e+07	536.00	4.45	0.10	0.08	0.04	37,16,11
1243	2.50	2.38	2.46	1.282e+07	536.00	4.27	0.11	0.08	0.03	37,16,11
1244	2.50	2.31	2.39	1.282e+07	536.00	4.16	0.11	0.09	0.03	37,16,40
1245	2.41	2.19	2.39	1.242e+07	536.00	4.16	0.10	0.09	0.03	37,16,40
1246	2.26	2.13	2.33	1.170e+07	455.60	4.06	0.10	0.10	0.02	37,16,14
1247	2.21	2.13	2.13	8.305e+06	455.60	3.69	0.10	0.10	0.01	37,16,11
1250	2.72	2.59	2.56	1.379e+07	536.00	4.45	0.07	0.08	0.04	37,16,11
1251	2.61	2.57	2.56	1.328e+07	536.00	4.45	0.10	0.08	0.04	37,16,11
1252	2.50	2.38	2.46	1.282e+07	536.00	4.27	0.11	0.08	0.03	37,16,11
1253	2.50	2.31	2.39	1.282e+07	536.00	4.16	0.11	0.09	0.03	37,16,40
1254	2.41	2.19	2.39	1.242e+07	536.00	4.16	0.10	0.09	0.03	37,16,40
1255	2.26	2.13	2.33	1.170e+07	455.60	4.06	0.10	0.10	0.02	37,16,14
1256	2.21	2.13	2.13	8.305e+06	455.60	3.69	0.10	0.10	0.01	37,16,11
1941	2.72	2.59	2.56	1.379e+07	536.00	4.45	0.07	0.08	0.04	37,16,11
1942	2.75	2.59	2.86	1.389e+07	536.00	4.97	0.06	0.08	0.02	37,16,14
1943	2.61	2.57	2.56	1.328e+07	536.00	4.45	0.10	0.08	0.04	37,16,11
1944	2.50	2.38	2.46	1.282e+07	536.00	4.27	0.11	0.08	0.03	37,16,11
1945	2.50	2.31	2.39	1.282e+07	536.00	4.16	0.11	0.09	0.03	37,16,40
1946	2.41	2.19	2.39	1.242e+07	536.00	4.16	0.10	0.09	0.03	37,16,40
1947	2.26	2.13	2.33	1.170e+07	455.60	4.06	0.10	0.10	0.02	37,16,14
1948	2.21	2.13	2.13	8.305e+06	455.60	3.69	0.10	0.10	0.01	37,16,11

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
	2.75	2.59	2.86	8.305e+06	455.60	3.69			
				1.389e+07	536.00	4.97	0.11	0.10	0.04

Setto	Mat.	Spessore	Stato
		cm	
7	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
1115	2.02	1.95	1.95	7.649e+06	455.60	3.39	0.14	0.08	0.02	37,16,16
1117	2.02	1.95	1.95	7.649e+06	455.60	3.39	0.14	0.08	0.02	37,16,16
1119	1.87	1.83	1.87	9.888e+06	536.00	3.26	0.13	0.08	0.02	37,16,37
1181	1.93	1.88	1.88	1.017e+07	536.00	3.27	0.15	0.08	0.04	37,16,16
1182	1.93	1.88	1.88	1.017e+07	536.00	3.27	0.15	0.08	0.04	37,16,16
1183	1.93	1.88	1.88	1.017e+07	536.00	3.27	0.15	0.08	0.04	37,16,16
1184	1.93	1.88	1.88	1.017e+07	536.00	3.27	0.15	0.08	0.04	37,16,16
1185	1.87	1.83	1.87	9.888e+06	536.00	3.26	0.13	0.08	0.02	37,16,37
1186	1.87	1.83	1.87	9.888e+06	536.00	3.26	0.13	0.08	0.02	37,16,37
1193	1.93	1.91	1.88	1.017e+07	495.80	3.27	0.15	0.08	0.04	37,16,16
1194	1.93	1.91	1.88	1.017e+07	495.80	3.27	0.15	0.08	0.04	37,16,16
1195	1.87	1.83	1.87	9.888e+06	536.00	3.26	0.13	0.08	0.02	37,16,37
1202	1.97	1.95	1.91	8.867e+06	455.60	3.32	0.14	0.08	0.03	37,16,16
1203	1.97	1.95	1.91	8.867e+06	455.60	3.32	0.14	0.08	0.03	37,16,16
1204	1.87	1.83	1.87	9.888e+06	536.00	3.26	0.13	0.08	0.02	37,16,37
1211	2.02	1.95	1.95	7.649e+06	455.60	3.39	0.14	0.08	0.02	37,16,16
1212	2.02	1.95	1.95	7.649e+06	455.60	3.39	0.14	0.08	0.02	37,16,16
1213	1.87	1.83	1.87	9.888e+06	536.00	3.26	0.13	0.08	0.02	37,16,37
1220	2.02	1.95	1.95	7.649e+06	455.60	3.39	0.14	0.08	0.02	37,16,16
1221	2.02	1.95	1.95	7.649e+06	455.60	3.39	0.14	0.08	0.02	37,16,16
1222	1.87	1.83	1.87	9.888e+06	536.00	3.26	0.13	0.08	0.02	37,16,37
1229	2.02	1.95	1.95	7.649e+06	455.60	3.39	0.14	0.08	0.02	37,16,16
1230	2.02	1.95	1.95	7.649e+06	455.60	3.39	0.14	0.08	0.02	37,16,16
1231	1.87	1.83	1.87	9.888e+06	536.00	3.26	0.13	0.08	0.02	37,16,37
1238	2.02	1.95	1.95	7.649e+06	455.60	3.39	0.14	0.08	0.02	37,16,16
1239	2.02	1.95	1.95	7.649e+06	455.60	3.39	0.14	0.08	0.02	37,16,16
1240	1.87	1.83	1.87	9.888e+06	536.00	3.26	0.13	0.08	0.02	37,16,37
1247	2.02	1.95	1.95	7.649e+06	455.60	3.39	0.14	0.08	0.02	37,16,16
1248	2.02	1.95	1.95	7.649e+06	455.60	3.39	0.14	0.08	0.02	37,16,16
1249	1.87	1.83	1.87	9.888e+06	536.00	3.26	0.13	0.08	0.02	37,16,37
1256	2.02	1.95	1.95	7.649e+06	455.60	3.39	0.14	0.08	0.02	37,16,16
1257	2.02	1.95	1.95	7.649e+06	455.60	3.39	0.14	0.08	0.02	37,16,16
1258	1.87	1.83	1.87	9.888e+06	536.00	3.26	0.13	0.08	0.02	37,16,37
1948	2.02	1.95	1.95	7.649e+06	455.60	3.39	0.14	0.08	0.02	37,16,16
1949	2.02	1.95	1.95	7.649e+06	455.60	3.39	0.14	0.08	0.02	37,16,16
1950	1.87	1.83	1.87	9.888e+06	536.00	3.26	0.13	0.08	0.02	37,16,37
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	2.02	1.95	1.95	7.649e+06	455.60	3.26				
				1.017e+07	536.00	3.39	0.15	0.08	0.04	

Setto	Mat.	Spessore	Stato
		cm	
9	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
3067	0.25	0.24	0.24	5.071e+05	323.00	0.42	0.09	0.02	0.09	19,26,32
3070	0.25	0.24	0.24	5.071e+05	323.00	0.42	0.09	0.02	0.09	19,26,32
3073	0.25	0.24	0.24	5.071e+05	323.00	0.42	0.09	0.02	0.09	19,26,32
3076	0.25	0.24	0.24	5.071e+05	323.00	0.42	0.09	0.02	0.09	19,26,32
3079	0.25	0.24	0.24	5.071e+05	323.00	0.42	0.09	0.02	0.09	19,26,32
3082	0.25	0.24	0.24	5.071e+05	323.00	0.42	0.09	0.02	0.09	19,26,32
3085	0.25	0.24	0.24	5.071e+05	323.00	0.42	0.09	0.02	0.09	19,26,32
3088	0.25	0.24	0.24	5.071e+05	323.00	0.42	0.09	0.02	0.09	19,26,32
3243	0.25	0.24	0.24	5.071e+05	323.00	0.42	0.09	0.02	0.09	19,26,32
3244	0.22	0.21	0.22	4.539e+05	323.00	0.38	0.07	0.02	0.06	19,26,32
3245	0.10	0.16	0.10	2.004e+05	323.00	0.17	0.04	9.31e-03	0.09	14,22,42
3246	0.10	0.10	0.10	2.004e+05	323.00	0.17	0.04	6.00e-03	0.09	14,22,42
3247	0.25	0.24	0.24	5.071e+05	323.00	0.42	0.09	0.02	0.09	19,26,32
3248	0.22	0.21	0.22	4.539e+05	323.00	0.38	0.07	0.02	0.06	19,26,32
3249	0.10	0.16	0.10	2.004e+05	323.00	0.17	0.04	9.31e-03	0.09	14,22,42
3250	0.10	0.10	0.10	2.004e+05	323.00	0.17	0.04	6.00e-03	0.09	14,22,42
3251	0.25	0.24	0.24	5.071e+05	323.00	0.42	0.09	0.02	0.09	19,26,32
3252	0.22	0.21	0.22	4.539e+05	323.00	0.38	0.07	0.02	0.06	19,26,32

3253	0.10	0.16	0.10	2.004e+05	323.00	0.17	0.04	9.31e-03	0.09	14,22,42
3254	0.10	0.10	0.10	2.004e+05	323.00	0.17	0.04	6.00e-03	0.09	14,22,42
3300	0.25	0.24	0.24	5.071e+05	323.00	0.42	0.09	0.02	0.09	19,26,32
3301	0.25	0.24	0.24	5.071e+05	323.00	0.42	0.09	0.02	0.09	19,26,32
3302	0.22	0.21	0.22	4.539e+05	323.00	0.38	0.07	0.02	0.06	19,26,32
3303	0.22	0.21	0.22	4.539e+05	323.00	0.38	0.07	0.02	0.06	19,26,32
3304	0.10	0.16	0.10	2.004e+05	323.00	0.17	0.04	9.31e-03	0.09	14,22,42
3305	0.10	0.16	0.10	2.004e+05	323.00	0.17	0.04	9.31e-03	0.09	14,22,42
3306	0.10	0.10	0.10	2.004e+05	323.00	0.17	0.04	6.00e-03	0.09	14,22,42
3307	0.10	0.10	0.10	2.004e+05	323.00	0.17	0.04	6.00e-03	0.09	14,22,42
3308	0.25	0.24	0.24	5.071e+05	323.00	0.42	0.09	0.02	0.09	19,26,32
3309	0.22	0.21	0.22	4.539e+05	323.00	0.38	0.07	0.02	0.06	19,26,32
3310	0.10	0.16	0.10	2.004e+05	323.00	0.17	0.04	9.31e-03	0.09	14,22,42
3311	0.10	0.10	0.10	2.004e+05	323.00	0.17	0.04	6.00e-03	0.09	14,22,42
3312	0.25	0.24	0.24	5.071e+05	323.00	0.42	0.09	0.02	0.09	19,26,32
3313	0.22	0.21	0.22	4.539e+05	323.00	0.38	0.07	0.02	0.06	19,26,32
3314	0.10	0.16	0.10	2.004e+05	323.00	0.17	0.04	9.31e-03	0.09	14,22,42
3315	0.09	0.10	0.09	1.793e+05	323.00	0.15	0.04	6.00e-03	0.10	14,22,42
3316	0.25	0.24	0.24	5.071e+05	323.00	0.42	0.09	0.02	0.09	19,26,32
3317	0.22	0.21	0.22	4.539e+05	323.00	0.38	0.07	0.02	0.06	19,26,32
3318	0.09	0.16	0.09	1.793e+05	323.00	0.15	0.04	9.31e-03	0.10	14,22,42
3319	0.10	0.10	0.10	2.004e+05	323.00	0.17	0.04	6.00e-03	0.09	14,22,42
3350	0.09	0.10	0.09	1.793e+05	323.00	0.15	0.04	6.00e-03	0.10	14,22,42

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				1.793e+05	323.00	0.15			
	0.25	0.24	0.24	5.071e+05	323.00	0.42	0.09	0.02	0.10

Setto	Mat.	Spessore	Stato
		cm	
10	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1459	2.97	2.96	2.80	4.020e+05	87.50	4.38	0.13	0.21	0.04	11,15,33
1481	3.27	3.26	2.97	4.366e+05	87.50	4.66	0.23	0.31	0.02	11,15,14
1491	3.27	3.26	2.80	4.366e+05	87.50	4.38	0.23	0.31	0.04	11,15,33
1492	2.97	2.96	2.80	4.020e+05	87.50	4.38	0.13	0.21	0.04	11,15,33
1574	3.27	3.26	2.97	4.366e+05	87.50	4.66	0.23	0.31	0.02	11,15,14
1575	3.27	3.26	2.80	4.366e+05	87.50	4.38	0.23	0.31	0.04	11,15,33
1576	2.97	2.96	2.80	4.020e+05	87.50	4.38	0.13	0.21	0.04	11,15,33
1589	3.27	3.26	2.97	4.366e+05	87.50	4.66	0.23	0.31	0.02	11,15,14
1590	3.27	3.26	2.80	4.366e+05	87.50	4.38	0.23	0.31	0.04	11,15,33

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				4.020e+05	87.50	4.38			
	3.27	3.26	2.97	4.366e+05	87.50	4.66	0.23	0.31	0.04

Setto	Mat.	Spessore	Stato
		cm	
20	mattoni pieni e malta di calce	37.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
3	2.47	2.43	2.92	1.354e+05	57.25	4.23	0.21	0.08	0.03	21,30,24
653	2.47	3.50	2.92	1.354e+05	57.25	4.23	0.21	0.08	0.03	21,11,24
654	2.47	3.50	2.92	1.354e+05	57.25	4.23	0.21	0.08	0.03	21,11,24
655	2.47	2.43	2.92	1.354e+05	57.25	4.23	0.21	0.08	0.03	21,30,24
656	2.87	3.50	2.75	1.544e+05	57.25	3.99	0.04	0.08	0.04	14,11,14
657	2.87	3.50	2.75	1.544e+05	57.25	3.99	0.04	0.08	0.04	14,11,14
658	3.07	2.71	2.71	1.639e+05	57.25	3.93	0.02	0.03	0.06	11,14,14
659	3.07	2.71	2.71	1.639e+05	57.25	3.93	0.02	0.03	0.06	11,14,14
660	2.99	2.71	2.83	1.598e+05	57.25	4.10	0.02	0.06	0.07	11,14,40
661	2.99	2.71	2.83	1.598e+05	57.25	4.10	0.02	0.06	0.07	11,14,40
662	2.99	2.79	2.83	1.598e+05	57.25	4.10	0.02	0.08	0.07	11,14,40
663	2.99	2.79	2.83	1.598e+05	57.25	4.10	0.02	0.08	0.07	11,14,40

Nodo	P / A	P / A	P / A.3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				1.354e+05	57.25	3.93			
	3.09	3.50	3.08	1.645e+05	57.25	4.47	0.21	0.11	0.07

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
666	2.90	2.90	2.90	5.916e+05	343.50	4.21	0.16	0.01	0.04	30,30,34
667	2.90	2.90	2.90	5.916e+05	343.50	4.21	0.16	0.01	0.04	30,30,34
668	2.90	1.46	1.39	5.916e+05	343.50	2.02	0.16	0.03	0.05	30,11,32
669	2.90	1.46	1.39	5.916e+05	343.50	2.02	0.16	0.03	0.05	30,11,32
670	1.37	1.46	1.39	1.238e+06	343.50	2.02	0.11	0.03	0.05	30,11,32
671	1.37	1.46	1.39	1.238e+06	343.50	2.02	0.11	0.03	0.05	30,11,32
679	1.37	1.46	1.39	1.238e+06	343.50	2.02	0.11	0.03	0.05	30,11,32
680	1.37	1.46	1.39	1.238e+06	343.50	2.02	0.11	0.03	0.05	30,11,32
682	2.90	2.90	2.90	5.916e+05	343.50	4.21	0.16	0.01	0.04	30,30,34
683	2.90	1.46	1.39	5.916e+05	343.50	2.02	0.16	0.03	0.05	30,11,32
684	1.37	1.46	1.39	1.238e+06	343.50	2.02	0.11	0.03	0.05	30,11,32
689	1.37	1.46	1.39	1.238e+06	343.50	2.02	0.11	0.03	0.05	30,11,32
690	1.37	1.46	1.39	1.238e+06	343.50	2.02	0.11	0.03	0.05	30,11,32
698	1.37	1.46	1.39	1.238e+06	343.50	2.02	0.11	0.03	0.05	30,11,32
699	1.37	1.46	1.39	1.238e+06	343.50	2.02	0.11	0.03	0.05	30,11,32
707	2.90	2.90	2.90	5.916e+05	343.50	4.21	0.16	0.01	0.04	30,30,34
708	2.90	1.46	1.39	5.916e+05	343.50	2.02	0.16	0.03	0.05	30,11,32
709	1.37	1.46	1.39	1.238e+06	343.50	2.02	0.11	0.03	0.05	30,11,32
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	2.90	2.90	2.90	5.916e+05	343.50	2.02				
	2.90	2.90	2.90	1.238e+06	343.50	4.21	0.16	0.03	0.05	

[illegible]

1976	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0,0,0
1977	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0,0,0

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				0.0	0.0	0.0			
	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Setto	Mat.	Spessore	Stato
		cm	
23	mattoni pieni e malta di calce	37.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
15	3.26	3.26	3.34	1.550e+05	54.25	4.85	0.08	0.11	0.03	27,27,23
681	3.25	3.26	3.14	1.545e+05	54.25	4.55	0.07	0.07	0.03	15,27,20
682	3.25	3.26	3.14	1.545e+05	54.25	4.55	0.07	0.07	0.01	15,27,20
700	3.26	3.26	3.34	1.550e+05	54.25	4.85	0.08	0.11	0.03	27,27,23
701	3.26	3.26	3.34	1.550e+05	54.25	4.85	0.08	0.11	0.03	27,27,23
702	3.27	3.27	3.28	1.552e+05	54.25	4.76	0.04	0.06	0.02	27,27,20
703	2.88	3.14	2.95	1.391e+05	54.25	4.28	0.02	0.05	0.03	14,33,21
704	2.88	3.14	2.95	1.391e+05	54.25	4.28	0.03	0.05	0.03	30,33,21
705	3.14	3.23	3.14	1.498e+05	54.25	4.55	0.05	0.06	0.03	20,27,20
706	3.25	3.26	3.14	1.545e+05	54.25	4.55	0.07	0.07	0.03	15,27,20
707	3.25	3.26	3.14	1.545e+05	54.25	4.55	0.07	0.07	0.01	15,27,20
710	3.26	3.26	3.34	1.550e+05	54.25	4.85	0.08	0.11	0.03	27,27,23
711	3.27	3.27	3.28	1.552e+05	54.25	4.76	0.04	0.06	0.02	27,27,20
712	2.88	3.14	2.95	1.391e+05	54.25	4.28	0.02	0.05	0.03	14,33,21
713	2.88	3.14	2.95	1.391e+05	54.25	4.28	0.03	0.05	0.03	30,33,21
714	3.14	3.23	3.14	1.498e+05	54.25	4.55	0.05	0.06	0.03	20,27,20

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				1.391e+05	54.25	4.28			
	3.27	3.27	3.34	1.552e+05	54.25	4.85	0.08	0.11	0.03

Setto	Mat.	Spessore	Stato
		cm	
26	mattoni pieni e malta di calce	42.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
15	3.20	3.30	2.90	1.484e+05	50.25	4.78	0.08	0.07	0.03	20,27,22
22	3.20	3.30	2.90	1.484e+05	50.25	4.78	0.08	0.07	0.03	20,27,22
681	2.83	2.79	2.90	1.334e+05	50.25	4.78	0.06	0.03	0.05	20,21,11
682	2.83	2.59	2.90	1.334e+05	50.25	4.78	0.06	0.02	0.05	20,21,11
710	3.20	3.30	2.90	1.484e+05	50.25	4.78	0.08	0.07	0.03	20,27,22
711	3.32	3.35	2.99	1.531e+05	50.25	4.93	0.06	0.03	0.02	23,27,22
712	3.14	3.14	3.03	1.461e+05	50.25	4.99	0.03	0.04	0.01	21,21,14
713	3.14	3.14	2.86	1.461e+05	50.25	4.72	0.03	0.04	0.03	21,21,18
714	2.81	2.96	3.09	1.327e+05	50.25	5.09	0.04	0.04	0.04	32,21,11
715	3.20	3.30	2.90	1.484e+05	50.25	4.78	0.08	0.07	0.03	20,27,22
716	3.32	3.35	2.99	1.531e+05	50.25	4.93	0.06	0.03	0.02	23,27,22
717	3.14	3.14	3.03	1.461e+05	50.25	4.99	0.03	0.04	0.01	21,21,14
718	3.14	3.14	2.86	1.461e+05	50.25	4.72	0.03	0.04	0.03	21,21,18
719	2.81	2.96	3.09	1.327e+05	50.25	5.09	0.04	0.04	0.04	32,21,11
720	2.83	2.79	2.90	1.334e+05	50.25	4.78	0.06	0.03	0.05	20,21,11
721	2.83	2.59	2.90	1.334e+05	50.25	4.78	0.06	0.02	0.05	20,21,11

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				1.327e+05	50.25	4.72			
	3.32	3.35	3.09	1.531e+05	50.25	5.09	0.08	0.07	0.05

Setto	Mat.	Spessore	Stato
		cm	
27	mattoni pieni e malta di calce	42.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
682	2.00	2.00	2.18	9.764e+04	50.25	3.59	0.09	0.11	0.04	21,17,11
683	1.65	1.77	2.18	8.190e+04	50.25	3.59	0.12	0.21	0.04	21,20,11
684	1.65	1.77	1.60	8.190e+04	50.25	2.63	0.12	0.21	0.02	21,20,14
721	2.00	2.00	2.18	9.764e+04	50.25	3.59	0.09	0.11	0.04	21,17,11
722	1.65	1.77	2.18	8.190e+04	50.25	3.59	0.12	0.21	0.04	21,20,11
723	1.65	1.77	1.60	8.190e+04	50.25	2.63	0.12	0.21	0.02	21,20,14
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				8.190e+04	50.25	2.63				
	2.00	2.00	2.18	9.764e+04	50.25	3.59	0.12	0.21	0.04	

Setto	Mat.	Spessore	Stato
		cm	
29	mattoni pieni e malta di calce	42.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
25	1.99	1.87	1.89	7.216e+06	433.25	3.11	0.08	0.12	2.29e-03	20,26,14
26	1.99	1.87	1.89	7.216e+06	433.25	3.11	0.08	0.12	2.29e-03	20,26,14
27	1.99	1.87	1.89	7.216e+06	433.25	3.11	0.08	0.12	2.29e-03	20,26,14
28	1.99	1.87	1.89	7.216e+06	433.25	3.11	0.08	0.12	2.29e-03	20,26,14
727	1.94	1.84	1.80	7.074e+06	433.25	2.97	0.08	0.12	0.01	20,26,34
728	1.76	1.77	1.72	6.458e+06	433.25	2.84	0.08	0.12	0.01	24,26,34
729	1.66	1.70	1.64	6.104e+06	433.25	2.71	0.08	0.12	0.02	40,26,42
730	1.66	1.63	1.52	6.104e+06	433.25	2.51	0.08	0.12	0.03	40,26,42
737	1.52	1.51	1.40	5.651e+06	433.25	2.31	0.05	0.11	0.05	42,26,42
738	1.39	1.39	1.40	5.188e+06	433.25	2.31	7.10e-03	0.08	0.05	39,26,42
762	1.52	1.51	1.40	5.651e+06	433.25	2.31	0.05	0.11	0.05	42,26,42
763	1.39	1.39	1.40	5.188e+06	433.25	2.31	7.10e-03	0.08	0.05	39,26,42
766	1.94	1.84	1.86	7.074e+06	433.25	3.06	0.08	0.12	6.26e-03	20,26,14
772	1.94	1.84	1.86	7.074e+06	433.25	3.06	0.08	0.12	6.26e-03	20,26,14
773	1.94	1.84	1.80	7.074e+06	433.25	2.97	0.08	0.12	0.01	20,26,34
774	1.76	1.77	1.72	6.458e+06	433.25	2.84	0.08	0.12	0.01	24,26,34
775	1.66	1.70	1.64	6.104e+06	433.25	2.71	0.08	0.12	0.02	40,26,42
776	1.66	1.63	1.52	6.104e+06	433.25	2.51	0.08	0.12	0.03	40,26,42
777	1.52	1.51	1.40	5.651e+06	433.25	2.31	0.05	0.11	0.05	42,26,42
778	1.39	1.39	1.40	5.188e+06	433.25	2.31	7.10e-03	0.08	0.05	39,26,42
781	1.94	1.84	1.86	7.074e+06	433.25	3.06	0.08	0.12	6.26e-03	20,26,14
782	1.99	1.87	1.89	7.216e+06	433.25	3.11	0.08	0.12	2.29e-03	20,26,14
783	1.94	1.84	1.80	7.074e+06	433.25	2.97	0.08	0.12	0.01	20,26,34
784	1.76	1.77	1.72	6.458e+06	433.25	2.84	0.08	0.12	0.01	24,26,34
785	1.66	1.70	1.64	6.104e+06	433.25	2.71	0.08	0.12	0.02	40,26,42
786	1.66	1.63	1.52	6.104e+06	433.25	2.51	0.08	0.12	0.03	40,26,42
787	1.52	1.51	1.40	5.651e+06	433.25	2.31	0.05	0.11	0.05	42,26,42
788	1.39	1.39	1.40	5.188e+06	433.25	2.31	7.10e-03	0.08	0.05	39,26,42
791	1.94	1.84	1.86	7.074e+06	433.25	3.06	0.08	0.12	6.26e-03	20,26,14
792	1.99	1.87	1.89	7.216e+06	433.25	3.11	0.08	0.12	2.29e-03	20,26,14
793	1.94	1.84	1.80	7.074e+06	433.25	2.97	0.08	0.12	0.01	20,26,34
794	1.76	1.77	1.72	6.458e+06	433.25	2.84	0.08	0.12	0.01	24,26,34
795	1.66	1.70	1.64	6.104e+06	433.25	2.71	0.08	0.12	0.02	40,26,42
796	1.66	1.63	1.52	6.104e+06	433.25	2.51	0.08	0.12	0.03	40,26,42
797	1.52	1.51	1.40	5.651e+06	433.25	2.31	0.05	0.11	0.05	42,26,42
798	1.39	1.39	1.40	5.188e+06	433.25	2.31	7.10e-03	0.08	0.05	39,26,42
801	1.94	1.84	1.86	7.074e+06	433.25	3.06	0.08	0.12	6.26e-03	20,26,14
802	1.99	1.87	1.89	7.216e+06	433.25	3.11	0.08	0.12	2.29e-03	20,26,14
803	1.94	1.84	1.80	7.074e+06	433.25	2.97	0.08	0.12	0.01	20,26,34
804	1.76	1.77	1.72	6.458e+06	433.25	2.84	0.08	0.12	0.01	24,26,34
805	1.66	1.70	1.64	6.104e+06	433.25	2.71	0.08	0.12	0.02	40,26,42
806	1.66	1.63	1.52	6.104e+06	433.25	2.51	0.08	0.12	0.03	40,26,42
807	1.52	1.51	1.40	5.651e+06	433.25	2.31	0.05	0.11	0.05	42,26,42
808	1.39	1.39	1.40	5.188e+06	433.25	2.31	7.10e-03	0.08	0.05	39,26,42
811	1.94	1.84	1.86	7.074e+06	433.25	3.06	0.08	0.12	6.26e-03	20,26,14
812	1.99	1.87	1.89	7.216e+06	433.25	3.11	0.08	0.12	2.29e-03	20,26,14
813	1.94	1.84	1.80	7.074e+06	433.25	2.97	0.08	0.12	0.01	20,26,34
814	1.76	1.77	1.72	6.458e+06	433.25	2.84	0.08	0.12	0.01	24,26,34

815	1.66	1.70	1.64	6.104e+06	433.25	2.71	0.08	0.12	0.02	40,26,42
816	1.66	1.63	1.52	6.104e+06	433.25	2.51	0.08	0.12	0.03	40,26,42
817	1.52	1.51	1.40	5.651e+06	433.25	2.31	0.05	0.11	0.05	42,26,42
818	1.39	1.39	1.40	5.188e+06	433.25	2.31	7.10e-03	0.08	0.05	39,26,42
821	1.94	1.84	1.86	7.074e+06	433.25	3.06	0.08	0.12	6.26e-03	20,26,14
822	1.94	1.84	1.80	7.074e+06	433.25	2.97	0.08	0.12	0.01	20,26,34
823	1.76	1.77	1.72	6.458e+06	433.25	2.84	0.08	0.12	0.01	24,26,34
824	1.66	1.70	1.64	6.104e+06	433.25	2.71	0.08	0.12	0.02	40,26,42
825	1.66	1.63	1.52	6.104e+06	433.25	2.51	0.08	0.12	0.03	40,26,42
826	1.52	1.51	1.40	5.651e+06	433.25	2.31	0.05	0.11	0.05	42,26,42
827	1.39	1.39	1.40	5.188e+06	433.25	2.31	7.10e-03	0.08	0.05	39,26,42
840	1.94	1.84	1.86	7.074e+06	433.25	3.06	0.08	0.12	6.26e-03	20,26,14
841	1.99	1.87	1.89	7.216e+06	433.25	3.11	0.08	0.12	2.29e-03	20,26,14
842	1.94	1.84	1.80	7.074e+06	433.25	2.97	0.08	0.12	0.01	20,26,34
843	1.76	1.77	1.72	6.458e+06	433.25	2.84	0.08	0.12	0.01	24,26,34
844	1.66	1.70	1.64	6.104e+06	433.25	2.71	0.08	0.12	0.02	40,26,42
845	1.66	1.63	1.52	6.104e+06	433.25	2.51	0.08	0.12	0.03	40,26,42
846	1.52	1.51	1.40	5.651e+06	433.25	2.31	0.05	0.11	0.05	42,26,42
847	1.39	1.39	1.40	5.188e+06	433.25	2.31	7.10e-03	0.08	0.05	39,26,42
850	1.94	1.84	1.86	7.074e+06	433.25	3.06	0.08	0.12	6.26e-03	20,26,14
851	1.94	1.84	1.80	7.074e+06	433.25	2.97	0.08	0.12	0.01	20,26,34
852	1.76	1.77	1.72	6.458e+06	433.25	2.84	0.08	0.12	0.01	24,26,34
853	1.66	1.70	1.64	6.104e+06	433.25	2.71	0.08	0.12	0.02	40,26,42
854	1.66	1.63	1.52	6.104e+06	433.25	2.51	0.08	0.12	0.03	40,26,42

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				5.188e+06	433.25	2.31			
	1.99	1.87	1.89	7.216e+06	433.25	3.11	0.08	0.12	0.05

Setto	Mat.	Spessore	Stato
		cm	
30	mattoni pieni e malta di calce	42.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
738	1.19	1.19	1.19	4.472e+06	433.25	1.96	0.05	0.07	0.08	19,23,42
739	1.17	1.17	1.15	4.322e+06	429.63	1.90	0.08	0.08	0.10	19,23,26
740	1.17	1.17	1.15	4.322e+06	429.63	1.90	0.08	0.08	0.10	19,23,26
763	1.19	1.19	1.19	4.472e+06	433.25	1.96	0.05	0.07	0.08	19,23,42
764	1.17	1.17	1.15	4.322e+06	429.63	1.90	0.08	0.08	0.10	19,23,26
765	1.17	1.17	1.15	4.322e+06	429.63	1.90	0.08	0.08	0.10	19,23,26
778	1.19	1.19	1.19	4.472e+06	433.25	1.96	0.05	0.07	0.08	19,23,42
779	1.17	1.17	1.15	4.322e+06	429.63	1.90	0.08	0.08	0.10	19,23,26
780	1.17	1.17	1.15	4.322e+06	429.63	1.90	0.08	0.08	0.10	19,23,26
788	1.19	1.19	1.19	4.472e+06	433.25	1.96	0.05	0.07	0.08	19,23,42
789	1.17	1.17	1.15	4.322e+06	429.63	1.90	0.08	0.08	0.10	19,23,26
790	1.17	1.17	1.15	4.322e+06	429.63	1.90	0.08	0.08	0.10	19,23,26
798	1.19	1.19	1.19	4.472e+06	433.25	1.96	0.05	0.07	0.08	19,23,42
799	1.17	1.17	1.15	4.322e+06	429.63	1.90	0.08	0.08	0.10	19,23,26
800	1.17	1.17	1.15	4.322e+06	429.63	1.90	0.08	0.08	0.10	19,23,26
808	1.19	1.19	1.19	4.472e+06	433.25	1.96	0.05	0.07	0.08	19,23,42
809	1.17	1.17	1.15	4.322e+06	429.63	1.90	0.08	0.08	0.10	19,23,26
810	1.17	1.17	1.15	4.322e+06	429.63	1.90	0.08	0.08	0.10	19,23,26
818	1.19	1.19	1.19	4.472e+06	433.25	1.96	0.05	0.07	0.08	19,23,42
819	1.17	1.17	1.15	4.322e+06	429.63	1.90	0.08	0.08	0.10	19,23,26
820	1.17	1.17	1.15	4.322e+06	429.63	1.90	0.08	0.08	0.10	19,23,26
827	1.19	1.19	1.19	4.472e+06	433.25	1.96	0.05	0.07	0.08	19,23,42
828	1.17	1.17	1.15	4.322e+06	429.63	1.90	0.08	0.08	0.10	19,23,26
829	1.17	1.17	1.15	4.322e+06	429.63	1.90	0.08	0.08	0.10	19,23,26
847	1.19	1.19	1.19	4.472e+06	433.25	1.96	0.05	0.07	0.08	19,23,42
848	1.17	1.17	1.15	4.322e+06	429.63	1.90	0.08	0.08	0.10	19,23,26
849	1.17	1.17	1.15	4.322e+06	429.63	1.90	0.08	0.08	0.10	19,23,26
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				4.322e+06	429.63	1.90				
	1.19	1.19	1.19	4.472e+06	433.25	1.96	0.08	0.08	0.10	

Setto	Mat.	Spessore	Stato
		cm	
34	mattoni pieni e malta di calce	42.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
23	2.10	2.24	2.24	2.251e+05	74.50	3.69	0.05	0.06	0.04	22,20,32
24	2.10	2.24	2.24	2.251e+05	74.50	3.69	0.05	0.06	0.04	22,20,32
744	2.10	2.24	2.24	2.251e+05	74.50	3.69	0.05	0.06	0.04	22,20,32
745	2.43	2.22	2.29	2.562e+05	74.50	3.77	0.05	0.04	0.04	19,21,34
746	2.43	2.22	2.34	2.562e+05	74.50	3.85	0.05	0.04	0.03	19,21,34
747	2.46	2.25	2.43	2.588e+05	74.50	4.01	0.04	0.03	0.04	23,21,20
748	2.16	2.28	2.43	2.304e+05	74.50	4.01	0.04	0.09	0.04	26,33,20
749	2.12	2.24	2.16	2.261e+05	74.50	3.56	0.17	0.25	0.09	26,33,21
750	2.12	2.24	2.16	2.261e+05	74.50	3.56	0.17	0.25	0.09	26,33,21
753	2.10	2.24	2.24	2.251e+05	74.50	3.69	0.05	0.06	0.04	22,20,32
754	2.44	2.22	2.29	2.571e+05	74.50	3.77	0.05	0.04	0.04	19,21,34
755	2.44	2.22	2.34	2.571e+05	74.50	3.85	0.05	0.04	0.03	19,21,34
756	2.46	2.25	2.43	2.588e+05	74.50	4.01	0.04	0.03	0.04	23,21,20
757	2.16	2.28	2.43	2.304e+05	74.50	4.01	0.04	0.09	0.04	26,33,20
758	2.12	2.24	2.16	2.261e+05	74.50	3.56	0.17	0.25	0.09	26,33,21
759	2.12	2.24	2.16	2.261e+05	74.50	3.56	0.17	0.25	0.09	26,33,21
830	2.10	2.24	2.24	2.251e+05	74.50	3.69	0.05	0.06	0.04	22,20,32
831	2.10	2.24	2.24	2.251e+05	74.50	3.69	0.05	0.06	0.04	22,20,32
832	2.44	2.22	2.29	2.571e+05	74.50	3.77	0.05	0.04	0.04	19,21,34
833	2.44	2.22	2.34	2.571e+05	74.50	3.85	0.05	0.04	0.03	19,21,34
834	2.46	2.25	2.43	2.588e+05	74.50	4.01	0.04	0.03	0.04	23,21,20
835	2.16	2.28	2.43	2.304e+05	74.50	4.01	0.04	0.09	0.04	26,33,20
836	2.12	2.24	2.16	2.261e+05	74.50	3.56	0.17	0.25	0.09	26,33,21
837	2.12	2.24	2.16	2.261e+05	74.50	3.56	0.17	0.25	0.09	26,33,21
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				2.251e+05	74.50	3.56				
	2.46	2.28	2.43	2.588e+05	74.50	4.01	0.17	0.25	0.09	

Setto	Mat.	Spessore	Stato
		cm	
35	mattoni pieni e malta di calce	42.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
750	1.66	1.66	1.71	1.806e+05	74.50	2.82	0.08	0.23	0.11	13,21,33
751	1.66	1.22	1.71	1.806e+05	74.50	2.82	0.08	0.31	0.11	13,21,33
752	1.22	1.22	1.22	1.353e+05	74.50	2.01	0.06	0.31	0.07	13,21,21
759	1.66	1.66	1.71	1.806e+05	74.50	2.82	0.08	0.23	0.11	13,21,33
760	1.66	1.22	1.71	1.806e+05	74.50	2.82	0.08	0.31	0.11	13,21,33
761	1.22	1.22	1.22	1.353e+05	74.50	2.01	0.06	0.31	0.07	13,21,21
837	1.66	1.66	1.71	1.806e+05	74.50	2.82	0.08	0.23	0.11	13,21,33
838	1.66	1.22	1.71	1.806e+05	74.50	2.82	0.08	0.31	0.11	13,21,33
839	1.22	1.22	1.22	1.353e+05	74.50	2.01	0.06	0.31	0.07	13,21,21
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				1.353e+05	74.50	2.01				
	1.66	1.66	1.71	1.806e+05	74.50	2.82	0.08	0.31	0.11	

Setto	Mat.	Spessore	Stato
		cm	
37	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
28	2.05	2.05	2.20	4.506e+05	109.86	3.82	0.04	0.06	4.67e-03	37,37,34
30	2.05	2.05	2.20	4.506e+05	109.86	3.82	0.04	0.06	4.67e-03	37,37,34
727	2.12	2.04	2.12	4.655e+05	109.86	3.69	0.03	0.08	0.01	36,37,34
728	2.06	2.07	2.06	4.535e+05	109.86	3.58	0.04	0.10	0.02	36,37,28

729	2.09	2.09	2.00	4.585e+05	109.86	3.48	0.06	0.10	0.02	37,37,28
730	2.08	2.08	1.93	4.564e+05	109.86	3.35	0.12	0.11	0.03	37,37,24
737	2.08	2.08	1.64	4.564e+05	109.86	2.85	0.12	0.11	0.04	37,37,24
738	1.79	1.79	1.64	3.984e+05	109.86	2.85	0.06	0.05	0.04	37,37,24
766	2.05	2.05	2.18	4.506e+05	109.86	3.79	0.04	0.06	9.73e-03	37,37,30
855	2.05	2.05	2.18	4.506e+05	109.86	3.79	0.04	0.06	9.73e-03	37,37,30
856	2.05	2.05	2.18	4.506e+05	109.86	3.79	0.04	0.06	9.73e-03	37,37,30
857	2.05	2.05	2.20	4.506e+05	109.86	3.82	0.04	0.06	4.67e-03	37,37,34
858	2.12	2.04	2.12	4.655e+05	109.86	3.69	0.03	0.08	0.01	36,37,34
859	2.12	2.04	2.12	4.655e+05	109.86	3.69	0.03	0.08	0.01	36,37,34
860	2.06	2.07	2.06	4.535e+05	109.86	3.58	0.04	0.10	0.02	36,37,28
861	2.06	2.07	2.06	4.535e+05	109.86	3.58	0.04	0.10	0.02	36,37,28
862	2.09	2.09	2.00	4.585e+05	109.86	3.48	0.06	0.10	0.02	37,37,28
863	2.09	2.09	2.00	4.585e+05	109.86	3.48	0.06	0.10	0.02	37,37,28
864	2.08	2.08	1.93	4.564e+05	109.86	3.35	0.12	0.11	0.03	37,37,24
865	2.08	2.08	1.93	4.564e+05	109.86	3.35	0.12	0.11	0.03	37,37,24
866	2.08	2.08	1.64	4.564e+05	109.86	2.85	0.12	0.11	0.04	37,37,24
867	2.08	2.08	1.64	4.564e+05	109.86	2.85	0.12	0.11	0.04	37,37,24
868	1.79	1.79	1.64	3.984e+05	109.86	2.85	0.06	0.05	0.04	37,37,24
869	1.79	1.79	1.64	3.984e+05	109.86	2.85	0.06	0.05	0.04	37,37,24

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				3.984e+05	109.86	2.85			
	2.12	2.09	2.20	4.655e+05	109.86	3.82	0.12	0.11	0.04

Setto	Mat.	Spessore	Stato
		cm	
38	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
738	1.20	1.27	1.22	2.738e+05	109.86	2.12	0.15	0.02	0.03	36,37,23
739	0.78	1.27	1.22	1.815e+05	109.86	2.12	0.19	0.02	0.03	36,37,23
740	0.78	0.83	0.79	1.815e+05	109.86	1.38	0.19	0.02	0.01	36,37,23
868	1.20	1.27	1.22	2.738e+05	109.86	2.12	0.15	0.02	0.03	36,37,23
869	1.20	1.27	1.22	2.738e+05	109.86	2.12	0.15	0.02	0.03	36,37,23
870	0.78	1.27	1.22	1.815e+05	109.86	2.12	0.19	0.02	0.03	36,37,23
871	0.78	1.27	1.22	1.815e+05	109.86	2.12	0.19	0.02	0.03	36,37,23
872	0.78	0.83	0.79	1.815e+05	109.86	1.38	0.19	0.02	0.01	36,37,23
873	0.78	0.83	0.79	1.815e+05	109.86	1.38	0.19	0.02	0.01	36,37,23

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				1.815e+05	109.86	1.38			
	1.20	1.27	1.22	2.738e+05	109.86	2.12	0.19	0.02	0.03

Setto	Mat.	Spessore	Stato
		cm	
39	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
2	3.50	3.54	3.45	4.437e+06	273.36	5.99	0.08	0.07	0.04	17,37,22
31	3.50	3.54	3.45	4.437e+06	273.36	5.99	0.08	0.07	0.04	17,37,22
32	3.50	3.54	3.45	4.437e+06	273.36	5.99	0.08	0.07	0.04	17,37,22
638	3.50	3.54	3.45	4.437e+06	273.36	5.99	0.08	0.07	0.04	17,37,22
645	3.50	3.54	3.45	4.437e+06	273.36	5.99	0.08	0.07	0.04	17,37,22
652	3.50	3.54	3.45	4.437e+06	273.36	5.99	0.08	0.07	0.04	17,37,22
874	3.50	3.47	3.45	4.437e+06	273.36	5.99	0.08	0.07	0.04	17,37,22
877	3.43	3.47	3.22	4.362e+06	273.36	5.60	0.07	0.07	0.03	17,37,11
878	3.50	3.47	3.45	4.437e+06	273.36	5.99	0.08	0.07	0.04	17,37,22
879	3.28	3.30	3.04	4.208e+06	273.36	5.27	0.05	0.07	0.05	17,39,16
880	3.50	3.54	3.45	4.437e+06	273.36	5.99	0.08	0.07	0.04	17,37,22
881	3.14	3.15	2.94	4.048e+06	273.36	5.12	0.04	0.07	0.08	13,39,26
882	3.43	3.47	3.22	4.362e+06	273.36	5.60	0.07	0.07	0.03	17,37,11
883	2.88	2.79	2.76	3.766e+06	273.36	4.80	0.02	0.07	0.09	42,39,22
884	3.28	3.30	3.04	4.208e+06	273.36	5.27	0.05	0.07	0.05	17,39,16

885	2.53	2.79	2.76	3.367e+06	273.36	4.80	0.03	0.07	0.09	37,39,22
887	2.53	2.51	2.49	3.367e+06	273.36	4.33	0.03	0.06	0.06	37,39,26
893	3.14	3.15	2.94	4.048e+06	273.36	5.12	0.04	0.07	0.08	13,39,26
894	2.88	2.79	2.76	3.766e+06	273.36	4.80	0.02	0.07	0.09	42,39,22
895	2.53	2.79	2.76	3.367e+06	273.36	4.80	0.03	0.07	0.09	37,39,22
896	2.53	2.51	2.49	3.367e+06	273.36	4.33	0.03	0.06	0.06	37,39,26
903	3.50	3.47	3.45	4.437e+06	273.36	5.99	0.08	0.07	0.04	17,37,22
904	3.50	3.47	3.45	4.437e+06	273.36	5.99	0.08	0.07	0.04	17,37,22
905	3.50	3.54	3.45	4.437e+06	273.36	5.99	0.08	0.07	0.04	17,37,22
906	3.43	3.47	3.22	4.362e+06	273.36	5.60	0.07	0.07	0.03	17,37,11
907	3.43	3.47	3.22	4.362e+06	273.36	5.60	0.07	0.07	0.03	17,37,11
908	3.28	3.30	3.04	4.208e+06	273.36	5.27	0.05	0.07	0.05	17,39,16
909	3.28	3.30	3.04	4.208e+06	273.36	5.27	0.05	0.07	0.05	17,39,16
910	3.14	3.15	2.94	4.048e+06	273.36	5.12	0.04	0.07	0.08	13,39,26
911	3.14	3.15	2.94	4.048e+06	273.36	5.12	0.04	0.07	0.08	13,39,26
912	2.88	2.79	2.76	3.766e+06	273.36	4.80	0.02	0.07	0.09	42,39,22
913	2.88	2.79	2.76	3.766e+06	273.36	4.80	0.02	0.07	0.09	42,39,22
914	2.53	2.79	2.76	3.367e+06	273.36	4.80	0.03	0.07	0.09	37,39,22
915	2.53	2.79	2.76	3.367e+06	273.36	4.80	0.03	0.07	0.09	37,39,22
916	2.53	2.51	2.49	3.367e+06	273.36	4.33	0.03	0.06	0.06	37,39,26
917	2.53	2.51	2.49	3.367e+06	273.36	4.33	0.03	0.06	0.06	37,39,26
1124	3.50	3.47	3.45	4.437e+06	273.36	5.99	0.08	0.07	0.04	17,37,22
1130	3.43	3.47	3.22	4.362e+06	273.36	5.60	0.07	0.07	0.03	17,37,11
1131	3.28	3.30	3.04	4.208e+06	273.36	5.27	0.05	0.07	0.05	17,39,16
1132	3.14	3.15	2.94	4.048e+06	273.36	5.12	0.04	0.07	0.08	13,39,26
1133	2.88	2.79	2.76	3.766e+06	273.36	4.80	0.02	0.07	0.09	42,39,22
1139	2.53	2.79	2.76	3.367e+06	273.36	4.80	0.03	0.07	0.09	37,39,22
1140	2.53	2.51	2.49	3.367e+06	273.36	4.33	0.03	0.06	0.06	37,39,26
1259	3.50	3.47	3.45	4.437e+06	273.36	5.99	0.08	0.07	0.04	17,37,22
1260	3.43	3.47	3.22	4.362e+06	273.36	5.60	0.07	0.07	0.03	17,37,11
1261	3.28	3.30	3.04	4.208e+06	273.36	5.27	0.05	0.07	0.05	17,39,16
1262	3.14	3.15	2.94	4.048e+06	273.36	5.12	0.04	0.07	0.08	13,39,26
1263	2.88	2.79	2.76	3.766e+06	273.36	4.80	0.02	0.07	0.09	42,39,22
1264	2.53	2.79	2.76	3.367e+06	273.36	4.80	0.03	0.07	0.09	37,39,22
1265	2.53	2.51	2.49	3.367e+06	273.36	4.33	0.03	0.06	0.06	37,39,26
1268	3.50	3.47	3.45	4.437e+06	273.36	5.99	0.08	0.07	0.04	17,37,22
1269	3.43	3.47	3.22	4.362e+06	273.36	5.60	0.07	0.07	0.03	17,37,11
1270	3.28	3.30	3.04	4.208e+06	273.36	5.27	0.05	0.07	0.05	17,39,16
1271	3.14	3.15	2.94	4.048e+06	273.36	5.12	0.04	0.07	0.08	13,39,26
1272	2.88	2.79	2.76	3.766e+06	273.36	4.80	0.02	0.07	0.09	42,39,22
1273	2.53	2.79	2.76	3.367e+06	273.36	4.80	0.03	0.07	0.09	37,39,22
1274	2.53	2.51	2.49	3.367e+06	273.36	4.33	0.03	0.06	0.06	37,39,26
1277	3.50	3.47	3.45	4.437e+06	273.36	5.99	0.08	0.07	0.04	17,37,22
1278	3.43	3.47	3.22	4.362e+06	273.36	5.60	0.07	0.07	0.03	17,37,11
1279	3.28	3.30	3.04	4.208e+06	273.36	5.27	0.05	0.07	0.05	17,39,16
1280	3.14	3.15	2.94	4.048e+06	273.36	5.12	0.04	0.07	0.08	13,39,26
1281	2.88	2.79	2.76	3.766e+06	273.36	4.80	0.02	0.07	0.09	42,39,22
1282	2.53	2.79	2.76	3.367e+06	273.36	4.80	0.03	0.07	0.09	37,39,22
1283	2.53	2.51	2.49	3.367e+06	273.36	4.33	0.03	0.06	0.06	37,39,26
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				3.367e+06	273.36	4.33				
	3.50	3.54	3.45	4.437e+06	273.36	5.99	0.08	0.07	0.09	

Setto	Mat.	Spessore	Stato
		cm	
42	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
875	1.85	1.85	1.77	2.542e+06	273.36	3.07	0.07	0.06	0.02	39,39,36
876	1.85	1.85	1.77	2.542e+06	273.36	3.07	0.07	0.06	0.02	39,39,36
887	2.17	2.14	2.06	2.933e+06	273.36	3.58	0.05	0.04	9.46e-03	37,39,16
889	1.85	1.85	1.77	2.542e+06	273.36	3.07	0.07	0.06	0.02	39,39,36
891	1.85	1.85	1.77	2.542e+06	273.36	3.07	0.07	0.06	0.02	39,39,36
896	2.17	2.14	2.06	2.933e+06	273.36	3.58	0.05	0.04	9.46e-03	37,39,16
897	1.85	1.85	1.77	2.542e+06	273.36	3.07	0.07	0.06	0.02	39,39,36
898	1.85	1.85	1.77	2.542e+06	273.36	3.07	0.07	0.06	0.02	39,39,36
916	2.17	2.14	2.06	2.933e+06	273.36	3.58	0.05	0.04	9.46e-03	37,39,16
917	2.17	2.14	2.06	2.933e+06	273.36	3.58	0.05	0.04	9.46e-03	37,39,16
918	1.85	1.85	1.77	2.542e+06	273.36	3.07	0.07	0.06	0.02	39,39,36
919	1.85	1.85	1.77	2.542e+06	273.36	3.07	0.07	0.06	0.02	39,39,36

1140	2.17	2.14	2.06	2.933e+06	273.36	3.58	0.05	0.04	9.46e-03	37,39,16
1141	1.85	1.85	1.77	2.542e+06	273.36	3.07	0.07	0.06	0.02	39,39,36
1142	1.85	1.85	1.77	2.542e+06	273.36	3.07	0.07	0.06	0.02	39,39,36
1265	2.17	2.14	2.06	2.933e+06	273.36	3.58	0.05	0.04	9.46e-03	37,39,16
1266	1.85	1.85	1.77	2.542e+06	273.36	3.07	0.07	0.06	0.02	39,39,36
1267	1.85	1.85	1.77	2.542e+06	273.36	3.07	0.07	0.06	0.02	39,39,36
1274	2.17	2.14	2.06	2.933e+06	273.36	3.58	0.05	0.04	9.46e-03	37,39,16
1275	1.85	1.85	1.77	2.542e+06	273.36	3.07	0.07	0.06	0.02	39,39,36
1276	1.85	1.85	1.77	2.542e+06	273.36	3.07	0.07	0.06	0.02	39,39,36
1283	2.17	2.14	2.06	2.933e+06	273.36	3.58	0.05	0.04	9.46e-03	37,39,16
1284	1.85	1.85	1.77	2.542e+06	273.36	3.07	0.07	0.06	0.02	39,39,36
1285	1.85	1.85	1.77	2.542e+06	273.36	3.07	0.07	0.06	0.02	39,39,36

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
	2.17	2.14	2.06	2.542e+06	273.36	3.07			
				2.933e+06	273.36	3.58	0.07	0.06	0.02

Setto	Mat.	Spessore	Stato
		cm	
43	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
2	2.10	2.10	2.26	8.138e+04	46.00	3.54	0.11	0.15	0.04	26,26,37
16	2.10	2.10	2.26	8.138e+04	46.00	3.54	0.11	0.15	0.04	26,26,37
903	2.10	2.25	2.26	8.138e+04	46.00	3.54	0.11	0.17	0.04	26,26,37
906	2.63	2.61	2.39	9.966e+04	46.00	3.74	0.04	0.17	0.01	20,25,37
908	2.85	2.93	2.84	1.073e+05	46.00	4.45	0.06	0.19	7.73e-03	12,25,28
910	3.33	3.36	3.25	1.226e+05	46.00	5.10	0.10	0.25	0.01	26,25,30
912	3.90	3.91	3.25	1.399e+05	46.00	5.10	0.23	0.45	0.01	26,22,30
914	3.90	3.54	3.79	1.399e+05	46.00	5.94	0.23	0.68	0.01	26,14,30
916	3.54	3.54	3.56	1.289e+05	46.00	5.59	0.18	0.68	6.45e-03	26,14,13
920	2.10	2.25	2.26	8.138e+04	46.00	3.54	0.11	0.17	0.04	26,26,37
922	2.63	2.61	2.39	9.966e+04	46.00	3.74	0.04	0.17	0.01	20,25,37
923	2.85	2.93	2.84	1.073e+05	46.00	4.45	0.06	0.19	7.73e-03	12,25,28
924	3.33	3.36	3.25	1.226e+05	46.00	5.10	0.10	0.25	0.01	26,25,30
925	3.90	3.91	3.25	1.399e+05	46.00	5.10	0.23	0.45	0.01	26,22,30
926	3.90	3.54	3.79	1.399e+05	46.00	5.94	0.23	0.68	0.01	26,14,30
927	3.54	3.54	3.56	1.289e+05	46.00	5.59	0.18	0.68	6.45e-03	26,14,13

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				8.138e+04	46.00	3.54			
	3.90	3.91	3.79	1.399e+05	46.00	5.94	0.23	0.68	0.04

Setto	Mat.	Spessore	Stato
		cm	
44	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
875	3.15	3.02	3.01	1.168e+05	46.00	4.72	1.08e-03	0.92	4.48e-03	33,23,36
916	2.61	2.71	2.75	9.922e+04	46.00	4.32	0.01	0.87	9.54e-03	16,39,37
918	2.61	3.02	2.75	9.922e+04	46.00	4.32	0.01	0.92	9.54e-03	16,23,37
927	2.61	2.71	2.75	9.922e+04	46.00	4.32	0.01	0.87	9.54e-03	16,39,37
928	2.61	3.02	2.75	9.922e+04	46.00	4.32	0.01	0.92	9.54e-03	16,23,37
929	3.15	3.02	3.01	1.168e+05	46.00	4.72	1.08e-03	0.92	4.48e-03	33,23,36

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				9.922e+04	46.00	4.32			
	3.15	3.02	3.01	1.168e+05	46.00	4.72	0.01	0.92	9.54e-03

Setto	Mat.	Spessore	Stato
		cm	
47	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
3	3.45	3.45	3.54	2.444e+05	64.00	5.55	0.12	0.12	0.02	20,24,27
21	3.45	3.45	3.54	2.444e+05	64.00	5.55	0.12	0.12	0.02	20,24,27
653	3.45	3.29	3.36	2.444e+05	64.00	5.28	0.12	0.14	0.02	20,24,27
656	3.27	3.43	3.36	2.333e+05	64.00	5.28	0.06	0.15	0.02	18,20,27
658	3.37	3.61	3.47	2.397e+05	64.00	5.44	0.09	0.17	9.29e-03	18,20,27
660	3.70	3.84	3.62	2.590e+05	64.00	5.68	0.11	0.20	8.38e-03	40,20,30
662	4.06	4.06	3.94	2.797e+05	64.00	6.18	0.19	0.27	0.01	24,20,27
664	4.06	3.51	3.41	2.797e+05	64.00	5.35	0.19	0.45	0.02	24,32,34
666	3.60	3.51	3.41	2.534e+05	64.00	5.35	0.12	0.45	0.02	16,32,34
930	3.70	3.84	3.62	2.590e+05	64.00	5.68	0.11	0.20	8.38e-03	40,20,30
931	4.06	4.06	3.94	2.797e+05	64.00	6.18	0.19	0.27	0.01	24,20,27
932	4.06	3.51	3.41	2.797e+05	64.00	5.35	0.19	0.45	0.02	24,32,34
933	3.60	3.51	3.41	2.534e+05	64.00	5.35	0.12	0.45	0.02	16,32,34
1042	3.45	3.29	3.36	2.444e+05	64.00	5.28	0.12	0.14	0.02	20,24,27
1043	3.27	3.43	3.36	2.333e+05	64.00	5.28	0.06	0.15	0.02	18,20,27
1044	3.37	3.61	3.47	2.397e+05	64.00	5.44	0.09	0.17	9.29e-03	18,20,27

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				2.333e+05	64.00	5.28			
	4.06	4.06	3.94	2.797e+05	64.00	6.18	0.19	0.45	0.02

Setto	Mat.	Spessore	Stato
		cm	
50	mattoni pieni e malta di calce	37.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
684	0.81	0.78	0.72	9.877e+05	261.50	1.05	0.13	0.15	0.09	23,21,34
723	0.81	0.78	0.72	9.877e+05	261.50	1.05	0.13	0.15	0.09	23,21,34
733	0.81	0.78	0.72	9.877e+05	261.50	1.05	0.13	0.15	0.09	23,21,34
743	0.81	0.78	0.72	9.877e+05	261.50	1.05	0.13	0.15	0.09	23,21,34
752	0.81	0.78	0.72	9.877e+05	261.50	1.05	0.13	0.15	0.09	23,21,34
839	0.81	0.78	0.72	9.877e+05	261.50	1.05	0.13	0.15	0.09	23,21,34
2264	0.23	0.25	0.22	2.929e+05	261.50	0.32	0.10	0.16	0.02	21,33,28
2274	0.81	0.73	0.72	9.877e+05	261.50	1.05	0.13	0.16	0.09	23,21,34
2281	0.62	0.59	0.55	7.666e+05	261.50	0.79	0.10	0.17	0.09	15,21,34
2282	0.62	0.43	0.55	7.666e+05	261.50	0.79	0.10	0.17	0.09	15,21,34
2283	0.23	0.43	0.40	2.929e+05	261.50	0.58	0.10	0.17	0.06	21,21,34
2455	0.23	0.43	0.40	2.929e+05	261.50	0.58	0.10	0.17	0.06	21,21,34
2456	0.23	0.25	0.22	2.929e+05	261.50	0.32	0.10	0.16	0.02	21,33,28
2459	0.81	0.73	0.72	9.877e+05	261.50	1.05	0.13	0.16	0.09	23,21,34
2460	0.62	0.59	0.55	7.666e+05	261.50	0.79	0.10	0.17	0.09	15,21,34
2461	0.62	0.43	0.55	7.666e+05	261.50	0.79	0.10	0.17	0.09	15,21,34
2462	0.23	0.43	0.40	2.929e+05	261.50	0.58	0.10	0.17	0.06	21,21,34
2463	0.23	0.25	0.22	2.929e+05	261.50	0.32	0.10	0.16	0.02	21,33,28
2464	0.81	0.73	0.72	9.877e+05	261.50	1.05	0.13	0.16	0.09	23,21,34
2465	0.62	0.59	0.55	7.666e+05	261.50	0.79	0.10	0.17	0.09	15,21,34
2466	0.62	0.43	0.55	7.666e+05	261.50	0.79	0.10	0.17	0.09	15,21,34
2467	0.23	0.43	0.40	2.929e+05	261.50	0.58	0.10	0.17	0.06	21,21,34
2468	0.23	0.25	0.22	2.929e+05	261.50	0.32	0.10	0.16	0.02	21,33,28
2469	0.81	0.73	0.72	9.877e+05	261.50	1.05	0.13	0.16	0.09	23,21,34
2470	0.62	0.59	0.55	7.666e+05	261.50	0.79	0.10	0.17	0.09	15,21,34
2471	0.62	0.43	0.55	7.666e+05	261.50	0.79	0.10	0.17	0.09	15,21,34
2472	0.23	0.43	0.40	2.929e+05	261.50	0.58	0.10	0.17	0.06	21,21,34
2473	0.23	0.25	0.22	2.929e+05	261.50	0.32	0.10	0.16	0.02	21,33,28
2474	0.81	0.73	0.72	9.877e+05	261.50	1.05	0.13	0.16	0.09	23,21,34
2475	0.62	0.59	0.55	7.666e+05	261.50	0.79	0.10	0.17	0.09	15,21,34
2476	0.62	0.43	0.55	7.666e+05	261.50	0.79	0.10	0.17	0.09	15,21,34
2477	0.23	0.43	0.40	2.929e+05	261.50	0.58	0.10	0.17	0.06	21,21,34
2478	0.23	0.25	0.22	2.929e+05	261.50	0.32	0.10	0.16	0.02	21,33,28
2479	0.81	0.73	0.72	9.877e+05	261.50	1.05	0.13	0.16	0.09	23,21,34
2480	0.62	0.59	0.55	7.666e+05	261.50	0.79	0.10	0.17	0.09	15,21,34
2481	0.62	0.43	0.55	7.666e+05	261.50	0.79	0.10	0.17	0.09	15,21,34

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
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			2.929e+05	261.50	0.32			
0.81	0.78	0.72	9.877e+05	261.50	1.05	0.13	0.17	0.09

Setto	Mat.	Spessore	Stato
		cm	
51	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
666	2.62	2.81	2.72	1.928e+05	64.00	4.26	0.03	0.69	0.03	17,20,30
668	2.54	2.73	2.72	1.875e+05	64.00	4.26	0.04	0.82	0.03	21,20,30
670	2.54	2.73	2.63	1.875e+05	64.00	4.12	0.04	0.82	0.02	21,20,27
933	2.62	2.81	2.72	1.928e+05	64.00	4.26	0.03	0.69	0.03	17,20,30
934	2.54	2.73	2.72	1.875e+05	64.00	4.26	0.04	0.82	0.03	21,20,30
935	2.54	2.73	2.63	1.875e+05	64.00	4.12	0.04	0.82	0.02	21,20,27

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				1.875e+05	64.00	4.12			
	2.62	2.81	2.72	1.928e+05	64.00	4.26	0.04	0.82	0.03

Setto	Mat.	Spessore	Stato
		cm	
52	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
19	4.27	4.27	4.13	7.729e+05	104.29	6.47	0.02	0.06	0.14	25,25,29
585	4.27	4.27	4.13	7.729e+05	104.29	6.47	0.02	0.06	0.14	25,25,29
592	4.27	4.27	4.13	7.729e+05	104.29	6.47	0.02	0.06	0.14	25,25,29
967	4.27	4.27	4.13	7.729e+05	104.29	6.47	0.02	0.06	0.14	25,25,29
968	4.45	4.16	4.26	7.996e+05	104.29	6.69	0.02	0.13	0.11	25,19,33
969	4.40	4.22	4.37	7.916e+05	104.29	6.85	0.03	0.16	0.07	25,19,33
970	4.37	4.31	4.35	7.871e+05	104.29	6.83	0.05	0.21	0.05	41,23,29
971	4.41	4.41	4.36	7.930e+05	104.29	6.85	0.10	0.26	0.02	15,23,29
972	4.41	4.07	4.01	7.930e+05	104.29	6.29	0.10	0.33	0.03	15,23,29
973	4.07	4.07	4.01	7.434e+05	104.29	6.29	0.06	0.33	0.03	15,23,29
976	4.27	4.27	4.13	7.729e+05	104.29	6.47	0.02	0.06	0.14	25,25,29
977	4.45	4.16	4.26	7.996e+05	104.29	6.69	0.02	0.13	0.11	25,19,33
978	4.40	4.22	4.37	7.916e+05	104.29	6.85	0.03	0.16	0.07	25,19,33
979	4.37	4.31	4.35	7.871e+05	104.29	6.83	0.05	0.21	0.05	41,23,29
980	4.41	4.41	4.36	7.930e+05	104.29	6.85	0.10	0.26	0.02	15,23,29
981	4.41	4.07	4.01	7.930e+05	104.29	6.29	0.10	0.33	0.03	15,23,29
982	4.07	4.07	4.01	7.434e+05	104.29	6.29	0.06	0.33	0.03	15,23,29
985	4.27	4.27	4.13	7.729e+05	104.29	6.47	0.02	0.06	0.14	25,25,29
986	4.45	4.16	4.26	7.996e+05	104.29	6.69	0.02	0.13	0.11	25,19,33
987	4.40	4.22	4.37	7.916e+05	104.29	6.85	0.03	0.16	0.07	25,19,33
988	4.37	4.31	4.35	7.871e+05	104.29	6.83	0.05	0.21	0.05	41,23,29
989	4.41	4.41	4.36	7.930e+05	104.29	6.85	0.10	0.26	0.02	15,23,29
990	4.41	4.07	4.01	7.930e+05	104.29	6.29	0.10	0.33	0.03	15,23,29
991	4.07	4.07	4.01	7.434e+05	104.29	6.29	0.06	0.33	0.03	15,23,29

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				7.434e+05	104.29	6.29			
	4.45	4.41	4.37	7.996e+05	104.29	6.85	0.10	0.33	0.14

Setto	Mat.	Spessore	Stato
		cm	
53	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
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973	3.38	3.50	3.44	6.376e+05	104.29	5.40	0.05	0.34	0.05	14,23,33
974	3.33	3.50	3.28	6.292e+05	104.29	5.15	0.06	0.34	0.07	20,23,33
975	3.33	3.34	3.28	6.292e+05	104.29	5.15	0.06	0.22	0.07	20,23,33
982	3.38	3.50	3.44	6.376e+05	104.29	5.40	0.05	0.34	0.05	14,23,33
983	3.33	3.50	3.28	6.292e+05	104.29	5.15	0.06	0.34	0.07	20,23,33
984	3.33	3.34	3.28	6.292e+05	104.29	5.15	0.06	0.22	0.07	20,23,33
991	3.38	3.50	3.44	6.376e+05	104.29	5.40	0.05	0.34	0.05	14,23,33
992	3.33	3.50	3.28	6.292e+05	104.29	5.15	0.06	0.34	0.07	20,23,33
993	3.33	3.34	3.28	6.292e+05	104.29	5.15	0.06	0.22	0.07	20,23,33

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				6.292e+05	104.29	5.15			
	3.38	3.50	3.44	6.376e+05	104.29	5.40	0.06	0.34	0.07

Setto	Mat.	Spessore	Stato
		cm	
56	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
20	4.34	4.31	4.09	7.367e+05	101.14	6.42	0.05	0.03	0.11	23,24,29
557	4.34	4.31	4.09	7.367e+05	101.14	6.42	0.05	0.03	0.11	23,24,29
564	4.34	4.31	4.09	7.367e+05	101.14	6.42	0.05	0.03	0.11	23,24,29
1012	4.34	4.03	4.09	7.367e+05	104.29	6.42	0.05	0.05	0.11	23,25,29
1013	4.41	4.39	4.18	7.934e+05	104.29	6.55	0.04	0.06	0.09	23,24,29
1014	4.25	4.08	4.23	7.706e+05	104.29	6.64	0.02	0.09	0.06	23,25,29
1015	4.07	4.07	4.15	7.433e+05	104.29	6.51	0.04	0.13	0.04	21,25,29
1016	4.06	4.06	4.10	7.431e+05	104.29	6.43	0.08	0.16	0.02	25,25,29
1017	4.06	3.72	3.62	7.431e+05	104.29	5.67	0.08	0.25	0.02	25,25,28
1018	3.72	3.72	3.62	6.915e+05	104.29	5.67	0.03	0.25	0.02	25,25,28
1021	4.34	4.03	4.09	7.367e+05	104.29	6.42	0.05	0.05	0.11	23,25,29
1023	4.41	4.39	4.18	7.934e+05	104.29	6.55	0.04	0.06	0.09	23,24,29
1024	4.25	4.08	4.23	7.706e+05	104.29	6.64	0.02	0.09	0.06	23,25,29
1025	4.07	4.07	4.15	7.433e+05	104.29	6.51	0.04	0.13	0.04	21,25,29
1026	4.06	4.06	4.10	7.431e+05	104.29	6.43	0.08	0.16	0.02	25,25,29
1027	4.06	3.72	3.62	7.431e+05	104.29	5.67	0.08	0.25	0.02	25,25,28
1028	3.72	3.72	3.62	6.915e+05	104.29	5.67	0.03	0.25	0.02	25,25,28
1031	4.34	4.03	4.09	7.367e+05	104.29	6.42	0.05	0.05	0.11	23,25,29
1032	4.41	4.39	4.18	7.934e+05	104.29	6.55	0.04	0.06	0.09	23,24,29
1033	4.25	4.08	4.23	7.706e+05	104.29	6.64	0.02	0.09	0.06	23,25,29
1034	4.07	4.07	4.15	7.433e+05	104.29	6.51	0.04	0.13	0.04	21,25,29
1035	4.06	4.06	4.10	7.431e+05	104.29	6.43	0.08	0.16	0.02	25,25,29
1036	4.06	3.72	3.62	7.431e+05	104.29	5.67	0.08	0.25	0.02	25,25,28
1037	3.72	3.72	3.62	6.915e+05	104.29	5.67	0.03	0.25	0.02	25,25,28
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				6.915e+05	101.14	5.67				
	4.41	4.39	4.23	7.934e+05	104.29	6.64	0.08	0.25	0.11	

Setto	Mat.	Spessore	Stato
		cm	
57	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1018	3.12	3.26	3.23	9.319e+05	104.29	5.06	0.05	0.37	0.05	16,25,29
1019	3.08	3.26	3.16	1.063e+06	104.29	4.96	0.06	0.37	0.07	11,25,29
1020	3.08	3.19	3.16	1.063e+06	122.76	4.96	0.06	0.22	0.07	11,17,29
1028	3.12	3.26	3.23	9.319e+05	104.29	5.06	0.05	0.37	0.05	16,25,29
1029	3.09	3.26	3.18	1.130e+06	104.29	4.98	0.05	0.37	0.07	11,25,29
1030	3.09	3.20	3.18	1.130e+06	118.14	4.98	0.05	0.26	0.07	11,17,29
1037	3.12	3.26	3.23	9.319e+05	104.29	5.06	0.05	0.37	0.05	16,25,29
1038	3.09	3.26	3.18	1.130e+06	104.29	4.98	0.05	0.37	0.07	11,25,29
1039	3.09	3.20	3.18	1.130e+06	118.14	4.98	0.05	0.26	0.07	11,17,29
2425	3.08	3.20	3.16	1.063e+06	118.14	4.96	0.06	0.26	0.07	11,17,29

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
	3.12	3.26	3.23	9.319e+05 1.130e+06	104.29 122.76	4.96 5.06	0.06	0.37	0.07

Setto	Mat.	Spessore	Stato
		cm	
59	Tamponatura 1100 daN/mc per elemento pannello	20.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
28	1.53	1.61	1.52	1.483e+06	323.00	1.45	0.14	0.15	6.33e-03	23,26,24
29	1.53	1.61	1.52	1.483e+06	323.00	1.45	0.14	0.15	6.33e-03	23,26,24
481	1.51	1.59	1.58	1.465e+06	323.00	1.51	0.10	0.18	0.04	16,21,37
727	1.52	1.58	1.47	1.469e+06	323.00	1.41	0.14	0.17	0.03	23,21,24
728	1.48	1.55	1.45	1.439e+06	323.00	1.39	0.14	0.17	0.04	23,21,20
729	1.46	1.53	1.52	1.418e+06	323.00	1.45	0.13	0.18	0.05	23,21,37
730	1.44	1.53	1.53	1.398e+06	323.00	1.46	0.12	0.18	0.06	20,21,37
737	1.45	1.54	1.53	1.411e+06	323.00	1.46	0.11	0.18	0.06	20,21,37
738	1.51	1.59	1.58	1.465e+06	323.00	1.51	0.10	0.18	0.04	16,21,37
766	1.52	1.60	1.50	1.469e+06	323.00	1.44	0.14	0.16	0.02	23,26,24
1047	1.52	1.60	1.50	1.469e+06	323.00	1.44	0.14	0.16	0.02	23,26,24
1048	1.52	1.60	1.50	1.469e+06	323.00	1.44	0.14	0.16	0.02	23,26,24
1049	1.53	1.61	1.52	1.483e+06	323.00	1.45	0.14	0.15	6.33e-03	23,26,24
1050	1.52	1.58	1.47	1.469e+06	323.00	1.41	0.14	0.17	0.03	23,21,24
1051	1.52	1.58	1.47	1.469e+06	323.00	1.41	0.14	0.17	0.03	23,21,24
1052	1.48	1.55	1.45	1.439e+06	323.00	1.39	0.14	0.17	0.04	23,21,20
1053	1.48	1.55	1.45	1.439e+06	323.00	1.39	0.14	0.17	0.04	23,21,20
1054	1.46	1.53	1.52	1.418e+06	323.00	1.45	0.13	0.18	0.05	23,21,37
1055	1.46	1.53	1.52	1.418e+06	323.00	1.45	0.13	0.18	0.05	23,21,37
1056	1.44	1.53	1.53	1.398e+06	323.00	1.46	0.12	0.18	0.06	20,21,37
1057	1.44	1.53	1.53	1.398e+06	323.00	1.46	0.12	0.18	0.06	20,21,37
1058	1.45	1.54	1.53	1.411e+06	323.00	1.46	0.11	0.18	0.06	20,21,37
1059	1.45	1.54	1.53	1.411e+06	323.00	1.46	0.11	0.18	0.06	20,21,37
1060	1.51	1.59	1.58	1.465e+06	323.00	1.51	0.10	0.18	0.04	16,21,37
1061	1.51	1.59	1.58	1.465e+06	323.00	1.51	0.10	0.18	0.04	16,21,37
1066	1.52	1.60	1.50	1.469e+06	323.00	1.44	0.14	0.16	0.02	23,26,24
1067	1.53	1.61	1.52	1.483e+06	323.00	1.45	0.14	0.15	6.33e-03	23,26,24
1068	1.52	1.58	1.47	1.469e+06	323.00	1.41	0.14	0.17	0.03	23,21,24
1069	1.48	1.55	1.45	1.439e+06	323.00	1.39	0.14	0.17	0.04	23,21,20
1070	1.46	1.53	1.52	1.418e+06	323.00	1.45	0.13	0.18	0.05	23,21,37
1071	1.44	1.53	1.53	1.398e+06	323.00	1.46	0.12	0.18	0.06	20,21,37
1072	1.45	1.54	1.53	1.411e+06	323.00	1.46	0.11	0.18	0.06	20,21,37
1073	1.51	1.59	1.58	1.465e+06	323.00	1.51	0.10	0.18	0.04	16,21,37
1076	1.52	1.60	1.50	1.469e+06	323.00	1.44	0.14	0.16	0.02	23,26,24
1077	1.53	1.61	1.52	1.483e+06	323.00	1.45	0.14	0.15	6.33e-03	23,26,24
1078	1.52	1.58	1.47	1.469e+06	323.00	1.41	0.14	0.17	0.03	23,21,24
1079	1.48	1.55	1.45	1.439e+06	323.00	1.39	0.14	0.17	0.04	23,21,20
1080	1.46	1.53	1.52	1.418e+06	323.00	1.45	0.13	0.18	0.05	23,21,37
1081	1.44	1.53	1.53	1.398e+06	323.00	1.46	0.12	0.18	0.06	20,21,37
1082	1.45	1.54	1.53	1.411e+06	323.00	1.46	0.11	0.18	0.06	20,21,37
1083	1.51	1.59	1.58	1.465e+06	323.00	1.51	0.10	0.18	0.04	16,21,37
1086	1.52	1.60	1.50	1.469e+06	323.00	1.44	0.14	0.16	0.02	23,26,24
1087	1.53	1.61	1.52	1.483e+06	323.00	1.45	0.14	0.15	6.33e-03	23,26,24
1088	1.52	1.58	1.47	1.469e+06	323.00	1.41	0.14	0.17	0.03	23,21,24
1089	1.48	1.55	1.45	1.439e+06	323.00	1.39	0.14	0.17	0.04	23,21,20
1090	1.46	1.53	1.52	1.418e+06	323.00	1.45	0.13	0.18	0.05	23,21,37
1091	1.44	1.53	1.53	1.398e+06	323.00	1.46	0.12	0.18	0.06	20,21,37
1092	1.45	1.54	1.53	1.411e+06	323.00	1.46	0.11	0.18	0.06	20,21,37
1093	1.51	1.59	1.58	1.465e+06	323.00	1.51	0.10	0.18	0.04	16,21,37
1096	1.52	1.60	1.50	1.469e+06	323.00	1.44	0.14	0.16	0.02	23,26,24
1097	1.53	1.61	1.52	1.483e+06	323.00	1.45	0.14	0.15	6.33e-03	23,26,24
1098	1.52	1.58	1.47	1.469e+06	323.00	1.41	0.14	0.17	0.03	23,21,24
1099	1.48	1.55	1.45	1.439e+06	323.00	1.39	0.14	0.17	0.04	23,21,20
1100	1.46	1.53	1.52	1.418e+06	323.00	1.45	0.13	0.18	0.05	23,21,37
1101	1.44	1.53	1.53	1.398e+06	323.00	1.46	0.12	0.18	0.06	20,21,37
1102	1.45	1.54	1.53	1.411e+06	323.00	1.46	0.11	0.18	0.06	20,21,37

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
	1.53	1.61	1.58	1.398e+06 1.483e+06	323.00 323.00	1.39 1.51	0.14	0.18	0.06

Setto	Mat.	Spessore	Stato
		cm	
60	Tamponatura 1100 daN/mc per elemento pannello	20.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
481	1.64	1.70	1.61	1.581e+06	323.00	1.54	0.09	0.17	0.03	42,21,12
738	1.64	1.70	1.61	1.581e+06	323.00	1.54	0.09	0.17	0.03	42,21,12
739	1.64	1.97	1.90	1.581e+06	323.00	1.82	0.09	0.20	0.12	42,21,15
740	1.95	1.97	1.90	1.849e+06	323.00	1.82	0.03	0.20	0.12	26,21,15
921	1.64	1.97	1.90	1.581e+06	323.00	1.82	0.09	0.20	0.12	42,21,15
1022	1.95	1.97	1.90	1.849e+06	323.00	1.82	0.03	0.20	0.12	26,21,15
1060	1.64	1.70	1.61	1.581e+06	323.00	1.54	0.09	0.17	0.03	42,21,12
1061	1.64	1.70	1.61	1.581e+06	323.00	1.54	0.09	0.17	0.03	42,21,12
1062	1.64	1.97	1.90	1.581e+06	323.00	1.82	0.09	0.20	0.12	42,21,15
1063	1.64	1.97	1.90	1.581e+06	323.00	1.82	0.09	0.20	0.12	42,21,15
1064	1.95	1.97	1.90	1.849e+06	323.00	1.82	0.03	0.20	0.12	26,21,15
1065	1.95	1.97	1.90	1.849e+06	323.00	1.82	0.03	0.20	0.12	26,21,15
1073	1.64	1.70	1.61	1.581e+06	323.00	1.54	0.09	0.17	0.03	42,21,12
1074	1.64	1.97	1.90	1.581e+06	323.00	1.82	0.09	0.20	0.12	42,21,15
1075	1.95	1.97	1.90	1.849e+06	323.00	1.82	0.03	0.20	0.12	26,21,15
1083	1.64	1.70	1.61	1.581e+06	323.00	1.54	0.09	0.17	0.03	42,21,12
1084	1.64	1.97	1.90	1.581e+06	323.00	1.82	0.09	0.20	0.12	42,21,15
1085	1.95	1.97	1.90	1.849e+06	323.00	1.82	0.03	0.20	0.12	26,21,15
1093	1.64	1.70	1.61	1.581e+06	323.00	1.54	0.09	0.17	0.03	42,21,12
1094	1.64	1.97	1.90	1.581e+06	323.00	1.82	0.09	0.20	0.12	42,21,15
1095	1.95	1.97	1.90	1.849e+06	323.00	1.82	0.03	0.20	0.12	26,21,15
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				1.581e+06	323.00	1.54				
	1.95	1.97	1.90	1.849e+06	323.00	1.82	0.09	0.20	0.12	

Setto	Mat.	Spessore	Stato
		cm	
61	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
37	3.34	3.49	3.29	2.564e+05	67.00	5.72	0.06	0.03	0.01	16,23,36
38	3.34	3.49	3.29	2.564e+05	67.00	5.72	0.06	0.03	0.01	16,23,36
1103	3.34	3.55	3.29	2.564e+05	67.00	5.72	0.06	0.03	0.01	16,26,36
1104	3.34	3.55	3.29	2.564e+05	67.00	5.72	0.06	0.03	0.01	16,26,36
1105	3.32	3.53	3.72	2.550e+05	67.00	6.47	0.06	0.04	9.02e-03	16,26,37
1106	3.32	3.53	3.72	2.550e+05	67.00	6.47	0.06	0.04	9.02e-03	16,26,37
1107	3.23	3.54	3.64	2.493e+05	67.00	6.33	0.05	0.04	4.48e-03	16,26,37
1108	3.23	3.54	3.64	2.493e+05	67.00	6.33	0.05	0.04	4.48e-03	16,26,37
1109	3.50	3.50	3.13	2.663e+05	67.00	5.45	0.08	0.05	4.68e-03	26,26,23
1110	3.50	3.50	3.13	2.663e+05	67.00	5.45	0.08	0.05	4.68e-03	26,26,23
1111	3.50	3.07	2.88	2.663e+05	67.00	5.00	0.08	0.09	9.73e-03	26,26,42
1112	3.50	3.07	2.88	2.663e+05	67.00	5.00	0.08	0.09	9.73e-03	26,26,42
1113	2.37	3.07	2.61	1.906e+05	67.00	4.54	0.13	0.09	0.02	24,26,26
1114	2.37	3.07	2.61	1.906e+05	67.00	4.54	0.13	0.09	0.02	24,26,26
1115	2.37	2.48	2.61	1.906e+05	67.00	4.54	0.13	0.08	0.02	24,42,26
1116	2.37	2.48	2.61	1.906e+05	67.00	4.54	0.13	0.08	0.02	24,42,26
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				1.906e+05	67.00	4.54				
	3.50	3.55	3.72	2.663e+05	67.00	6.47	0.13	0.09	0.02	

Setto	Mat.	Spessore	Stato
		cm	
62	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
1115	2.47	2.54	2.54	1.979e+05	67.00	4.41	0.13	0.05	0.04	42,39,26
1116	2.47	2.54	2.54	1.979e+05	67.00	4.41	0.13	0.05	0.04	42,39,26
1117	2.78	2.83	2.76	2.193e+05	67.00	4.80	0.18	0.14	0.09	42,39,16
1118	2.78	2.83	2.76	2.193e+05	67.00	4.80	0.18	0.14	0.09	42,39,16
1119	2.78	2.83	2.76	2.193e+05	67.00	4.80	0.18	0.14	0.09	42,39,16
1120	2.78	2.83	2.76	2.193e+05	67.00	4.80	0.18	0.14	0.09	42,39,16

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
	2.78	2.83	2.76	1.979e+05	67.00	4.41			
				2.193e+05	67.00	4.80	0.18	0.14	0.09

Setto	Mat.	Spessore	Stato
		cm	
63	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
32	3.11	3.14	3.15	9.958e+05	136.00	5.47	0.04	0.07	0.04	16,23,36
39	3.11	3.14	3.15	9.958e+05	136.00	5.47	0.04	0.07	0.04	16,23,36
150	3.11	3.14	3.15	9.958e+05	136.00	5.47	0.04	0.07	0.04	16,23,36
157	3.11	3.14	3.15	9.958e+05	136.00	5.47	0.04	0.07	0.04	16,23,36
1121	2.16	2.13	2.02	7.234e+05	136.00	3.51	0.08	0.05	6.05e-03	17,19,36
1124	3.11	3.12	3.15	9.958e+05	136.00	5.47	0.04	0.07	0.04	16,23,36
1130	3.28	3.08	3.19	1.040e+06	136.00	5.55	0.04	0.08	0.02	17,23,37
1131	3.12	3.05	3.11	9.969e+05	136.00	5.41	0.04	0.09	0.02	17,23,13
1132	2.96	3.01	3.11	9.548e+05	136.00	5.41	0.07	0.10	0.02	20,23,13
1133	2.96	3.01	2.90	9.548e+05	136.00	5.04	0.07	0.10	0.02	20,23,42
1139	2.16	2.67	2.54	7.234e+05	136.00	4.42	0.08	0.08	9.64e-03	17,23,36
1140	2.16	2.13	2.02	7.234e+05	136.00	3.51	0.08	0.05	6.05e-03	17,19,36
1143	2.96	3.01	2.90	9.548e+05	136.00	5.04	0.07	0.10	0.02	20,23,42
1144	2.16	2.67	2.54	7.234e+05	136.00	4.42	0.08	0.08	9.64e-03	17,23,36
1145	2.16	2.13	2.02	7.234e+05	136.00	3.51	0.08	0.05	6.05e-03	17,19,36
1149	3.11	3.12	3.15	9.958e+05	136.00	5.47	0.04	0.07	0.04	16,23,36
1150	3.11	3.12	3.15	9.958e+05	136.00	5.47	0.04	0.07	0.04	16,23,36
1152	3.28	3.08	3.19	1.040e+06	136.00	5.55	0.04	0.08	0.02	17,23,37
1153	3.28	3.08	3.19	1.040e+06	136.00	5.55	0.04	0.08	0.02	17,23,37
1154	3.12	3.05	3.11	9.969e+05	136.00	5.41	0.04	0.09	0.02	17,23,13
1155	3.12	3.05	3.11	9.969e+05	136.00	5.41	0.04	0.09	0.02	17,23,13
1156	2.96	3.01	3.11	9.548e+05	136.00	5.41	0.07	0.10	0.02	20,23,13
1157	2.96	3.01	3.11	9.548e+05	136.00	5.41	0.07	0.10	0.02	20,23,13
1158	3.28	3.08	3.19	1.040e+06	136.00	5.55	0.04	0.08	0.02	17,23,37
1159	2.96	3.01	2.90	9.548e+05	136.00	5.04	0.07	0.10	0.02	20,23,42
1160	3.12	3.05	3.11	9.969e+05	136.00	5.41	0.04	0.09	0.02	17,23,13
1161	2.16	2.67	2.54	7.234e+05	136.00	4.42	0.08	0.08	9.64e-03	17,23,36
1162	2.96	3.01	3.11	9.548e+05	136.00	5.41	0.07	0.10	0.02	20,23,13
1163	2.16	2.13	2.02	7.234e+05	136.00	3.51	0.08	0.05	6.05e-03	17,19,36
1164	2.96	3.01	2.90	9.548e+05	136.00	5.04	0.07	0.10	0.02	20,23,42
1166	2.16	2.67	2.54	7.234e+05	136.00	4.42	0.08	0.08	9.64e-03	17,23,36
1168	3.11	3.12	3.15	9.958e+05	136.00	5.47	0.04	0.07	0.04	16,23,36

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
	3.28	3.14	3.19	7.234e+05	136.00	3.51			
				1.040e+06	136.00	5.55	0.08	0.10	0.04

Setto	Mat.	Spessore	Stato
		cm	
64	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
1121	1.84	1.71	1.84	6.257e+05	136.00	3.20	0.06	0.02	2.72e-03	39,16,13
1122	1.84	1.79	1.67	6.257e+05	136.00	2.91	0.06	0.03	0.01	39,17,34
1123	1.77	1.79	1.67	6.052e+05	136.00	2.91	0.06	0.03	0.01	39,17,34
1140	1.84	1.71	1.84	6.257e+05	136.00	3.20	0.06	0.02	2.72e-03	39,16,13

1141	1.84	1.79	1.67	6.257e+05	136.00	2.91	0.06	0.03	0.01	39,17,34
1142	1.77	1.79	1.67	6.052e+05	136.00	2.91	0.06	0.03	0.01	39,17,34
1145	1.84	1.71	1.84	6.257e+05	136.00	3.20	0.06	0.02	2.72e-03	39,16,13
1146	1.84	1.79	1.67	6.257e+05	136.00	2.91	0.06	0.03	0.01	39,17,34
1147	1.77	1.79	1.67	6.052e+05	136.00	2.91	0.06	0.03	0.01	39,17,34
1163	1.84	1.71	1.84	6.257e+05	136.00	3.20	0.06	0.02	2.72e-03	39,16,13
1165	1.84	1.79	1.67	6.257e+05	136.00	2.91	0.06	0.03	0.01	39,17,34
1167	1.77	1.79	1.67	6.052e+05	136.00	2.91	0.06	0.03	0.01	39,17,34

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	1.84	1.79	1.84	6.052e+05	136.00	2.91				
				6.257e+05	136.00	3.20	0.06	0.03	0.01	

Setto	Mat.	Spessore	Stato
		cm	
67	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1179	1.71	1.79	1.71	6.423e+05	142.40	2.97	0.06	0.06	0.13	17,16,17
1180	1.71	1.79	1.71	6.423e+05	142.40	2.97	0.06	0.06	0.13	17,16,17
1181	1.71	1.79	1.71	6.423e+05	142.40	2.97	0.06	0.06	0.13	17,16,17
1182	1.71	1.79	1.71	6.423e+05	142.40	2.97	0.06	0.06	0.13	17,16,17
1192	1.73	1.80	1.71	7.343e+05	151.60	2.97	0.06	0.07	0.13	17,16,17
1193	1.73	1.80	1.71	7.343e+05	151.60	2.97	0.06	0.07	0.13	17,16,17
1201	1.73	1.80	1.73	7.343e+05	151.60	3.00	0.06	0.07	0.12	17,16,17
1202	1.73	1.80	1.73	7.343e+05	151.60	3.00	0.06	0.07	0.12	17,16,17

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				6.423e+05	142.40	2.97				
	1.73	1.80	1.73	7.343e+05	151.60	3.00	0.06	0.07	0.13	

Setto	Mat.	Spessore	Stato
		cm	
70	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1	3.02	2.94	2.94	1.119e+07	462.00	5.11	0.06	0.04	0.02	36,37,14
33	3.02	2.94	2.94	1.119e+07	462.00	5.11	0.06	0.04	0.02	36,37,14
231	3.02	2.94	2.94	1.119e+07	462.00	5.11	0.06	0.04	0.02	36,37,14
238	3.02	2.94	2.94	1.119e+07	462.00	5.11	0.06	0.04	0.02	36,37,14
245	3.02	2.94	2.94	1.119e+07	462.00	5.11	0.06	0.04	0.02	36,37,14
252	3.02	2.94	2.94	1.119e+07	462.00	5.11	0.06	0.04	0.02	36,37,14
259	3.02	2.94	2.94	1.119e+07	462.00	5.11	0.06	0.04	0.02	36,37,14
266	3.02	2.94	2.94	1.119e+07	462.00	5.11	0.06	0.04	0.02	36,37,14
273	3.02	2.94	2.94	1.119e+07	462.00	5.11	0.06	0.04	0.02	36,37,14
280	3.02	2.94	2.94	1.119e+07	462.00	5.11	0.06	0.04	0.02	36,37,14
1295	3.02	2.94	2.91	1.119e+07	462.00	5.06	0.06	0.04	0.03	36,37,14
1296	2.99	2.78	2.91	1.109e+07	462.00	5.06	0.04	0.04	0.03	36,37,14
1297	2.78	2.67	2.77	1.044e+07	462.00	4.81	0.03	0.04	0.02	37,37,16
1298	2.67	2.67	2.58	1.008e+07	462.00	4.48	0.03	0.04	0.03	37,37,37
1299	2.51	2.58	2.58	9.542e+06	462.00	4.48	0.03	0.04	0.03	36,37,37
1300	2.23	2.31	2.48	5.974e+06	385.00	4.32	0.03	0.04	0.02	18,36,11
1301	2.23	2.31	2.23	5.974e+06	385.00	3.87	0.03	0.04	0.01	18,36,14
1304	3.02	2.94	2.91	1.119e+07	462.00	5.06	0.06	0.04	0.03	36,37,14
1305	2.99	2.78	2.91	1.109e+07	462.00	5.06	0.04	0.04	0.03	36,37,14
1306	2.78	2.67	2.77	1.044e+07	462.00	4.81	0.03	0.04	0.02	37,37,16
1307	2.67	2.67	2.58	1.008e+07	462.00	4.48	0.03	0.04	0.03	37,37,37
1308	2.51	2.58	2.58	9.542e+06	462.00	4.48	0.03	0.04	0.03	36,37,37
1309	2.23	2.31	2.48	5.974e+06	385.00	4.32	0.03	0.04	0.02	18,36,11
1310	2.23	2.31	2.23	5.974e+06	385.00	3.87	0.03	0.04	0.01	18,36,14
1313	3.02	2.94	2.91	1.119e+07	462.00	5.06	0.06	0.04	0.03	36,37,14
1314	2.99	2.78	2.91	1.109e+07	462.00	5.06	0.04	0.04	0.03	36,37,14
1315	2.78	2.67	2.77	1.044e+07	462.00	4.81	0.03	0.04	0.02	37,37,16
1316	2.67	2.67	2.58	1.008e+07	462.00	4.48	0.03	0.04	0.03	37,37,37

1317	2.51	2.58	2.58	9.542e+06	462.00	4.48	0.03	0.04	0.03	36,37,37
1318	2.23	2.31	2.48	5.974e+06	385.00	4.32	0.03	0.04	0.02	18,36,11
1319	2.23	2.31	2.23	5.974e+06	385.00	3.87	0.03	0.04	0.01	18,36,14
1322	3.02	2.94	2.91	1.119e+07	462.00	5.06	0.06	0.04	0.03	36,37,14
1323	2.99	2.78	2.91	1.109e+07	462.00	5.06	0.04	0.04	0.03	36,37,14
1324	2.78	2.67	2.77	1.044e+07	462.00	4.81	0.03	0.04	0.02	37,37,16
1325	2.67	2.67	2.58	1.008e+07	462.00	4.48	0.03	0.04	0.03	37,37,37
1326	2.51	2.58	2.58	9.542e+06	462.00	4.48	0.03	0.04	0.03	36,37,37
1327	2.23	2.31	2.48	5.974e+06	385.00	4.32	0.03	0.04	0.02	18,36,11
1328	2.23	2.31	2.23	5.974e+06	385.00	3.87	0.03	0.04	0.01	18,36,14
1331	3.02	2.94	2.91	1.119e+07	462.00	5.06	0.06	0.04	0.03	36,37,14
1332	2.99	2.78	2.91	1.109e+07	462.00	5.06	0.04	0.04	0.03	36,37,14
1333	2.78	2.67	2.77	1.044e+07	462.00	4.81	0.03	0.04	0.02	37,37,16
1334	2.67	2.67	2.58	1.008e+07	462.00	4.48	0.03	0.04	0.03	37,37,37
1335	2.51	2.58	2.58	9.542e+06	462.00	4.48	0.03	0.04	0.03	36,37,37
1336	2.23	2.31	2.48	5.974e+06	385.00	4.32	0.03	0.04	0.02	18,36,11
1337	2.23	2.31	2.23	5.974e+06	385.00	3.87	0.03	0.04	0.01	18,36,14
1340	3.02	2.94	2.91	1.119e+07	462.00	5.06	0.06	0.04	0.03	36,37,14
1341	2.99	2.78	2.91	1.109e+07	462.00	5.06	0.04	0.04	0.03	36,37,14
1342	2.78	2.67	2.77	1.044e+07	462.00	4.81	0.03	0.04	0.02	37,37,16
1343	2.67	2.67	2.58	1.008e+07	462.00	4.48	0.03	0.04	0.03	37,37,37
1344	2.51	2.58	2.58	9.542e+06	462.00	4.48	0.03	0.04	0.03	36,37,37
1345	2.23	2.31	2.48	5.974e+06	385.00	4.32	0.03	0.04	0.02	18,36,11
1346	2.23	2.31	2.23	5.974e+06	385.00	3.87	0.03	0.04	0.01	18,36,14
1349	3.02	2.87	2.91	1.119e+07	462.00	5.06	0.06	0.04	0.03	36,37,14
1350	2.99	2.74	2.91	1.109e+07	462.00	5.06	0.04	0.04	0.03	36,37,14
1351	2.74	2.67	2.77	1.031e+07	462.00	4.81	0.03	0.04	0.02	37,37,16
1352	2.67	2.67	2.58	1.008e+07	462.00	4.48	0.03	0.04	0.03	37,37,37
1353	2.51	2.58	2.58	9.542e+06	462.00	4.48	0.03	0.04	0.03	36,37,37
1354	2.23	2.31	2.48	5.974e+06	385.00	4.32	0.03	0.04	0.02	18,36,11
1355	2.23	2.31	2.23	5.974e+06	385.00	3.87	0.03	0.04	0.01	18,36,14
1358	3.02	2.83	2.87	1.119e+07	462.00	4.99	0.06	0.05	0.03	36,37,14
1359	2.95	2.70	2.87	1.099e+07	462.00	4.99	0.04	0.05	0.03	36,37,14
1360	2.70	2.70	2.80	1.018e+07	462.00	4.87	0.03	0.05	0.02	37,37,16
1361	2.67	2.67	2.58	1.008e+07	462.00	4.48	0.03	0.04	0.03	37,37,37
1362	2.51	2.58	2.58	9.542e+06	462.00	4.48	0.03	0.04	0.03	36,37,37
1363	2.51	2.40	2.48	9.542e+06	462.00	4.32	0.03	0.04	0.02	36,37,11
1367	3.02	2.83	2.82	1.119e+07	462.00	4.90	0.06	0.05	0.02	36,37,17
1368	2.92	2.70	2.80	1.088e+07	462.00	4.87	0.04	0.05	0.02	36,37,16
1369	2.70	2.70	2.80	1.018e+07	462.00	4.87	0.03	0.05	0.02	37,37,16
1370	2.67	2.67	2.58	1.008e+07	462.00	4.48	0.03	0.04	0.03	37,37,37
1371	2.51	2.58	2.58	9.542e+06	462.00	4.48	0.03	0.04	0.03	36,37,37
1372	2.51	2.40	2.48	9.542e+06	462.00	4.32	0.03	0.04	0.02	36,37,11
1376	3.02	2.83	2.82	1.119e+07	462.00	4.90	0.06	0.05	0.02	36,37,17
1377	2.92	2.70	2.80	1.088e+07	462.00	4.87	0.04	0.05	0.02	36,37,16
1378	2.70	2.70	2.80	1.018e+07	462.00	4.87	0.03	0.05	0.02	37,37,16
1379	2.67	2.67	2.58	1.008e+07	462.00	4.48	0.03	0.04	0.03	37,37,37
1380	2.51	2.58	2.58	9.542e+06	462.00	4.48	0.03	0.04	0.03	36,37,37
1381	2.51	2.40	2.48	9.542e+06	462.00	4.32	0.03	0.04	0.02	36,37,11
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				5.974e+06	385.00	3.87				
	3.02	2.94	2.94	1.119e+07	462.00	5.11	0.06	0.05	0.03	

Setto	Mat.	Spessore	Stato
		cm	
71	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1301	1.97	1.90	1.92	5.337e+06	385.00	3.34	0.01	0.03	0.02	38,37,14
1302	1.89	1.82	1.92	7.405e+06	462.00	3.34	0.04	0.04	0.02	38,37,14
1303	1.89	1.82	1.88	7.405e+06	462.00	3.26	0.04	0.04	0.01	38,37,19
1310	1.97	1.90	1.92	5.337e+06	385.00	3.34	0.01	0.03	0.02	38,37,14
1311	1.89	1.82	1.92	7.405e+06	462.00	3.34	0.04	0.04	0.02	38,37,14
1312	1.89	1.82	1.88	7.405e+06	462.00	3.26	0.04	0.04	0.01	38,37,19
1319	1.97	1.90	1.92	5.337e+06	385.00	3.34	0.01	0.03	0.02	38,37,14
1320	1.89	1.82	1.92	7.405e+06	462.00	3.34	0.04	0.04	0.02	38,37,14
1321	1.89	1.82	1.88	7.405e+06	462.00	3.26	0.04	0.04	0.01	38,37,19
1328	1.97	1.90	1.92	5.337e+06	385.00	3.34	0.01	0.03	0.02	38,37,14
1329	1.89	1.82	1.92	7.405e+06	462.00	3.34	0.04	0.04	0.02	38,37,14
1330	1.89	1.82	1.88	7.405e+06	462.00	3.26	0.04	0.04	0.01	38,37,19

1337	1.97	1.90	1.92	5.337e+06	385.00	3.34	0.01	0.03	0.02	38,37,14
1338	1.89	1.82	1.92	7.405e+06	462.00	3.34	0.04	0.04	0.02	38,37,14
1339	1.89	1.82	1.88	7.405e+06	462.00	3.26	0.04	0.04	0.01	38,37,19
1346	1.97	1.90	1.92	5.337e+06	385.00	3.34	0.01	0.03	0.02	38,37,14
1347	1.89	1.82	1.92	7.405e+06	462.00	3.34	0.04	0.04	0.02	38,37,14
1348	1.89	1.82	1.88	7.405e+06	462.00	3.26	0.04	0.04	0.01	38,37,19
1355	1.97	1.89	1.91	5.337e+06	392.50	3.32	0.01	0.03	0.02	38,37,14
1356	1.89	1.82	1.91	7.405e+06	462.00	3.32	0.04	0.04	0.02	38,37,14
1357	1.89	1.82	1.88	7.405e+06	462.00	3.26	0.04	0.04	0.01	38,37,19
1364	1.96	1.88	1.90	5.517e+06	400.00	3.30	8.97e-03	0.03	0.02	38,37,14
1365	1.89	1.82	1.90	7.405e+06	462.00	3.30	0.04	0.04	0.02	38,37,14
1366	1.89	1.82	1.88	7.405e+06	462.00	3.26	0.04	0.04	0.01	38,37,19
1373	1.95	1.88	1.90	5.700e+06	400.00	3.30	7.74e-03	0.03	0.02	38,37,14
1374	1.89	1.82	1.90	7.405e+06	462.00	3.30	0.04	0.04	0.02	38,37,14
1375	1.89	1.82	1.88	7.405e+06	462.00	3.26	0.04	0.04	0.01	38,37,19
1382	1.95	1.88	1.90	5.700e+06	400.00	3.30	7.74e-03	0.03	0.02	38,37,14
1383	1.89	1.82	1.90	7.405e+06	462.00	3.30	0.04	0.04	0.02	38,37,14
1384	1.89	1.82	1.88	7.405e+06	462.00	3.26	0.04	0.04	0.01	38,37,19

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
	1.97	1.90	1.92	5.337e+06	385.00	3.26			
				7.405e+06	462.00	3.34	0.04	0.04	0.02

Setto	Mat.	Spessore	Stato
		cm	
72	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1354	2.41	2.28	2.36	9.250e+05	146.50	4.09	0.02	0.07	0.05	38,39,11
1355	2.41	2.28	2.36	9.250e+05	146.50	4.09	0.02	0.07	0.05	38,39,11
1363	2.40	2.27	2.36	8.298e+05	139.00	4.09	0.02	0.08	0.05	38,39,11
1364	2.40	2.27	2.36	8.298e+05	139.00	4.09	0.02	0.08	0.05	38,39,11
1372	2.40	2.27	2.34	8.298e+05	139.00	4.07	0.02	0.08	0.05	38,39,11
1373	2.40	2.27	2.34	8.298e+05	139.00	4.07	0.02	0.08	0.05	38,39,11
1381	2.40	2.27	2.34	8.298e+05	139.00	4.07	0.02	0.08	0.05	38,39,11
1382	2.40	2.27	2.34	8.298e+05	139.00	4.07	0.02	0.08	0.05	38,39,11

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				8.298e+05	139.00	4.07			
	2.41	2.28	2.36	9.250e+05	146.50	4.09	0.02	0.08	0.05

Setto	Mat.	Spessore	Stato
		cm	
73	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
35	2.56	2.74	2.74	3.683e+05	90.00	4.76	0.04	0.09	0.02	23,16,16
36	2.56	2.74	2.74	3.683e+05	90.00	4.76	0.04	0.09	0.02	23,16,16
188	2.56	2.74	2.74	3.683e+05	90.00	4.76	0.04	0.09	0.02	23,16,16
1169	2.30	2.74	2.58	3.355e+05	90.00	4.48	0.07	0.09	0.02	17,16,36
1171	2.30	2.19	2.58	3.355e+05	90.00	4.48	0.07	0.06	0.02	17,17,36
1173	2.31	2.19	2.11	3.362e+05	90.00	3.66	0.08	0.11	9.07e-03	11,17,37
1175	2.28	2.24	2.13	3.334e+05	90.00	3.71	0.10	0.14	0.01	11,17,37
1177	2.27	2.27	2.13	3.317e+05	90.00	3.71	0.14	0.15	0.01	17,17,37
1179	2.27	2.27	2.38	3.317e+05	90.00	4.13	0.14	0.15	0.01	17,17,30
1385	2.30	2.74	2.58	3.355e+05	90.00	4.48	0.07	0.09	0.02	17,16,36
1386	2.30	2.19	2.58	3.355e+05	90.00	4.48	0.07	0.06	0.02	17,17,36
1387	2.31	2.19	2.11	3.362e+05	90.00	3.66	0.08	0.11	9.07e-03	11,17,37
1388	2.28	2.24	2.13	3.334e+05	90.00	3.71	0.10	0.14	0.01	11,17,37
1389	2.27	2.27	2.13	3.317e+05	90.00	3.71	0.14	0.15	0.01	17,17,37
1390	2.27	2.27	2.38	3.317e+05	90.00	4.13	0.14	0.15	0.01	17,17,30
1394	2.30	2.74	2.58	3.355e+05	90.00	4.48	0.07	0.09	0.02	17,16,36
1395	2.30	2.19	2.58	3.355e+05	90.00	4.48	0.07	0.06	0.02	17,17,36
1396	2.31	2.19	2.11	3.362e+05	90.00	3.66	0.08	0.11	9.07e-03	11,17,37

1397	2.28	2.24	2.13	3.334e+05	90.00	3.71	0.10	0.14	0.01	11,17,37
1398	2.27	2.27	2.13	3.317e+05	90.00	3.71	0.14	0.15	0.01	17,17,37
1399	2.27	2.27	2.38	3.317e+05	90.00	4.13	0.14	0.15	0.01	17,17,30

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				3.317e+05	90.00	3.66			
	2.56	2.74	2.74	3.683e+05	90.00	4.76	0.14	0.15	0.02

Setto	Mat.	Spessore	Stato
		cm	
74	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1179	1.75	1.75	1.88	2.614e+05	90.00	3.27	0.04	0.03	3.15e-03	16,16,38
1181	1.54	1.75	1.88	2.325e+05	90.00	3.27	0.09	0.03	3.15e-03	12,16,38
1183	1.54	1.46	1.42	2.325e+05	90.00	2.46	0.09	0.03	0.01	12,17,31
1185	1.51	1.48	1.54	2.285e+05	90.00	2.67	0.05	0.06	0.02	14,17,11
1390	1.75	1.75	1.88	2.614e+05	90.00	3.27	0.04	0.03	3.15e-03	16,16,38
1391	1.54	1.75	1.88	2.325e+05	90.00	3.27	0.09	0.03	3.15e-03	12,16,38
1392	1.54	1.46	1.42	2.325e+05	90.00	2.46	0.09	0.03	0.01	12,17,31
1393	1.51	1.48	1.54	2.285e+05	90.00	2.67	0.05	0.06	0.02	14,17,11
1399	1.75	1.75	1.88	2.614e+05	90.00	3.27	0.04	0.03	3.15e-03	16,16,38
1400	1.54	1.75	1.88	2.325e+05	90.00	3.27	0.09	0.03	3.15e-03	12,16,38
1401	1.54	1.46	1.42	2.325e+05	90.00	2.46	0.09	0.03	0.01	12,17,31
1402	1.51	1.48	1.54	2.285e+05	90.00	2.67	0.05	0.06	0.02	14,17,11
2643	1.56	1.49	1.56	2.363e+05	90.00	2.72	0.06	0.08	0.02	16,17,16
2644	1.49	1.49	1.56	2.261e+05	90.00	2.72	0.09	0.09	0.02	17,17,16
2645	1.49	1.49	1.46	2.261e+05	90.00	2.53	0.09	0.09	0.01	17,17,16
2646	1.03	1.31	1.06	1.601e+05	90.00	1.84	0.13	0.06	0.01	15,17,12
2647	1.03	1.01	1.06	1.601e+05	90.00	1.84	0.13	0.11	0.01	15,17,12
2648	1.01	1.04	1.03	1.570e+05	90.00	1.80	0.08	0.15	9.98e-03	25,17,16
2649	1.07	1.07	1.00	1.654e+05	90.00	1.73	0.21	0.15	0.03	17,17,27
2650	0.91	1.07	0.86	1.415e+05	90.00	1.49	0.21	0.15	0.04	17,17,33
2651	0.91	0.91	0.86	1.415e+05	90.00	1.49	0.21	0.10	0.04	17,25,33
2652	1.56	1.49	1.56	2.363e+05	90.00	2.72	0.06	0.08	0.02	16,17,16
2653	1.49	1.49	1.56	2.261e+05	90.00	2.72	0.09	0.09	0.02	17,17,16
2654	1.49	1.49	1.46	2.261e+05	90.00	2.53	0.09	0.09	0.01	17,17,16
2655	1.03	1.31	1.06	1.601e+05	90.00	1.84	0.13	0.06	0.01	15,17,12
2656	1.03	1.01	1.06	1.601e+05	90.00	1.84	0.13	0.11	0.01	15,17,12
2657	1.01	1.04	1.03	1.570e+05	90.00	1.80	0.08	0.15	9.98e-03	25,17,16
2658	1.07	1.07	1.00	1.654e+05	90.00	1.73	0.21	0.15	0.03	17,17,27
2659	0.91	1.07	0.86	1.415e+05	90.00	1.49	0.21	0.15	0.04	17,17,33
2660	0.91	0.91	0.86	1.415e+05	90.00	1.49	0.21	0.10	0.04	17,25,33
2661	1.56	1.49	1.56	2.363e+05	90.00	2.72	0.06	0.08	0.02	16,17,16
2662	1.49	1.49	1.56	2.261e+05	90.00	2.72	0.09	0.09	0.02	17,17,16
2663	1.49	1.49	1.46	2.261e+05	90.00	2.53	0.09	0.09	0.01	17,17,16
2664	1.03	1.31	1.06	1.601e+05	90.00	1.84	0.13	0.06	0.01	15,17,12
2665	1.03	1.01	1.06	1.601e+05	90.00	1.84	0.13	0.11	0.01	15,17,12
2666	1.01	1.04	1.03	1.570e+05	90.00	1.80	0.08	0.15	9.98e-03	25,17,16
2667	1.07	1.07	1.00	1.654e+05	90.00	1.73	0.21	0.15	0.03	17,17,27
2668	0.91	1.07	0.86	1.415e+05	90.00	1.49	0.21	0.15	0.04	17,17,33
2669	0.91	0.91	0.86	1.415e+05	90.00	1.49	0.21	0.10	0.04	17,25,33
3080	0.64	0.47	0.61	1.008e+05	90.00	1.06	0.08	0.02	0.04	25,35,33
3081	0.51	0.47	0.49	8.084e+04	90.00	0.86	0.04	0.02	0.03	25,35,32
3083	0.64	0.47	0.61	1.008e+05	90.00	1.06	0.08	0.02	0.04	25,35,33
3084	0.51	0.47	0.49	8.084e+04	90.00	0.86	0.04	0.02	0.03	25,35,32
3086	0.64	0.47	0.61	1.008e+05	90.00	1.06	0.08	0.02	0.04	25,35,33
3087	0.51	0.47	0.49	8.084e+04	90.00	0.86	0.04	0.02	0.03	25,35,32

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				8.084e+04	90.00	0.86			
	1.75	1.75	1.88	2.614e+05	90.00	3.27	0.21	0.15	0.04

Setto	Mat.	Spessore	Stato
		cm	
77	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
1	3.13	3.23	3.33	4.287e+05	89.00	5.79	0.02	0.10	0.01	17,18,36
34	3.13	3.23	3.33	4.287e+05	89.00	5.79	0.02	0.10	0.01	17,18,36
219	3.13	3.23	3.33	4.287e+05	89.00	5.79	0.02	0.10	0.01	17,18,36
1376	2.99	3.23	3.33	4.126e+05	89.00	5.79	0.07	0.10	0.01	16,18,36
1377	2.99	3.01	3.11	4.126e+05	89.00	5.40	0.07	0.10	0.01	16,14,36
1378	2.92	3.10	3.11	4.042e+05	89.00	5.40	0.05	0.14	1.87e-03	16,18,40
1379	3.01	3.02	2.81	4.148e+05	89.00	4.89	0.04	0.14	1.98e-03	17,18,35
1380	3.02	3.02	2.65	4.152e+05	89.00	4.61	0.03	0.14	8.32e-03	18,18,37
1381	2.95	2.75	2.65	4.074e+05	89.00	4.61	0.02	0.11	8.32e-03	16,14,37
1421	2.99	3.23	3.33	4.126e+05	89.00	5.79	0.07	0.10	0.01	16,18,36
1422	2.99	3.01	3.11	4.126e+05	89.00	5.40	0.07	0.10	0.01	16,14,36
1423	2.92	3.10	3.11	4.042e+05	89.00	5.40	0.05	0.14	1.87e-03	16,18,40
1424	3.01	3.02	2.81	4.148e+05	89.00	4.89	0.04	0.14	1.98e-03	17,18,35
1425	3.02	3.02	2.65	4.152e+05	89.00	4.61	0.03	0.14	8.32e-03	18,18,37
1426	2.95	2.75	2.65	4.074e+05	89.00	4.61	0.02	0.11	8.32e-03	16,14,37
1430	2.99	3.23	3.33	4.126e+05	89.00	5.79	0.07	0.10	0.01	16,18,36
1431	2.99	3.01	3.11	4.126e+05	89.00	5.40	0.07	0.10	0.01	16,14,36
1432	2.92	3.10	3.11	4.042e+05	89.00	5.40	0.05	0.14	1.87e-03	16,18,40
1433	3.01	3.02	2.81	4.148e+05	89.00	4.89	0.04	0.14	1.98e-03	17,18,35
1434	3.02	3.02	2.65	4.152e+05	89.00	4.61	0.03	0.14	8.32e-03	18,18,37
1435	2.95	2.75	2.65	4.074e+05	89.00	4.61	0.02	0.11	8.32e-03	16,14,37
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				4.042e+05	89.00	4.61				
	3.13	3.23	3.33	4.287e+05	89.00	5.79	0.07	0.14	0.01	

Setto	Mat.	Spessore	Stato
		cm	
78	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
1381	2.15	2.34	2.15	3.092e+05	89.00	3.74	0.11	0.06	0.01	17,11,37
1382	1.91	2.07	2.15	2.772e+05	89.00	3.74	0.13	0.10	0.01	17,11,37
1383	1.91	2.05	1.90	2.772e+05	89.00	3.31	0.13	0.15	0.01	17,11,37
1384	2.04	2.05	2.05	2.949e+05	89.00	3.55	0.09	0.15	0.01	19,11,35
1426	2.15	2.34	2.15	3.092e+05	89.00	3.74	0.11	0.06	0.01	17,11,37
1427	1.91	2.07	2.15	2.772e+05	89.00	3.74	0.13	0.10	0.01	17,11,37
1428	1.91	2.05	1.90	2.772e+05	89.00	3.31	0.13	0.15	0.01	17,11,37
1429	2.04	2.05	2.05	2.949e+05	89.00	3.55	0.09	0.15	0.01	19,11,35
1435	2.15	2.34	2.15	3.092e+05	89.00	3.74	0.11	0.06	0.01	17,11,37
1436	1.91	2.07	2.15	2.772e+05	89.00	3.74	0.13	0.10	0.01	17,11,37
1437	1.91	2.05	1.90	2.772e+05	89.00	3.31	0.13	0.15	0.01	17,11,37
1438	2.04	2.05	2.05	2.949e+05	89.00	3.55	0.09	0.15	0.01	19,11,35
1724	2.10	2.11	2.02	3.021e+05	89.00	3.52	0.08	0.14	0.02	22,11,29
1726	1.98	1.91	2.02	2.873e+05	89.00	3.52	0.09	0.13	0.02	16,14,29
1728	1.98	1.60	1.86	2.873e+05	89.00	3.23	0.09	0.13	0.02	16,14,37
1730	1.68	1.60	1.44	2.473e+05	89.00	2.49	0.04	0.13	0.01	16,14,28
1732	1.37	1.29	1.34	2.037e+05	89.00	2.34	0.02	0.14	0.02	17,17,36
1734	1.14	1.29	1.14	1.714e+05	89.00	1.98	0.06	0.14	0.05	17,17,13
1736	0.97	1.14	1.00	1.477e+05	89.00	1.75	0.09	0.12	0.13	17,17,29
1738	0.90	1.04	0.95	1.377e+05	89.00	1.65	0.16	0.14	0.14	17,19,33
1740	0.80	0.80	0.95	1.225e+05	89.00	1.65	0.21	0.20	0.14	17,17,33
2607	2.10	2.11	2.02	3.021e+05	89.00	3.52	0.08	0.14	0.02	22,11,29
2608	1.98	1.91	2.02	2.873e+05	89.00	3.52	0.09	0.13	0.02	16,14,29
2609	1.98	1.60	1.86	2.873e+05	89.00	3.23	0.09	0.13	0.02	16,14,37
2610	1.68	1.60	1.44	2.473e+05	89.00	2.49	0.04	0.13	0.01	16,14,28
2611	1.37	1.29	1.34	2.037e+05	89.00	2.34	0.02	0.14	0.02	17,17,36
2612	1.14	1.29	1.14	1.714e+05	89.00	1.98	0.06	0.14	0.05	17,17,13
2613	0.97	1.14	1.00	1.477e+05	89.00	1.75	0.09	0.12	0.13	17,17,29
2614	0.90	1.04	0.95	1.377e+05	89.00	1.65	0.16	0.14	0.14	17,19,33
2615	0.80	0.80	0.95	1.225e+05	89.00	1.65	0.21	0.20	0.14	17,17,33
2616	2.10	2.11	2.02	3.021e+05	89.00	3.52	0.08	0.14	0.02	22,11,29
2617	1.98	1.91	2.02	2.873e+05	89.00	3.52	0.09	0.13	0.02	16,14,29
2618	1.98	1.60	1.86	2.873e+05	89.00	3.23	0.09	0.13	0.02	16,14,37
2619	1.68	1.60	1.44	2.473e+05	89.00	2.49	0.04	0.13	0.01	16,14,28
2620	1.37	1.29	1.34	2.037e+05	89.00	2.34	0.02	0.14	0.02	17,17,36

2621	1.14	1.29	1.14	1.714e+05	89.00	1.98	0.06	0.14	0.05	17,17,13
2622	0.97	1.14	1.00	1.477e+05	89.00	1.75	0.09	0.12	0.13	17,17,29
2623	0.90	1.04	0.95	1.377e+05	89.00	1.65	0.16	0.14	0.14	17,19,33
2624	0.80	0.80	0.95	1.225e+05	89.00	1.65	0.21	0.20	0.14	17,17,33
3065	0.80	0.64	0.88	1.225e+05	89.00	1.53	0.21	0.20	0.13	17,25,32
3066	0.64	0.64	0.72	9.809e+04	89.00	1.24	0.11	0.20	0.12	17,25,20
3068	0.80	0.64	0.88	1.225e+05	89.00	1.53	0.21	0.20	0.13	17,25,32
3069	0.64	0.64	0.72	9.809e+04	89.00	1.24	0.11	0.20	0.12	17,25,20
3071	0.80	0.64	0.88	1.225e+05	89.00	1.53	0.21	0.20	0.13	17,25,32
3072	0.64	0.64	0.72	9.809e+04	89.00	1.24	0.11	0.20	0.12	17,25,20

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				9.809e+04	89.00	1.24			
	2.15	2.34	2.15	3.092e+05	89.00	3.74	0.21	0.20	0.14

Setto	Mat.	Spessore	Stato
		cm	
79	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1	1.88	2.47	1.97	3.052e+05	93.50	3.10	0.09	0.06	0.02	17,16,37
5	1.88	2.47	1.97	3.052e+05	93.50	3.10	0.09	0.06	0.02	17,16,37
295	1.88	2.47	1.97	3.052e+05	93.50	3.10	0.09	0.06	0.02	17,16,37
1376	1.88	2.04	1.97	3.052e+05	93.50	3.10	0.09	0.07	0.02	17,17,37
1377	2.79	2.11	2.56	4.340e+05	93.50	4.02	0.06	0.10	0.02	16,17,36
1378	2.79	2.17	2.46	4.340e+05	93.50	3.86	0.06	0.14	0.01	16,17,30
1379	2.76	2.29	2.42	4.307e+05	93.50	3.80	0.06	0.20	7.55e-03	16,17,35
1380	2.44	2.46	2.48	3.855e+05	93.50	3.89	0.05	0.25	0.01	37,17,27
1381	2.44	2.46	2.48	3.855e+05	93.50	3.89	0.05	0.25	0.01	37,17,27
1439	1.88	2.03	2.54	3.052e+05	93.50	3.99	0.09	0.07	0.02	17,17,36
1440	2.79	2.10	2.54	4.340e+05	93.50	3.99	0.06	0.11	0.02	16,17,36
1441	2.79	2.17	2.45	4.340e+05	93.50	3.84	0.06	0.14	0.02	16,17,30
1442	2.76	2.29	2.42	4.307e+05	93.50	3.80	0.06	0.20	7.55e-03	16,17,35
1443	2.44	2.46	2.48	3.855e+05	93.50	3.89	0.05	0.25	0.01	37,17,27
1444	2.77	2.77	2.67	2.426e+05	70.12	4.19	0.07	0.25	0.01	17,17,27
1445	2.77	2.77	2.67	2.426e+05	70.12	4.19	0.07	0.25	0.01	17,17,27
1448	1.88	2.03	2.54	3.052e+05	93.50	3.99	0.09	0.07	0.02	17,17,36
1449	2.76	2.10	2.54	4.307e+05	93.50	3.99	0.05	0.11	0.02	16,17,36
1450	2.76	2.17	2.45	4.307e+05	93.50	3.84	0.06	0.14	0.02	16,17,30
1451	2.76	2.29	2.42	4.307e+05	93.50	3.80	0.06	0.20	7.55e-03	16,17,35
1452	2.44	2.46	2.48	3.855e+05	93.50	3.89	0.05	0.25	0.01	37,17,27
1453	2.77	2.77	2.67	2.426e+05	70.12	4.19	0.07	0.25	0.01	17,17,27
1454	2.77	2.77	2.67	2.426e+05	70.12	4.19	0.07	0.25	0.01	17,17,27
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				2.426e+05	70.12	3.10				
	2.79	2.77	2.67	4.340e+05	93.50	4.19	0.09	0.25	0.02	

Setto	Mat.	Spessore	Stato
		cm	
80	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1381	2.50	2.49	2.41	1.538e+05	58.44	3.78	0.16	0.40	5.57e-03	13,17,37
1382	2.78	2.78	2.65	3.315e+05	81.81	4.15	0.24	0.45	0.01	13,17,41
1383	2.78	2.78	2.30	3.315e+05	81.81	3.61	0.24	0.45	0.02	13,17,37
1384	2.40	2.40	1.35	3.806e+05	93.50	2.12	0.17	0.30	0.04	17,17,37
1444	2.50	2.49	2.41	1.538e+05	58.44	3.78	0.16	0.40	5.57e-03	13,17,37
1445	2.69	2.69	2.65	2.367e+05	70.12	4.15	0.26	0.46	0.01	13,17,41
1446	2.69	2.69	2.30	2.367e+05	70.12	3.61	0.26	0.46	0.02	13,17,37
1447	2.40	2.40	1.35	3.806e+05	93.50	2.12	0.17	0.30	0.04	17,17,37
1454	2.69	2.69	2.57	2.367e+05	70.12	4.04	0.26	0.46	0.01	13,17,37
1455	2.69	2.69	2.30	2.367e+05	70.12	3.61	0.26	0.46	0.02	13,17,37
1456	2.40	2.40	1.35	3.806e+05	93.50	2.12	0.17	0.30	0.04	17,17,37

1724	0.76	0.78	0.77	1.291e+05	93.50	1.20	0.31	0.47	0.06	35,37,27
1725	0.76	0.78	0.77	1.291e+05	93.50	1.20	0.31	0.47	0.06	35,37,27
1726	0.69	0.73	0.77	1.181e+05	93.50	1.20	0.32	0.63	0.06	41,17,27
1727	0.69	0.73	0.77	1.181e+05	93.50	1.20	0.32	0.63	0.06	41,17,27
1728	0.69	0.73	0.70	1.181e+05	93.50	1.10	0.32	0.63	0.03	41,17,33
1729	0.69	0.73	0.70	1.181e+05	93.50	1.10	0.32	0.63	0.03	41,17,33
1730	0.80	0.82	1.01	1.350e+05	93.50	1.59	0.14	0.59	0.04	41,17,27
1731	0.80	0.82	1.01	1.350e+05	93.50	1.59	0.14	0.59	0.04	41,17,27
1732	1.27	1.27	1.22	2.114e+05	93.50	1.91	0.08	0.49	0.04	13,17,27
1733	1.27	1.27	1.22	2.114e+05	93.50	1.91	0.08	0.49	0.04	13,17,27
1734	1.51	1.51	1.43	2.490e+05	93.50	2.25	0.14	0.56	0.04	17,17,27
1735	1.51	1.51	1.43	2.490e+05	93.50	2.25	0.14	0.56	0.04	17,17,27
1736	1.61	1.61	1.56	2.633e+05	93.50	2.44	0.21	0.64	0.05	17,17,33
1737	1.61	1.61	1.56	2.633e+05	93.50	2.44	0.21	0.64	0.05	17,17,33
1738	1.61	1.61	1.56	2.633e+05	93.50	2.44	0.21	0.64	0.05	17,17,33
1739	1.61	1.61	1.56	2.633e+05	93.50	2.44	0.21	0.64	0.05	17,17,33
1740	1.50	1.50	0.97	2.475e+05	93.50	1.52	0.18	0.51	0.07	17,25,20
1741	1.50	1.50	0.97	2.475e+05	93.50	1.52	0.18	0.51	0.07	17,25,20
1742	0.76	0.78	0.77	1.291e+05	93.50	1.20	0.31	0.47	0.06	35,37,27
1743	0.69	0.73	0.77	1.181e+05	93.50	1.20	0.32	0.63	0.06	41,17,27
1744	0.69	0.73	0.70	1.181e+05	93.50	1.10	0.32	0.63	0.03	41,17,33
1745	0.80	0.82	1.01	1.350e+05	93.50	1.59	0.14	0.59	0.04	41,17,27
1746	1.27	1.27	1.22	2.114e+05	93.50	1.91	0.08	0.49	0.04	13,17,27
1747	1.51	1.51	1.43	2.490e+05	93.50	2.25	0.14	0.56	0.04	17,17,27
1748	1.61	1.61	1.56	2.633e+05	93.50	2.44	0.21	0.64	0.05	17,17,33
1749	1.61	1.61	1.56	2.633e+05	93.50	2.44	0.21	0.64	0.05	17,17,33
1750	1.50	1.50	0.97	2.475e+05	93.50	1.52	0.18	0.51	0.07	17,25,20
3059	1.06	1.03	0.43	1.771e+05	93.50	0.68	0.08	0.31	0.11	17,33,24
3060	0.47	0.47	0.43	8.128e+04	93.50	0.68	0.04	0.26	0.11	14,29,24
3062	1.06	1.03	0.43	1.771e+05	93.50	0.68	0.08	0.31	0.11	17,33,24
3063	0.47	0.47	0.43	8.128e+04	93.50	0.68	0.04	0.26	0.11	14,29,24
3065	1.06	1.03	0.43	1.771e+05	93.50	0.68	0.08	0.31	0.11	17,33,24
3066	0.47	0.47	0.43	8.128e+04	93.50	0.68	0.04	0.26	0.11	14,29,24

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
	2.78	2.78	2.65	8.128e+04	58.44	0.68			
				3.806e+05	93.50	4.15	0.32	0.64	0.11

Setto	Mat.	Spessore	Stato
		cm	
82	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1148	4.04	3.84	3.93	4.035e+05	77.00	6.17	0.11	0.02	0.08	16,14,30
1151	4.04	3.84	3.93	4.035e+05	77.00	6.17	0.11	0.02	0.08	16,14,30
1526	5.23	5.23	3.93	2.774e+05	57.75	6.17	0.14	0.05	0.08	16,16,30
1544	5.23	5.23	5.01	2.774e+05	57.75	7.87	0.14	0.05	0.07	16,16,30
1566	5.23	5.23	5.01	2.774e+05	57.75	7.87	0.14	0.05	0.07	16,16,30
1567	5.23	5.23	3.93	2.774e+05	57.75	6.17	0.14	0.05	0.08	16,16,30
1584	5.23	5.23	5.01	2.774e+05	57.75	7.87	0.14	0.05	0.07	16,16,30
1585	5.23	5.23	3.93	2.774e+05	57.75	6.17	0.14	0.05	0.08	16,16,30
1586	4.04	3.84	3.93	4.035e+05	77.00	6.17	0.11	0.02	0.08	16,14,30

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
	5.23	5.23	5.01	2.774e+05	57.75	6.17			
				4.035e+05	77.00	7.87	0.14	0.05	0.08

Setto	Mat.	Spessore	Stato
		cm	
83	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
8	3.57	3.59	3.64	3.642e+05	77.00	5.71	0.03	0.02	0.22	17,14,30
9	3.57	3.59	3.64	3.642e+05	77.00	5.71	0.03	0.02	0.22	17,14,30

320	3.57	3.53	3.53	3.642e+05	77.00	5.54	0.03	0.02	0.27	17,11,30
1525	5.54	5.47	5.54	5.142e+05	77.00	8.69	0.02	0.05	0.08	11,16,30
1536	4.72	4.55	3.53	4.558e+05	77.00	5.54	0.06	0.08	0.27	16,13,30
1537	5.35	5.38	5.44	5.014e+05	77.00	8.53	0.03	0.06	0.05	11,16,30
1538	5.55	4.55	4.65	5.150e+05	77.00	7.29	0.08	0.08	0.12	16,13,30
1544	5.26	5.29	5.18	4.949e+05	77.00	8.13	0.06	0.06	0.05	11,16,27
1545	5.55	5.52	5.47	5.150e+05	77.00	8.59	0.08	0.08	0.12	16,11,30
1560	4.72	4.55	3.64	4.558e+05	77.00	5.71	0.06	0.08	0.22	16,13,30
1561	5.55	4.55	4.65	5.150e+05	77.00	7.29	0.08	0.08	0.12	16,13,30
1562	5.55	5.52	5.47	5.150e+05	77.00	8.59	0.08	0.08	0.12	16,11,30
1563	5.54	5.47	5.54	5.142e+05	77.00	8.69	0.02	0.05	0.08	11,16,30
1564	5.35	5.38	5.44	5.014e+05	77.00	8.53	0.03	0.06	0.05	11,16,30
1565	5.26	5.38	5.18	4.949e+05	77.00	8.13	0.06	0.06	0.05	11,16,27
1566	5.26	5.29	5.18	4.949e+05	77.00	8.13	0.06	0.06	0.05	11,16,27
1568	5.26	5.38	5.18	4.949e+05	77.00	8.13	0.06	0.06	0.05	11,16,27
1577	3.57	3.53	3.53	3.642e+05	77.00	5.54	0.03	0.02	0.27	17,11,30
1578	4.72	4.55	3.64	4.558e+05	77.00	5.71	0.06	0.08	0.22	16,13,30
1579	5.55	4.55	4.65	5.150e+05	77.00	7.29	0.08	0.08	0.12	16,13,30
1580	5.55	5.52	5.47	5.150e+05	77.00	8.59	0.08	0.08	0.12	16,11,30
1581	5.54	5.47	5.54	5.142e+05	77.00	8.69	0.02	0.05	0.08	11,16,30
1582	5.35	5.38	5.44	5.014e+05	77.00	8.53	0.03	0.06	0.05	11,16,30
1583	5.26	5.38	5.18	4.949e+05	77.00	8.13	0.06	0.06	0.05	11,16,27
1584	5.26	5.29	5.18	4.949e+05	77.00	8.13	0.06	0.06	0.05	11,16,27

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				3.642e+05	77.00	5.54			
	5.55	5.52	5.54	5.150e+05	77.00	8.69	0.08	0.08	0.27

Setto	Mat.	Spessore	Stato
		cm	
86	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
4	2.16	2.47	2.16	3.027e+05	87.50	3.38	0.19	0.05	0.03	15,14,11
10	2.16	2.47	2.16	3.027e+05	87.50	3.38	0.19	0.05	0.03	15,14,11
307	2.16	2.47	2.16	3.027e+05	87.50	3.38	0.19	0.05	0.03	15,14,11
1460	2.16	2.21	2.54	3.027e+05	87.50	3.99	0.19	0.12	0.04	15,11,30
1461	2.21	2.27	2.54	3.094e+05	87.50	3.99	0.15	0.25	0.04	15,15,30
1472	2.73	2.40	2.62	3.732e+05	87.50	4.12	0.10	0.26	0.03	18,15,34
1473	2.70	2.59	2.59	3.701e+05	87.50	4.07	0.12	0.27	0.02	17,15,29
1479	2.81	2.81	2.74	3.824e+05	87.50	4.30	0.14	0.27	0.02	11,15,29
1480	3.05	3.05	2.74	4.109e+05	87.50	4.30	0.18	0.28	0.02	11,15,29
1481	3.05	3.05	2.91	4.109e+05	87.50	4.56	0.18	0.28	0.02	11,15,29
1524	2.16	2.21	2.55	3.027e+05	87.50	4.00	0.19	0.12	0.04	15,11,30
1548	2.16	2.21	2.54	3.027e+05	87.50	3.99	0.19	0.11	0.04	15,11,30
1553	2.21	2.27	2.54	3.094e+05	87.50	3.99	0.15	0.23	0.04	15,15,30
1554	2.73	2.40	2.62	3.732e+05	87.50	4.12	0.10	0.26	0.03	18,15,34
1555	2.70	2.59	2.59	3.701e+05	87.50	4.07	0.12	0.27	0.02	17,15,29
1556	2.81	2.81	2.74	3.824e+05	87.50	4.30	0.14	0.27	0.02	11,15,29
1557	3.05	3.05	2.74	4.109e+05	87.50	4.30	0.18	0.28	0.02	11,15,29
1569	2.21	2.27	2.55	3.091e+05	87.50	4.00	0.13	0.25	0.04	15,15,30
1570	2.73	2.40	2.54	3.732e+05	87.50	3.99	0.10	0.26	0.03	18,15,28
1571	2.70	2.59	2.59	3.701e+05	87.50	4.07	0.12	0.27	0.02	17,15,29
1572	2.81	2.81	2.74	3.824e+05	87.50	4.30	0.14	0.27	0.02	11,15,29
1573	3.05	3.05	2.74	4.109e+05	87.50	4.30	0.18	0.28	0.02	11,15,29
1574	3.05	3.05	2.91	4.109e+05	87.50	4.56	0.18	0.28	0.02	11,15,29
1589	3.05	3.05	2.91	4.109e+05	87.50	4.56	0.18	0.28	0.02	11,15,29
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				3.027e+05	87.50	3.38				
	3.05	3.05	2.91	4.109e+05	87.50	4.56	0.19	0.28	0.04	

Setto	Mat.	Spessore	Stato
		cm	
89	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
6	3.44	3.48	3.49	3.533e+05	77.00	5.47	0.02	0.04	0.26	17,16,30
7	3.44	3.48	3.49	3.533e+05	77.00	5.47	0.02	0.04	0.26	17,16,30
333	3.44	3.48	3.49	3.533e+05	77.00	5.47	0.02	0.04	0.26	17,16,30
1495	4.32	3.48	3.49	4.259e+05	77.00	5.47	0.03	0.04	0.26	17,16,30
1496	5.17	4.36	4.38	4.886e+05	77.00	6.86	0.04	0.04	0.12	17,16,30
1497	5.17	5.36	5.24	4.886e+05	77.00	8.23	0.04	0.05	0.11	17,17,30
1498	5.29	5.26	5.44	4.969e+05	77.00	8.54	0.03	0.05	0.09	11,17,30
1499	5.17	5.26	5.34	4.888e+05	77.00	8.38	0.03	0.05	0.05	17,17,30
1500	5.08	5.17	5.06	4.822e+05	77.00	7.93	0.06	0.05	0.04	17,17,27
1501	5.08	5.08	5.06	4.822e+05	77.00	7.93	0.06	0.05	0.04	17,17,27
1504	4.32	3.48	3.49	4.259e+05	77.00	5.47	0.03	0.04	0.26	17,16,30
1505	5.17	4.36	4.38	4.886e+05	77.00	6.86	0.04	0.04	0.12	17,16,30
1506	5.17	5.36	5.24	4.886e+05	77.00	8.23	0.04	0.05	0.11	17,17,30
1507	5.29	5.26	5.44	4.969e+05	77.00	8.54	0.03	0.05	0.09	11,17,30
1508	5.17	5.26	5.34	4.888e+05	77.00	8.38	0.03	0.05	0.05	17,17,30
1509	5.08	5.17	5.06	4.822e+05	77.00	7.93	0.06	0.05	0.04	17,17,27
1510	5.08	5.08	5.06	4.822e+05	77.00	7.93	0.06	0.05	0.04	17,17,27
1513	4.32	3.48	3.49	4.259e+05	77.00	5.47	0.03	0.04	0.26	17,16,30
1514	5.17	4.36	4.38	4.886e+05	77.00	6.86	0.04	0.04	0.12	17,16,30
1515	5.17	5.36	5.24	4.886e+05	77.00	8.23	0.04	0.05	0.11	17,17,30
1516	5.29	5.26	5.44	4.969e+05	77.00	8.54	0.03	0.05	0.09	11,17,30
1517	5.17	5.26	5.34	4.888e+05	77.00	8.38	0.03	0.05	0.05	17,17,30
1518	5.08	5.17	5.06	4.822e+05	77.00	7.93	0.06	0.05	0.04	17,17,27
1519	5.08	5.08	5.06	4.822e+05	77.00	7.93	0.06	0.05	0.04	17,17,27

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				3.533e+05	77.00	5.47			
	5.29	5.36	5.44	4.969e+05	77.00	8.54	0.06	0.05	0.26

Setto	Mat.	Spessore	Stato
		cm	
90	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
1501	4.94	4.94	5.03	4.725e+05	77.00	7.89	0.10	0.05	0.07	17,17,30
1502	4.94	4.94	4.03	4.725e+05	77.00	6.32	0.10	0.05	0.08	17,17,30
1503	3.97	3.99	4.03	3.971e+05	77.00	6.32	0.07	9.21e-03	0.08	17,16,30
1510	4.94	4.94	5.03	4.725e+05	77.00	7.89	0.10	0.05	0.07	17,17,30
1511	4.94	4.94	4.03	4.725e+05	77.00	6.32	0.10	0.05	0.08	17,17,30
1512	3.97	3.99	4.03	3.971e+05	77.00	6.32	0.07	9.21e-03	0.08	17,16,30
1519	4.94	4.94	5.03	4.725e+05	77.00	7.89	0.10	0.05	0.07	17,17,30
1520	4.94	4.94	4.03	4.725e+05	77.00	6.32	0.10	0.05	0.08	17,17,30
1521	3.97	3.99	4.03	3.971e+05	77.00	6.32	0.07	9.21e-03	0.08	17,16,30

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				3.971e+05	77.00	6.32			
	4.94	4.94	5.03	4.725e+05	77.00	7.89	0.10	0.05	0.08

Setto	Mat.	Spessore	Stato
		cm	
92	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
3	5.55	5.74	5.78	8.629e+04	32.00	10.04	0.03	0.06	0.09	32,27,24
533	5.55	5.74	5.78	8.629e+04	32.00	10.04	0.03	0.06	0.09	32,27,24
653	4.22	5.74	5.78	7.062e+04	32.00	10.04	0.03	0.06	0.09	12,27,24
656	3.87	3.50	3.47	6.587e+04	32.00	6.03	0.04	0.11	0.04	11,30,17
658	3.87	3.38	3.30	6.587e+04	32.00	5.74	0.04	0.19	0.06	11,30,18
660	3.68	3.41	3.53	6.332e+04	32.00	6.13	0.03	0.26	0.08	11,32,24
662	3.28	3.41	3.53	5.766e+04	32.00	6.13	0.04	0.32	0.08	26,32,24
664	3.34	3.41	3.50	5.854e+04	32.00	6.08	0.05	0.39	0.07	18,30,24
666	3.34	3.41	3.53	5.854e+04	32.00	6.13	0.05	0.39	0.02	18,30,19

1591	4.22	5.74	5.78	7.062e+04	32.00	10.04	0.03	0.06	0.09	12,27,24
1592	3.87	3.50	3.47	6.587e+04	32.00	6.03	0.04	0.11	0.04	11,30,17
1593	3.87	3.38	3.30	6.587e+04	32.00	5.74	0.04	0.19	0.06	11,30,18
1594	3.68	3.41	3.53	6.332e+04	32.00	6.13	0.03	0.26	0.08	11,32,24
1595	3.28	3.41	3.53	5.766e+04	32.00	6.13	0.04	0.32	0.08	26,32,24
1596	3.34	3.41	3.50	5.854e+04	32.00	6.08	0.05	0.39	0.07	18,30,24
1597	3.34	3.41	3.53	5.854e+04	32.00	6.13	0.05	0.39	0.02	18,30,19

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				5.766e+04	32.00	5.74				
	5.55	5.74	5.78	8.629e+04	32.00	10.04	0.05	0.39	0.09	

Setto	Mat.	Spessore	Stato
		cm	
93	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
666	3.29	3.36	3.27	5.781e+04	32.00	5.67	0.05	0.47	0.04	29,30,22
668	3.46	3.56	3.56	6.018e+04	32.00	6.18	0.08	0.57	0.04	33,30,30
670	3.46	3.56	3.56	6.018e+04	32.00	6.18	0.08	0.57	0.04	33,30,30
1597	3.29	3.36	3.27	5.781e+04	32.00	5.67	0.05	0.47	0.04	29,30,22
1598	3.46	3.56	3.56	6.018e+04	32.00	6.18	0.08	0.57	0.04	33,30,30
1599	3.46	3.56	3.56	6.018e+04	32.00	6.18	0.08	0.57	0.04	33,30,30

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				5.781e+04	32.00	5.67				
	3.46	3.56	3.56	6.018e+04	32.00	6.18	0.08	0.57	0.04	

Setto	Mat.	Spessore	Stato
		cm	
96	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
487	3.53	3.40	3.52	1.728e+06	170.00	6.12	0.07	0.14	0.06	23,30,12
495	3.53	3.40	3.52	1.728e+06	170.00	6.12	0.07	0.14	0.06	23,30,12
502	3.53	3.40	3.52	1.728e+06	170.00	6.12	0.07	0.14	0.06	23,30,12
509	3.53	3.40	3.52	1.728e+06	170.00	6.12	0.07	0.14	0.06	23,30,12
515	3.53	3.40	3.52	1.728e+06	170.00	6.12	0.07	0.14	0.06	23,30,12
1610	3.53	2.87	3.52	1.728e+06	170.00	6.12	0.07	0.14	0.06	23,30,12
1611	2.99	2.52	2.98	1.505e+06	170.00	5.18	0.06	0.16	0.04	23,30,12
1612	2.33	2.28	2.24	1.212e+06	170.00	3.90	0.05	0.17	0.03	35,30,17
1613	2.12	2.07	2.04	1.111e+06	170.00	3.54	0.05	0.18	0.03	35,30,17
1614	2.12	1.88	2.04	1.111e+06	170.00	3.54	0.05	0.18	0.03	35,30,17
1615	1.92	1.88	1.76	1.017e+06	170.00	3.06	0.05	0.18	0.03	35,30,12
1616	1.73	1.70	1.76	9.269e+05	170.00	3.06	0.04	0.17	0.03	35,30,12
1619	3.53	2.87	3.52	1.728e+06	170.00	6.12	0.07	0.14	0.06	23,30,12
1620	2.99	2.52	2.98	1.505e+06	170.00	5.18	0.06	0.16	0.04	23,30,12
1621	2.33	2.28	2.24	1.212e+06	170.00	3.90	0.05	0.17	0.03	35,30,17
1622	2.12	2.07	2.04	1.111e+06	170.00	3.54	0.05	0.18	0.03	35,30,17
1623	2.12	1.88	2.04	1.111e+06	170.00	3.54	0.05	0.18	0.03	35,30,17
1624	1.92	1.88	1.76	1.017e+06	170.00	3.06	0.05	0.18	0.03	35,30,12
1625	1.73	1.70	1.76	9.269e+05	170.00	3.06	0.04	0.17	0.03	35,30,12
1628	3.53	2.87	3.52	1.728e+06	170.00	6.12	0.07	0.14	0.06	23,30,12
1629	2.99	2.52	2.98	1.505e+06	170.00	5.18	0.06	0.16	0.04	23,30,12
1630	2.33	2.28	2.24	1.212e+06	170.00	3.90	0.05	0.17	0.03	35,30,17
1631	2.12	2.07	2.04	1.111e+06	170.00	3.54	0.05	0.18	0.03	35,30,17
1632	2.12	1.88	2.04	1.111e+06	170.00	3.54	0.05	0.18	0.03	35,30,17
1633	1.92	1.88	1.76	1.017e+06	170.00	3.06	0.05	0.18	0.03	35,30,12
1634	1.73	1.70	1.76	9.269e+05	170.00	3.06	0.04	0.17	0.03	35,30,12
1637	3.53	2.87	3.52	1.728e+06	170.00	6.12	0.07	0.14	0.06	23,30,12
1638	2.99	2.52	2.98	1.505e+06	170.00	5.18	0.06	0.16	0.04	23,30,12
1639	2.33	2.28	2.24	1.212e+06	170.00	3.90	0.05	0.17	0.03	35,30,17
1640	2.12	2.07	2.04	1.111e+06	170.00	3.54	0.05	0.18	0.03	35,30,17
1641	2.12	1.88	2.04	1.111e+06	170.00	3.54	0.05	0.18	0.03	35,30,17

1642	1.92	1.88	1.76	1.017e+06	170.00	3.06	0.05	0.18	0.03	35,30,12
1643	1.73	1.70	1.76	9.269e+05	170.00	3.06	0.04	0.17	0.03	35,30,12
1646	3.53	2.87	3.52	1.728e+06	170.00	6.12	0.07	0.14	0.06	23,30,12
1647	2.99	2.52	2.98	1.505e+06	170.00	5.18	0.06	0.16	0.04	23,30,12
1648	2.33	2.28	2.24	1.212e+06	170.00	3.90	0.05	0.17	0.03	35,30,17
1649	2.12	2.07	2.04	1.111e+06	170.00	3.54	0.05	0.18	0.03	35,30,17
1650	2.12	1.88	2.04	1.111e+06	170.00	3.54	0.05	0.18	0.03	35,30,17
1651	1.92	1.88	1.76	1.017e+06	170.00	3.06	0.05	0.18	0.03	35,30,12
1652	1.73	1.70	1.76	9.269e+05	170.00	3.06	0.04	0.17	0.03	35,30,12

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				9.269e+05	170.00	3.06			
	3.53	3.40	3.52	1.728e+06	170.00	6.12	0.07	0.18	0.06

Setto	Mat.	Spessore	Stato
		cm	
97	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1616	1.53	1.50	1.55	8.233e+05	170.00	2.69	0.03	0.15	0.03	27,30,12
1617	1.53	1.50	1.55	8.233e+05	170.00	2.69	0.03	0.15	0.03	27,30,12
1618	1.49	1.49	1.51	5.954e+05	146.00	2.63	0.02	0.12	0.03	30,30,28
1625	1.53	1.50	1.55	8.233e+05	170.00	2.69	0.03	0.15	0.03	27,30,12
1626	1.53	1.50	1.55	8.233e+05	170.00	2.69	0.03	0.15	0.03	27,30,12
1627	1.49	1.49	1.51	5.954e+05	146.00	2.63	0.02	0.12	0.03	30,30,28
1634	1.53	1.50	1.55	8.233e+05	170.00	2.69	0.03	0.15	0.03	27,30,12
1635	1.53	1.50	1.55	8.233e+05	170.00	2.69	0.03	0.15	0.03	27,30,12
1636	1.49	1.49	1.51	5.954e+05	146.00	2.63	0.02	0.12	0.03	30,30,28
1643	1.53	1.50	1.55	8.233e+05	170.00	2.69	0.03	0.15	0.03	27,30,12
1644	1.53	1.50	1.55	8.233e+05	170.00	2.69	0.03	0.15	0.03	27,30,12
1645	1.49	1.49	1.51	5.954e+05	146.00	2.63	0.02	0.12	0.03	30,30,28
1652	1.53	1.50	1.55	8.233e+05	170.00	2.69	0.03	0.15	0.03	27,30,12
1653	1.53	1.50	1.55	8.233e+05	170.00	2.69	0.03	0.15	0.03	27,30,12
1654	1.49	1.49	1.51	5.954e+05	146.00	2.63	0.02	0.12	0.03	30,30,28

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				5.954e+05	146.00	2.63			
	1.53	1.50	1.55	8.233e+05	170.00	2.69	0.03	0.15	0.03

Setto	Mat.	Spessore	Stato
		cm	
100	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
452	3.15	3.04	3.11	1.573e+06	170.00	5.41	0.03	0.08	0.08	16,27,11
453	3.15	3.04	3.11	1.573e+06	170.00	5.41	0.03	0.08	0.08	16,27,11
460	3.15	3.04	3.11	1.573e+06	170.00	5.41	0.03	0.08	0.08	16,27,11
467	3.15	3.04	3.11	1.573e+06	170.00	5.41	0.03	0.08	0.08	16,27,11
473	3.15	3.04	3.11	1.573e+06	170.00	5.41	0.03	0.08	0.08	16,27,11
1665	3.15	2.56	3.11	1.573e+06	170.00	5.41	0.03	0.09	0.08	16,27,11
1666	2.66	2.24	2.63	1.362e+06	170.00	4.56	0.02	0.10	0.06	16,27,11
1667	2.35	2.03	2.05	1.219e+06	170.00	3.57	0.02	0.12	0.04	36,27,14
1668	2.13	1.85	1.88	1.115e+06	170.00	3.26	0.02	0.13	0.05	32,27,14
1669	1.93	1.74	1.72	1.020e+06	170.00	2.98	0.02	0.14	0.05	30,11,22
1670	1.76	1.60	1.62	9.413e+05	170.00	2.81	0.02	0.15	0.05	30,11,16
1671	1.56	1.60	1.62	8.401e+05	170.00	2.81	5.77e-03	0.15	0.05	27,11,16
1674	3.15	2.56	3.11	1.573e+06	170.00	5.41	0.03	0.09	0.08	16,27,11
1675	2.66	2.24	2.63	1.362e+06	170.00	4.56	0.02	0.10	0.06	16,27,11
1676	2.35	2.03	2.05	1.219e+06	170.00	3.57	0.02	0.12	0.04	36,27,14
1677	2.13	1.85	1.88	1.115e+06	170.00	3.26	0.02	0.13	0.05	32,27,14
1678	1.93	1.74	1.72	1.020e+06	170.00	2.98	0.02	0.14	0.05	30,11,22
1679	1.76	1.60	1.62	9.413e+05	170.00	2.81	0.02	0.15	0.05	30,11,16
1680	1.56	1.60	1.62	8.401e+05	170.00	2.81	5.77e-03	0.15	0.05	27,11,16
1683	3.15	2.56	3.11	1.573e+06	170.00	5.41	0.03	0.09	0.08	16,27,11

1684	2.66	2.24	2.63	1.362e+06	170.00	4.56	0.02	0.10	0.06	16,27,11
1685	2.35	2.03	2.05	1.219e+06	170.00	3.57	0.02	0.12	0.04	36,27,14
1686	2.13	1.85	1.88	1.115e+06	170.00	3.26	0.02	0.13	0.05	32,27,14
1687	1.93	1.74	1.72	1.020e+06	170.00	2.98	0.02	0.14	0.05	30,11,22
1688	1.76	1.60	1.62	9.413e+05	170.00	2.81	0.02	0.15	0.05	30,11,16
1689	1.56	1.60	1.62	8.401e+05	170.00	2.81	5.77e-03	0.15	0.05	27,11,16
1692	3.15	2.56	3.11	1.573e+06	170.00	5.41	0.03	0.09	0.08	16,27,11
1693	2.66	2.24	2.63	1.362e+06	170.00	4.56	0.02	0.10	0.06	16,27,11
1694	2.35	2.03	2.05	1.219e+06	170.00	3.57	0.02	0.12	0.04	36,27,14
1695	2.13	1.85	1.88	1.115e+06	170.00	3.26	0.02	0.13	0.05	32,27,14
1696	1.93	1.74	1.72	1.020e+06	170.00	2.98	0.02	0.14	0.05	30,11,22
1697	1.76	1.60	1.62	9.413e+05	170.00	2.81	0.02	0.15	0.05	30,11,16
1698	1.56	1.60	1.62	8.401e+05	170.00	2.81	5.77e-03	0.15	0.05	27,11,16
1701	3.15	2.56	3.11	1.573e+06	170.00	5.41	0.03	0.09	0.08	16,27,11
1702	2.66	2.24	2.63	1.362e+06	170.00	4.56	0.02	0.10	0.06	16,27,11
1703	2.35	2.03	2.05	1.219e+06	170.00	3.57	0.02	0.12	0.04	36,27,14
1704	2.13	1.85	1.88	1.115e+06	170.00	3.26	0.02	0.13	0.05	32,27,14
1705	1.93	1.74	1.72	1.020e+06	170.00	2.98	0.02	0.14	0.05	30,11,22
1706	1.76	1.60	1.62	9.413e+05	170.00	2.81	0.02	0.15	0.05	30,11,16
1707	1.56	1.60	1.62	8.401e+05	170.00	2.81	5.77e-03	0.15	0.05	27,11,16

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				8.401e+05	170.00	2.81			
	3.15	3.04	3.11	1.573e+06	170.00	5.41	0.03	0.15	0.08

Setto	Mat.	Spessore	Stato
		cm	
101	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1671	1.41	1.44	1.41	7.628e+05	170.00	2.44	0.04	0.14	0.05	27,11,27
1672	1.42	1.41	1.41	6.648e+05	170.00	2.44	0.06	0.14	0.05	27,11,27
1673	1.42	1.45	1.42	6.648e+05	158.00	2.47	0.06	0.12	0.04	27,11,27
1680	1.41	1.44	1.41	7.628e+05	170.00	2.44	0.04	0.14	0.05	27,11,27
1681	1.42	1.44	1.41	6.648e+05	170.00	2.44	0.06	0.14	0.05	27,11,27
1682	1.42	1.45	1.42	6.648e+05	158.00	2.47	0.06	0.12	0.04	27,11,27
1689	1.41	1.44	1.41	7.628e+05	170.00	2.44	0.04	0.14	0.05	27,11,27
1690	1.42	1.44	1.41	6.648e+05	170.00	2.44	0.06	0.14	0.05	27,11,27
1691	1.42	1.45	1.42	6.648e+05	158.00	2.47	0.06	0.12	0.04	27,11,27
1698	1.41	1.44	1.41	7.628e+05	170.00	2.44	0.04	0.14	0.05	27,11,27
1699	1.42	1.44	1.41	6.648e+05	170.00	2.44	0.06	0.14	0.05	27,11,27
1700	1.42	1.45	1.42	6.648e+05	158.00	2.47	0.06	0.12	0.04	27,11,27
1707	1.41	1.44	1.41	7.628e+05	170.00	2.44	0.04	0.14	0.05	27,11,27
1708	1.42	1.44	1.41	6.648e+05	170.00	2.44	0.06	0.14	0.05	27,11,27
1709	1.42	1.45	1.42	6.648e+05	158.00	2.47	0.06	0.12	0.04	27,11,27

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				6.648e+05	158.00	2.44			
	1.42	1.45	1.42	7.628e+05	170.00	2.47	0.06	0.14	0.05

Setto	Mat.	Spessore	Stato
		cm	
102	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
4	4.34	4.32	4.34	6.343e+04	30.00	7.55	0.01	0.14	0.09	11,14,11
432	4.34	4.32	4.34	6.343e+04	30.00	7.55	0.01	0.14	0.09	11,14,11
1524	3.21	4.32	4.34	4.976e+04	30.00	7.55	0.07	0.14	0.09	27,14,11
1569	3.21	2.92	3.40	4.976e+04	30.00	5.91	0.07	0.11	0.06	27,11,11
1570	3.00	2.61	2.54	4.697e+04	30.00	4.42	0.04	0.20	0.06	16,11,18
1571	2.68	2.41	2.39	4.263e+04	30.00	4.15	0.02	0.26	0.08	16,11,14
1572	2.25	2.26	2.37	3.651e+04	30.00	4.12	0.02	0.30	0.10	21,11,28
1573	2.28	2.18	2.22	3.698e+04	30.00	3.86	0.02	0.33	0.13	26,11,16
1574	2.28	2.18	2.22	3.698e+04	30.00	3.86	0.02	0.33	0.13	26,11,16

1710	3.21	4.32	4.34	4.976e+04	30.00	7.55	0.07	0.14	0.09	27,14,11
1711	3.21	2.92	3.40	4.976e+04	30.00	5.91	0.07	0.11	0.06	27,11,11
1712	3.00	2.61	2.54	4.697e+04	30.00	4.42	0.04	0.20	0.06	16,11,18
1713	2.68	2.41	2.39	4.263e+04	30.00	4.15	0.02	0.26	0.08	16,11,14
1714	2.25	2.26	2.37	3.651e+04	30.00	4.12	0.02	0.30	0.10	21,11,28
1715	2.28	2.18	2.22	3.698e+04	30.00	3.86	0.02	0.33	0.13	26,11,16
1716	2.28	2.18	2.22	3.698e+04	30.00	3.86	0.02	0.33	0.13	26,11,16

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				3.651e+04	30.00	3.86			
	4.34	4.32	4.34	6.343e+04	30.00	7.55	0.07	0.33	0.13

Setto	Mat.	Spessore	Stato
		cm	
103	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1574	2.37	2.21	2.24	3.826e+04	30.00	3.90	0.02	0.33	0.15	18,11,16
1575	2.92	2.80	2.24	4.585e+04	30.00	3.90	0.08	0.34	0.15	14,11,16
1576	2.92	2.80	2.83	4.585e+04	30.00	4.92	0.08	0.34	0.06	14,11,16
1716	2.37	2.21	2.24	3.826e+04	30.00	3.90	0.02	0.33	0.15	18,11,16
1717	2.92	2.80	2.24	4.585e+04	30.00	3.90	0.08	0.34	0.15	14,11,16
1718	2.92	2.80	2.83	4.585e+04	30.00	4.92	0.08	0.34	0.06	14,11,16

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				3.826e+04	30.00	3.90			
	2.92	2.80	2.83	4.585e+04	30.00	4.92	0.08	0.34	0.15

Setto	Mat.	Spessore	Stato
		cm	
105	mattoni pieni e malta di calce	38.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1888	0.72	0.76	0.72	3.990e+05	172.75	1.08	0.09	0.02	0.02	20,23,16
1890	0.49	0.49	0.50	2.724e+05	172.75	0.75	0.16	0.03	0.08	20,20,37
1897	0.67	0.67	0.66	3.677e+05	172.75	0.99	0.13	0.02	0.03	20,26,16
1898	0.59	0.59	0.58	3.247e+05	172.75	0.87	0.15	0.02	0.04	20,20,26
1991	0.72	0.76	0.72	3.990e+05	172.75	1.08	0.09	0.02	0.02	20,23,16
1992	0.67	0.67	0.66	3.677e+05	172.75	0.99	0.13	0.02	0.03	20,26,16
1993	0.59	0.59	0.58	3.247e+05	172.75	0.87	0.15	0.02	0.04	20,20,26
2045	0.39	0.49	0.39	2.163e+05	172.75	0.59	0.19	0.03	0.12	20,20,37
2046	0.25	0.25	0.25	1.431e+05	172.75	0.38	0.16	0.02	0.09	39,23,39
2099	0.25	0.25	0.25	1.431e+05	172.75	0.38	0.16	0.02	0.09	39,23,39
2123	0.39	0.39	0.39	2.163e+05	172.75	0.59	0.19	0.02	0.12	20,20,37
2133	0.25	0.25	0.25	1.431e+05	172.75	0.38	0.16	0.02	0.09	39,23,39
2146	0.72	0.76	0.72	3.990e+05	172.75	1.08	0.09	0.02	0.02	20,23,16
2151	0.74	0.76	0.73	4.097e+05	172.75	1.09	0.07	0.02	0.02	20,23,36
2152	0.74	0.76	0.73	4.097e+05	172.75	1.09	0.07	0.02	0.02	20,23,36
2155	0.74	0.76	0.73	4.097e+05	172.75	1.09	0.07	0.02	0.02	20,23,36
2156	0.74	0.76	0.73	4.097e+05	172.75	1.09	0.07	0.02	0.02	20,23,36
2157	0.49	0.49	0.50	2.724e+05	172.75	0.75	0.16	0.03	0.08	20,20,37
2159	0.72	0.76	0.72	3.990e+05	172.75	1.08	0.09	0.02	0.02	20,23,16
2161	0.67	0.67	0.66	3.677e+05	172.75	0.99	0.13	0.02	0.03	20,26,16
2163	0.59	0.59	0.58	3.247e+05	172.75	0.87	0.15	0.02	0.04	20,20,26
2165	0.49	0.49	0.50	2.724e+05	172.75	0.75	0.16	0.03	0.08	20,20,37
2167	0.39	0.49	0.39	2.163e+05	172.75	0.59	0.19	0.03	0.12	20,20,37
2169	0.39	0.39	0.39	2.163e+05	172.75	0.59	0.19	0.02	0.12	20,20,37
2171	0.25	0.25	0.25	1.431e+05	172.75	0.38	0.16	0.02	0.09	39,23,39
2172	0.39	0.49	0.39	2.163e+05	172.75	0.59	0.19	0.03	0.12	20,20,37
2173	0.67	0.67	0.66	3.677e+05	172.75	0.99	0.13	0.02	0.03	20,26,16
2174	0.39	0.39	0.39	2.163e+05	172.75	0.59	0.19	0.02	0.12	20,20,37
2182	0.25	0.25	0.25	1.431e+05	172.75	0.38	0.16	0.02	0.09	39,23,39
2187	0.49	0.49	0.50	2.724e+05	172.75	0.75	0.16	0.03	0.08	20,20,37
2188	0.39	0.49	0.39	2.163e+05	172.75	0.59	0.19	0.03	0.12	20,20,37

2189	0.39	0.39	0.39	2.163e+05	172.75	0.59	0.19	0.02	0.12	20,20,37
2212	0.59	0.59	0.58	3.247e+05	172.75	0.87	0.15	0.02	0.04	20,20,26
2213	0.72	0.76	0.72	3.990e+05	172.75	1.08	0.09	0.02	0.02	20,23,16
2216	0.74	0.76	0.73	4.097e+05	172.75	1.09	0.07	0.02	0.02	20,23,36
2218	0.67	0.67	0.66	3.677e+05	172.75	0.99	0.13	0.02	0.03	20,26,16
2220	0.59	0.59	0.58	3.247e+05	172.75	0.87	0.15	0.02	0.04	20,20,26
2222	0.49	0.49	0.50	2.724e+05	172.75	0.75	0.16	0.03	0.08	20,20,37
2224	0.39	0.49	0.39	2.163e+05	172.75	0.59	0.19	0.03	0.12	20,20,37
2226	0.39	0.39	0.39	2.163e+05	172.75	0.59	0.19	0.02	0.12	20,20,37

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				1.431e+05	172.75	0.38			
	0.74	0.76	0.73	4.097e+05	172.75	1.09	0.19	0.03	0.12

Setto	Mat.	Spessore	Stato
		cm	
106	mattoni pieni e malta di calce	38.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
1763	0.24	0.37	0.38	1.568e+05	184.50	0.56	0.19	0.08	0.10	31,20,27
1764	0.54	0.53	0.51	3.404e+05	184.50	0.76	0.08	0.08	0.08	26,20,30
1765	0.47	0.45	0.48	2.956e+05	184.50	0.71	0.11	0.08	0.09	21,20,27
1889	0.24	0.24	0.24	1.568e+05	184.50	0.36	0.19	0.06	0.07	31,32,27
1891	0.38	0.37	0.38	2.397e+05	184.50	0.56	0.19	0.08	0.10	33,20,27
1892	0.24	0.37	0.38	1.568e+05	184.50	0.56	0.19	0.08	0.10	31,20,27
1989	0.24	0.24	0.24	1.568e+05	184.50	0.36	0.19	0.06	0.07	31,32,27
2132	0.72	0.68	0.65	4.511e+05	184.50	0.97	0.11	0.06	0.05	20,20,34
2142	0.71	0.61	0.58	4.444e+05	184.50	0.87	0.09	0.07	0.08	23,20,30
2147	0.72	0.72	0.68	4.511e+05	184.50	1.02	0.11	0.06	0.02	20,20,34
2148	0.72	0.72	0.68	4.511e+05	184.50	1.02	0.11	0.06	0.02	20,20,34
2203	0.72	0.68	0.65	4.511e+05	184.50	0.97	0.11	0.06	0.05	20,20,34
2204	0.71	0.61	0.58	4.444e+05	184.50	0.87	0.09	0.07	0.08	23,20,30
2205	0.54	0.53	0.51	3.404e+05	184.50	0.76	0.08	0.08	0.08	26,20,30
2206	0.47	0.45	0.48	2.956e+05	184.50	0.71	0.11	0.08	0.09	21,20,27
2207	0.38	0.37	0.38	2.397e+05	184.50	0.56	0.19	0.08	0.10	33,20,27
2208	0.24	0.37	0.38	1.568e+05	184.50	0.56	0.19	0.08	0.10	31,20,27
2209	0.24	0.24	0.24	1.568e+05	184.50	0.36	0.19	0.06	0.07	31,32,27
2214	0.72	0.68	0.65	4.511e+05	184.50	0.97	0.11	0.06	0.05	20,20,34
2215	0.72	0.72	0.68	4.511e+05	184.50	1.02	0.11	0.06	0.02	20,20,34
2217	0.71	0.61	0.58	4.444e+05	184.50	0.87	0.09	0.07	0.08	23,20,30
2219	0.54	0.53	0.51	3.404e+05	184.50	0.76	0.08	0.08	0.08	26,20,30
2221	0.47	0.45	0.48	2.956e+05	184.50	0.71	0.11	0.08	0.09	21,20,27
2223	0.38	0.37	0.38	2.397e+05	184.50	0.56	0.19	0.08	0.10	33,20,27
2225	0.24	0.37	0.38	1.568e+05	184.50	0.56	0.19	0.08	0.10	31,20,27
2227	0.24	0.24	0.24	1.568e+05	184.50	0.36	0.19	0.06	0.07	31,32,27
2232	0.72	0.68	0.65	4.511e+05	184.50	0.97	0.11	0.06	0.05	20,20,34
2233	0.72	0.72	0.68	4.511e+05	184.50	1.02	0.11	0.06	0.02	20,20,34
2234	0.71	0.61	0.58	4.444e+05	184.50	0.87	0.09	0.07	0.08	23,20,30
2235	0.54	0.53	0.51	3.404e+05	184.50	0.76	0.08	0.08	0.08	26,20,30
2236	0.47	0.45	0.48	2.956e+05	184.50	0.71	0.11	0.08	0.09	21,20,27
2237	0.38	0.37	0.38	2.397e+05	184.50	0.56	0.19	0.08	0.10	33,20,27
2238	0.24	0.37	0.38	1.568e+05	184.50	0.56	0.19	0.08	0.10	31,20,27
2239	0.24	0.24	0.24	1.568e+05	184.50	0.36	0.19	0.06	0.07	31,32,27
2242	0.72	0.68	0.65	4.511e+05	184.50	0.97	0.11	0.06	0.05	20,20,34
2243	0.72	0.72	0.68	4.511e+05	184.50	1.02	0.11	0.06	0.02	20,20,34
2244	0.71	0.61	0.58	4.444e+05	184.50	0.87	0.09	0.07	0.08	23,20,30
2245	0.54	0.53	0.51	3.404e+05	184.50	0.76	0.08	0.08	0.08	26,20,30
2246	0.47	0.45	0.48	2.956e+05	184.50	0.71	0.11	0.08	0.09	21,20,27
2247	0.38	0.37	0.38	2.397e+05	184.50	0.56	0.19	0.08	0.10	33,20,27
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				1.568e+05	184.50	0.36				
	0.72	0.72	0.68	4.511e+05	184.50	1.02	0.19	0.08	0.10	

Setto	Mat.	Spessore	Stato
		cm	
109	mattoni pieni e malta di calce	38.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
24	1.95	2.04	1.98	1.823e+05	73.00	2.96	0.08	0.13	0.03	34,31,21
753	1.95	2.04	1.98	1.823e+05	73.00	2.96	0.08	0.13	0.03	34,31,21
754	1.97	2.12	2.10	1.842e+05	73.00	3.13	0.07	0.13	0.02	34,27,23
755	1.80	2.00	2.10	1.691e+05	73.00	3.13	0.10	0.18	0.02	34,27,23
756	1.79	1.79	1.82	1.686e+05	73.00	2.71	0.17	0.21	0.02	20,31,19
757	1.29	1.29	1.82	1.244e+05	73.00	2.71	0.23	0.30	0.02	31,31,19
758	0.45	1.29	0.44	7.480e+04	73.00	0.66	0.32	0.30	0.06	27,31,26
759	0.45	0.45	0.44	7.480e+04	94.25	0.66	0.32	0.28	0.06	27,27,26
1771	1.29	1.29	1.82	1.244e+05	73.00	2.71	0.23	0.30	0.02	31,31,19
1772	0.45	1.29	0.44	7.480e+04	73.00	0.66	0.32	0.30	0.06	27,31,26
2126	0.45	0.45	0.44	7.480e+04	94.25	0.66	0.32	0.28	0.06	27,27,26
2127	1.95	2.04	1.98	1.823e+05	73.00	2.96	0.08	0.13	0.03	34,31,21
2154	1.95	2.04	1.98	1.823e+05	73.00	2.96	0.08	0.13	0.03	34,31,21
2175	1.95	2.04	1.98	1.823e+05	73.00	2.96	0.08	0.13	0.03	34,31,21
2176	1.97	2.12	2.10	1.842e+05	73.00	3.13	0.07	0.13	0.02	34,27,23
2177	1.80	2.00	2.10	1.691e+05	73.00	3.13	0.10	0.18	0.02	34,27,23
2178	1.79	1.79	1.82	1.686e+05	73.00	2.71	0.17	0.21	0.02	20,31,19
2179	1.29	1.29	1.82	1.244e+05	73.00	2.71	0.23	0.30	0.02	31,31,19
2180	0.45	1.29	0.44	7.480e+04	73.00	0.66	0.32	0.30	0.06	27,31,26
2181	0.45	0.45	0.44	7.480e+04	94.25	0.66	0.32	0.28	0.06	27,27,26
2183	1.95	2.04	1.98	1.823e+05	73.00	2.96	0.08	0.13	0.03	34,31,21
2190	0.45	0.45	0.44	7.480e+04	94.25	0.66	0.32	0.28	0.06	27,27,26
2191	0.45	0.45	0.44	7.480e+04	94.25	0.66	0.32	0.28	0.06	27,27,26
2192	1.97	2.12	2.10	1.842e+05	73.00	3.13	0.07	0.13	0.02	34,27,23
2240	1.80	2.00	2.10	1.691e+05	73.00	3.13	0.10	0.18	0.02	34,27,23
2241	1.79	1.79	1.82	1.686e+05	73.00	2.71	0.17	0.21	0.02	20,31,19
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	1.97	2.12	2.10	7.480e+04	73.00	0.66				
				1.842e+05	94.25	3.13	0.32	0.30	0.06	

Setto	Mat.	Spessore	Stato
		cm	
112	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
1503	1.92	2.01	2.01	2.101e+05	77.00	3.15	0.03	0.24	0.09	15,17,30
1512	1.92	2.01	2.01	2.101e+05	77.00	3.15	0.03	0.24	0.09	15,17,30
1521	1.92	2.01	2.01	2.101e+05	77.00	3.15	0.03	0.24	0.09	15,17,30
1787	1.64	1.69	1.67	1.815e+05	77.00	2.62	0.10	0.30	0.09	41,17,30
1788	1.57	1.57	1.67	1.752e+05	77.00	2.62	0.13	0.39	0.09	17,17,30
1789	1.57	1.57	1.37	1.752e+05	77.00	2.15	0.13	0.39	0.10	17,17,30
1790	1.40	1.40	1.11	1.572e+05	77.00	1.73	0.09	0.35	0.13	17,17,30
1791	1.13	1.12	0.89	1.275e+05	77.00	1.39	0.03	0.23	0.16	18,17,30
1792	0.63	0.63	0.68	7.307e+04	77.00	1.07	0.11	0.25	0.20	17,17,30
1793	0.47	0.47	0.68	5.524e+04	77.00	1.07	0.30	0.36	0.20	17,17,30
1794	0.42	0.47	0.55	4.854e+04	77.00	0.86	0.40	0.36	0.19	17,17,30
1795	0.42	0.46	0.43	4.854e+04	70.01	0.67	0.40	0.22	0.17	17,17,14
1796	1.64	1.69	1.67	1.815e+05	77.00	2.62	0.10	0.30	0.09	41,17,30
1797	1.57	1.57	1.67	1.752e+05	77.00	2.62	0.13	0.39	0.09	17,17,30
1798	1.57	1.57	1.37	1.752e+05	77.00	2.15	0.13	0.39	0.10	17,17,30
1799	1.40	1.40	1.11	1.572e+05	77.00	1.73	0.09	0.35	0.13	17,17,30
1800	1.13	1.12	0.89	1.275e+05	77.00	1.39	0.03	0.23	0.16	18,17,30
1801	0.63	0.63	0.68	7.307e+04	77.00	1.07	0.11	0.25	0.20	17,17,30
1802	0.47	0.47	0.68	5.524e+04	77.00	1.07	0.30	0.36	0.20	17,17,30
1803	0.42	0.47	0.55	4.854e+04	77.00	0.86	0.40	0.36	0.19	17,17,30
1804	0.42	0.46	0.43	4.854e+04	70.01	0.67	0.40	0.22	0.17	17,17,14
1805	1.64	1.69	1.67	1.815e+05	77.00	2.62	0.10	0.30	0.09	41,17,30
1806	1.57	1.57	1.67	1.752e+05	77.00	2.62	0.13	0.39	0.09	17,17,30
1807	1.57	1.57	1.37	1.752e+05	77.00	2.15	0.13	0.39	0.10	17,17,30
1808	1.40	1.40	1.11	1.572e+05	77.00	1.73	0.09	0.35	0.13	17,17,30
1809	1.13	1.12	0.89	1.275e+05	77.00	1.39	0.03	0.23	0.16	18,17,30
1810	0.63	0.63	0.68	7.307e+04	77.00	1.07	0.11	0.25	0.20	17,17,30
1811	0.47	0.47	0.68	5.524e+04	77.00	1.07	0.30	0.36	0.20	17,17,30
1812	0.42	0.47	0.55	4.854e+04	77.00	0.86	0.40	0.36	0.19	17,17,30
1813	0.42	0.46	0.43	4.854e+04	70.01	0.67	0.40	0.22	0.17	17,17,14

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
	1.92	2.01	2.01	4.854e+04 2.101e+05	70.01 77.00	0.67 3.15	0.40	0.39	0.20

Setto	Mat.	Spessore	Stato
		cm	
114	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1148	1.90	2.06	1.98	2.084e+05	77.00	3.10	0.03	0.13	0.10	17,15,30
1151	1.90	2.06	1.98	2.084e+05	77.00	3.10	0.03	0.13	0.10	17,15,30
1586	1.90	2.06	1.98	2.084e+05	77.00	3.10	0.03	0.13	0.10	17,15,30
1850	1.57	1.69	1.59	1.748e+05	77.00	2.50	0.09	0.22	0.11	29,15,30
1851	1.57	1.57	1.59	1.750e+05	77.00	2.50	0.12	0.34	0.11	11,15,30
1852	1.57	1.57	1.31	1.750e+05	77.00	2.05	0.12	0.34	0.12	11,15,30
1853	1.43	1.43	1.11	1.602e+05	77.00	1.74	0.09	0.30	0.14	11,15,30
1854	1.18	1.18	0.97	1.337e+05	77.00	1.51	0.03	0.18	0.15	11,15,30
1855	0.77	0.77	0.83	8.884e+04	77.00	1.30	0.06	0.19	0.17	15,15,30
1856	0.64	0.64	0.67	7.376e+04	77.00	1.05	0.18	0.29	0.19	15,15,27
1857	0.58	0.64	0.61	6.672e+04	77.00	0.96	0.26	0.29	0.20	15,15,27
1858	0.58	0.58	0.61	6.672e+04	77.00	0.96	0.26	0.14	0.20	15,15,27
1859	1.57	1.69	1.59	1.748e+05	77.00	2.50	0.09	0.22	0.11	29,15,30
1860	1.57	1.57	1.59	1.750e+05	77.00	2.50	0.12	0.34	0.11	11,15,30
1861	1.57	1.57	1.31	1.750e+05	77.00	2.05	0.12	0.34	0.12	11,15,30
1862	1.43	1.43	1.11	1.602e+05	77.00	1.74	0.09	0.30	0.14	11,15,30
1863	1.18	1.18	0.97	1.337e+05	77.00	1.51	0.03	0.18	0.15	11,15,30
1864	0.77	0.77	0.83	8.884e+04	77.00	1.30	0.06	0.19	0.17	15,15,30
1865	0.64	0.64	0.67	7.376e+04	77.00	1.05	0.18	0.29	0.19	15,15,27
1866	0.58	0.64	0.61	6.672e+04	77.00	0.96	0.26	0.29	0.20	15,15,27
1867	0.58	0.58	0.61	6.672e+04	77.00	0.96	0.26	0.14	0.20	15,15,27
1868	1.57	1.69	1.59	1.748e+05	77.00	2.50	0.09	0.22	0.11	29,15,30
1869	1.57	1.57	1.59	1.750e+05	77.00	2.50	0.12	0.34	0.11	11,15,30
1870	1.57	1.57	1.31	1.750e+05	77.00	2.05	0.12	0.34	0.12	11,15,30
1871	1.43	1.43	1.11	1.602e+05	77.00	1.74	0.09	0.30	0.14	11,15,30
1872	1.18	1.18	0.97	1.337e+05	77.00	1.51	0.03	0.18	0.15	11,15,30
1873	0.77	0.77	0.83	8.884e+04	77.00	1.30	0.06	0.19	0.17	15,15,30
1874	0.64	0.64	0.67	7.376e+04	77.00	1.05	0.18	0.29	0.19	15,15,27
1875	0.58	0.64	0.61	6.672e+04	77.00	0.96	0.26	0.29	0.20	15,15,27
1876	0.58	0.58	0.61	6.672e+04	77.00	0.96	0.26	0.14	0.20	15,15,27

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
	1.90	2.06	1.98	6.672e+04 2.084e+05	77.00 77.00	0.96 3.10	0.26	0.34	0.20

Setto	Mat.	Spessore	Stato
		cm	
118	murazione E = 4.550e+04	40.0	NV L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1576	3.28	3.17	3.17	5.065e+04	30.00	5.51	0.01	0.29	0.06	28,13,14
1718	3.28	3.17	3.17	5.065e+04	30.00	5.51	0.01	0.29	0.06	28,13,14
1931	3.28	3.17	3.86	5.065e+04	30.00	6.72	0.01	0.29	0.10	28,13,30
1932	4.18	3.80	3.86	6.162e+04	30.00	6.72	0.05	0.16	0.10	27,18,30
1933	4.18	3.55	4.13	6.162e+04	30.00	7.18	0.05	0.16	0.09	27,27,28
1934	3.55	2.59	3.46	5.409e+04	30.00	6.02	0.04	0.16	0.07	27,15,28
1935	1.56	1.58	1.56	2.622e+04	30.00	2.71	0.04	0.17	0.06	31,15,27
1936	0.58	0.60	0.58	1.026e+04	30.00	1.02	0.23	0.19	0.40	27,11,27
1937	3.86e-03	0.60	3.86e-03	69.44	30.00	6.70e-03	79.02	0.19	70.30	26,11,26
1938	3.86e-03	0.0	3.86e-03	69.44	0.0	6.70e-03	79.02	0.0	70.30	26,0,26
1939	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0,0,0
1978	3.28	3.17	3.86	5.065e+04	30.00	6.72	0.01	0.29	0.10	28,13,30
1979	4.18	3.80	3.86	6.162e+04	30.00	6.72	0.05	0.16	0.10	27,18,30
1980	4.18	3.55	4.13	6.162e+04	30.00	7.18	0.05	0.16	0.09	27,27,28

1981	3.55	2.59	3.46	5.409e+04	30.00	6.02	0.04	0.16	0.07	27,15,28
1982	1.56	1.58	1.56	2.622e+04	30.00	2.71	0.04	0.17	0.06	31,15,27
1983	0.58	0.60	0.58	1.026e+04	30.00	1.02	0.23	0.19	0.40	27,11,27
1984	3.86e-03	0.60	3.86e-03	69.44	30.00	6.70e-03	79.02	0.19	70.30	26,11,26
1985	3.86e-03	0.0	3.86e-03	69.44	0.0	6.70e-03	79.02	0.0	70.30	26,0,26
1986	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0,0,0

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				0.0	0.0	0.0			
	4.18	3.80	4.13	6.162e+04	30.00	7.18	79.02	0.29	70.30

Setto	Mat.	Spessore	Stato
		cm	
121	mattoni pieni e malta di calce	38.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1762	0.51	0.89	0.89	6172.53	25.50	1.33	0.10	0.02	0.03	20,20,33
1766	0.51	0.51	0.51	6172.53	25.50	0.77	0.10	0.01	0.03	20,24,27
2128	0.85	0.70	0.70	1.018e+04	25.50	1.04	0.02	0.04	0.18	20,20,41
2129	1.05	1.05	0.85	1.242e+04	25.50	1.27	0.04	5.35e-03	0.15	20,21,33
2130	1.05	1.07	1.06	1.242e+04	25.50	1.58	0.04	0.02	0.03	20,20,32
2131	0.98	1.07	1.06	1.161e+04	25.50	1.58	0.03	0.02	0.03	20,20,32
2134	0.89	0.98	0.89	1.057e+04	25.50	1.33	0.08	0.02	0.03	20,20,33
2135	0.51	0.89	0.89	6172.53	25.50	1.33	0.10	0.02	0.03	20,20,33
2136	0.51	0.51	0.51	6172.53	25.50	0.77	0.10	0.01	0.03	20,24,27
2139	0.85	0.70	0.70	1.018e+04	25.50	1.04	0.02	0.04	0.18	20,20,41
2140	1.05	1.05	0.85	1.242e+04	25.50	1.27	0.04	5.35e-03	0.15	20,21,33
2141	1.05	1.07	1.06	1.242e+04	25.50	1.58	0.04	0.02	0.03	20,20,32
2144	0.98	1.07	1.06	1.161e+04	25.50	1.58	0.03	0.02	0.03	20,20,32
2145	0.89	0.98	0.89	1.057e+04	25.50	1.33	0.08	0.02	0.03	20,20,33
2149	0.71	0.70	0.70	8473.43	25.50	1.04	6.76e-03	0.04	0.18	32,20,41
2150	0.71	0.70	0.70	8473.43	25.50	1.04	6.76e-03	0.04	0.18	32,20,41

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				6172.53	25.50	0.77			
	1.05	1.07	1.06	1.242e+04	25.50	1.58	0.10	0.04	0.18

Setto	Mat.	Spessore	Stato
		cm	
122	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1673	1.40	1.40	1.40	5.602e+05	146.00	2.43	0.10	0.03	0.04	27,27,27
1682	1.40	1.40	1.40	5.602e+05	146.00	2.43	0.10	0.03	0.04	27,27,27
1691	1.40	1.40	1.40	5.602e+05	146.00	2.43	0.10	0.03	0.04	27,27,27
1700	1.40	1.40	1.40	5.602e+05	146.00	2.43	0.10	0.03	0.04	27,27,27
1709	1.40	1.40	1.40	5.602e+05	146.00	2.43	0.10	0.03	0.04	27,27,27
1996	1.51	1.51	1.40	6.022e+05	146.00	2.43	0.13	0.03	0.04	27,27,27
1997	1.55	1.55	1.55	6.176e+05	146.00	2.70	0.13	0.07	0.04	27,27,27
1998	1.55	1.51	1.53	6.176e+05	146.00	2.66	0.13	0.10	0.05	27,27,11
1999	1.51	1.43	1.46	6.004e+05	146.00	2.53	0.08	0.10	0.07	27,27,11
2000	1.36	1.36	1.39	5.447e+05	146.00	2.41	0.09	0.10	0.08	27,27,15
2001	1.28	1.28	1.31	5.162e+05	146.00	2.27	0.19	0.10	0.08	27,27,15
2002	1.21	1.21	1.31	4.870e+05	146.00	2.27	0.30	0.10	0.08	27,27,15
2003	1.21	1.21	1.23	4.870e+05	146.00	2.14	0.30	0.10	0.08	27,27,15
2004	0.91	0.91	0.94	4.361e+05	158.00	1.63	0.28	0.08	0.07	27,27,19
2005	1.51	1.51	1.40	6.022e+05	146.00	2.43	0.13	0.03	0.04	27,27,27
2006	1.55	1.55	1.55	6.176e+05	146.00	2.70	0.13	0.07	0.04	27,27,27
2007	1.55	1.51	1.53	6.176e+05	146.00	2.66	0.13	0.10	0.05	27,27,11
2008	1.51	1.43	1.46	6.004e+05	146.00	2.53	0.08	0.10	0.07	27,27,11
2009	1.36	1.36	1.39	5.447e+05	146.00	2.41	0.09	0.10	0.08	27,27,15
2010	1.28	1.28	1.31	5.162e+05	146.00	2.27	0.19	0.10	0.08	27,27,15
2011	1.21	1.21	1.31	4.870e+05	146.00	2.27	0.30	0.10	0.08	27,27,15
2012	1.21	1.21	1.23	4.870e+05	146.00	2.14	0.30	0.10	0.08	27,27,15

2013	0.91	0.91	0.94	4.361e+05	158.00	1.63	0.28	0.08	0.07	27,27,19
2014	1.51	1.51	1.40	6.022e+05	146.00	2.43	0.13	0.03	0.04	27,27,27
2015	1.55	1.55	1.55	6.176e+05	146.00	2.70	0.13	0.07	0.04	27,27,27
2016	1.55	1.51	1.53	6.176e+05	146.00	2.66	0.13	0.10	0.05	27,27,11
2017	1.51	1.43	1.46	6.004e+05	146.00	2.53	0.08	0.10	0.07	27,27,11
2018	1.36	1.36	1.39	5.447e+05	146.00	2.41	0.09	0.10	0.08	27,27,15
2019	1.28	1.28	1.31	5.162e+05	146.00	2.27	0.19	0.10	0.08	27,27,15
2020	1.21	1.21	1.31	4.870e+05	146.00	2.27	0.30	0.10	0.08	27,27,15
2021	1.21	1.21	1.23	4.870e+05	146.00	2.14	0.30	0.10	0.08	27,27,15
2022	0.91	0.91	0.94	4.361e+05	158.00	1.63	0.28	0.08	0.07	27,27,19
2023	1.51	1.51	1.40	6.022e+05	146.00	2.43	0.13	0.03	0.04	27,27,27
2024	1.55	1.55	1.55	6.176e+05	146.00	2.70	0.13	0.07	0.04	27,27,27
2025	1.55	1.51	1.53	6.176e+05	146.00	2.66	0.13	0.10	0.05	27,27,11
2026	1.51	1.43	1.46	6.004e+05	146.00	2.53	0.08	0.10	0.07	27,27,11
2027	1.36	1.36	1.39	5.447e+05	146.00	2.41	0.09	0.10	0.08	27,27,15
2028	1.28	1.28	1.31	5.162e+05	146.00	2.27	0.19	0.10	0.08	27,27,15
2029	1.21	1.21	1.31	4.870e+05	146.00	2.27	0.30	0.10	0.08	27,27,15
2030	1.21	1.21	1.23	4.870e+05	146.00	2.14	0.30	0.10	0.08	27,27,15
2031	0.91	0.91	0.94	4.361e+05	158.00	1.63	0.28	0.08	0.07	27,27,19
2032	1.51	1.51	1.40	6.022e+05	146.00	2.43	0.13	0.03	0.04	27,27,27
2033	1.55	1.55	1.55	6.176e+05	146.00	2.70	0.13	0.07	0.04	27,27,27
2034	1.55	1.51	1.53	6.176e+05	146.00	2.66	0.13	0.10	0.05	27,27,11
2035	1.51	1.43	1.46	6.004e+05	146.00	2.53	0.08	0.10	0.07	27,27,11
2036	1.36	1.36	1.39	5.447e+05	146.00	2.41	0.09	0.10	0.08	27,27,15
2037	1.28	1.28	1.31	5.162e+05	146.00	2.27	0.19	0.10	0.08	27,27,15
2038	1.21	1.21	1.31	4.870e+05	146.00	2.27	0.30	0.10	0.08	27,27,15
2039	1.21	1.21	1.23	4.870e+05	146.00	2.14	0.30	0.10	0.08	27,27,15
2040	0.91	0.91	0.94	4.361e+05	158.00	1.63	0.28	0.08	0.07	27,27,19

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				4.361e+05	146.00	1.63			
	1.55	1.55	1.55	6.176e+05	158.00	2.70	0.30	0.10	0.08

Setto	Mat.	Spessore	Stato
		cm	
124	muratura E = 4.550e+04	40.0	NV L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
670	3.43	3.43	3.43	5.973e+04	32.00	5.97	0.04	0.58	0.04	28,32,32
1599	3.43	3.43	3.43	5.973e+04	32.00	5.97	0.04	0.58	0.04	28,32,32
2104	3.60	3.43	3.43	6.217e+04	32.00	5.97	0.04	0.58	0.04	32,32,32
2105	3.37	3.60	3.36	5.892e+04	32.00	5.84	0.06	0.44	0.01	32,20,28
2106	3.37	3.37	2.50	5.892e+04	32.00	4.34	0.06	0.32	0.02	32,32,30
2107	2.30	2.54	1.69	4.242e+04	32.00	2.93	0.04	0.22	0.02	33,32,30
2108	1.13	1.72	1.15	2.202e+04	32.00	2.00	0.04	0.13	0.02	30,32,28
2109	0.63	0.63	1.15	1.246e+04	32.00	2.00	0.18	0.10	0.02	30,28,28
2110	5.58e-03	0.63	5.58e-03	114.16	32.00	9.69e-03	64.54	0.10	2.65	30,28,30
2111	5.58e-03	0.0	9.41e-03	114.16	0.0	0.02	64.54	0.0	6.50	30,0,39
2112	9.41e-03	0.0	9.41e-03	192.72	0.0	0.02	27.39	0.0	6.50	39,0,39
2113	3.60	3.43	3.43	6.217e+04	32.00	5.97	0.04	0.58	0.04	32,32,32
2114	3.37	3.60	3.36	5.892e+04	32.00	5.84	0.06	0.44	0.01	32,20,28
2115	3.37	3.37	2.50	5.892e+04	32.00	4.34	0.06	0.32	0.02	32,32,30
2116	2.30	2.54	1.69	4.242e+04	32.00	2.93	0.04	0.22	0.02	33,32,30
2117	1.13	1.72	1.15	2.202e+04	32.00	2.00	0.04	0.13	0.02	30,32,28
2118	0.63	0.63	1.15	1.246e+04	32.00	2.00	0.18	0.10	0.02	30,28,28
2119	5.58e-03	0.63	5.58e-03	114.16	32.00	9.69e-03	64.54	0.10	2.65	30,28,30
2120	5.58e-03	0.0	9.41e-03	114.16	0.0	0.02	64.54	0.0	6.50	30,0,39
2121	9.41e-03	0.0	9.41e-03	192.72	0.0	0.02	27.39	0.0	6.50	39,0,39

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				114.16	0.0	9.69e-03			
	3.60	3.60	3.43	6.217e+04	32.00	5.97	64.54	0.58	6.50

Setto	Mat.	Spessore	Stato
		cm	
126	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
1618	1.47	1.47	1.49	4.099e+05	122.00	2.59	0.10	0.04	0.04	30,30,28
1627	1.47	1.47	1.49	4.099e+05	122.00	2.59	0.10	0.04	0.04	30,30,28
1636	1.47	1.47	1.49	4.099e+05	122.00	2.59	0.10	0.04	0.04	30,30,28
1645	1.47	1.47	1.49	4.099e+05	122.00	2.59	0.10	0.04	0.04	30,30,28
1654	1.47	1.47	1.49	4.099e+05	122.00	2.59	0.10	0.04	0.04	30,30,28
2050	1.58	1.47	1.60	4.383e+05	122.00	2.78	0.15	0.04	0.04	30,30,28
2051	1.64	1.66	1.67	4.540e+05	122.00	2.89	0.17	0.07	0.04	30,32,28
2052	1.64	1.63	1.66	4.540e+05	122.00	2.88	0.17	0.10	0.04	30,32,12
2053	1.61	1.56	1.58	4.462e+05	122.00	2.74	0.11	0.10	0.05	30,28,12
2054	1.46	1.48	1.50	4.081e+05	122.00	2.61	0.09	0.10	0.05	30,28,12
2055	1.39	1.41	1.50	3.884e+05	122.00	2.61	0.21	0.10	0.05	30,28,12
2056	1.31	1.33	1.43	3.682e+05	122.00	2.48	0.33	0.11	0.05	30,32,16
2057	1.31	1.33	1.36	3.682e+05	122.00	2.36	0.33	0.11	0.04	30,32,11
2058	0.91	0.92	0.94	3.717e+05	146.00	1.64	0.32	0.06	0.03	30,32,11
2059	1.58	1.47	1.60	4.383e+05	122.00	2.78	0.15	0.04	0.04	30,30,28
2060	1.64	1.66	1.67	4.540e+05	122.00	2.89	0.17	0.07	0.04	30,32,28
2061	1.64	1.63	1.66	4.540e+05	122.00	2.88	0.17	0.10	0.04	30,32,12
2062	1.61	1.56	1.58	4.462e+05	122.00	2.74	0.11	0.10	0.05	30,28,12
2063	1.46	1.48	1.50	4.081e+05	122.00	2.61	0.09	0.10	0.05	30,28,12
2064	1.39	1.41	1.50	3.884e+05	122.00	2.61	0.21	0.10	0.05	30,28,12
2065	1.31	1.33	1.43	3.682e+05	122.00	2.48	0.33	0.11	0.05	30,32,16
2066	1.31	1.33	1.36	3.682e+05	122.00	2.36	0.33	0.11	0.04	30,32,11
2067	0.91	0.92	0.94	3.717e+05	146.00	1.64	0.32	0.06	0.03	30,32,11
2068	1.58	1.47	1.60	4.383e+05	122.00	2.78	0.15	0.04	0.04	30,30,28
2069	1.64	1.66	1.67	4.540e+05	122.00	2.89	0.17	0.07	0.04	30,32,28
2070	1.64	1.63	1.66	4.540e+05	122.00	2.88	0.17	0.10	0.04	30,32,12
2071	1.61	1.56	1.58	4.462e+05	122.00	2.74	0.11	0.10	0.05	30,28,12
2072	1.46	1.48	1.50	4.081e+05	122.00	2.61	0.09	0.10	0.05	30,28,12
2073	1.39	1.41	1.50	3.884e+05	122.00	2.61	0.21	0.10	0.05	30,28,12
2074	1.31	1.33	1.43	3.682e+05	122.00	2.48	0.33	0.11	0.05	30,32,16
2075	1.31	1.33	1.36	3.682e+05	122.00	2.36	0.33	0.11	0.04	30,32,11
2076	0.91	0.92	0.94	3.717e+05	146.00	1.64	0.32	0.06	0.03	30,32,11
2077	1.58	1.47	1.60	4.383e+05	122.00	2.78	0.15	0.04	0.04	30,30,28
2078	1.64	1.66	1.67	4.540e+05	122.00	2.89	0.17	0.07	0.04	30,32,28
2079	1.64	1.63	1.66	4.540e+05	122.00	2.88	0.17	0.10	0.04	30,32,12
2080	1.61	1.56	1.58	4.462e+05	122.00	2.74	0.11	0.10	0.05	30,28,12
2081	1.46	1.48	1.50	4.081e+05	122.00	2.61	0.09	0.10	0.05	30,28,12
2082	1.39	1.41	1.50	3.884e+05	122.00	2.61	0.21	0.10	0.05	30,28,12
2083	1.31	1.33	1.43	3.682e+05	122.00	2.48	0.33	0.11	0.05	30,32,16
2084	1.31	1.33	1.36	3.682e+05	122.00	2.36	0.33	0.11	0.04	30,32,11
2085	0.91	0.92	0.94	3.717e+05	146.00	1.64	0.32	0.06	0.03	30,32,11
2086	1.58	1.47	1.60	4.383e+05	122.00	2.78	0.15	0.04	0.04	30,30,28
2087	1.64	1.66	1.67	4.540e+05	122.00	2.89	0.17	0.07	0.04	30,32,28
2088	1.64	1.63	1.66	4.540e+05	122.00	2.88	0.17	0.10	0.04	30,32,12
2089	1.61	1.56	1.58	4.462e+05	122.00	2.74	0.11	0.10	0.05	30,28,12
2090	1.46	1.48	1.50	4.081e+05	122.00	2.61	0.09	0.10	0.05	30,28,12
2091	1.39	1.41	1.50	3.884e+05	122.00	2.61	0.21	0.10	0.05	30,28,12
2092	1.31	1.33	1.43	3.682e+05	122.00	2.48	0.33	0.11	0.05	30,32,16
2093	1.31	1.33	1.36	3.682e+05	122.00	2.36	0.33	0.11	0.04	30,32,11
2094	0.91	0.92	0.94	3.717e+05	146.00	1.64	0.32	0.06	0.03	30,32,11
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				3.682e+05	122.00	1.64				
	1.64	1.66	1.67	4.540e+05	146.00	2.89	0.33	0.11	0.05	

Setto	Mat.	Spessore	Stato
		cm	
128	mattoni pieni e malta di calce	38.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
2146	0.62	0.55	0.67	6135.68	23.16	0.99	0.07	0.04	0.03	37,36,26
2152	0.66	0.55	0.67	6590.15	23.16	0.99	0.04	0.04	0.03	29,36,26
2157	0.38	0.45	0.39	3816.75	23.16	0.59	0.09	0.03	0.08	20,35,32
2172	0.40	0.40	0.37	3975.70	23.16	0.55	0.25	0.09	0.10	23,15,32
2173	0.62	0.59	0.48	6135.68	23.16	0.72	0.07	0.04	0.04	37,42,20
2174	0.40	0.24	0.22	3975.70	23.16	0.33	0.25	0.09	0.12	23,15,20

2182	0.29	0.24	0.22	2875.12	23.16	0.33	0.20	0.09	0.12	39,15,20
2193	0.66	0.55	0.67	6590.15	23.16	0.99	0.04	0.04	0.03	29,36,26
2202	0.62	0.55	0.67	6135.68	23.16	0.99	0.07	0.04	0.03	37,36,26
2210	0.62	0.59	0.48	6135.68	23.16	0.72	0.07	0.04	0.04	37,42,20
2211	0.52	0.48	0.43	5147.31	23.16	0.64	0.06	0.03	0.06	39,35,20
2212	0.52	0.48	0.43	5147.31	23.16	0.64	0.06	0.03	0.06	39,35,20
2228	0.38	0.45	0.39	3816.75	23.16	0.59	0.09	0.03	0.08	20,35,32
2229	0.40	0.40	0.37	3975.70	23.16	0.55	0.25	0.09	0.10	23,15,32
2230	0.40	0.24	0.22	3975.70	23.16	0.33	0.25	0.09	0.12	23,15,20
2231	0.29	0.24	0.22	2875.12	23.16	0.33	0.20	0.09	0.12	39,15,20

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				2875.12	23.16	0.33			
	0.66	0.59	0.67	6590.15	23.16	0.99	0.25	0.09	0.12

Setto	Mat.	Spessore	Stato
		cm	
129	mattoni pieni e malta di calce	38.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
28	1.36	1.56	1.55	6.386e+04	51.16	2.31	0.05	0.15	0.02	36,37,29
727	1.66	1.64	1.44	7.732e+04	51.16	2.14	0.02	0.14	0.01	37,37,28
728	1.29	1.66	1.44	6.086e+04	51.16	2.14	0.04	0.13	0.01	36,37,28
729	1.10	1.46	1.46	5.232e+04	51.16	2.18	0.05	0.13	9.68e-03	20,37,41
730	0.84	0.84	0.84	4.034e+04	51.16	1.26	0.15	0.15	9.25e-03	37,37,27
737	0.43	0.50	0.46	2.122e+04	44.67	0.69	0.43	0.17	0.02	37,37,24
738	0.43	0.50	0.46	2.122e+04	44.67	0.69	0.43	0.17	0.02	37,37,24
766	1.36	1.56	1.55	6.386e+04	51.16	2.31	0.05	0.15	0.02	36,37,29
2158	1.36	1.56	1.55	6.386e+04	51.16	2.31	0.05	0.15	0.02	36,37,29
2160	1.66	1.64	1.44	7.732e+04	51.16	2.14	0.02	0.14	0.01	37,37,28
2162	1.29	1.66	1.44	6.086e+04	51.16	2.14	0.04	0.13	0.01	36,37,28
2164	1.10	1.46	1.46	5.232e+04	51.16	2.18	0.05	0.13	9.68e-03	20,37,41
2166	0.84	0.84	0.84	4.034e+04	51.16	1.26	0.15	0.15	9.25e-03	37,37,27
2168	0.43	0.50	0.46	2.122e+04	44.67	0.69	0.43	0.17	0.02	37,37,24
2170	0.43	0.50	0.46	2.122e+04	44.67	0.69	0.43	0.17	0.02	37,37,24
2201	1.36	1.56	1.55	6.386e+04	51.16	2.31	0.05	0.15	0.02	36,37,29

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				2.122e+04	44.67	0.69			
	1.66	1.66	1.55	7.732e+04	51.16	2.31	0.43	0.17	0.02

Setto	Mat.	Spessore	Stato
		cm	
132	mattoni pieni e malta di calce	38.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
2147	0.87	0.82	0.75	1.954e+04	35.00	1.12	0.03	0.07	0.05	31,30,26
2153	0.87	0.82	0.75	1.954e+04	35.00	1.12	0.03	0.07	0.05	31,30,26
2194	0.81	0.82	0.75	1.830e+04	35.00	1.12	0.04	0.07	0.05	31,30,26
2195	0.83	0.80	0.73	1.863e+04	35.00	1.09	0.08	0.06	0.03	34,30,26
2196	0.72	0.76	0.64	1.638e+04	35.00	0.95	0.10	0.06	0.02	34,32,26
2197	0.72	0.76	0.53	1.638e+04	35.00	0.79	0.10	0.06	0.03	34,32,42
2198	0.51	0.54	0.53	1.169e+04	35.00	0.79	0.22	0.06	0.03	33,27,42
2199	0.51	0.54	0.20	1.169e+04	35.00	0.31	0.22	0.06	0.15	33,27,32
2200	0.31	0.31	0.20	7016.31	35.00	0.31	0.17	0.04	0.15	29,33,32
2203	0.81	0.82	0.75	1.830e+04	35.00	1.12	0.04	0.07	0.05	31,30,26
2204	0.83	0.80	0.73	1.863e+04	35.00	1.09	0.08	0.06	0.03	34,30,26
2205	0.72	0.76	0.64	1.638e+04	35.00	0.95	0.10	0.06	0.02	34,32,26
2206	0.72	0.76	0.53	1.638e+04	35.00	0.79	0.10	0.06	0.03	34,32,42
2207	0.51	0.54	0.53	1.169e+04	35.00	0.79	0.22	0.06	0.03	33,27,42
2208	0.51	0.54	0.20	1.169e+04	35.00	0.31	0.22	0.06	0.15	33,27,32
2209	0.31	0.31	0.20	7016.31	35.00	0.31	0.17	0.04	0.15	29,33,32

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
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			7016.31	35.00	0.31			
0.87	0.82	0.75	1.954e+04	35.00	1.12	0.22	0.07	0.15

Setto	Mat.	Spessore	Stato
		cm	
133	mattoni pieni e malta di calce	37.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
670	0.70	0.70	0.70	1.481e+06	343.50	1.02	0.09	0.25	0.06	27,27,23
671	0.70	0.70	0.70	1.481e+06	343.50	1.02	0.09	0.25	0.06	27,27,23
680	0.70	0.70	0.70	1.481e+06	343.50	1.02	0.09	0.25	0.06	27,27,23
684	0.70	0.70	0.70	1.481e+06	343.50	1.02	0.09	0.25	0.06	27,27,23
690	0.70	0.70	0.70	1.481e+06	343.50	1.02	0.09	0.25	0.06	27,27,23
699	0.70	0.70	0.70	1.481e+06	343.50	1.02	0.09	0.25	0.06	27,27,23
709	0.70	0.70	0.70	1.481e+06	343.50	1.02	0.09	0.25	0.06	27,27,23
2113	0.70	0.70	0.70	1.481e+06	343.50	1.02	0.09	0.25	0.06	27,27,23
2114	0.63	0.71	0.71	1.351e+06	343.50	1.03	0.13	0.25	0.04	30,27,19
2115	0.77	0.68	0.68	9.961e+05	343.50	0.99	0.15	0.21	0.04	30,27,31
2116	0.77	0.82	0.78	9.961e+05	343.50	1.13	0.15	0.14	0.02	30,27,34
2117	0.78	0.84	0.61	1.006e+06	343.50	0.88	0.09	0.11	0.03	30,27,34
2118	0.61	0.48	0.51	8.983e+05	157.44	0.74	0.03	0.17	0.04	30,30,20
2119	0.24	0.48	0.26	3.284e+04	157.44	0.37	0.24	0.17	0.08	18,30,21
2120	0.24	0.24	0.26	3.284e+04	85.88	0.37	0.24	0.15	0.08	18,30,21
2248	0.70	0.70	0.70	1.481e+06	343.50	1.02	0.09	0.25	0.06	27,27,23
2249	0.63	0.71	0.71	1.351e+06	343.50	1.03	0.13	0.25	0.04	30,27,19
2250	0.77	0.68	0.68	9.961e+05	343.50	0.99	0.15	0.21	0.04	30,27,31
2251	0.77	0.82	0.78	9.961e+05	343.50	1.13	0.15	0.14	0.02	30,27,34
2252	0.78	0.84	0.61	1.006e+06	343.50	0.88	0.09	0.11	0.03	30,27,34
2253	0.61	0.48	0.51	8.983e+05	157.44	0.74	0.03	0.17	0.04	30,30,20
2254	0.24	0.48	0.26	3.284e+04	157.44	0.37	0.24	0.17	0.08	18,30,21
2255	0.77	0.82	0.78	9.961e+05	343.50	1.13	0.15	0.14	0.02	30,27,34
2256	0.78	0.84	0.59	1.006e+06	343.50	0.86	0.09	0.11	0.03	30,27,34
2257	0.70	0.70	0.70	1.481e+06	343.50	1.02	0.09	0.25	0.06	27,27,23
2258	0.63	0.71	0.71	1.351e+06	343.50	1.03	0.13	0.25	0.04	30,27,19
2259	0.77	0.68	0.68	9.961e+05	343.50	0.99	0.15	0.21	0.04	30,27,31
2260	0.77	0.82	0.78	9.961e+05	343.50	1.13	0.15	0.14	0.02	30,27,34
2261	0.78	0.84	0.58	1.006e+06	343.50	0.85	0.09	0.11	0.03	30,27,28
2262	0.45	0.45	0.48	2.427e+05	171.75	0.69	0.06	0.18	0.05	38,30,20
2263	0.45	0.45	0.48	2.427e+05	171.75	0.69	0.06	0.18	0.05	38,30,20
2264	0.78	0.84	0.59	1.006e+06	343.50	0.86	0.09	0.11	0.03	30,27,34
2265	0.59	0.59	0.59	1.134e+06	301.31	0.86	0.06	0.08	0.03	30,30,34
2266	0.70	0.70	0.70	1.481e+06	343.50	1.02	0.09	0.25	0.06	27,27,23
2267	0.63	0.71	0.71	1.351e+06	343.50	1.03	0.13	0.25	0.04	30,27,19
2268	0.77	0.68	0.68	9.961e+05	343.50	0.99	0.15	0.21	0.04	30,27,31
2269	0.77	0.82	0.78	9.961e+05	343.50	1.13	0.15	0.14	0.02	30,27,34
2270	0.78	0.84	0.58	1.006e+06	343.50	0.85	0.09	0.11	0.03	30,27,28
2271	0.45	0.45	0.48	2.427e+05	171.75	0.69	0.06	0.18	0.05	38,30,20
2274	0.70	0.70	0.70	1.481e+06	343.50	1.02	0.09	0.25	0.06	27,27,23
2275	0.70	0.70	0.70	1.481e+06	343.50	1.02	0.09	0.25	0.06	27,27,23
2276	0.63	0.71	0.71	1.351e+06	343.50	1.03	0.13	0.25	0.04	30,27,19
2277	0.77	0.68	0.68	9.961e+05	343.50	0.99	0.15	0.21	0.04	30,27,31
2278	0.77	0.82	0.78	9.961e+05	343.50	1.13	0.15	0.14	0.02	30,27,34
2279	0.78	0.84	0.58	1.006e+06	343.50	0.85	0.09	0.11	0.03	30,27,28
2280	0.59	0.59	0.58	9.665e+05	301.31	0.85	0.06	0.08	0.03	30,30,28
2281	0.63	0.71	0.71	1.351e+06	343.50	1.03	0.13	0.25	0.04	30,27,19
2282	0.77	0.68	0.68	9.961e+05	343.50	0.99	0.15	0.21	0.04	30,27,31
2283	0.77	0.82	0.78	9.961e+05	343.50	1.13	0.15	0.14	0.02	30,27,34
2284	0.70	0.70	0.70	1.481e+06	343.50	1.02	0.09	0.25	0.06	27,27,23
2285	0.63	0.71	0.71	1.351e+06	343.50	1.03	0.13	0.25	0.04	30,27,19
2286	0.77	0.68	0.68	9.961e+05	343.50	0.99	0.15	0.21	0.04	30,27,31
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				3.284e+04	85.88	0.37				
	0.78	0.84	0.78	1.481e+06	343.50	1.13	0.24	0.25	0.08	

Setto	Mat.	Spessore	Stato
		cm	
134	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
670	1.53	1.67	1.62	1.180e+05	64.00	2.54	0.26	0.89	0.02	21,24,30
935	1.53	1.67	1.62	1.180e+05	64.00	2.54	0.26	0.89	0.02	21,24,30
2113	1.53	1.67	1.55	1.180e+05	64.00	2.43	0.26	0.89	0.07	21,24,31
2114	1.59	1.63	1.41	1.222e+05	64.00	2.22	0.12	0.67	0.10	30,24,31
2115	1.48	1.49	1.41	1.142e+05	64.00	2.22	0.08	0.56	0.10	32,20,31
2116	1.37	1.37	1.16	1.059e+05	64.00	1.81	0.07	0.46	0.04	32,24,30
2117	1.18	1.18	0.94	9.190e+04	64.00	1.47	0.04	0.37	0.06	20,24,30
2118	0.77	0.96	0.77	6.148e+04	64.00	1.21	0.03	0.33	0.13	32,24,30
2119	0.77	0.79	0.65	6.148e+04	64.00	1.02	0.03	0.32	0.30	32,20,28
2120	0.44	0.50	0.65	3.560e+04	64.00	1.02	0.27	0.32	0.30	30,12,28
2121	0.44	0.50	0.45	3.560e+04	64.00	0.71	0.27	0.32	0.28	30,12,32
2287	1.53	1.67	1.55	1.180e+05	64.00	2.43	0.26	0.89	0.07	21,24,31
2288	1.59	1.63	1.41	1.222e+05	64.00	2.22	0.12	0.67	0.10	30,24,31
2289	1.48	1.49	1.41	1.142e+05	64.00	2.22	0.08	0.56	0.10	32,20,31
2290	1.37	1.37	1.16	1.059e+05	64.00	1.81	0.07	0.46	0.04	32,24,30
2291	1.18	1.18	0.94	9.190e+04	64.00	1.47	0.04	0.37	0.06	20,24,30
2292	0.77	0.96	0.77	6.148e+04	64.00	1.21	0.03	0.33	0.13	32,24,30
2293	0.77	0.79	0.65	6.148e+04	64.00	1.02	0.03	0.32	0.30	32,20,28
2294	0.44	0.50	0.65	3.560e+04	64.00	1.02	0.27	0.32	0.30	30,12,28
2295	0.44	0.50	0.45	3.560e+04	64.00	0.71	0.27	0.32	0.28	30,12,32

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
	1.59	1.67	1.62	3.560e+04	64.00	0.71			
				1.222e+05	64.00	2.54	0.27	0.89	0.30

Setto	Mat.	Spessore	Stato
		cm	
136	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
1020	1.38	1.38	1.28	4.559e+05	132.00	2.01	0.19	0.14	0.20	21,21,28
1030	1.38	1.38	1.28	4.559e+05	132.00	2.01	0.19	0.14	0.20	21,21,28
1039	1.38	1.38	1.28	4.559e+05	132.00	2.01	0.19	0.14	0.20	21,21,28
2305	1.38	1.38	1.28	4.559e+05	132.00	2.01	0.19	0.14	0.20	21,21,28
2306	1.36	1.24	1.27	4.473e+05	132.00	1.99	0.13	0.10	0.17	21,20,28
2307	1.31	1.26	1.25	4.318e+05	132.00	1.96	0.10	0.17	0.12	21,20,28
2308	1.29	1.29	1.27	4.262e+05	132.00	1.99	0.14	0.24	0.09	24,20,28
2309	1.29	1.18	1.29	4.262e+05	132.00	2.03	0.14	0.29	0.08	24,20,28
2310	1.18	0.98	0.95	3.924e+05	132.00	1.49	0.11	0.33	0.11	20,20,27
2311	0.98	0.86	0.82	3.294e+05	132.00	1.29	0.02	0.34	0.16	20,20,27
2312	0.81	0.86	0.72	2.744e+05	132.00	1.13	8.66e-03	0.34	0.20	21,20,27
2313	0.71	0.75	0.72	2.357e+05	130.50	1.13	4.00e-03	0.31	0.20	21,20,27
2314	1.38	1.38	1.28	4.559e+05	132.00	2.01	0.19	0.14	0.20	21,21,28
2315	1.36	1.24	1.27	4.473e+05	132.00	1.99	0.13	0.10	0.17	21,20,28
2316	1.31	1.26	1.25	4.318e+05	132.00	1.96	0.10	0.17	0.12	21,20,28
2317	1.29	1.29	1.27	4.262e+05	132.00	1.99	0.14	0.24	0.09	24,20,28
2318	1.29	1.18	1.29	4.262e+05	132.00	2.03	0.14	0.29	0.08	24,20,28
2319	1.18	0.98	0.95	3.924e+05	132.00	1.49	0.11	0.33	0.11	20,20,27
2320	0.98	0.86	0.82	3.294e+05	132.00	1.29	0.02	0.34	0.16	20,20,27
2321	0.81	0.86	0.72	2.744e+05	132.00	1.13	8.66e-03	0.34	0.20	21,20,27
2322	0.71	0.75	0.72	2.357e+05	130.50	1.13	4.00e-03	0.31	0.20	21,20,27
2327	1.29	1.18	1.29	4.262e+05	132.00	2.03	0.14	0.29	0.08	24,20,28
2328	1.18	0.98	0.95	3.924e+05	132.00	1.49	0.11	0.33	0.11	20,20,27
2329	0.98	0.86	0.82	3.294e+05	132.00	1.29	0.02	0.34	0.16	20,20,27
2330	0.81	0.86	0.72	2.744e+05	132.00	1.13	8.66e-03	0.34	0.20	21,20,27
2331	0.71	0.75	0.72	2.357e+05	130.50	1.13	4.00e-03	0.31	0.20	21,20,27
2386	1.36	1.24	1.27	4.473e+05	132.00	1.99	0.13	0.10	0.17	21,20,28
2387	1.31	1.26	1.25	4.318e+05	132.00	1.96	0.10	0.17	0.12	21,20,28
2388	1.29	1.29	1.27	4.262e+05	132.00	1.99	0.14	0.24	0.09	24,20,28
2404	0.98	0.86	0.82	3.294e+05	132.00	1.29	0.02	0.34	0.16	20,20,27
2406	0.81	0.86	0.72	2.744e+05	132.00	1.13	8.66e-03	0.34	0.20	21,20,27
2407	0.71	0.75	0.72	2.357e+05	130.50	1.13	4.00e-03	0.31	0.20	21,20,27
2408	1.38	1.38	1.28	4.559e+05	132.00	2.01	0.19	0.14	0.20	21,21,28
2424	1.38	1.38	1.28	4.559e+05	132.00	2.01	0.19	0.14	0.20	21,21,28
2425	1.38	1.38	1.28	4.559e+05	132.00	2.01	0.19	0.14	0.20	21,21,28
2426	1.36	1.24	1.27	4.473e+05	132.00	1.99	0.13	0.10	0.17	21,20,28

2427	1.31	1.26	1.25	4.318e+05	132.00	1.96	0.10	0.17	0.12	21,20,28
2428	1.29	1.29	1.27	4.262e+05	132.00	1.99	0.14	0.24	0.09	24,20,28
2429	1.29	1.18	1.29	4.262e+05	132.00	2.03	0.14	0.29	0.08	24,20,28
2430	1.18	0.98	0.95	3.924e+05	132.00	1.49	0.11	0.33	0.11	20,20,27

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				2.357e+05	130.50	1.13				
	1.38	1.38	1.29	4.559e+05	132.00	2.03	0.19	0.34	0.20	

Setto	Mat.	Spessore	Stato
		cm	
137	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
875	2.13	2.36	2.36	8.279e+04	46.00	3.69	0.23	0.77	0.02	36,21,13
929	2.13	2.36	2.36	8.279e+04	46.00	3.69	0.23	0.77	0.02	36,21,13
2323	2.23	2.02	2.22	8.610e+04	46.00	3.48	0.07	0.61	0.03	21,26,29
2324	2.06	2.02	1.71	8.007e+04	46.00	2.68	0.06	0.61	0.05	21,26,28
2325	1.83	1.80	1.55	7.175e+04	46.00	2.44	0.03	0.60	0.10	39,26,42
2326	1.44	1.60	1.55	5.766e+04	46.00	2.44	0.02	0.51	0.10	26,26,42
2332	1.45	1.44	1.41	5.802e+04	46.00	2.21	0.02	0.34	0.08	26,26,42
2333	1.82	1.42	1.86	7.137e+04	46.00	2.92	0.11	0.21	0.14	20,42,35
2334	1.88	1.77	1.95	7.352e+04	46.00	3.05	0.33	0.07	0.17	42,42,41
2335	1.88	1.96	1.95	7.352e+04	46.00	3.05	0.33	0.06	0.17	42,39,41
2414	2.13	2.36	2.22	8.279e+04	46.00	3.48	0.23	0.77	0.03	36,21,29
2415	2.23	2.02	2.22	8.610e+04	46.00	3.48	0.07	0.61	0.03	21,26,29
2416	2.06	2.02	1.71	8.007e+04	46.00	2.68	0.06	0.61	0.05	21,26,28
2417	1.83	1.80	1.55	7.175e+04	46.00	2.44	0.03	0.60	0.10	39,26,42
2418	1.44	1.60	1.55	5.766e+04	46.00	2.44	0.02	0.51	0.10	26,26,42
2419	1.45	1.44	1.41	5.802e+04	46.00	2.21	0.02	0.34	0.08	26,26,42
2420	1.82	1.42	1.86	7.137e+04	46.00	2.92	0.11	0.21	0.14	20,42,35
2421	1.88	1.77	1.95	7.352e+04	46.00	3.05	0.33	0.07	0.17	42,42,41
2422	1.88	1.96	1.95	7.352e+04	46.00	3.05	0.33	0.06	0.17	42,39,41
2423	2.13	2.36	2.22	8.279e+04	46.00	3.48	0.23	0.77	0.03	36,21,29

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				5.766e+04	46.00	2.21				
	2.23	2.36	2.36	8.610e+04	46.00	3.69	0.33	0.77	0.17	

Setto	Mat.	Spessore	Stato
		cm	
139	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
975	1.65	1.65	1.57	5.449e+05	133.00	2.46	0.18	0.16	0.22	23,23,28
984	1.65	1.65	1.57	5.449e+05	133.00	2.46	0.18	0.16	0.22	23,23,28
993	1.65	1.65	1.57	5.449e+05	133.00	2.46	0.18	0.16	0.22	23,23,28
1002	1.65	1.65	1.57	5.449e+05	133.00	2.46	0.18	0.16	0.22	23,23,28
2341	1.65	1.65	1.57	5.449e+05	133.00	2.46	0.18	0.16	0.22	23,23,28
2342	1.56	1.40	1.49	5.168e+05	133.00	2.34	0.14	0.14	0.21	23,23,28
2343	1.36	1.40	1.36	4.540e+05	133.00	2.13	0.12	0.14	0.18	36,23,28
2344	1.11	1.24	1.22	3.751e+05	133.00	1.91	0.12	0.14	0.14	26,23,28
2345	1.11	1.08	1.08	3.751e+05	133.00	1.69	0.12	0.12	0.11	26,23,28
2346	0.94	0.76	0.73	3.187e+05	133.00	1.15	0.08	0.16	0.12	22,26,39
2347	0.66	0.66	0.62	2.260e+05	133.00	0.97	0.07	0.22	0.20	26,26,31
2348	0.56	0.56	0.62	1.933e+05	133.00	0.97	0.10	0.24	0.20	26,26,31
2349	0.56	0.56	0.53	1.933e+05	133.00	0.84	0.10	0.24	0.19	26,26,31
2350	1.65	1.65	1.57	5.449e+05	133.00	2.46	0.18	0.16	0.22	23,23,28
2351	1.56	1.40	1.49	5.168e+05	133.00	2.34	0.14	0.14	0.21	23,23,28
2352	1.36	1.40	1.36	4.540e+05	133.00	2.13	0.12	0.14	0.18	36,23,28
2353	1.11	1.24	1.22	3.751e+05	133.00	1.91	0.12	0.14	0.14	26,23,28
2354	1.11	1.08	1.08	3.751e+05	133.00	1.69	0.12	0.12	0.11	26,23,28
2355	0.94	0.76	0.73	3.187e+05	133.00	1.15	0.08	0.16	0.12	22,26,39
2356	0.66	0.66	0.62	2.260e+05	133.00	0.97	0.07	0.22	0.20	26,26,31

2357	0.56	0.56	0.62	1.933e+05	133.00	0.97	0.10	0.24	0.20	26,26,31
2358	0.56	0.56	0.53	1.933e+05	133.00	0.84	0.10	0.24	0.19	26,26,31
2359	1.65	1.65	1.57	5.449e+05	133.00	2.46	0.18	0.16	0.22	23,23,28
2360	1.56	1.40	1.49	5.168e+05	133.00	2.34	0.14	0.14	0.21	23,23,28
2361	1.36	1.40	1.36	4.540e+05	133.00	2.13	0.12	0.14	0.18	36,23,28
2362	1.11	1.24	1.22	3.751e+05	133.00	1.91	0.12	0.14	0.14	26,23,28
2363	1.11	1.08	1.08	3.751e+05	133.00	1.69	0.12	0.12	0.11	26,23,28
2364	0.94	0.76	0.73	3.187e+05	133.00	1.15	0.08	0.16	0.12	22,26,39
2365	0.66	0.66	0.62	2.260e+05	133.00	0.97	0.07	0.22	0.20	26,26,31
2366	0.56	0.56	0.62	1.933e+05	133.00	0.97	0.10	0.24	0.20	26,26,31
2367	0.56	0.56	0.53	1.933e+05	133.00	0.84	0.10	0.24	0.19	26,26,31
2368	1.65	1.65	1.57	5.449e+05	133.00	2.46	0.18	0.16	0.22	23,23,28
2369	1.56	1.40	1.49	5.168e+05	133.00	2.34	0.14	0.14	0.21	23,23,28
2370	1.36	1.40	1.36	4.540e+05	133.00	2.13	0.12	0.14	0.18	36,23,28
2371	1.11	1.24	1.22	3.751e+05	133.00	1.91	0.12	0.14	0.14	26,23,28
2372	1.11	1.08	1.08	3.751e+05	133.00	1.69	0.12	0.12	0.11	26,23,28
2373	0.94	0.76	0.73	3.187e+05	133.00	1.15	0.08	0.16	0.12	22,26,39
2374	0.66	0.66	0.62	2.260e+05	133.00	0.97	0.07	0.22	0.20	26,26,31
2375	0.56	0.56	0.62	1.933e+05	133.00	0.97	0.10	0.24	0.20	26,26,31
2376	0.56	0.56	0.53	1.933e+05	133.00	0.84	0.10	0.24	0.19	26,26,31

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				1.933e+05	133.00	0.84			
	1.65	1.65	1.57	5.449e+05	133.00	2.46	0.18	0.24	0.22

Setto	Mat.	Spessore	Stato
		cm	
140	mattoni pieni e malta di calce	37.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
771	1.01	1.02	1.04	6.392e+05	188.75	1.51	0.11	0.04	0.07	26,31,34
780	1.01	1.02	1.04	6.392e+05	188.75	1.51	0.11	0.04	0.07	26,31,34
790	1.01	1.02	1.04	6.392e+05	188.75	1.51	0.11	0.04	0.07	26,31,34
800	1.01	1.02	1.04	6.392e+05	188.75	1.51	0.11	0.04	0.07	26,31,34
810	1.01	1.02	1.04	6.392e+05	188.75	1.51	0.11	0.04	0.07	26,31,34
2444	1.01	1.10	1.12	6.392e+05	188.75	1.62	0.11	0.09	0.08	26,31,34
2445	1.01	1.10	1.12	6.392e+05	188.75	1.62	0.11	0.09	0.08	26,31,34
2446	1.04	1.05	1.12	6.601e+05	188.75	1.62	0.17	0.14	0.08	21,31,34
2447	1.04	1.05	1.12	6.601e+05	188.75	1.62	0.17	0.14	0.08	21,31,34
2448	0.96	0.97	0.96	6.094e+05	188.75	1.40	0.24	0.14	0.08	33,39,29
2449	0.96	0.97	0.96	6.094e+05	188.75	1.40	0.24	0.14	0.08	33,39,29
2450	0.86	0.97	0.86	5.463e+05	188.75	1.24	0.35	0.14	0.16	33,39,33
2451	0.86	0.97	0.86	5.463e+05	188.75	1.24	0.35	0.14	0.16	33,39,33
2452	0.82	0.87	0.82	4.302e+05	188.75	1.19	0.37	0.09	0.20	33,31,33
2453	0.86	0.87	0.86	5.463e+05	188.75	1.24	0.35	0.09	0.16	33,31,33
2482	1.01	1.10	1.12	6.392e+05	188.75	1.62	0.11	0.09	0.08	26,31,34
2483	1.04	1.05	1.12	6.601e+05	188.75	1.62	0.17	0.14	0.08	21,31,34
2484	0.96	0.97	0.96	6.094e+05	188.75	1.40	0.24	0.14	0.08	33,39,29
2485	0.86	0.97	0.86	5.463e+05	188.75	1.24	0.35	0.14	0.16	33,39,33
2486	0.82	0.87	0.82	4.302e+05	188.75	1.19	0.37	0.09	0.20	33,31,33
2487	0.82	0.80	0.82	4.302e+05	153.50	1.19	0.37	0.17	0.20	33,33,33
2488	0.82	0.80	0.82	4.302e+05	153.50	1.19	0.37	0.17	0.20	33,33,33
2489	0.80	0.71	0.79	3.398e+05	153.50	1.14	0.22	0.17	0.13	33,33,21
2490	0.80	0.71	0.79	3.398e+05	153.50	1.14	0.22	0.17	0.13	33,33,21
2491	0.60	0.71	0.63	2.536e+05	153.50	0.92	0.12	0.17	0.26	21,33,39
2492	0.60	0.71	0.63	2.536e+05	153.50	0.92	0.12	0.17	0.26	21,33,39
2493	0.60	0.61	0.63	2.536e+05	153.50	0.92	0.12	0.13	0.26	21,33,39
2494	0.60	0.61	0.63	2.536e+05	153.50	0.92	0.12	0.13	0.26	21,33,39
2495	1.01	1.10	1.12	6.392e+05	188.75	1.62	0.11	0.09	0.09	26,31,34
2496	1.04	1.05	1.12	6.601e+05	188.75	1.62	0.17	0.14	0.09	21,31,34
2497	0.96	0.97	0.96	6.094e+05	188.75	1.40	0.24	0.14	0.08	33,39,29
2498	0.86	0.97	0.86	5.463e+05	188.75	1.24	0.35	0.14	0.16	33,39,33
2499	0.82	0.87	0.82	4.302e+05	188.75	1.19	0.37	0.09	0.20	33,31,33
2500	0.82	0.80	0.82	4.302e+05	153.50	1.19	0.37	0.17	0.20	33,33,33
2501	0.80	0.71	0.79	3.398e+05	153.50	1.14	0.22	0.17	0.13	33,33,21
2502	0.60	0.71	0.63	2.536e+05	153.50	0.92	0.12	0.17	0.26	21,33,39
2503	0.60	0.61	0.63	2.536e+05	153.50	0.92	0.12	0.13	0.26	21,33,39
2504	1.01	1.10	1.12	6.392e+05	188.75	1.62	0.11	0.09	0.09	26,31,34
2505	1.04	1.05	1.12	6.596e+05	188.75	1.62	0.16	0.13	0.09	21,31,34
2506	0.96	0.97	0.96	6.094e+05	188.75	1.40	0.24	0.14	0.08	33,39,29
2507	0.86	0.97	0.86	5.463e+05	188.75	1.24	0.35	0.14	0.16	33,39,33

2508	0.82	0.87	0.82	4.302e+05	188.75	1.19	0.37	0.09	0.20	33,31,33
2509	0.82	0.80	0.82	4.302e+05	153.50	1.19	0.37	0.17	0.20	33,33,33
2510	0.80	0.71	0.79	3.398e+05	153.50	1.14	0.22	0.17	0.13	33,33,21
2511	0.60	0.71	0.63	2.536e+05	153.50	0.92	0.12	0.17	0.26	21,33,39
2512	0.60	0.61	0.63	2.536e+05	153.50	0.92	0.12	0.13	0.26	21,33,39

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
	1.04	1.10	1.12	2.536e+05 6.601e+05	153.50 188.75	0.92 1.62	0.37	0.17	0.26

Setto	Mat.	Spessore	Stato
		cm	
144	mattoni pieni e malta di calce	40.0	NV L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
2772	0.34	0.62	0.34	6.971e+04	56.32	0.53	0.64	0.12	0.18	37,37,25
2773	0.34	0.62	0.34	6.971e+04	56.32	0.53	0.64	0.12	0.18	37,37,25
2774	0.34	0.62	0.34	6.971e+04	56.32	0.53	0.64	0.12	0.18	37,37,25
2805	0.34	0.62	0.34	6.971e+04	56.32	0.53	0.64	0.12	0.18	37,37,25
2806	0.74	1.10	0.61	1.484e+05	68.23	0.96	0.57	0.12	0.09	37,37,21
2807	0.74	0.86	0.66	1.484e+05	82.97	1.03	0.57	0.19	0.05	37,37,19
2808	0.70	0.86	0.57	1.415e+05	82.97	0.89	0.47	0.19	0.07	37,37,19
2809	0.61	0.52	0.48	1.237e+05	101.90	0.75	0.26	0.16	0.09	37,37,23
2810	0.43	0.46	0.39	8.795e+04	94.89	0.60	0.39	0.18	0.11	37,37,23
2811	0.34	4.62	0.39	6.949e+04	7.49	0.60	0.96	1.31	0.11	37,37,23
2812	0.34	4.62	0.28	6.949e+04	7.49	0.45	0.96	1.31	0.07	37,37,25
2813	0.29	2.36	0.28	5.905e+04	12.39	0.45	0.93	0.14	0.07	37,37,25
2814	0.34	0.62	0.34	6.971e+04	56.32	0.53	0.64	0.12	0.18	37,37,25
2815	0.74	1.10	0.61	1.484e+05	68.23	0.96	0.57	0.12	0.09	37,37,21
2816	0.74	0.86	0.66	1.484e+05	82.97	1.03	0.57	0.19	0.05	37,37,19
2817	0.70	0.86	0.57	1.415e+05	82.97	0.89	0.47	0.19	0.07	37,37,19
2818	0.61	0.52	0.48	1.237e+05	101.90	0.75	0.26	0.16	0.09	37,37,23
2819	0.43	0.46	0.39	8.795e+04	94.89	0.60	0.39	0.18	0.11	37,37,23
2820	0.34	4.62	0.39	6.949e+04	7.49	0.60	0.96	1.31	0.11	37,37,23
2821	0.34	4.62	0.28	6.949e+04	7.49	0.45	0.96	1.31	0.07	37,37,25
2822	0.29	2.36	0.28	5.905e+04	12.39	0.45	0.93	0.14	0.07	37,37,25
2823	0.34	0.62	0.34	6.971e+04	56.32	0.53	0.64	0.12	0.18	37,37,25
2824	0.74	1.10	0.61	1.484e+05	68.23	0.96	0.57	0.12	0.09	37,37,21
2825	0.74	0.86	0.66	1.484e+05	82.97	1.03	0.57	0.19	0.05	37,37,19
2826	0.70	0.86	0.57	1.415e+05	82.97	0.89	0.47	0.19	0.07	37,37,19
2827	0.61	0.52	0.48	1.237e+05	101.90	0.75	0.26	0.16	0.09	37,37,23
2828	0.43	0.46	0.39	8.795e+04	94.89	0.60	0.39	0.18	0.11	37,37,23
2829	0.34	4.62	0.39	6.949e+04	7.49	0.60	0.96	1.31	0.11	37,37,23
2830	0.34	4.62	0.28	6.949e+04	7.49	0.45	0.96	1.31	0.07	37,37,25
2831	0.29	2.36	0.28	5.905e+04	12.39	0.45	0.93	0.14	0.07	37,37,25

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
	0.74	4.62	0.66	5.905e+04 1.484e+05	7.49 101.90	0.45 1.03	0.96	1.31	0.18

Setto	Mat.	Spessore	Stato
		cm	
146	mattoni pieni e malta di calce	37.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
740	1.52	1.52	1.52	1.337e+06	224.67	2.21	0.04	0.05	0.10	21,23,33
765	1.52	1.52	1.52	1.337e+06	224.67	2.21	0.04	0.05	0.10	21,23,33
829	1.52	1.52	1.52	1.337e+06	224.67	2.21	0.04	0.05	0.10	21,23,33
849	1.52	1.52	1.52	1.337e+06	224.67	2.21	0.04	0.05	0.10	21,23,33
1022	1.52	1.52	1.52	1.337e+06	224.67	2.21	0.04	0.05	0.10	21,23,33
1095	1.52	1.52	1.52	1.337e+06	224.67	2.21	0.04	0.05	0.10	21,23,33
2522	1.61	1.52	1.52	1.405e+06	224.67	2.21	0.05	0.05	0.10	21,23,33
2523	1.61	1.60	1.61	1.407e+06	224.67	2.34	0.06	0.04	0.08	21,20,33
2524	1.61	1.54	1.55	1.407e+06	224.67	2.25	0.06	0.04	0.06	21,20,39

2525	1.55	1.54	1.47	1.360e+06	224.67	2.13	0.05	0.04	0.15	21,20,37
2526	1.46	1.45	1.38	1.288e+06	224.67	2.00	0.04	0.04	0.25	21,20,37
2527	1.27	1.36	1.29	1.125e+06	224.67	1.87	0.05	0.04	0.37	20,20,41
2528	1.18	1.27	1.19	1.049e+06	224.67	1.73	0.07	0.04	0.50	20,20,25
2529	0.98	1.18	0.98	8.766e+05	224.67	1.42	0.08	0.04	0.76	20,20,42
2530	0.98	0.98	0.98	8.766e+05	224.67	1.42	0.08	0.03	0.76	20,20,42
2531	1.61	1.52	1.52	1.405e+06	224.67	2.21	0.05	0.05	0.10	21,23,33
2532	1.61	1.60	1.61	1.406e+06	224.67	2.34	0.06	0.04	0.08	21,20,33
2533	1.61	1.54	1.55	1.406e+06	224.67	2.25	0.06	0.04	0.06	21,20,39
2534	1.55	1.54	1.47	1.360e+06	224.67	2.13	0.05	0.04	0.15	21,20,37
2535	1.46	1.45	1.38	1.288e+06	224.67	2.00	0.04	0.04	0.25	21,20,37
2536	1.27	1.36	1.29	1.125e+06	224.67	1.87	0.05	0.04	0.37	20,20,41
2537	1.18	1.27	1.19	1.049e+06	224.67	1.73	0.07	0.04	0.50	20,20,25
2538	0.98	1.18	0.98	8.766e+05	224.67	1.42	0.08	0.04	0.76	20,20,42
2539	0.98	0.98	0.98	8.766e+05	224.67	1.42	0.08	0.03	0.76	20,20,42
2540	1.61	1.52	1.52	1.405e+06	224.67	2.21	0.05	0.05	0.10	21,23,33
2541	1.61	1.60	1.61	1.406e+06	224.67	2.33	0.06	0.04	0.08	21,20,33
2542	1.61	1.54	1.55	1.406e+06	224.67	2.25	0.06	0.04	0.06	21,20,39
2543	1.55	1.54	1.47	1.360e+06	224.67	2.13	0.05	0.04	0.15	21,20,37
2544	1.46	1.45	1.38	1.288e+06	224.67	2.00	0.04	0.04	0.25	21,20,37
2545	1.27	1.36	1.29	1.125e+06	224.67	1.87	0.05	0.04	0.37	20,20,41
2546	1.18	1.27	1.19	1.049e+06	224.67	1.73	0.07	0.04	0.50	20,20,25
2547	0.98	1.18	0.98	8.766e+05	224.67	1.42	0.08	0.04	0.76	20,20,42
2548	0.98	0.98	0.98	8.766e+05	224.67	1.42	0.08	0.03	0.76	20,20,42
2549	1.61	1.52	1.52	1.405e+06	224.67	2.21	0.05	0.05	0.10	21,23,33
2550	1.61	1.60	1.61	1.406e+06	224.67	2.33	0.06	0.04	0.08	21,20,33
2551	1.61	1.54	1.55	1.406e+06	224.67	2.25	0.06	0.04	0.06	21,20,39
2552	1.55	1.54	1.47	1.360e+06	224.67	2.13	0.05	0.04	0.15	21,20,37
2553	1.46	1.45	1.38	1.288e+06	224.67	2.00	0.04	0.04	0.25	21,20,37
2554	1.27	1.36	1.29	1.125e+06	224.67	1.87	0.05	0.04	0.37	20,20,41
2555	1.18	1.27	1.19	1.049e+06	224.67	1.73	0.07	0.04	0.50	20,20,25
2556	0.98	1.18	0.98	8.766e+05	224.67	1.42	0.08	0.04	0.76	20,20,42
2557	0.98	0.98	0.98	8.766e+05	224.67	1.42	0.08	0.03	0.76	20,20,42
2587	1.46	1.45	1.38	1.288e+06	224.67	2.00	0.04	0.04	0.25	21,20,37
2588	1.27	1.36	1.29	1.125e+06	224.67	1.87	0.05	0.04	0.37	20,20,41
2589	1.18	1.27	1.19	1.049e+06	224.67	1.73	0.07	0.04	0.50	20,20,25
2590	0.98	1.18	0.98	8.766e+05	224.67	1.42	0.08	0.04	0.76	20,20,42
2591	0.98	0.98	0.98	8.766e+05	224.67	1.42	0.08	0.03	0.76	20,20,42
2594	1.61	1.52	1.52	1.405e+06	224.67	2.21	0.05	0.05	0.10	21,23,33
2595	1.61	1.60	1.61	1.407e+06	224.67	2.34	0.06	0.04	0.08	21,20,33
2596	1.61	1.54	1.55	1.407e+06	224.67	2.25	0.06	0.04	0.06	21,20,39
2597	1.55	1.54	1.47	1.360e+06	224.67	2.13	0.05	0.04	0.15	21,20,37
2598	1.46	1.45	1.38	1.288e+06	224.67	2.00	0.04	0.04	0.25	21,20,37
2599	1.27	1.36	1.29	1.125e+06	224.67	1.87	0.05	0.04	0.37	20,20,41
2600	1.18	1.27	1.19	1.049e+06	224.67	1.73	0.07	0.04	0.50	20,20,25
2601	0.98	1.18	0.98	8.766e+05	224.67	1.42	0.08	0.04	0.76	20,20,42
2602	0.98	0.98	0.98	8.766e+05	224.67	1.42	0.08	0.03	0.76	20,20,42
2603	1.61	1.52	1.52	1.405e+06	224.67	2.21	0.05	0.05	0.10	21,23,33
2604	1.61	1.60	1.61	1.406e+06	224.67	2.34	0.06	0.04	0.08	21,20,33
2605	1.61	1.54	1.55	1.406e+06	224.67	2.25	0.06	0.04	0.06	21,20,39
2606	1.55	1.54	1.47	1.360e+06	224.67	2.13	0.05	0.04	0.15	21,20,37
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	1.61	1.60	1.61	8.766e+05	224.67	1.42				
				1.407e+06	224.67	2.34	0.08	0.05	0.76	

Setto	Mat.	Spessore	Stato
		cm	
147	mattoni pieni e malta di calce	37.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1064	2.22	2.22	2.24	2.919e+05	88.17	3.25	0.21	0.12	0.06	21,21,41
1065	2.22	2.22	2.24	2.919e+05	88.17	3.25	0.21	0.12	0.06	21,21,41
1075	2.22	2.22	2.24	2.919e+05	88.17	3.25	0.21	0.12	0.06	21,21,41
2558	2.22	2.22	2.46	2.919e+05	88.17	3.56	0.21	0.12	0.13	21,21,37
2559	2.22	2.22	2.46	2.919e+05	88.17	3.56	0.21	0.12	0.13	21,21,37
2560	2.43	2.33	2.44	3.156e+05	88.17	3.54	0.14	0.07	0.15	21,20,37
2561	2.42	2.33	2.44	3.147e+05	88.17	3.54	0.14	0.07	0.15	21,20,37
2562	2.39	2.15	2.44	3.119e+05	88.17	3.54	0.11	0.07	0.15	21,23,37
2563	2.39	2.15	2.44	3.110e+05	88.17	3.54	0.11	0.07	0.15	21,23,37
2564	2.21	1.88	2.23	2.906e+05	88.17	3.24	0.08	0.08	0.10	21,23,37

2565	2.21	1.88	2.23	2.906e+05	88.17	3.24	0.08	0.08	0.10	21,23,37
2566	1.98	1.63	1.70	2.627e+05	88.17	2.46	0.03	0.08	0.07	13,23,39
2567	1.98	1.63	1.70	2.627e+05	88.17	2.46	0.03	0.08	0.07	13,23,39
2568	1.51	1.63	1.44	2.049e+05	88.17	2.10	0.08	0.08	0.19	21,23,39
2569	1.51	1.63	1.44	2.049e+05	88.17	2.10	0.08	0.08	0.19	21,23,39
2570	1.30	1.38	1.23	1.780e+05	88.17	1.78	0.15	0.08	0.31	21,23,39
2571	1.30	1.38	1.23	1.780e+05	88.17	1.78	0.15	0.08	0.31	21,23,39
2572	1.30	1.16	1.23	1.780e+05	88.17	1.78	0.15	0.06	0.31	21,20,39
2573	1.30	1.16	1.23	1.780e+05	88.17	1.78	0.15	0.06	0.31	21,20,39
2574	1.03	0.98	0.98	1.416e+05	88.17	1.42	0.06	0.05	0.26	13,35,39
2575	1.03	0.98	0.98	1.416e+05	88.17	1.42	0.06	0.05	0.26	13,35,39
2576	2.22	2.22	2.44	2.919e+05	88.17	3.55	0.21	0.12	0.12	21,21,37
2577	2.42	2.31	2.43	3.147e+05	88.17	3.52	0.14	0.06	0.14	21,20,37
2578	2.39	2.15	2.43	3.110e+05	88.17	3.52	0.11	0.07	0.14	21,23,37
2579	2.21	1.88	2.23	2.906e+05	88.17	3.24	0.08	0.08	0.10	21,23,37
2580	1.98	1.63	1.70	2.627e+05	88.17	2.46	0.03	0.08	0.07	13,23,39
2581	1.51	1.63	1.44	2.049e+05	88.17	2.10	0.08	0.08	0.19	21,23,39
2582	1.30	1.38	1.23	1.780e+05	88.17	1.78	0.15	0.08	0.31	21,23,39
2583	1.30	1.16	1.23	1.780e+05	88.17	1.78	0.15	0.06	0.31	21,20,39
2584	1.03	0.98	0.98	1.416e+05	88.17	1.42	0.06	0.05	0.26	13,35,39

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				1.416e+05	88.17	1.42			
	2.43	2.33	2.46	3.156e+05	88.17	3.56	0.21	0.12	0.31

Setto	Mat.	Spessore	Stato
		cm	
151	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
875	4.82	4.95	5.11	1.312e+05	41.50	8.89	0.09	0.22	0.05	40,42,21
1285	4.82	4.95	5.11	1.312e+05	41.50	8.89	0.09	0.22	0.05	40,42,21
2323	4.10	4.10	4.20	1.160e+05	41.50	7.29	0.03	0.20	0.06	38,42,33
2324	2.30	2.41	3.33	7.133e+04	41.50	5.79	0.04	0.20	0.06	42,26,29
2325	1.51	1.59	1.53	4.852e+04	41.50	2.66	0.20	0.24	0.03	42,26,34
2326	1.12	1.59	1.25	3.668e+04	41.50	2.17	0.27	0.24	0.08	42,26,21
2332	1.12	1.34	1.25	3.668e+04	41.50	2.17	0.27	0.34	0.08	42,42,21
2333	2.02	1.93	1.94	6.351e+04	41.50	3.38	0.26	0.70	0.07	31,42,36
2334	2.34	1.93	2.34	7.242e+04	41.50	4.07	0.47	0.70	0.09	39,42,15
2335	2.34	2.63	2.34	7.242e+04	36.75	4.07	0.47	0.65	0.09	39,42,15
2423	4.82	4.95	4.20	1.312e+05	41.50	7.29	0.09	0.22	0.06	40,42,33
2625	4.10	4.10	4.20	1.160e+05	41.50	7.29	0.03	0.20	0.06	38,42,33
2626	2.30	2.41	3.33	7.133e+04	41.50	5.79	0.04	0.20	0.06	42,26,29
2634	1.51	1.59	1.53	4.852e+04	41.50	2.66	0.20	0.24	0.03	42,26,34
2635	1.12	1.59	1.25	3.668e+04	41.50	2.17	0.27	0.24	0.08	42,26,21
2640	4.82	4.95	4.20	1.312e+05	41.50	7.29	0.09	0.22	0.06	40,42,33
2981	2.34	1.93	2.34	7.242e+04	41.50	4.07	0.47	0.70	0.09	39,42,15
2982	2.34	2.63	2.34	7.242e+04	36.75	4.07	0.47	0.65	0.09	39,42,15
2990	1.12	1.34	1.25	3.668e+04	41.50	2.17	0.27	0.34	0.08	42,42,21
2991	2.02	1.93	1.94	6.351e+04	41.50	3.38	0.26	0.70	0.07	31,42,36

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				3.668e+04	36.75	2.17			
	4.82	4.95	5.11	1.312e+05	41.50	8.89	0.47	0.70	0.09

Setto	Mat.	Spessore	Stato
		cm	
155	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1119	1.58	1.59	1.63	8.433e+06	536.00	2.84	0.05	0.04	0.04	37,36,18
1185	1.58	1.59	1.63	8.433e+06	536.00	2.84	0.05	0.04	0.04	37,36,18
1186	1.58	1.59	1.63	8.433e+06	536.00	2.84	0.05	0.04	0.04	37,36,18
1195	1.58	1.59	1.63	8.433e+06	536.00	2.84	0.05	0.04	0.04	37,36,18

1204	1.58	1.59	1.63	8.433e+06	536.00	2.84	0.05	0.04	0.04	37,36,18
1213	1.58	1.59	1.63	8.433e+06	536.00	2.84	0.05	0.04	0.04	37,36,18
1222	1.58	1.59	1.63	8.433e+06	536.00	2.84	0.05	0.04	0.04	37,36,18
1231	1.58	1.59	1.63	8.433e+06	536.00	2.84	0.05	0.04	0.04	37,36,18
1240	1.58	1.59	1.63	8.433e+06	536.00	2.84	0.05	0.04	0.04	37,36,18
1249	1.58	1.59	1.63	8.433e+06	536.00	2.84	0.05	0.04	0.04	37,36,18
1258	1.58	1.59	1.63	8.433e+06	536.00	2.84	0.05	0.04	0.04	37,36,18
1950	1.58	1.59	1.63	8.433e+06	536.00	2.84	0.05	0.04	0.04	37,36,18
2661	1.58	1.53	1.63	8.433e+06	536.00	2.84	0.05	0.04	0.04	37,36,18
2662	1.51	1.44	1.55	8.087e+06	536.00	2.70	0.03	0.06	0.02	37,36,38
2663	1.41	1.34	1.31	7.628e+06	536.00	2.27	0.02	0.07	0.01	37,36,19
2664	1.22	1.25	1.22	6.623e+06	536.00	2.11	0.02	0.07	0.02	39,36,19
2665	1.12	1.15	1.22	6.134e+06	536.00	2.11	0.03	0.07	0.02	39,36,19
2666	1.02	1.15	1.12	5.593e+06	536.00	1.95	0.04	0.07	0.02	39,36,11
2667	0.92	1.04	0.92	5.054e+06	536.00	1.60	0.05	0.07	0.05	39,36,20
2668	0.83	0.93	0.83	4.611e+06	536.00	1.44	0.06	0.06	0.09	37,36,20
2669	0.83	0.84	0.83	4.611e+06	536.00	1.44	0.06	0.03	0.09	37,36,20
2670	1.58	1.53	1.63	8.433e+06	536.00	2.84	0.05	0.04	0.04	37,36,18
2671	1.51	1.44	1.55	8.087e+06	536.00	2.70	0.03	0.06	0.02	37,36,38
2672	1.41	1.34	1.31	7.628e+06	536.00	2.27	0.02	0.07	0.01	37,36,19
2673	1.22	1.25	1.22	6.623e+06	536.00	2.11	0.02	0.07	0.02	39,36,19
2674	1.12	1.15	1.22	6.134e+06	536.00	2.11	0.03	0.07	0.02	39,36,19
2675	1.02	1.15	1.12	5.593e+06	536.00	1.95	0.04	0.07	0.02	39,36,11
2676	0.92	1.04	0.92	5.054e+06	536.00	1.60	0.05	0.07	0.05	39,36,20
2677	0.83	0.93	0.83	4.611e+06	536.00	1.44	0.06	0.06	0.09	37,36,20
2678	0.83	0.84	0.83	4.611e+06	536.00	1.44	0.06	0.03	0.09	37,36,20
2679	1.58	1.53	1.63	8.433e+06	536.00	2.84	0.05	0.04	0.04	37,36,18
2680	1.51	1.44	1.55	8.087e+06	536.00	2.70	0.03	0.06	0.02	37,36,38
2681	1.41	1.34	1.31	7.628e+06	536.00	2.27	0.02	0.07	0.01	37,36,19
2682	1.22	1.25	1.22	6.623e+06	536.00	2.11	0.02	0.07	0.02	39,36,19
2683	1.12	1.15	1.22	6.134e+06	536.00	2.11	0.03	0.07	0.02	39,36,19
2684	1.02	1.15	1.12	5.593e+06	536.00	1.95	0.04	0.07	0.02	39,36,11
2685	0.92	1.04	0.92	5.054e+06	536.00	1.60	0.05	0.07	0.05	39,36,20
2686	0.83	0.93	0.83	4.611e+06	536.00	1.44	0.06	0.06	0.09	37,36,20
2687	0.83	0.84	0.83	4.611e+06	536.00	1.44	0.06	0.03	0.09	37,36,20
2688	1.58	1.53	1.63	8.433e+06	536.00	2.84	0.05	0.04	0.04	37,

2730	0.92	1.04	0.92	5.054e+06	536.00	1.60	0.05	0.07	0.05	39,36,20
2731	0.83	0.93	0.83	4.611e+06	536.00	1.44	0.06	0.06	0.09	37,36,20
2732	0.83	0.84	0.83	4.611e+06	536.00	1.44	0.06	0.03	0.09	37,36,20
2733	1.58	1.53	1.63	8.433e+06	536.00	2.84	0.05	0.04	0.04	37,36,18
2734	1.51	1.44	1.55	8.087e+06	536.00	2.70	0.03	0.06	0.02	37,36,38
2735	1.41	1.34	1.31	7.628e+06	536.00	2.27	0.02	0.07	0.01	37,36,19
2736	1.22	1.25	1.22	6.623e+06	536.00	2.11	0.02	0.07	0.02	39,36,19
2737	1.12	1.15	1.22	6.134e+06	536.00	2.11	0.03	0.07	0.02	39,36,19
2738	1.02	1.15	1.12	5.593e+06	536.00	1.95	0.04	0.07	0.02	39,36,11
2739	0.92	1.04	0.92	5.054e+06	536.00	1.60	0.05	0.07	0.05	39,36,20
2740	0.83	0.93	0.83	4.611e+06	536.00	1.44	0.06	0.06	0.09	37,36,20
2741	0.83	0.84	0.83	4.611e+06	536.00	1.44	0.06	0.03	0.09	37,36,20
2742	1.58	1.53	1.63	8.433e+06	536.00	2.84	0.05	0.04	0.04	37,36,18
2743	1.51	1.44	1.55	8.087e+06	536.00	2.70	0.03	0.06	0.02	37,36,38
2744	1.41	1.34	1.31	7.628e+06	536.00	2.27	0.02	0.07	0.01	37,36,19
2745	1.22	1.25	1.22	6.623e+06	536.00	2.11	0.02	0.07	0.02	39,36,19
2746	1.12	1.15	1.22	6.134e+06	536.00	2.11	0.03	0.07	0.02	39,36,19
2747	1.02	1.15	1.12	5.593e+06	536.00	1.95	0.04	0.07	0.02	39,36,11
2748	0.92	1.04	0.92	5.054e+06	536.00	1.60	0.05	0.07	0.05	39,36,20
2749	0.83	0.93	0.83	4.611e+06	536.00	1.44	0.06	0.06	0.09	37,36,20
2750	0.83	0.84	0.83	4.611e+06	536.00	1.44	0.06	0.03	0.09	37,36,20
2751	1.58	1.53	1.63	8.433e+06	536.00	2.84	0.05	0.04	0.04	37,36,18
2752	1.51	1.44	1.55	8.087e+06	536.00	2.70	0.03	0.06	0.02	37,36,38
2753	1.41	1.34	1.31	7.628e+06	536.00	2.27	0.02	0.07	0.01	37,36,19
2754	1.22	1.25	1.22	6.623e+06	536.00	2.11	0.02	0.07	0.02	39,36,19
2755	1.12	1.15	1.22	6.134e+06	536.00	2.11	0.03	0.07	0.02	39,36,19
2756	1.02	1.15	1.12	5.593e+06	536.00	1.95	0.04	0.07	0.02	39,36,11
2757	0.92	1.04	0.92	5.054e+06	536.00	1.60	0.05	0.07	0.05	39,36,20
2758	0.83	0.93	0.83	4.611e+06	536.00	1.44	0.06	0.06	0.09	37,36,20
2759	0.83	0.84	0.83	4.611e+06	536.00	1.44	0.06	0.03	0.09	37,36,20
2760	1.58	1.53	1.63	8.433e+06	536.00	2.84	0.05	0.04	0.04	37,36,18
2761	1.51	1.44	1.55	8.087e+06	536.00	2.70	0.03	0.06	0.02	37,36,38
2762	1.41	1.34	1.31	7.628e+06	536.00	2.27	0.02	0.07	0.01	37,36,19
2763	1.22	1.25	1.22	6.623e+06	536.00	2.11	0.02	0.07	0.02	39,36,19
2764	1.12	1.15	1.22	6.134e+06	536.00	2.11	0.03	0.07	0.02	39,36,19
2765	1.02	1.15	1.12	5.593e+06	536.00	1.95	0.04	0.07	0.02	39,36,11
2766	0.92	1.04	0.92	5.054e+06	536.00	1.60	0.05	0.07	0.05	39,36,20
2767	0.83	0.93	0.83	4.611e+06	536.00	1.44	0.06	0.06	0.09	37,36,20
2768	0.83	0.84	0.83	4.611e+06	536.00	1.44	0.06	0.03	0.09	37,36,20

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				4.611e+06	536.00	1.44			
	1.58	1.59	1.63	8.433e+06	536.00	2.84	0.06	0.07	0.09

Setto	Mat.	Spessore	Stato
		cm	
156	mattoni pieni e malta di calce	40.0	NV L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1119	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0,0,0
2760	3.51e-03	0.0	3.51e-03	182.47	0.0	5.51e-03	62.54	0.0	20.95	33,0,33
2761	3.51e-03	0.63	3.51e-03	182.47	14.65	5.51e-03	62.54	1.07	20.95	33,26,33
2762	0.11	0.63	0.11	5479.99	14.65	0.17	1.69	1.07	0.50	36,26,36
2763	0.45	0.43	0.74	2.308e+04	50.95	1.16	0.10	0.25	0.07	16,36,15
2764	0.72	0.70	0.90	3.639e+04	50.95	1.41	0.02	0.15	0.09	16,36,23
2765	1.05	1.05	0.90	5.244e+04	50.95	1.41	0.06	0.18	0.09	36,36,23
2766	1.33	1.33	1.04	6.552e+04	50.95	1.63	0.22	0.39	0.05	36,36,35
2767	1.33	1.24	1.21	6.552e+04	50.95	1.89	0.22	0.49	0.10	36,16,23
2768	1.24	1.24	1.21	6.139e+04	50.95	1.89	0.21	0.49	0.10	36,16,23
2769	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0,0,0
2778	3.51e-03	0.0	3.51e-03	182.47	0.0	5.51e-03	62.54	0.0	20.95	33,0,33
2779	3.51e-03	0.63	3.51e-03	182.47	14.65	5.51e-03	62.54	1.07	20.95	33,26,33
2780	0.11	0.63	0.11	5479.99	14.65	0.17	1.69	1.07	0.50	36,26,36
2781	0.45	0.43	0.74	2.308e+04	50.95	1.16	0.10	0.25	0.07	16,36,15
2782	0.72	0.70	0.90	3.639e+04	50.95	1.41	0.02	0.15	0.09	16,36,23
2783	1.05	1.05	0.90	5.244e+04	50.95	1.41	0.06	0.18	0.09	36,36,23
2784	1.33	1.33	1.04	6.552e+04	50.95	1.63	0.22	0.39	0.05	36,36,35
2785	1.33	1.24	1.21	6.552e+04	50.95	1.89	0.22	0.49	0.10	36,16,23
2786	1.24	1.24	1.21	6.139e+04	50.95	1.89	0.21	0.49	0.10	36,16,23

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
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1.33 1.33 1.21 6.552e+04 0.0 50.95 0.0 1.89 62.54 1.07 20.95

Setto	Mat.	Spessore	Stato
		cm	
159	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
1064	2.46	2.33	2.57	1.155e+05	50.95	4.04	0.28	0.23	0.04	39,20,13
2516	1.85	2.33	1.75	8.911e+04	50.95	2.74	0.31	0.23	0.06	39,20,12
2517	1.61	1.53	1.74	7.816e+04	50.95	2.74	0.34	0.13	0.07	39,23,21
2518	1.61	1.71	1.74	7.816e+04	50.95	2.74	0.34	0.21	0.07	39,39,21
2519	1.71	1.71	1.83	8.291e+04	50.95	2.88	0.16	0.21	0.05	39,39,21
2558	1.85	2.33	1.75	8.911e+04	50.95	2.74	0.31	0.23	0.06	39,20,12
2560	1.61	1.53	1.74	7.816e+04	50.95	2.74	0.34	0.13	0.07	39,23,21
2562	1.61	1.71	1.74	7.816e+04	50.95	2.74	0.34	0.21	0.07	39,39,21
2564	1.71	1.71	1.83	8.291e+04	50.95	2.88	0.16	0.21	0.05	39,39,21
2566	2.12	1.90	1.97	1.007e+05	50.95	3.09	0.08	0.20	0.02	37,35,13
2568	2.28	2.16	2.26	1.076e+05	50.95	3.55	0.18	0.20	0.03	37,23,21
2570	2.39	2.28	2.36	1.126e+05	50.95	3.70	0.32	0.24	0.03	37,23,21
2572	2.39	2.28	2.36	1.126e+05	50.95	3.70	0.32	0.24	0.03	37,23,21
2574	1.87	1.77	1.78	8.976e+04	50.95	2.79	0.26	0.20	0.02	29,24,20
2777	2.46	2.33	2.57	1.155e+05	50.95	4.04	0.28	0.23	0.04	39,20,13
2793	2.12	1.90	1.97	1.007e+05	50.95	3.09	0.08	0.20	0.02	37,35,13
2798	2.28	2.16	2.26	1.076e+05	50.95	3.55	0.18	0.20	0.03	37,23,21
2799	2.39	2.28	2.36	1.126e+05	50.95	3.70	0.32	0.24	0.03	37,23,21
2800	2.39	2.28	2.36	1.126e+05	50.95	3.70	0.32	0.24	0.03	37,23,21
2801	1.87	1.77	1.78	8.976e+04	50.95	2.79	0.26	0.20	0.02	29,24,20

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
	2.46	2.33	2.57	7.816e+04	50.95	2.74			
				1.155e+05	50.95	4.04	0.34	0.24	0.07

Setto	Mat.	Spessore	Stato
		cm	
162	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
1119	2.09	2.08	1.95	1.705e+05	67.00	3.39	0.21	0.22	0.05	39,23,42
1120	2.09	2.08	1.95	1.705e+05	67.00	3.39	0.21	0.22	0.05	39,23,42
2760	2.09	2.08	1.61	1.705e+05	67.00	2.80	0.21	0.22	0.06	39,23,42
2761	1.72	1.72	1.34	1.431e+05	67.00	2.33	0.17	0.17	0.07	39,23,36
2762	1.40	1.39	1.34	1.180e+05	67.00	2.33	0.12	0.13	0.07	37,23,36
2763	0.89	0.89	1.11	7.659e+04	67.00	1.94	0.11	0.12	0.05	23,23,16
2764	0.74	0.89	0.85	6.397e+04	67.00	1.48	0.24	0.12	0.03	23,23,18
2765	0.67	0.76	0.73	5.875e+04	67.00	1.26	0.25	0.07	0.05	23,39,42
2766	0.60	0.60	0.61	5.283e+04	67.00	1.07	0.27	0.14	0.08	23,39,16
2767	0.38	0.48	0.39	3.370e+04	54.75	0.68	0.47	0.24	0.08	27,23,36
2768	0.38	0.48	0.39	3.370e+04	54.75	0.68	0.47	0.24	0.08	27,23,36
2832	2.09	2.08	1.61	1.705e+05	67.00	2.80	0.21	0.22	0.06	39,23,42
2833	1.72	1.72	1.34	1.431e+05	67.00	2.33	0.17	0.17	0.07	39,23,36
2834	1.40	1.39	1.34	1.180e+05	67.00	2.33	0.12	0.13	0.07	37,23,36
2835	0.89	0.89	1.11	7.659e+04	67.00	1.94	0.11	0.12	0.05	23,23,16
2836	0.74	0.89	0.85	6.397e+04	67.00	1.48	0.24	0.12	0.03	23,23,18
2837	0.67	0.76	0.73	5.875e+04	67.00	1.26	0.25	0.07	0.05	23,39,42
2838	0.60	0.60	0.61	5.283e+04	67.00	1.07	0.27	0.14	0.08	23,39,16
2839	0.38	0.48	0.39	3.370e+04	54.75	0.68	0.47	0.24	0.08	27,23,36
2840	0.38	0.48	0.39	3.370e+04	54.75	0.68	0.47	0.24	0.08	27,23,36

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
	2.09	2.08	1.95	3.370e+04	54.75	0.68			
				1.705e+05	67.00	3.39	0.47	0.24	0.08

Setto	Mat.	Spessore	Stato
		cm	
163	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
1123	1.45	1.45	1.48	5.039e+05	136.00	2.57	0.04	0.06	0.03	23,23,42
1142	1.45	1.45	1.48	5.039e+05	136.00	2.57	0.04	0.06	0.03	23,23,42
1147	1.45	1.45	1.48	5.039e+05	136.00	2.57	0.04	0.06	0.03	23,23,42
1167	1.45	1.45	1.48	5.039e+05	136.00	2.57	0.04	0.06	0.03	23,23,42
2841	1.46	1.44	1.47	5.054e+05	136.00	2.55	0.03	0.06	0.02	23,23,38
2842	1.41	1.41	1.48	4.905e+05	136.00	2.56	0.01	0.06	0.02	23,23,18
2843	1.35	1.35	1.29	4.687e+05	136.00	2.23	0.07	0.07	0.06	23,23,42
2844	1.35	1.35	1.04	4.687e+05	136.00	1.80	0.07	0.07	0.11	23,23,42
2850	0.70	0.71	0.69	2.517e+05	136.00	1.21	0.09	0.06	0.13	26,21,42
2851	0.41	0.42	0.41	1.473e+05	136.00	0.70	0.13	0.07	0.18	26,33,26
2852	0.16	0.42	0.16	5.699e+04	136.00	0.28	0.22	0.07	0.26	26,33,29
2853	0.16	0.16	0.16	5.699e+04	136.00	0.28	0.22	0.06	0.26	26,27,29
2859	1.45	1.46	1.48	5.039e+05	136.00	2.57	0.04	0.06	0.03	23,23,42
2860	1.46	1.44	1.47	5.054e+05	136.00	2.55	0.03	0.06	0.02	23,23,38
2861	1.41	1.41	1.48	4.905e+05	136.00	2.56	0.01	0.06	0.02	23,23,18
2862	1.35	1.35	1.29	4.687e+05	136.00	2.23	0.07	0.07	0.06	23,23,42
2863	1.35	1.35	1.04	4.687e+05	136.00	1.80	0.07	0.07	0.11	23,23,42
2864	0.70	0.71	0.69	2.517e+05	136.00	1.21	0.09	0.06	0.13	26,21,42
2865	0.41	0.42	0.41	1.473e+05	136.00	0.70	0.13	0.07	0.18	26,33,26
2866	0.16	0.42	0.16	5.699e+04	136.00	0.28	0.22	0.07	0.26	26,33,29
2867	0.16	0.16	0.16	5.699e+04	136.00	0.28	0.22	0.06	0.26	26,27,29
2868	1.45	1.46	1.48	5.039e+05	136.00	2.57	0.04	0.06	0.03	23,23,42
2869	1.46	1.44	1.47	5.054e+05	136.00	2.55	0.03	0.06	0.02	23,23,38
2870	1.41	1.41	1.48	4.905e+05	136.00	2.56	0.01	0.06	0.02	23,23,18
2871	1.35	1.35	1.29	4.687e+05	136.00	2.23	0.07	0.07	0.06	23,23,42
2872	1.35	1.35	1.04	4.687e+05	136.00	1.80	0.07	0.07	0.11	23,23,42
2873	0.70	0.71	0.69	2.517e+05	136.00	1.21	0.09	0.06	0.13	26,21,42
2874	0.41	0.42	0.41	1.473e+05	136.00	0.70	0.13	0.07	0.18	26,33,26
2875	0.16	0.42	0.16	5.699e+04	136.00	0.28	0.22	0.07	0.26	26,33,29
2876	0.16	0.16	0.16	5.699e+04	136.00	0.28	0.22	0.06	0.26	26,27,29
2877	1.45	1.46	1.48	5.039e+05	136.00	2.57	0.04	0.06	0.03	23,23,42
2878	1.46	1.44	1.47	5.054e+05	136.00	2.55	0.03	0.06	0.02	23,23,38
2879	1.41	1.41	1.48	4.905e+05	136.00	2.56	0.01	0.06	0.02	23,23,18
2880	1.35	1.35	1.29	4.687e+05	136.00	2.23	0.07	0.07	0.06	23,23,42
2881	1.35	1.35	1.04	4.687e+05	136.00	1.80	0.07	0.07	0.11	23,23,42
2882	0.70	0.71	0.69	2.517e+05	136.00	1.21	0.09	0.06	0.13	26,21,42
2883	0.41	0.42	0.41	1.473e+05	136.00	0.70	0.13	0.07	0.18	26,33,26
2884	0.16	0.42	0.16	5.699e+04	136.00	0.28	0.22	0.07	0.26	26,33,29
2885	0.16	0.16	0.16	5.699e+04	136.00	0.28	0.22	0.06	0.26	26,27,29
2886	1.45	1.46	1.48	5.039e+05	136.00	2.57	0.04	0.06	0.03	23,23,42
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	1.46	1.46	1.48	5.699e+04	136.00	0.28				
				5.054e+05	136.00	2.57	0.22	0.07	0.26	

Setto	Mat.	Spessore	Stato
		cm	
165	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
1303	1.56	1.52	1.51	6.222e+06	462.00	2.62	0.08	0.06	0.05	38,35,37
1312	1.56	1.52	1.51	6.222e+06	462.00	2.62	0.08	0.06	0.05	38,35,37
1321	1.56	1.52	1.51	6.222e+06	462.00	2.62	0.08	0.06	0.05	38,35,37
1330	1.56	1.52	1.51	6.222e+06	462.00	2.62	0.08	0.06	0.05	38,35,37
1339	1.56	1.52	1.51	6.222e+06	462.00	2.62	0.08	0.06	0.05	38,35,37
1348	1.56	1.52	1.51	6.222e+06	462.00	2.62	0.08	0.06	0.05	38,35,37
1357	1.56	1.52	1.51	6.222e+06	462.00	2.62	0.08	0.06	0.05	38,35,37
1366	1.56	1.52	1.51	6.222e+06	462.00	2.62	0.08	0.06	0.05	38,35,37
1375	1.56	1.52	1.51	6.222e+06	462.00	2.62	0.08	0.06	0.05	38,35,37
1384	1.56	1.52	1.51	6.222e+06	462.00	2.62	0.08	0.06	0.05	38,35,37
1724	1.56	1.43	1.51	6.222e+06	462.00	2.62	0.08	0.06	0.05	38,39,37

1726	1.47	1.30	1.42	5.889e+06	462.00	2.47	0.07	0.07	0.02	38,39,37
1728	1.18	1.15	1.18	4.791e+06	462.00	2.05	0.06	0.09	0.02	38,39,16
1730	1.02	1.00	1.18	4.176e+06	462.00	2.05	0.07	0.11	0.02	42,37,16
1732	0.86	0.86	1.02	3.550e+06	462.00	1.78	0.09	0.16	0.01	26,41,16
1734	0.86	0.73	0.73	3.550e+06	462.00	1.27	0.09	0.19	0.02	26,41,13
1736	0.73	0.60	0.60	3.012e+06	462.00	1.04	0.09	0.21	0.02	21,41,33
1738	0.60	0.60	0.60	2.498e+06	462.00	1.04	0.06	0.21	0.02	33,41,33
1740	0.44	0.44	0.44	1.825e+06	462.00	0.76	0.04	0.14	0.01	32,41,33
2891	1.56	1.43	1.51	6.222e+06	462.00	2.62	0.08	0.06	0.05	38,39,37
2892	1.47	1.30	1.42	5.889e+06	462.00	2.47	0.07	0.07	0.02	38,39,37
2893	1.18	1.15	1.18	4.791e+06	462.00	2.05	0.06	0.09	0.02	38,39,16
2894	1.02	1.00	1.18	4.176e+06	462.00	2.05	0.07	0.11	0.02	42,37,16
2895	0.86	0.86	1.02	3.550e+06	462.00	1.78	0.09	0.16	0.01	26,41,16
2896	0.86	0.73	0.73	3.550e+06	462.00	1.27	0.09	0.19	0.02	26,41,13
2897	0.73	0.60	0.60	3.012e+06	462.00	1.04	0.09	0.21	0.02	21,41,33
2898	0.60	0.60	0.60	2.498e+06	462.00	1.04	0.06	0.21	0.02	33,41,33
2899	0.44	0.44	0.44	1.825e+06	462.00	0.76	0.04	0.14	0.01	32,41,33
2900	1.56	1.43	1.51	6.222e+06	462.00	2.62	0.08	0.06	0.05	38,39,37
2901	1.47	1.30	1.42	5.889e+06	462.00	2.47	0.07	0.07	0.02	38,39,37
2902	1.18	1.15	1.18	4.791e+06	462.00	2.05	0.06	0.09	0.02	38,39,16
2903	1.02	1.00	1.18	4.176e+06	462.00	2.05	0.07	0.11	0.02	42,37,16
2904	0.86	0.86	1.02	3.550e+06	462.00	1.78	0.09	0.16	0.01	26,41,16
2905	0.86	0.73	0.73	3.550e+06	462.00	1.27	0.09	0.19	0.02	26,41,13
2906	0.73	0.60	0.60	3.012e+06	462.00	1.04	0.09	0.21	0.02	21,41,33
2907	0.60	0.60	0.60	2.498e+06	462.00	1.04	0.06	0.21	0.02	33,41,33
2908	0.44	0.44	0.44	1.825e+06	462.00	0.76	0.04	0.14	0.01	32,41,33
2909	1.56	1.43	1.51	6.222e+06	462.00	2.62	0.08	0.06	0.05	38,39,37
2910	1.47	1.30	1.42	5.889e+06	462.00	2.47	0.07	0.07	0.02	38,39,37
2911	1.18	1.15	1.18	4.791e+06	462.00	2.05	0.06	0.09	0.02	38,39,16
2912	1.02	1.00	1.18	4.176e+06	462.00	2.05	0.07	0.11	0.02	42,37,16
2913	0.86	0.86	1.02	3.550e+06	462.00	1.78	0.09	0.16	0.01	26,41,16
2914	0.86	0.73	0.73	3.550e+06	462.00	1.27	0.09	0.19	0.02	26,41,13
2915	0.73	0.60	0.60	3.012e+06	462.00	1.04	0.09	0.21	0.02	21,41,33
2916	0.60	0.60	0.60	2.498e+06	462.00	1.04	0.06	0.21	0.02	33,41,33
2917	0.44	0.44	0.44	1.825e+06	462.00	0.76	0.04	0.14	0.01	32,41,33
2918	1.56	1.43	1.51	6.222e+06	462.00	2.62	0.08	0.06	0.05	38,

2960	0.73	0.60	0.60	3.012e+06	462.00	1.04	0.09	0.21	0.02	21,41,33
2961	0.60	0.60	0.60	2.498e+06	462.00	1.04	0.06	0.21	0.02	33,41,33
2962	0.44	0.44	0.44	1.825e+06	462.00	0.76	0.04	0.14	0.01	32,41,33
2963	1.56	1.43	1.51	6.222e+06	462.00	2.62	0.08	0.06	0.05	38,39,37
2964	1.47	1.30	1.42	5.889e+06	462.00	2.47	0.07	0.07	0.02	38,39,37
2965	1.18	1.15	1.18	4.791e+06	462.00	2.05	0.06	0.09	0.02	38,39,16
2966	1.02	1.00	1.18	4.176e+06	462.00	2.05	0.07	0.11	0.02	42,37,16
2967	0.86	0.86	1.02	3.550e+06	462.00	1.78	0.09	0.16	0.01	26,41,16
2968	0.86	0.73	0.73	3.550e+06	462.00	1.27	0.09	0.19	0.02	26,41,13
2969	0.73	0.60	0.60	3.012e+06	462.00	1.04	0.09	0.21	0.02	21,41,33
2970	0.60	0.60	0.60	2.498e+06	462.00	1.04	0.06	0.21	0.02	33,41,33
2971	0.44	0.44	0.44	1.825e+06	462.00	0.76	0.04	0.14	0.01	32,41,33

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
	1.56	1.52	1.51	1.825e+06	462.00	0.76			
				6.222e+06	462.00	2.62	0.09	0.21	0.05

Setto	Mat.	Spessore	Stato
		cm	
166	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1142	1.74	1.74	1.53	5.549e+04	41.50	2.67	0.03	0.04	0.02	39,39,21
1267	1.74	1.74	1.53	5.549e+04	41.50	2.67	0.03	0.04	0.02	39,39,21
2841	1.38	1.51	1.62	4.468e+04	41.50	2.81	0.02	0.07	0.01	42,42,23
2842	1.83	1.79	1.75	5.803e+04	41.50	3.04	0.04	0.14	0.01	41,42,20
2843	2.22	2.35	2.19	6.915e+04	41.50	3.80	0.24	0.41	0.02	16,42,23
2844	1.94	2.09	1.88	6.106e+04	41.50	3.27	0.24	0.53	0.03	16,42,23
2850	1.94	2.09	1.88	6.106e+04	41.50	3.27	0.24	0.53	0.03	16,42,23
2851	0.55	1.13	0.61	1.842e+04	41.50	1.05	0.02	0.45	0.03	16,42,18
2852	0.29	0.60	0.32	9865.71	41.50	0.55	0.09	0.40	0.05	15,42,22
2853	0.29	0.31	0.32	9865.71	41.50	0.55	0.09	0.09	0.05	15,42,22
2886	1.74	1.38	1.53	5.549e+04	41.50	2.67	0.03	0.05	0.02	39,42,21
2985	1.94	2.09	1.88	6.106e+04	41.50	3.27	0.24	0.53	0.03	16,42,23
2986	1.94	2.09	1.88	6.106e+04	41.50	3.27	0.24	0.53	0.03	16,42,23
2987	0.55	1.13	0.61	1.842e+04	41.50	1.05	0.02	0.45	0.03	16,42,18
2988	0.29	0.60	0.32	9865.71	41.50	0.55	0.09	0.40	0.05	15,42,22
2989	0.29	0.31	0.32	9865.71	41.50	0.55	0.09	0.09	0.05	15,42,22
2992	1.74	1.38	1.53	5.549e+04	41.50	2.67	0.03	0.05	0.02	39,42,21
2993	1.38	1.51	1.62	4.468e+04	41.50	2.81	0.02	0.07	0.01	42,42,23
2994	1.83	1.79	1.75	5.803e+04	41.50	3.04	0.04	0.14	0.01	41,42,20
2995	2.22	2.35	2.19	6.915e+04	41.50	3.80	0.24	0.41	0.02	16,42,23

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
	2.22	2.35	2.19	9865.71	41.50	0.55			
				6.915e+04	41.50	3.80	0.24	0.53	0.05

Setto	Mat.	Spessore	Stato
		cm	
167	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1921	0.53	0.53	0.53	7.965e+04	87.50	0.83	0.34	0.18	0.10	31,34,27
1930	0.53	0.53	0.53	7.965e+04	87.50	0.83	0.34	0.18	0.10	31,34,27
1939	0.53	0.53	0.53	7.965e+04	87.50	0.83	0.34	0.18	0.10	31,34,27
2996	0.53	0.53	0.34	7.965e+04	87.50	0.53	0.34	0.18	0.20	31,34,15
2997	0.53	0.53	0.34	7.965e+04	87.50	0.53	0.34	0.18	0.20	31,34,15
2998	0.32	0.33	0.34	4.834e+04	87.50	0.53	0.15	0.18	0.20	31,34,15
2999	0.32	0.33	0.34	4.834e+04	87.50	0.53	0.15	0.18	0.20	31,34,15
3002	0.53	0.53	0.34	7.965e+04	87.50	0.53	0.34	0.18	0.20	31,34,15
3003	0.32	0.33	0.34	4.834e+04	87.50	0.53	0.15	0.18	0.20	31,34,15

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				4.834e+04	87.50	0.53			

0.53 0.53 0.53 7.965e+04 87.50 0.83 0.34 0.18 0.20

Setto	Mat.	Spessore	Stato
		cm	
168	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
2998	0.08	0.14	0.08	1.164e+04	46.99	0.12	0.64	0.19	0.80	28,28,28
2999	0.08	0.14	0.08	1.164e+04	46.99	0.12	0.64	0.19	0.80	28,28,28
3000	0.08	0.14	0.08	1.164e+04	46.99	0.12	0.64	0.19	0.80	28,28,28
3001	0.08	0.14	0.08	1.164e+04	46.99	0.12	0.64	0.19	0.80	28,28,28
3003	0.08	0.14	0.08	1.164e+04	46.99	0.12	0.64	0.19	0.80	28,28,28
3004	0.08	0.14	0.08	1.164e+04	46.99	0.12	0.64	0.19	0.80	28,28,28
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				1.164e+04	46.99	0.12				
	0.08	0.14	0.08	1.164e+04	46.99	0.12	0.64	0.19	0.80	

Setto	Mat.	Spessore	Stato
		cm	
171	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
1858	0.12	0.84	0.14	1.359e+04	10.52	0.22	0.91	0.46	0.64	15,15,27
1867	0.12	0.84	0.14	1.359e+04	10.52	0.22	0.91	0.46	0.64	15,15,27
1876	0.12	0.84	0.14	1.359e+04	10.52	0.22	0.91	0.46	0.64	15,15,27
3017	0.12	0.84	0.14	1.359e+04	10.52	0.22	0.91	0.46	0.64	15,15,27
3018	0.15	0.18	0.20	1.819e+04	65.83	0.31	0.43	0.06	0.43	15,11,34
3020	0.12	0.84	0.14	1.359e+04	10.52	0.22	0.91	0.46	0.64	15,15,27
3021	0.15	0.18	0.20	1.819e+04	65.83	0.31	0.43	0.06	0.43	15,11,34
3023	0.12	0.84	0.14	1.359e+04	10.52	0.22	0.91	0.46	0.64	15,15,27
3024	0.15	0.18	0.20	1.819e+04	65.83	0.31	0.43	0.06	0.43	15,11,34
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				1.359e+04	10.52	0.22				
	0.15	0.84	0.20	1.819e+04	65.83	0.31	0.91	0.46	0.64	

Setto	Mat.	Spessore	Stato
		cm	
172	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
3018	0.14	0.16	0.14	1.602e+04	65.37	0.22	0.44	0.02	0.17	15,11,30
3019	0.14	0.16	0.14	1.602e+04	65.37	0.22	0.44	0.02	0.17	15,11,30
3021	0.14	0.16	0.14	1.602e+04	65.37	0.22	0.44	0.02	0.17	15,11,30
3022	0.14	0.16	0.14	1.602e+04	65.37	0.22	0.44	0.02	0.17	15,11,30
3024	0.14	0.16	0.14	1.602e+04	65.37	0.22	0.44	0.02	0.17	15,11,30
3025	0.14	0.16	0.14	1.602e+04	65.37	0.22	0.44	0.02	0.17	15,11,30
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				1.602e+04	65.37	0.22				
	0.14	0.16	0.14	1.602e+04	65.37	0.22	0.44	0.02	0.17	

Setto	Mat.	Spessore	Stato
		cm	
175	mattoni pieni e malta di calce	40.0	NV L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1795	1.04e-03	0.64	1.04e-03	122.98	10.84	1.63e-03	97.46	0.06	42.47	26,23,26
1804	1.04e-03	0.64	1.04e-03	122.98	10.84	1.63e-03	97.46	0.06	42.47	26,23,26
1813	1.04e-03	0.64	1.04e-03	122.98	10.84	1.63e-03	97.46	0.06	42.47	26,23,26
3038	1.04e-03	0.64	1.04e-03	122.98	10.84	1.63e-03	97.46	0.06	42.47	26,23,26
3039	0.07	0.15	0.08	8342.74	39.15	0.12	0.72	0.01	0.37	17,14,14
3041	1.04e-03	0.64	1.04e-03	122.98	10.84	1.63e-03	97.46	0.06	42.47	26,23,26
3042	0.07	0.15	0.08	8342.74	39.15	0.12	0.72	0.01	0.37	17,14,14
3044	1.04e-03	0.64	1.04e-03	122.98	10.84	1.63e-03	97.46	0.06	42.47	26,23,26
3045	0.07	0.15	0.08	8342.74	39.15	0.12	0.72	0.01	0.37	17,14,14

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				122.98	10.84	1.63e-03			
	0.07	0.64	0.08	8342.74	39.15	0.12	97.46	0.06	42.47

Setto	Mat.	Spessore	Stato
		cm	
176	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
3039	0.08	0.08	0.08	9028.79	77.00	0.12	0.11	0.02	0.08	17,34,17
3040	0.08	0.08	0.08	9028.79	77.00	0.12	0.11	0.02	0.08	17,34,17
3042	0.08	0.08	0.08	9028.79	77.00	0.12	0.11	0.02	0.08	17,34,17
3043	0.08	0.08	0.08	9028.79	77.00	0.12	0.11	0.02	0.08	17,34,17
3045	0.08	0.08	0.08	9028.79	77.00	0.12	0.11	0.02	0.08	17,34,17
3046	0.08	0.08	0.08	9028.79	77.00	0.12	0.11	0.02	0.08	17,34,17

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				9028.79	77.00	0.12			
	0.08	0.08	0.08	9028.79	77.00	0.12	0.11	0.02	0.08

Setto	Mat.	Spessore	Stato
		cm	
179	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
3060	0.11	0.12	0.12	1.992e+04	93.50	0.19	0.17	0.17	0.09	26,13,39
3061	0.11	0.12	0.12	1.992e+04	93.50	0.19	0.17	0.17	0.09	26,13,39
3063	0.11	0.12	0.12	1.992e+04	93.50	0.19	0.17	0.17	0.09	26,13,39
3064	0.11	0.12	0.12	1.992e+04	93.50	0.19	0.17	0.17	0.09	26,13,39
3066	0.11	0.12	0.12	1.992e+04	93.50	0.19	0.17	0.17	0.09	26,13,39
3067	0.11	0.12	0.12	1.992e+04	93.50	0.19	0.17	0.17	0.09	26,13,39

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				1.992e+04	93.50	0.19			
	0.11	0.12	0.12	1.992e+04	93.50	0.19	0.17	0.17	0.09

Setto	Mat.	Spessore	Stato
		cm	
180	muratura E = 1.024e+05	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				

3066	0.46	0.50	0.49	7.220e+04	89.00	0.38	0.02	0.06	0.10	26,35,32
3067	0.46	0.50	0.49	7.220e+04	89.00	0.38	0.02	0.06	0.10	26,35,32
3069	0.46	0.50	0.49	7.220e+04	89.00	0.38	0.02	0.06	0.10	26,35,32
3070	0.46	0.50	0.49	7.220e+04	89.00	0.38	0.02	0.06	0.10	26,35,32
3072	0.46	0.50	0.49	7.220e+04	89.00	0.38	0.02	0.06	0.10	26,35,32
3073	0.46	0.50	0.49	7.220e+04	89.00	0.38	0.02	0.06	0.10	26,35,32

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				7.220e+04	89.00	0.38			
	0.46	0.50	0.49	7.220e+04	89.00	0.38	0.02	0.06	0.10

Setto	Mat.	Spessore	Stato
		cm	
183	muratura E = 1.024e+05	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
3081	0.35	0.36	0.36	5.655e+04	90.00	0.28	0.05	2.59e-03	0.04	36,38,34
3082	0.35	0.36	0.36	5.655e+04	90.00	0.28	0.05	2.59e-03	0.04	36,38,34
3084	0.35	0.36	0.36	5.655e+04	90.00	0.28	0.05	2.59e-03	0.04	36,38,34
3085	0.35	0.36	0.36	5.655e+04	90.00	0.28	0.05	2.59e-03	0.04	36,38,34
3087	0.35	0.36	0.36	5.655e+04	90.00	0.28	0.05	2.59e-03	0.04	36,38,34
3088	0.35	0.36	0.36	5.655e+04	90.00	0.28	0.05	2.59e-03	0.04	36,38,34

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				5.655e+04	90.00	0.28			
	0.35	0.36	0.36	5.655e+04	90.00	0.28	0.05	2.59e-03	0.04

Setto	Mat.	Spessore	Stato
		cm	
184	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
2669	0.52	0.52	0.53	2.920e+06	536.00	0.91	0.09	0.02	0.16	35,15,20
2678	0.52	0.52	0.53	2.920e+06	536.00	0.91	0.09	0.02	0.16	35,15,20
2687	0.52	0.52	0.53	2.920e+06	536.00	0.91	0.09	0.02	0.16	35,15,20
2696	0.52	0.52	0.53	2.920e+06	536.00	0.91	0.09	0.02	0.16	35,15,20
2705	0.52	0.52	0.53	2.920e+06	536.00	0.91	0.09	0.02	0.16	35,15,20
2714	0.52	0.52	0.53	2.920e+06	536.00	0.91	0.09	0.02	0.16	35,15,20
2723	0.52	0.52	0.53	2.920e+06	536.00	0.91	0.09	0.02	0.16	35,15,20
2732	0.52	0.52	0.53	2.920e+06	536.00	0.91	0.09	0.02	0.16	35,15,20
2741	0.52	0.52	0.53	2.920e+06	536.00	0.91	0.09	0.02	0.16	35,15,20
2750	0.52	0.52	0.53	2.920e+06	536.00	0.91	0.09	0.02	0.16	35,15,20
2759	0.52	0.52	0.53	2.920e+06	536.00	0.91	0.09	0.02	0.16	35,15,20
2768	0.52	0.52	0.53	2.920e+06	536.00	0.91	0.09	0.02	0.16	35,15,20
3086	0.52	0.52	0.53	2.920e+06	536.00	0.91	0.09	0.02	0.16	35,15,20
3087	0.47	0.47	0.48	2.658e+06	536.00	0.83	0.05	0.02	0.15	35,15,20
3089	0.52	0.52	0.53	2.920e+06	536.00	0.91	0.09	0.02	0.16	35,15,20
3090	0.47	0.47	0.48	2.658e+06	536.00	0.83	0.05	0.02	0.15	35,15,20
3092	0.52	0.52	0.53	2.920e+06	536.00	0.91	0.09	0.02	0.16	35,15,20
3093	0.47	0.47	0.48	2.658e+06	536.00	0.83	0.05	0.02	0.15	35,15,20
3095	0.52	0.52	0.53	2.920e+06	536.00	0.91	0.09	0.02	0.16	35,15,20
3096	0.47	0.47	0.48	2.658e+06	536.00	0.83	0.05	0.02	0.15	35,15,20
3098	0.52	0.52	0.53	2.920e+06	536.00	0.91	0.09	0.02	0.16	35,15,20
3099	0.47	0.47	0.48	2.658e+06	536.00	0.83	0.05	0.02	0.15	35,15,20
3101	0.52	0.52	0.53	2.920e+06	536.00	0.91	0.09	0.02	0.16	35,15,20
3102	0.47	0.47	0.48	2.658e+06	536.00	0.83	0.05	0.02	0.15	35,15,20
3104	0.52	0.52	0.53	2.920e+06	536.00	0.91	0.09	0.02	0.16	35,15,20
3105	0.47	0.47	0.48	2.658e+06	536.00	0.83	0.05	0.02	0.15	35,15,20
3107	0.52	0.52	0.53	2.920e+06	536.00	0.91	0.09	0.02	0.16	35,15,20
3108	0.47	0.47	0.48	2.658e+06	536.00	0.83	0.05	0.02	0.15	35,15,20
3110	0.52	0.52	0.53	2.920e+06	536.00	0.91	0.09	0.02	0.16	35,15,20
3111	0.47	0.47	0.48	2.658e+06	536.00	0.83	0.05	0.02	0.15	35,15,20
3113	0.52	0.52	0.53	2.920e+06	536.00	0.91	0.09	0.02	0.16	35,15,20
3114	0.47	0.47	0.48	2.658e+06	536.00	0.83	0.05	0.02	0.15	35,15,20

3116	0.52	0.52	0.53	2.920e+06	536.00	0.91	0.09	0.02	0.16	35,15,20
3117	0.47	0.47	0.48	2.658e+06	536.00	0.83	0.05	0.02	0.15	35,15,20
3119	0.52	0.52	0.53	2.920e+06	536.00	0.91	0.09	0.02	0.16	35,15,20
3120	0.47	0.47	0.48	2.658e+06	536.00	0.83	0.05	0.02	0.15	35,15,20
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				2.658e+06	536.00	0.83				
	0.52	0.52	0.53	2.920e+06	536.00	0.91	0.09	0.02	0.16	

Setto	Mat.	Spessore	Stato
		cm	
185	muratura E = 1.024e+05	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
3087	0.36	0.36	0.36	2.051e+06	536.00	0.28	0.02	8.15e-03	0.14	35,35,20
3088	0.36	0.36	0.36	2.051e+06	536.00	0.28	0.02	8.15e-03	0.14	35,35,20
3090	0.36	0.36	0.36	2.051e+06	536.00	0.28	0.02	8.15e-03	0.14	35,35,20
3091	0.36	0.36	0.36	2.051e+06	536.00	0.28	0.02	8.15e-03	0.14	35,35,20
3093	0.36	0.36	0.36	2.051e+06	536.00	0.28	0.02	8.15e-03	0.14	35,35,20
3094	0.36	0.36	0.36	2.051e+06	536.00	0.28	0.02	8.15e-03	0.14	35,35,20
3096	0.36	0.36	0.36	2.051e+06	536.00	0.28	0.02	8.15e-03	0.14	35,35,20
3097	0.36	0.36	0.36	2.051e+06	536.00	0.28	0.02	8.15e-03	0.14	35,35,20
3099	0.36	0.36	0.36	2.051e+06	536.00	0.28	0.02	8.15e-03	0.14	35,35,20
3100	0.36	0.36	0.36	2.051e+06	536.00	0.28	0.02	8.15e-03	0.14	35,35,20
3102	0.36	0.36	0.36	2.051e+06	536.00	0.28	0.02	8.15e-03	0.14	35,35,20
3103	0.36	0.36	0.36	2.051e+06	536.00	0.28	0.02	8.15e-03	0.14	35,35,20
3105	0.36	0.36	0.36	2.051e+06	536.00	0.28	0.02	8.15e-03	0.14	35,35,20
3106	0.36	0.36	0.36	2.051e+06	536.00	0.28	0.02	8.15e-03	0.14	35,35,20
3108	0.36	0.36	0.36	2.051e+06	536.00	0.28	0.02	8.15e-03	0.14	35,35,20
3109	0.36	0.36	0.36	2.051e+06	536.00	0.28	0.02	8.15e-03	0.14	35,35,20
3111	0.36	0.36	0.36	2.051e+06	536.00	0.28	0.02	8.15e-03	0.14	35,35,20
3112	0.36	0.36	0.36	2.051e+06	536.00	0.28	0.02	8.15e-03	0.14	35,35,20
3114	0.36	0.36	0.36	2.051e+06	536.00	0.28	0.02	8.15e-03	0.14	35,35,20
3115	0.36	0.36	0.36	2.051e+06	536.00	0.28	0.02	8.15e-03	0.14	35,35,20
3117	0.36	0.36	0.36	2.051e+06	536.00	0.28	0.02	8.15e-03	0.14	35,35,20
3118	0.36	0.36	0.36	2.051e+06	536.00	0.28	0.02	8.15e-03	0.14	35,35,20
3120	0.36	0.36	0.36	2.051e+06	536.00	0.28	0.02	8.15e-03	0.14	35,35,20
3121	0.36	0.36	0.36	2.051e+06	536.00	0.28	0.02	8.15e-03	0.14	35,35,20
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				2.051e+06	536.00	0.28				
	0.36	0.36	0.36	2.051e+06	536.00	0.28	0.02	8.15e-03	0.14	

Setto	Mat.	Spessore	Stato
		cm	
186	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
2768	0.57	0.57	0.62	2.877e+04	50.95	0.98	0.11	0.50	0.24	37,18,20
2786	0.57	0.57	0.62	2.877e+04	50.95	0.98	0.11	0.50	0.24	37,18,20
3119	0.57	0.57	0.31	2.877e+04	50.95	0.49	0.11	0.50	0.34	37,18,20
3120	0.30	0.30	0.31	1.516e+04	50.95	0.49	0.03	0.44	0.34	42,38,20
3122	0.57	0.57	0.31	2.877e+04	50.95	0.49	0.11	0.50	0.34	37,18,20
3123	0.30	0.30	0.31	1.516e+04	50.95	0.49	0.03	0.44	0.34	42,38,20
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				1.516e+04	50.95	0.49				
	0.57	0.57	0.62	2.877e+04	50.95	0.98	0.11	0.50	0.34	

Setto	Mat.	Spessore	Stato
		cm	
187	mattoni pieni e malta di calce	40.0	NV L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
3120	0.03	0.85	0.04	1692.28	2.16	0.07	1.12	5.65	0.53	38,18,20
3121	0.03	0.85	0.04	1692.28	2.16	0.07	1.12	5.65	0.53	38,18,20
3123	0.03	0.85	0.04	1692.28	2.16	0.07	1.12	5.65	0.53	38,18,20
3124	0.03	0.85	0.04	1692.28	2.16	0.07	1.12	5.65	0.53	38,18,20
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				1692.28	2.16	0.07				
	0.03	0.85	0.04	1692.28	2.16	0.07	1.12	5.65	0.53	

Setto	Mat.	Spessore	Stato
		cm	
190	mattoni pieni e malta di calce	40.0	NV L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
2813	3.96e-04	0.0	4.05e-04	82.31	0.0	6.35e-04	137.55	0.0	19.38	32,0,24
2822	3.96e-04	0.0	4.05e-04	82.31	0.0	6.35e-04	137.55	0.0	19.38	32,0,24
2831	3.96e-04	0.0	4.05e-04	82.31	0.0	6.35e-04	137.55	0.0	19.38	32,0,24
3131	3.96e-04	0.11	4.05e-04	82.31	88.47	6.35e-04	137.55	0.11	19.38	32,17,24
3132	0.09	0.11	0.09	1.932e+04	88.47	0.14	0.44	0.11	0.11	37,17,22
3134	3.96e-04	0.11	4.05e-04	82.31	88.47	6.35e-04	137.55	0.11	19.38	32,17,24
3135	0.09	0.11	0.09	1.932e+04	88.47	0.14	0.44	0.11	0.11	37,17,22
3137	3.96e-04	0.11	4.05e-04	82.31	88.47	6.35e-04	137.55	0.11	19.38	32,17,24
3138	0.09	0.11	0.09	1.932e+04	88.47	0.14	0.44	0.11	0.11	37,17,22
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				82.31	0.0	6.35e-04				
	0.09	0.11	0.09	1.932e+04	88.47	0.14	137.55	0.11	19.38	

Setto	Mat.	Spessore	Stato
		cm	
191	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
3132	0.06	0.06	0.06	1.294e+04	101.90	0.10	0.16	0.05	0.05	37,40,25
3133	0.06	0.06	0.06	1.294e+04	101.90	0.10	0.16	0.05	0.05	37,40,25
3135	0.06	0.06	0.06	1.294e+04	101.90	0.10	0.16	0.05	0.05	37,40,25
3136	0.06	0.06	0.06	1.294e+04	101.90	0.10	0.16	0.05	0.05	37,40,25
3138	0.06	0.06	0.06	1.294e+04	101.90	0.10	0.16	0.05	0.05	37,40,25
3139	0.06	0.06	0.06	1.294e+04	101.90	0.10	0.16	0.05	0.05	37,40,25
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				1.294e+04	101.90	0.10				
	0.06	0.06	0.06	1.294e+04	101.90	0.10	0.16	0.05	0.05	

Setto	Mat.	Spessore	Stato
		cm	
194	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
2574	0.88	0.89	0.89	4.392e+04	50.95	1.40	0.06	0.35	0.06	26,25,35
2801	0.88	0.89	0.89	4.392e+04	50.95	1.40	0.06	0.35	0.06	26,25,35

3146	0.56	0.89	0.57	2.844e+04	50.95	0.89	0.14	0.35	0.11	26,25,35
3147	0.56	0.58	0.57	2.844e+04	50.95	0.89	0.14	0.27	0.11	26,41,35
3149	0.56	0.89	0.57	2.844e+04	50.95	0.89	0.14	0.35	0.11	26,25,35
3150	0.56	0.58	0.57	2.844e+04	50.95	0.89	0.14	0.27	0.11	26,41,35
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				2.844e+04	50.95	0.89				
	0.88	0.89	0.89	4.392e+04	50.95	1.40	0.14	0.35	0.11	

Setto	Mat.	Spessore	Stato
		cm	
195	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
3147	0.20	0.64	0.25	1.046e+04	16.09	0.39	0.80	0.22	0.23	24,24,41
3148	0.20	0.64	0.25	1.046e+04	16.09	0.39	0.80	0.22	0.23	24,24,41
3150	0.20	0.64	0.25	1.046e+04	16.09	0.39	0.80	0.22	0.23	24,24,41
3151	0.20	0.64	0.25	1.046e+04	16.09	0.39	0.80	0.22	0.23	24,24,41
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				1.046e+04	16.09	0.39				
	0.20	0.64	0.25	1.046e+04	16.09	0.39	0.80	0.22	0.23	

Setto	Mat.	Spessore	Stato
		cm	
196	mattoni pieni e malta di calce	37.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
2574	0.55	0.54	0.54	7.705e+04	88.17	0.78	0.16	0.02	0.10	23,24,24
2575	0.55	0.54	0.54	7.705e+04	88.17	0.78	0.16	0.02	0.10	23,24,24
2584	0.55	0.54	0.54	7.705e+04	88.17	0.78	0.16	0.02	0.10	23,24,24
3149	0.36	0.54	0.54	5.059e+04	88.17	0.78	0.24	0.02	0.10	23,24,24
3150	0.36	0.35	0.35	5.059e+04	88.17	0.51	0.24	0.01	0.05	23,24,24
3152	0.36	0.54	0.54	5.059e+04	88.17	0.78	0.24	0.02	0.10	23,24,24
3153	0.36	0.35	0.35	5.059e+04	88.17	0.51	0.24	0.01	0.05	23,24,24
3155	0.36	0.54	0.54	5.059e+04	88.17	0.78	0.24	0.02	0.10	23,24,24
3156	0.36	0.35	0.35	5.059e+04	88.17	0.51	0.24	0.01	0.05	23,24,24
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				5.059e+04	88.17	0.51				
	0.55	0.54	0.54	7.705e+04	88.17	0.78	0.24	0.02	0.10	

Setto	Mat.	Spessore	Stato
		cm	
197	mattoni pieni e malta di calce	37.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
3150	0.16	0.38	0.16	2.277e+04	37.29	0.18	0.72	0.05	0.11	25,25,25
3151	0.16	0.38	0.16	2.277e+04	37.29	0.18	0.72	0.05	0.11	25,25,25
3153	0.16	0.38	0.16	2.277e+04	37.29	0.18	0.72	0.05	0.11	25,25,25
3154	0.16	0.38	0.16	2.277e+04	37.29	0.18	0.72	0.05	0.11	25,25,25
3156	0.16	0.38	0.16	2.277e+04	37.29	0.18	0.72	0.05	0.11	25,25,25
3157	0.16	0.38	0.16	2.277e+04	37.29	0.18	0.72	0.05	0.11	25,25,25
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				2.277e+04	37.29	0.18				
	0.16	0.38	0.16	2.277e+04	37.29	0.18	0.72	0.05	0.11	

Setto	Mat.	Spessore	Stato
		cm	
200	mattoni pieni e malta di calce	37.0	NV L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
2530	0.31	0.30	0.31	2.876e+05	224.67	0.45	0.14	0.02	1.04	21,38,39
2539	0.31	0.30	0.31	2.876e+05	224.67	0.45	0.14	0.02	1.04	21,38,39
2548	0.31	0.30	0.31	2.876e+05	224.67	0.45	0.14	0.02	1.04	21,38,39
2557	0.31	0.30	0.31	2.876e+05	224.67	0.45	0.14	0.02	1.04	21,38,39
2591	0.31	0.30	0.31	2.876e+05	224.67	0.45	0.14	0.02	1.04	21,38,39
2602	0.31	0.30	0.31	2.876e+05	224.67	0.45	0.14	0.02	1.04	21,38,39
3162	0.31	0.30	0.31	2.876e+05	224.67	0.45	0.14	0.02	1.04	21,38,39
3163	0.23	0.23	0.23	2.145e+05	224.67	0.34	0.11	0.01	0.75	21,18,39
3165	0.31	0.30	0.31	2.876e+05	224.67	0.45	0.14	0.02	1.04	21,38,39
3166	0.23	0.23	0.23	2.145e+05	224.67	0.34	0.11	0.01	0.75	21,18,39
3168	0.31	0.30	0.31	2.876e+05	224.67	0.45	0.14	0.02	1.04	21,38,39
3169	0.23	0.23	0.23	2.145e+05	224.67	0.34	0.11	0.01	0.75	21,18,39
3171	0.31	0.30	0.31	2.876e+05	224.67	0.45	0.14	0.02	1.04	21,38,39
3172	0.23	0.23	0.23	2.145e+05	224.67	0.34	0.11	0.01	0.75	21,18,39
3174	0.31	0.30	0.31	2.876e+05	224.67	0.45	0.14	0.02	1.04	21,38,39
3175	0.23	0.23	0.23	2.145e+05	224.67	0.34	0.11	0.01	0.75	21,18,39
3177	0.31	0.30	0.31	2.876e+05	224.67	0.45	0.14	0.02	1.04	21,38,39
3178	0.23	0.23	0.23	2.145e+05	224.67	0.34	0.11	0.01	0.75	21,18,39
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	0.31	0.30	0.31	2.145e+05	224.67	0.34				
				2.876e+05	224.67	0.45	0.14	0.02	1.04	

Setto	Mat.	Spessore	Stato
		cm	
201	mattoni pieni e malta di calce	37.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
3163	0.09	0.09	0.09	8.821e+04	224.67	0.11	0.04	6.99e-03	0.36	21,13,35
3164	0.09	0.09	0.09	8.821e+04	224.67	0.11	0.04	6.99e-03	0.36	21,13,35
3166	0.09	0.09	0.09	8.821e+04	224.67	0.11	0.04	6.99e-03	0.36	21,13,35
3167	0.09	0.09	0.09	8.821e+04	224.67	0.11	0.04	6.99e-03	0.36	21,13,35
3169	0.09	0.09	0.09	8.821e+04	224.67	0.11	0.04	6.99e-03	0.36	21,13,35
3170	0.09	0.09	0.09	8.821e+04	224.67	0.11	0.04	6.99e-03	0.36	21,13,35
3172	0.09	0.09	0.09	8.821e+04	224.67	0.11	0.04	6.99e-03	0.36	21,13,35
3173	0.09	0.09	0.09	8.821e+04	224.67	0.11	0.04	6.99e-03	0.36	21,13,35
3175	0.09	0.09	0.09	8.821e+04	224.67	0.11	0.04	6.99e-03	0.36	21,13,35
3176	0.09	0.09	0.09	8.821e+04	224.67	0.11	0.04	6.99e-03	0.36	21,13,35
3178	0.09	0.09	0.09	8.821e+04	224.67	0.11	0.04	6.99e-03	0.36	21,13,35
3179	0.09	0.09	0.09	8.821e+04	224.67	0.11	0.04	6.99e-03	0.36	21,13,35
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	0.09	0.09	0.09	8.821e+04	224.67	0.11				
				8.821e+04	224.67	0.11	0.04	6.99e-03	0.36	

Setto	Mat.	Spessore	Stato
		cm	
204	mattoni pieni e malta di calce	37.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
2493	0.40	0.40	0.40	1.704e+05	153.01	0.59	0.34	0.08	0.53	33,33,39
2494	0.40	0.40	0.40	1.704e+05	153.01	0.59	0.34	0.08	0.53	33,33,39

2503	0.40	0.40	0.40	1.704e+05	153.01	0.59	0.34	0.08	0.53	33,33,39
2512	0.40	0.40	0.40	1.704e+05	153.01	0.59	0.34	0.08	0.53	33,33,39
3183	0.32	0.39	0.40	1.376e+05	126.31	0.59	0.46	0.10	0.53	33,33,39
3184	0.32	0.39	0.32	1.376e+05	126.31	0.47	0.46	0.10	0.47	33,33,39
3186	0.32	0.39	0.40	1.376e+05	126.31	0.59	0.46	0.10	0.53	33,33,39
3187	0.32	0.39	0.32	1.376e+05	126.31	0.47	0.46	0.10	0.47	33,33,39
3189	0.32	0.39	0.40	1.376e+05	126.31	0.59	0.46	0.10	0.53	33,33,39
3190	0.32	0.39	0.32	1.376e+05	126.31	0.47	0.46	0.10	0.47	33,33,39
3192	0.32	0.39	0.40	1.376e+05	126.31	0.59	0.46	0.10	0.53	33,33,39
3193	0.32	0.39	0.32	1.376e+05	126.31	0.47	0.46	0.10	0.47	33,33,39

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				1.376e+05	126.31	0.47			
	0.40	0.40	0.40	1.704e+05	153.01	0.59	0.46	0.10	0.53

Setto	Mat.	Spessore	Stato
		cm	
205	mattoni pieni e malta di calce	37.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
3184	0.17	0.48	0.18	7.538e+04	55.68	0.20	0.76	0.18	0.28	41,37,39
3185	0.17	0.48	0.18	7.538e+04	55.68	0.20	0.76	0.18	0.28	41,37,39
3187	0.17	0.48	0.18	7.538e+04	55.68	0.20	0.76	0.18	0.28	41,37,39
3188	0.17	0.48	0.18	7.538e+04	55.68	0.20	0.76	0.18	0.28	41,37,39
3190	0.17	0.48	0.18	7.538e+04	55.68	0.20	0.76	0.18	0.28	41,37,39
3191	0.17	0.48	0.18	7.538e+04	55.68	0.20	0.76	0.18	0.28	41,37,39
3193	0.17	0.48	0.18	7.538e+04	55.68	0.20	0.76	0.18	0.28	41,37,39
3194	0.17	0.48	0.18	7.538e+04	55.68	0.20	0.76	0.18	0.28	41,37,39

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				7.538e+04	55.68	0.20			
	0.17	0.48	0.18	7.538e+04	55.68	0.20	0.76	0.18	0.28

Setto	Mat.	Spessore	Stato
		cm	
206	muratura E = 4.550e+04	40.0	NV L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
2112	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0,0,0
2121	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0,0,0
3195	1.96e-03	2.17	9.11e-03	40.15	1.23	0.02	31.11	5.16	0.58	34,16,28
3196	1.96e-03	2.17	9.11e-03	40.15	1.23	0.02	31.11	5.16	0.58	34,16,28
3197	1.96e-03	2.17	9.11e-03	40.15	1.23	0.02	31.11	5.16	0.58	34,16,28
3198	1.96e-03	2.17	9.11e-03	40.15	1.23	0.02	31.11	5.16	0.58	34,16,28

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				0.0	0.0	0.0			
	1.96e-03	2.17	9.11e-03	40.15	1.23	0.02	31.11	5.16	0.58

Setto	Mat.	Spessore	Stato
		cm	
207	muratura E = 1.024e+05	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
3197	0.09	0.74	0.09	1928.22	4.10	0.07	0.92	0.12	0.29	30,30,30
3198	0.09	0.74	0.09	1928.22	4.10	0.07	0.92	0.12	0.29	30,30,30
3199	0.09	0.74	0.09	1928.22	4.10	0.07	0.92	0.12	0.29	30,30,30
3200	0.09	0.74	0.09	1928.22	4.10	0.07	0.92	0.12	0.29	30,30,30

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
	0.09	0.74	0.09	1928.22	4.10	0.07			
				1928.22	4.10	0.07	0.92	0.12	0.29

Setto	Mat.	Spessore	Stato
		cm	
210	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
2058	0.49	0.50	0.50	2.778e+05	170.00	0.86	0.28	0.11	0.03	30,32,27
2067	0.49	0.50	0.50	2.778e+05	170.00	0.86	0.28	0.11	0.03	30,32,27
2076	0.49	0.50	0.50	2.778e+05	170.00	0.86	0.28	0.11	0.03	30,32,27
2085	0.49	0.50	0.50	2.778e+05	170.00	0.86	0.28	0.11	0.03	30,32,27
2094	0.49	0.50	0.50	2.778e+05	170.00	0.86	0.28	0.11	0.03	30,32,27
3204	0.49	0.50	0.31	2.778e+05	170.00	0.54	0.28	0.11	0.04	30,32,29
3205	0.31	0.32	0.31	1.785e+05	170.00	0.54	0.23	0.10	0.04	30,32,29
3207	0.49	0.50	0.31	2.778e+05	170.00	0.54	0.28	0.11	0.04	30,32,29
3208	0.31	0.32	0.31	1.785e+05	170.00	0.54	0.23	0.10	0.04	30,32,29
3210	0.49	0.50	0.31	2.778e+05	170.00	0.54	0.28	0.11	0.04	30,32,29
3211	0.31	0.32	0.31	1.785e+05	170.00	0.54	0.23	0.10	0.04	30,32,29
3213	0.49	0.50	0.31	2.778e+05	170.00	0.54	0.28	0.11	0.04	30,32,29
3214	0.31	0.32	0.31	1.785e+05	170.00	0.54	0.23	0.10	0.04	30,32,29
3216	0.49	0.50	0.31	2.778e+05	170.00	0.54	0.28	0.11	0.04	30,32,29
3217	0.31	0.32	0.31	1.785e+05	170.00	0.54	0.23	0.10	0.04	30,32,29
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	0.49	0.50	0.50	1.785e+05	170.00	0.54				
				2.778e+05	170.00	0.86	0.28	0.11	0.04	

Setto	Mat.	Spessore	Stato
		cm	
211	muratura E = 1.024e+05	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
3205	0.11	0.11	0.10	6.149e+04	170.00	0.08	0.12	0.02	0.05	32,30,29
3206	0.11	0.11	0.10	6.149e+04	170.00	0.08	0.12	0.02	0.05	32,30,29
3208	0.11	0.11	0.10	6.149e+04	170.00	0.08	0.12	0.02	0.05	32,30,29
3209	0.11	0.11	0.10	6.149e+04	170.00	0.08	0.12	0.02	0.05	32,30,29
3211	0.11	0.11	0.10	6.149e+04	170.00	0.08	0.12	0.02	0.05	32,30,29
3212	0.11	0.11	0.10	6.149e+04	170.00	0.08	0.12	0.02	0.05	32,30,29
3214	0.11	0.11	0.10	6.149e+04	170.00	0.08	0.12	0.02	0.05	32,30,29
3215	0.11	0.11	0.10	6.149e+04	170.00	0.08	0.12	0.02	0.05	32,30,29
3217	0.11	0.11	0.10	6.149e+04	170.00	0.08	0.12	0.02	0.05	32,30,29
3218	0.11	0.11	0.10	6.149e+04	170.00	0.08	0.12	0.02	0.05	32,30,29
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	0.11	0.11	0.10	6.149e+04	170.00	0.08				
				6.149e+04	170.00	0.08	0.12	0.02	0.05	

Setto	Mat.	Spessore	Stato
		cm	
214	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
2004	0.51	0.52	0.51	2.883e+05	170.00	0.89	0.21	0.12	0.06	27,32,31
2013	0.51	0.52	0.51	2.883e+05	170.00	0.89	0.21	0.12	0.06	27,32,31
2022	0.51	0.52	0.51	2.883e+05	170.00	0.89	0.21	0.12	0.06	27,32,31

2031	0.51	0.52	0.51	2.883e+05	170.00	0.89	0.21	0.12	0.06	27,32,31
2040	0.51	0.52	0.51	2.883e+05	170.00	0.89	0.21	0.12	0.06	27,32,31
3222	0.51	0.52	0.51	2.883e+05	170.00	0.89	0.21	0.12	0.06	27,32,31
3223	0.32	0.32	0.32	1.806e+05	170.00	0.55	0.18	0.11	0.06	27,32,31
3225	0.51	0.52	0.51	2.883e+05	170.00	0.89	0.21	0.12	0.06	27,32,31
3226	0.32	0.32	0.32	1.806e+05	170.00	0.55	0.18	0.11	0.06	27,32,31
3228	0.51	0.52	0.51	2.883e+05	170.00	0.89	0.21	0.12	0.06	27,32,31
3229	0.32	0.32	0.32	1.806e+05	170.00	0.55	0.18	0.11	0.06	27,32,31
3231	0.51	0.52	0.51	2.883e+05	170.00	0.89	0.21	0.12	0.06	27,32,31
3232	0.32	0.32	0.32	1.806e+05	170.00	0.55	0.18	0.11	0.06	27,32,31
3234	0.51	0.52	0.51	2.883e+05	170.00	0.89	0.21	0.12	0.06	27,32,31
3235	0.32	0.32	0.32	1.806e+05	170.00	0.55	0.18	0.11	0.06	27,32,31

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				1.806e+05	170.00	0.55			
	0.51	0.52	0.51	2.883e+05	170.00	0.89	0.21	0.12	0.06

Setto	Mat.	Spessore	Stato
		cm	
215	muratura E = 1.024e+05	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
3223	0.10	0.10	0.10	5.657e+04	170.00	0.07	0.10	0.03	0.07	27,32,14
3224	0.10	0.10	0.10	5.657e+04	170.00	0.07	0.10	0.03	0.07	27,32,14
3226	0.10	0.10	0.10	5.657e+04	170.00	0.07	0.10	0.03	0.07	27,32,14
3227	0.10	0.10	0.10	5.657e+04	170.00	0.07	0.10	0.03	0.07	27,32,14
3229	0.10	0.10	0.10	5.657e+04	170.00	0.07	0.10	0.03	0.07	27,32,14
3230	0.10	0.10	0.10	5.657e+04	170.00	0.07	0.10	0.03	0.07	27,32,14
3232	0.10	0.10	0.10	5.657e+04	170.00	0.07	0.10	0.03	0.07	27,32,14
3233	0.10	0.10	0.10	5.657e+04	170.00	0.07	0.10	0.03	0.07	27,32,14
3235	0.10	0.10	0.10	5.657e+04	170.00	0.07	0.10	0.03	0.07	27,32,14
3236	0.10	0.10	0.10	5.657e+04	170.00	0.07	0.10	0.03	0.07	27,32,14
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				5.657e+04	170.00	0.07				
	0.10	0.10	0.10	5.657e+04	170.00	0.07	0.10	0.03	0.07	

Setto	Mat.	Spessore	Stato
		cm	
218	muratura E = 4.550e+04	40.0	NV L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1939	4.79e-03	0.04	4.70e-03	86.27	20.88	8.17e-03	2.86	0.28	15.25	36,42,40
1986	4.79e-03	0.04	4.70e-03	86.27	20.88	8.17e-03	2.86	0.28	15.25	36,42,40
2996	4.79e-03	0.25	4.70e-03	86.27	21.17	8.17e-03	2.86	0.29	15.25	36,27,40
2998	0.17	0.25	0.36	3120.61	21.17	0.62	0.53	0.29	0.08	27,27,42
3240	4.79e-03	0.25	4.70e-03	86.27	21.17	8.17e-03	2.86	0.29	15.25	36,27,40
3241	0.17	0.25	0.36	3120.61	21.17	0.62	0.53	0.29	0.08	27,27,42
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				86.27	20.88	8.17e-03				
	0.17	0.25	0.36	3120.61	21.17	0.62	2.86	0.29	15.25	

Setto	Mat.	Spessore	Stato
		cm	
219	muratura E = 1.024e+05	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				

2998	0.29	0.89	0.31	5267.34	13.29	0.24	0.84	5.53e-03	0.29	29,11,31
3000	0.29	0.89	0.31	5267.34	13.29	0.24	0.84	5.53e-03	0.29	29,11,31
3241	0.29	0.89	0.31	5267.34	13.29	0.24	0.84	5.53e-03	0.29	29,11,31
3242	0.29	0.89	0.31	5267.34	13.29	0.24	0.84	5.53e-03	0.29	29,11,31
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				5267.34	13.29	0.24				
	0.29	0.89	0.31	5267.34	13.29	0.24	0.84	5.53e-03	0.29	

Setto	Mat.	Spessore	Stato
		cm	
220	mattoni pieni e malta di calce	25.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
3246	0.26	0.26	0.25	2017.14	25.00	0.24	0.11	0.02	0.58	26,21,41
3350	0.26	0.26	0.25	2017.14	25.00	0.24	0.11	0.02	0.58	26,21,41
3351	0.08	0.08	0.07	1549.66	40.00	0.07	0.10	0.01	0.39	25,22,40
3352	0.08	0.08	0.07	1549.66	40.00	0.07	0.10	0.01	0.39	25,22,40
3353	0.20	0.26	0.25	1567.14	25.00	0.24	0.13	0.02	0.58	23,21,41
3354	0.20	0.26	0.25	1567.14	25.00	0.24	0.13	0.02	0.58	23,21,41
3355	0.20	0.22	0.21	1567.14	25.00	0.21	0.13	0.02	0.50	23,25,41
3356	0.20	0.22	0.21	1567.14	25.00	0.21	0.13	0.02	0.50	23,25,41
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				1549.66	25.00	0.07				
	0.26	0.26	0.25	2017.14	40.00	0.24	0.13	0.02	0.58	

Setto	Mat.	Spessore	Stato
		cm	
222	muratura E = 4.550e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
3088	0.24	0.24	0.24	1.364e+06	536.00	0.42	0.03	0.01	0.16	42,42,20
3091	0.24	0.24	0.24	1.364e+06	536.00	0.42	0.03	0.01	0.16	42,42,20
3094	0.24	0.24	0.24	1.364e+06	536.00	0.42	0.03	0.01	0.16	42,42,20
3097	0.24	0.24	0.24	1.364e+06	536.00	0.42	0.03	0.01	0.16	42,42,20
3100	0.24	0.24	0.24	1.364e+06	536.00	0.42	0.03	0.01	0.16	42,42,20
3103	0.24	0.24	0.24	1.364e+06	536.00	0.42	0.03	0.01	0.16	42,42,20
3106	0.24	0.24	0.24	1.364e+06	536.00	0.42	0.03	0.01	0.16	42,42,20
3109	0.24	0.24	0.24	1.364e+06	536.00	0.42	0.03	0.01	0.16	42,42,20
3112	0.24	0.24	0.24	1.364e+06	536.00	0.42	0.03	0.01	0.16	42,42,20
3115	0.24	0.24	0.24	1.364e+06	536.00	0.42	0.03	0.01	0.16	42,42,20
3118	0.24	0.24	0.24	1.364e+06	536.00	0.42	0.03	0.01	0.16	42,42,20
3121	0.24	0.24	0.24	1.364e+06	536.00	0.42	0.03	0.01	0.16	42,42,20
3251	0.24	0.24	0.24	1.364e+06	536.00	0.42	0.03	0.01	0.16	42,42,20
3252	0.14	0.21	0.20	7.884e+05	536.00	0.36	0.03	9.48e-03	0.12	42,42,20
3253	0.14	0.14	0.14	7.884e+05	536.00	0.24	0.03	4.14e-03	0.06	42,41,20
3254	0.07	0.07	0.07	3.932e+05	536.00	0.12	0.02	3.05e-03	0.02	26,41,19
3255	0.24	0.24	0.24	1.364e+06	536.00	0.42	0.03	0.01	0.16	42,42,20
3256	0.14	0.21	0.20	7.884e+05	536.00	0.36	0.03	9.48e-03	0.12	42,42,20
3257	0.14	0.14	0.14	7.884e+05	536.00	0.24	0.03	4.14e-03	0.06	42,41,20
3258	0.07	0.07	0.07	3.932e+05	536.00	0.12	0.02	3.05e-03	0.02	26,41,19
3259	0.24	0.24	0.24	1.364e+06	536.00	0.42	0.03	0.01	0.16	42,42,20
3260	0.14	0.21	0.20	7.884e+05	536.00	0.36	0.03	9.48e-03	0.12	42,42,20
3261	0.14	0.14	0.14	7.884e+05	536.00	0.24	0.03	4.14e-03	0.06	42,41,20
3262	0.07	0.07	0.07	3.932e+05	536.00	0.12	0.02	3.05e-03	0.02	26,41,19
3263	0.24	0.24	0.24	1.364e+06	536.00	0.42	0.03	0.01	0.16	42,42,20
3264	0.14	0.21	0.20	7.884e+05	536.00	0.36	0.03	9.48e-03	0.12	42,42,20
3265	0.14	0.14	0.14	7.884e+05	536.00	0.24	0.03	4.14e-03	0.06	42,41,20
3266	0.07	0.07	0.07	3.932e+05	536.00	0.12	0.02	3.05e-03	0.02	26,41,19
3267	0.24	0.24	0.24	1.364e+06	536.00	0.42	0.03	0.01	0.16	42,42,20
3268	0.14	0.21	0.20	7.884e+05	536.00	0.36	0.03	9.48e-03	0.12	42,42,20
3269	0.14	0.14	0.14	7.884e+05	536.00	0.24	0.03	4.14e-03	0.06	42,41,20
3270	0.07	0.07	0.07	3.932e+05	536.00	0.12	0.02	3.05e-03	0.02	26,41,19

3271	0.24	0.24	0.24	1.364e+06	536.00	0.42	0.03	0.01	0.16	42,42,20
3272	0.14	0.21	0.20	7.884e+05	536.00	0.36	0.03	9.48e-03	0.12	42,42,20
3273	0.14	0.14	0.14	7.884e+05	536.00	0.24	0.03	4.14e-03	0.06	42,41,20
3274	0.07	0.07	0.07	3.932e+05	536.00	0.12	0.02	3.05e-03	0.02	26,41,19
3276	0.24	0.24	0.24	1.364e+06	536.00	0.42	0.03	0.01	0.16	42,42,20
3277	0.14	0.21	0.20	7.884e+05	536.00	0.36	0.03	9.48e-03	0.12	42,42,20
3278	0.14	0.14	0.14	7.884e+05	536.00	0.24	0.03	4.14e-03	0.06	42,41,20
3279	0.07	0.07	0.07	3.932e+05	536.00	0.12	0.02	3.05e-03	0.02	26,41,19
3280	0.24	0.24	0.24	1.364e+06	536.00	0.42	0.03	0.01	0.16	42,42,20
3281	0.14	0.21	0.20	7.884e+05	536.00	0.36	0.03	9.48e-03	0.12	42,42,20
3282	0.14	0.14	0.14	7.884e+05	536.00	0.24	0.03	4.14e-03	0.06	42,41,20
3283	0.07	0.07	0.07	3.932e+05	536.00	0.12	0.02	3.05e-03	0.02	26,41,19
3284	0.24	0.24	0.24	1.364e+06	536.00	0.42	0.03	0.01	0.16	42,42,20
3285	0.14	0.21	0.20	7.884e+05	536.00	0.36	0.03	9.48e-03	0.12	42,42,20
3286	0.14	0.14	0.14	7.884e+05	536.00	0.24	0.03	4.14e-03	0.06	42,41,20
3287	0.07	0.07	0.07	3.932e+05	536.00	0.12	0.02	3.05e-03	0.02	26,41,19
3288	0.24	0.24	0.24	1.364e+06	536.00	0.42	0.03	0.01	0.16	42,42,20
3289	0.14	0.21	0.20	7.884e+05	536.00	0.36	0.03	9.48e-03	0.12	42,42,20
3290	0.14	0.14	0.14	7.884e+05	536.00	0.24	0.03	4.14e-03	0.06	42,41,20
3291	0.07	0.07	0.07	3.932e+05	536.00	0.12	0.02	3.05e-03	0.02	26,41,19
3292	0.24	0.24	0.24	1.364e+06	536.00	0.42	0.03	0.01	0.16	42,42,20
3293	0.14	0.21	0.20	7.884e+05	536.00	0.36	0.03	9.48e-03	0.12	42,42,20
3294	0.14	0.14	0.14	7.884e+05	536.00	0.24	0.03	4.14e-03	0.06	42,41,20
3295	0.07	0.07	0.07	3.932e+05	536.00	0.12	0.02	3.05e-03	0.02	26,41,19
3296	0.24	0.24	0.24	1.364e+06	536.00	0.42	0.03	0.01	0.16	42,42,20
3297	0.14	0.21	0.20	7.884e+05	536.00	0.36	0.03	9.48e-03	0.12	42,42,20
3298	0.14	0.14	0.14	7.884e+05	536.00	0.24	0.03	4.14e-03	0.06	42,41,20
3299	0.07	0.07	0.07	3.932e+05	536.00	0.12	0.02	3.05e-03	0.02	26,41,19
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				3.932e+05	536.00	0.12				
	0.24	0.24	0.24	1.364e+06	536.00	0.42	0.03	0.01	0.16	

Setto	Mat.	Spessore	Stato
		cm	
223	mattoni pieni e malta di calce	40.0	NV L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
2121	4.53e-04	0.13	4.65e-04	37.14	18.86	7.29e-04	95.20	0.31	48.28	28,12,32
2295	4.53e-04	0.13	4.65e-04	37.14	18.86	7.29e-04	95.20	0.31	48.28	28,12,32
3195	4.53e-04	0.13	4.65e-04	37.14	18.86	7.29e-04	95.20	0.31	48.28	28,12,32
3197	0.14	0.13	0.06	1.154e+04	64.00	0.09	0.25	0.09	0.81	31,19,30
3323	4.53e-04	0.13	4.65e-04	37.14	18.86	7.29e-04	95.20	0.31	48.28	28,12,32
3325	0.14	0.13	0.06	1.154e+04	64.00	0.09	0.25	0.09	0.81	31,19,30
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				37.14	18.86	7.29e-04				
	0.14	0.13	0.06	1.154e+04	64.00	0.09	95.20	0.31	48.28	

Setto	Mat.	Spessore	Stato
		cm	
224	mattoni pieni e malta di calce	40.0	NV L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
3197	0.05	5.15	0.03	3987.64	0.76	0.05	1.12	1.56	1.19	20,37,32
3199	0.05	5.15	0.03	3987.64	0.76	0.05	1.12	1.56	1.19	20,37,32
3325	0.05	5.15	0.03	3987.64	0.76	0.05	1.12	1.56	1.19	20,37,32
3326	0.05	5.15	0.03	3987.64	0.76	0.05	1.12	1.56	1.19	20,37,32
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				3987.64	0.76	0.05				
	0.05	5.15	0.03	3987.64	0.76	0.05	1.12	1.56	1.19	

Setto	Mat.	Spessore	Stato
		cm	
227	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
2313	0.21	0.20	0.19	6.914e+04	129.00	0.30	0.08	0.03	0.59	40,19,31
2322	0.21	0.20	0.19	6.914e+04	129.00	0.30	0.08	0.03	0.59	40,19,31
2331	0.21	0.20	0.19	6.914e+04	129.00	0.30	0.08	0.03	0.59	40,19,31
2407	0.21	0.20	0.19	6.914e+04	129.00	0.30	0.08	0.03	0.59	40,19,31
3330	0.18	0.17	0.19	6.044e+04	129.00	0.30	0.08	0.04	0.59	32,22,31
3331	0.18	0.17	0.17	6.044e+04	129.00	0.26	0.08	0.04	0.47	32,22,31
3333	0.18	0.17	0.19	6.044e+04	129.00	0.30	0.08	0.04	0.59	32,22,31
3334	0.18	0.17	0.17	6.044e+04	129.00	0.26	0.08	0.04	0.47	32,22,31
3336	0.18	0.17	0.19	6.044e+04	129.00	0.30	0.08	0.04	0.59	32,22,31
3337	0.18	0.17	0.17	6.044e+04	129.00	0.26	0.08	0.04	0.47	32,22,31
3339	0.18	0.17	0.19	6.044e+04	129.00	0.30	0.08	0.04	0.59	32,22,31
3340	0.18	0.17	0.17	6.044e+04	129.00	0.26	0.08	0.04	0.47	32,22,31
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	0.21	0.20	0.19	6.044e+04	129.00	0.26				
				6.914e+04	129.00	0.30	0.08	0.04	0.59	

Setto	Mat.	Spessore	Stato
		cm	
228	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
3331	0.07	0.07	0.07	2.391e+04	129.00	0.11	0.07	0.03	0.26	32,26,31
3332	0.07	0.07	0.07	2.391e+04	129.00	0.11	0.07	0.03	0.26	32,26,31
3334	0.07	0.07	0.07	2.391e+04	129.00	0.11	0.07	0.03	0.26	32,26,31
3335	0.07	0.07	0.07	2.391e+04	129.00	0.11	0.07	0.03	0.26	32,26,31
3337	0.07	0.07	0.07	2.391e+04	129.00	0.11	0.07	0.03	0.26	32,26,31
3338	0.07	0.07	0.07	2.391e+04	129.00	0.11	0.07	0.03	0.26	32,26,31
3340	0.07	0.07	0.07	2.391e+04	129.00	0.11	0.07	0.03	0.26	32,26,31
3341	0.07	0.07	0.07	2.391e+04	129.00	0.11	0.07	0.03	0.26	32,26,31
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	0.07	0.07	0.07	2.391e+04	129.00	0.11				
				2.391e+04	129.00	0.11	0.07	0.03	0.26	

Setto	Mat.	Spessore	Stato
		cm	
230	mattoni pieni e malta di calce	25.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
286	0.20	0.26	0.25	1566.56	25.00	0.24	0.13	0.02	0.50	25,24,34
287	0.20	0.26	0.25	1566.56	25.00	0.24	0.13	0.02	0.50	25,24,34
288	0.20	0.22	0.21	1566.56	25.00	0.20	0.13	0.02	0.44	25,24,42
3159	0.08	0.08	0.07	1548.37	40.00	0.07	0.09	0.01	0.35	23,24,42
3315	0.26	0.26	0.25	2013.41	25.00	0.24	0.12	0.02	0.50	24,24,34
3319	0.26	0.26	0.25	2013.41	25.00	0.24	0.12	0.02	0.50	24,24,34
3324	0.20	0.22	0.21	1566.56	25.00	0.20	0.13	0.02	0.44	25,24,42
3352	0.08	0.08	0.07	1548.37	40.00	0.07	0.09	0.01	0.35	23,24,42
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	0.26	0.26	0.25	1548.37	25.00	0.07				
				2013.41	40.00	0.24	0.13	0.02	0.50	

Fascia	Mat.	Spessore	Stato
		cm	
24	muratura E = 4.550e+04	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
685	0.366.404e+04	1.750e+04		0.10	3.971e+06	11,11	1707	0.397.941e+04	1.750e+04		0.09	3.971e+06	11,11
1708	0.437.941e+04	1.750e+04		0.09	3.971e+06	11,11	1709	0.366.404e+04	1.750e+04		0.10	3.971e+06	11,11
1716	0.397.941e+04	1.750e+04		0.09	3.971e+06	11,11	1717	0.437.941e+04	1.750e+04		0.09	3.971e+06	11,11
1718	0.366.404e+04	1.750e+04		0.10	3.971e+06	11,11	1722	0.397.941e+04	1.750e+04		0.09	3.971e+06	11,11
1723	0.437.941e+04	1.750e+04		0.09	3.971e+06	11,11							

Nodo	Ver. V	Ver. M
	0.43	0.10

Fascia	Mat.	Spessore	Stato
		cm	
25	muratura E = 4.550e+04	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
432	0.207.941e+04	1.750e+04		0.04	3.971e+06	11,11	452	0.207.941e+04	1.750e+04		0.04	3.971e+06	11,11
693	0.227.941e+04	1.750e+04		0.05	3.971e+06	11,11	694	0.217.941e+04	1.750e+04		0.05	3.971e+06	11,11
695	0.247.941e+04	1.750e+04		0.05	3.971e+06	11,11	696	0.287.941e+04	1.750e+04		0.06	3.971e+06	11,11
1701	0.227.941e+04	1.750e+04		0.05	3.971e+06	11,11	1702	0.217.941e+04	1.750e+04		0.05	3.971e+06	11,11
1703	0.247.941e+04	1.750e+04		0.05	3.971e+06	11,11	1704	0.287.941e+04	1.750e+04		0.06	3.971e+06	11,11
1705	0.317.941e+04	1.750e+04		0.07	3.971e+06	11,11	1706	0.357.941e+04	1.750e+04		0.08	3.971e+06	11,11
1707	0.397.941e+04	1.750e+04		0.09	3.971e+06	11,11	1710	0.227.941e+04	1.750e+04		0.05	3.971e+06	11,11
1711	0.217.941e+04	1.750e+04		0.05	3.971e+06	11,11	1712	0.247.941e+04	1.750e+04		0.05	3.971e+06	11,11
1713	0.287.941e+04	1.750e+04		0.06	3.971e+06	11,11	1714	0.317.941e+04	1.750e+04		0.07	3.971e+06	11,11
1715	0.357.941e+04	1.750e+04		0.08	3.971e+06	11,11	1716	0.397.941e+04	1.750e+04		0.09	3.971e+06	11,11
1719	0.317.941e+04	1.750e+04		0.07	3.971e+06	11,11	1720	0.207.941e+04	1.750e+04		0.04	3.971e+06	11,11
1721	0.357.941e+04	1.750e+04		0.08	3.971e+06	11,11	1722	0.397.941e+04	1.750e+04		0.09	3.971e+06	11,11

Nodo	Ver. V	Ver. M
	0.39	0.09

Fascia	Mat.	Spessore	Stato
		cm	
28	mattoni pieni e malta di calce	25.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
22	0.062.724e+04	6937.50		0.02	2.233e+06	20,20	23	0.062.724e+04	6937.50		0.02	2.233e+06	20,20
715	0.062.724e+04	6937.50		0.02	2.233e+06	20,20	716	0.052.724e+04	6937.50		0.01	2.233e+06	21,21
724	0.062.724e+04	6937.50		0.02	2.233e+06	20,20	725	0.062.724e+04	6937.50		0.02	2.233e+06	20,20
726	0.052.724e+04	6937.50		0.01	2.233e+06	21,21	734	0.062.724e+04	6937.50		0.02	2.233e+06	20,20
735	0.062.724e+04	6937.50		0.02	2.233e+06	20,20	736	0.052.724e+04	6937.50		0.01	2.233e+06	21,21
744	0.062.724e+04	6937.50		0.02	2.233e+06	20,20	745	0.052.724e+04	6937.50		0.01	2.233e+06	21,21

Nodo	Ver. V	Ver. M
	0.06	0.02

Fascia	Mat.	Spessore	Stato
		cm	
31	mattoni pieni e malta di calce	42.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
721	0.134.576e+041.166e+04			0.03	3.752e+06	33,33	722	0.264.576e+041.166e+04			0.07	3.752e+06	33,33
723	0.224.576e+041.166e+04			0.05	3.752e+06	33,33	731	0.134.576e+041.166e+04			0.03	3.752e+06	33,33
732	0.264.576e+041.166e+04			0.07	3.752e+06	33,33	733	0.224.576e+041.166e+04			0.05	3.752e+06	33,33
741	0.134.576e+041.166e+04			0.03	3.752e+06	33,33	742	0.264.576e+041.166e+04			0.07	3.752e+06	33,33
743	0.224.576e+041.166e+04			0.05	3.752e+06	33,33	750	0.134.576e+041.166e+04			0.03	3.752e+06	33,33
751	0.264.576e+041.166e+04			0.07	3.752e+06	33,33	752	0.224.576e+041.166e+04			0.05	3.752e+06	33,33

Nodo	Ver. V	Ver. M
	0.26	0.07

Fascia	Mat.	Spessore	Stato
		cm	
32	mattoni pieni e malta di calce	42.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
757	0.116.254e+041.166e+04			0.02	3.752e+06	23,23	758	0.166.254e+041.166e+04			0.03	3.752e+06	23,23
759	0.236.254e+041.166e+04			0.04	3.752e+06	23,23	767	0.116.254e+041.166e+04			0.02	3.752e+06	23,23
768	0.166.254e+041.166e+04			0.03	3.752e+06	23,23	769	0.236.254e+041.166e+04			0.04	3.752e+06	23,23
776	0.116.254e+041.166e+04			0.02	3.752e+06	23,23	777	0.166.254e+041.166e+04			0.03	3.752e+06	23,23
778	0.236.254e+041.166e+04			0.04	3.752e+06	23,23							

Nodo	Ver. V	Ver. M
	0.23	0.04

Fascia	Mat.	Spessore	Stato
		cm	
33	mattoni pieni e malta di calce	42.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
759	0.236.254e+041.166e+04			0.04	3.752e+06	23,23	760	0.246.254e+041.166e+04			0.04	3.752e+06	23,23
761	0.255.897e+041.166e+04			0.05	3.752e+06	23,23	769	0.236.254e+041.166e+04			0.04	3.752e+06	23,23
770	0.246.254e+041.166e+04			0.04	3.752e+06	23,23	771	0.255.897e+041.166e+04			0.05	3.752e+06	23,23
778	0.236.254e+041.166e+04			0.04	3.752e+06	23,23	779	0.246.254e+041.166e+04			0.04	3.752e+06	23,23
780	0.255.897e+041.166e+04			0.05	3.752e+06	23,23							

Nodo	Ver. V	Ver. M
	0.25	0.05

Fascia	Mat.	Spessore	Stato
		cm	
36	muratura E = 4.550e+04	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2093	0.176.404e+041.750e+04			0.05	3.971e+06	32,32	2094	0.287.941e+041.750e+04			0.06	3.971e+06	32,32
2102	0.176.404e+041.750e+04			0.05	3.971e+06	32,32	2103	0.287.941e+041.750e+04			0.06	3.971e+06	32,32
2111	0.176.404e+041.750e+04			0.05	3.971e+06	32,32	2112	0.287.941e+041.750e+04			0.06	3.971e+06	32,32

Nodo	Ver. V	Ver. M
	0.28	0.06

Fascia	Mat.	Spessore	Stato
		cm	
40	muratura E = 4.550e+04	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
866	0.156.288e+041.750e+04			0.04	3.971e+06	37,37	868	0.276.288e+041.750e+04			0.08	3.971e+06	37,37
885	0.156.288e+041.750e+04			0.04	3.971e+06	37,37	886	0.156.288e+041.750e+04			0.04	3.971e+06	37,37
887	0.276.288e+041.750e+04			0.08	3.971e+06	37,37	888	0.276.288e+041.750e+04			0.08	3.971e+06	37,37
899	0.156.288e+041.750e+04			0.04	3.971e+06	37,37	900	0.276.288e+041.750e+04			0.08	3.971e+06	37,37
Nodo	Ver. V 0.27			Ver. M 0.08									

Fascia	Mat.	Spessore	Stato
		cm	
41	muratura E = 4.550e+04	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
868	0.266.288e+041.750e+04			0.07	3.971e+06	37,37	870	0.286.288e+041.750e+04			0.08	3.971e+06	37,37
872	0.236.288e+041.750e+04			0.06	3.971e+06	37,37	887	0.266.288e+041.750e+04			0.07	3.971e+06	37,37
888	0.266.288e+041.750e+04			0.07	3.971e+06	37,37	889	0.286.288e+041.750e+04			0.08	3.971e+06	37,37
890	0.286.288e+041.750e+04			0.08	3.971e+06	37,37	891	0.236.288e+041.750e+04			0.06	3.971e+06	37,37
892	0.236.288e+041.750e+04			0.06	3.971e+06	37,37	900	0.266.288e+041.750e+04			0.07	3.971e+06	37,37
901	0.286.288e+041.750e+04			0.08	3.971e+06	37,37	902	0.236.288e+041.750e+04			0.06	3.971e+06	37,37
Nodo	Ver. V 0.28			Ver. M 0.08									

Fascia	Mat.	Spessore	Stato
		cm	
45	mattoni pieni e malta di calce	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
932	0.165.956e+041.110e+04			0.03	3.573e+06	24,24	933	0.305.956e+041.110e+04			0.06	3.573e+06	24,24
1036	0.165.956e+041.110e+04			0.03	3.573e+06	24,24	1037	0.305.956e+041.110e+04			0.06	3.573e+06	24,24
1045	0.165.956e+041.110e+04			0.03	3.573e+06	24,24	1046	0.305.956e+041.110e+04			0.06	3.573e+06	24,24
Nodo	Ver. V 0.30			Ver. M 0.06									

Fascia	Mat.	Spessore	Stato
		cm	
46	mattoni pieni e malta di calce	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
933	0.285.956e+041.110e+04			0.05	3.573e+06	24,24	934	0.365.956e+041.110e+04			0.07	3.573e+06	24,24
935	0.385.956e+041.110e+04			0.07	3.573e+06	24,24	1037	0.285.956e+041.110e+04			0.05	3.573e+06	24,24
1038	0.365.956e+041.110e+04			0.07	3.573e+06	24,24	1039	0.385.956e+041.110e+04			0.07	3.573e+06	24,24
1040	0.365.956e+041.110e+04			0.07	3.573e+06	24,24	1041	0.385.956e+041.110e+04			0.07	3.573e+06	24,24
1046	0.285.956e+041.110e+04			0.05	3.573e+06	24,24							
Nodo	Ver. V 0.38			Ver. M 0.07									

Fascia	Mat.	Spessore	Stato
		cm	
48	mattoni pieni e malta di calce	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
17	0.041.588e+051.110e+043.09e-03			3.573e+06	26,26		18	0.041.588e+051.110e+043.09e-03			3.573e+06	26,26	
926	0.041.588e+051.110e+042.88e-03			3.573e+06	26,26		927	0.212.893e+041.110e+04	0.08		3.573e+06	26,26	
936	0.041.588e+051.110e+042.88e-03			3.573e+06	26,26		937	0.212.893e+041.110e+04	0.08		3.573e+06	26,26	
940	0.041.588e+051.110e+043.09e-03			3.573e+06	26,26		941	0.041.588e+051.110e+043.07e-03			3.573e+06	26,26	
942	0.051.588e+051.110e+043.15e-03			3.573e+06	26,26		943	0.041.588e+051.110e+042.82e-03			3.573e+06	26,26	
944	0.041.588e+051.110e+042.94e-03			3.573e+06	26,26		945	0.041.588e+051.110e+042.88e-03			3.573e+06	26,26	
946	0.212.893e+041.110e+04	0.08		3.573e+06	26,26		949	0.041.588e+051.110e+043.09e-03			3.573e+06	26,26	
950	0.041.588e+051.110e+043.07e-03			3.573e+06	26,26		951	0.051.588e+051.110e+043.15e-03			3.573e+06	26,26	
952	0.041.588e+051.110e+042.82e-03			3.573e+06	26,26		953	0.041.588e+051.110e+042.94e-03			3.573e+06	26,26	
954	0.041.588e+051.110e+042.88e-03			3.573e+06	26,26		955	0.212.893e+041.110e+04	0.08		3.573e+06	26,26	
963	0.041.588e+051.110e+042.88e-03			3.573e+06	26,26		964	0.212.893e+041.110e+04	0.08		3.573e+06	26,26	
972	0.041.588e+051.110e+042.88e-03			3.573e+06	26,26		973	0.212.893e+041.110e+04	0.08		3.573e+06	26,26	
Nodo	Ver. V			Ver. M									
	0.21			0.08									

Fascia	Mat.	Spessore	Stato
		cm	
49	mattoni pieni e malta di calce	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
927	0.222.893e+041.110e+04			0.08	3.573e+06	26,26	928	0.372.319e+041.110e+04			0.18	3.573e+06	18,18
929	0.242.893e+041.110e+04			0.09	3.573e+06	18,18	937	0.222.893e+041.110e+04			0.08	3.573e+06	26,26
938	0.372.319e+041.110e+04			0.18	3.573e+06	18,18	939	0.242.893e+041.110e+04			0.09	3.573e+06	18,18
946	0.222.893e+041.110e+04			0.08	3.573e+06	26,26	947	0.372.319e+041.110e+04			0.18	3.573e+06	18,18
948	0.242.893e+041.110e+04			0.09	3.573e+06	18,18	955	0.222.893e+041.110e+04			0.08	3.573e+06	26,26
956	0.372.319e+041.110e+04			0.18	3.573e+06	18,18	957	0.242.893e+041.110e+04			0.09	3.573e+06	18,18
964	0.222.893e+041.110e+04			0.08	3.573e+06	26,26	965	0.372.319e+041.110e+04			0.18	3.573e+06	18,18
966	0.242.893e+041.110e+04			0.09	3.573e+06	18,18	973	0.222.893e+041.110e+04			0.08	3.573e+06	26,26
974	0.372.319e+041.110e+04			0.18	3.573e+06	18,18	975	0.242.893e+041.110e+04			0.09	3.573e+06	18,18
2405	0.242.893e+041.110e+04			0.09	3.573e+06	18,18							
Nodo	Ver. V			Ver. M									
	0.37			0.18									

Fascia	Mat.	Spessore	Stato
		cm	
54	mattoni pieni e malta di calce	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
564	0.134.392e+041.110e+04			0.03	3.573e+06	24,24	571	0.134.392e+041.110e+04			0.03	3.573e+06	24,24
578	0.134.392e+041.110e+04			0.03	3.573e+06	24,24	585	0.134.392e+041.110e+04			0.03	3.573e+06	24,24
985	0.264.569e+041.110e+04			0.06	3.573e+06	24,24	986	0.254.569e+041.110e+04			0.06	3.573e+06	24,24
987	0.284.569e+041.110e+04			0.07	3.573e+06	24,24	988	0.284.569e+041.110e+04			0.07	3.573e+06	24,24
989	0.264.569e+041.110e+04			0.06	3.573e+06	24,24	990	0.214.569e+041.110e+04			0.05	3.573e+06	24,24
991	0.144.569e+041.110e+04			0.03	3.573e+06	24,24	994	0.264.569e+041.110e+04			0.06	3.573e+06	24,24
995	0.254.569e+041.110e+04			0.06	3.573e+06	24,24	996	0.284.569e+041.110e+04			0.07	3.573e+06	24,24
997	0.284.569e+041.110e+04			0.07	3.573e+06	24,24	998	0.264.569e+041.110e+04			0.06	3.573e+06	24,24
999	0.214.569e+041.110e+04			0.05	3.573e+06	24,24	1000	0.144.569e+041.110e+04			0.03	3.573e+06	24,24
1003	0.264.569e+041.110e+04			0.06	3.573e+06	24,24	1004	0.254.569e+041.110e+04			0.06	3.573e+06	24,24
1005	0.284.569e+041.110e+04			0.07	3.573e+06	24,24	1006	0.284.569e+041.110e+04			0.07	3.573e+06	24,24
1007	0.264.569e+041.110e+04			0.06	3.573e+06	24,24	1008	0.214.569e+041.110e+04			0.05	3.573e+06	24,24
1009	0.144.569e+041.110e+04			0.03	3.573e+06	24,24	1012	0.264.569e+041.110e+04			0.06	3.573e+06	24,24
1013	0.254.569e+041.110e+04			0.06	3.573e+06	24,24	1014	0.284.569e+041.110e+04			0.07	3.573e+06	24,24
1015	0.284.569e+041.110e+04			0.07	3.573e+06	24,24	1016	0.264.569e+041.110e+04			0.06	3.573e+06	24,24
1017	0.214.569e+041.110e+04			0.05	3.573e+06	24,24	1018	0.144.569e+041.110e+04			0.03	3.573e+06	24,24

Nodo **Ver. V** **Ver. M**
 0.28 0.07

Fascia	Mat.	Spessore	Stato
		cm	
55	mattoni pieni e malta di calce	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
991	0.124.569e+041.110e+04			0.03	3.573e+06	24,24	992	0.124.569e+041.110e+04			0.03	3.573e+06	24,24
993	0.185.553e+041.110e+04			0.04	3.573e+06	24,24	1000	0.124.569e+041.110e+04			0.03	3.573e+06	24,24
1001	0.124.569e+041.110e+04			0.03	3.573e+06	24,24	1002	0.185.553e+041.110e+04			0.04	3.573e+06	24,24
1009	0.124.569e+041.110e+04			0.03	3.573e+06	24,24	1010	0.124.569e+041.110e+04			0.03	3.573e+06	24,24
1011	0.185.553e+041.110e+04			0.04	3.573e+06	24,24	1018	0.124.569e+041.110e+04			0.03	3.573e+06	24,24
1019	0.124.569e+041.110e+04			0.03	3.573e+06	24,24	1020	0.185.553e+041.110e+04			0.04	3.573e+06	24,24

Nodo **Ver. V** **Ver. M**
 0.18 0.04

Fascia	Mat.	Spessore	Stato
		cm	
58	mattoni pieni e malta di calce	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
929	0.304.825e+041.110e+04			0.07	3.573e+06	26,26	939	0.304.825e+041.110e+04			0.07	3.573e+06	26,26
966	0.304.825e+041.110e+04			0.07	3.573e+06	26,26	975	0.304.825e+041.110e+04			0.07	3.573e+06	26,26
2368	0.334.825e+041.110e+04			0.08	3.573e+06	26,26	2369	0.344.825e+041.110e+04			0.08	3.573e+06	26,26
2370	0.334.825e+041.110e+04			0.08	3.573e+06	26,26	2371	0.344.825e+041.110e+04			0.08	3.573e+06	26,26
2372	0.404.825e+041.110e+04			0.09	3.573e+06	26,26	2373	0.282.893e+041.110e+04			0.11	3.573e+06	26,26
2374	0.292.893e+041.110e+04			0.11	3.573e+06	26,26	2375	0.322.893e+041.110e+04			0.12	3.573e+06	26,26
2376	0.342.893e+041.110e+04			0.13	3.573e+06	26,26	2377	0.334.825e+041.110e+04			0.08	3.573e+06	26,26
2378	0.344.825e+041.110e+04			0.08	3.573e+06	26,26	2379	0.334.825e+041.110e+04			0.08	3.573e+06	26,26
2380	0.344.825e+041.110e+04			0.08	3.573e+06	26,26	2381	0.404.825e+041.110e+04			0.09	3.573e+06	26,26
2382	0.282.893e+041.110e+04			0.11	3.573e+06	26,26	2383	0.292.893e+041.110e+04			0.11	3.573e+06	26,26
2384	0.322.893e+041.110e+04			0.12	3.573e+06	26,26	2385	0.342.893e+041.110e+04			0.13	3.573e+06	26,26
2390	0.404.825e+041.110e+04			0.09	3.573e+06	26,26	2391	0.282.893e+041.110e+04			0.11	3.573e+06	26,26
2392	0.292.893e+041.110e+04			0.11	3.573e+06	26,26	2393	0.322.893e+041.110e+04			0.12	3.573e+06	26,26
2394	0.342.893e+041.110e+04			0.13	3.573e+06	26,26	2399	0.404.825e+041.110e+04			0.09	3.573e+06	26,26
2400	0.282.893e+041.110e+04			0.11	3.573e+06	26,26	2401	0.292.893e+041.110e+04			0.11	3.573e+06	26,26
2402	0.322.893e+041.110e+04			0.12	3.573e+06	26,26	2403	0.342.893e+041.110e+04			0.13	3.573e+06	26,26
2405	0.304.825e+041.110e+04			0.07	3.573e+06	26,26	2409	0.404.825e+041.110e+04			0.09	3.573e+06	26,26
2410	0.282.893e+041.110e+04			0.11	3.573e+06	26,26	2411	0.292.893e+041.110e+04			0.11	3.573e+06	26,26
2412	0.322.893e+041.110e+04			0.12	3.573e+06	26,26	2413	0.342.893e+041.110e+04			0.13	3.573e+06	26,26
2414	0.334.825e+041.110e+04			0.08	3.573e+06	26,26	2415	0.344.825e+041.110e+04			0.08	3.573e+06	26,26
2416	0.334.825e+041.110e+04			0.08	3.573e+06	26,26	2417	0.344.825e+041.110e+04			0.08	3.573e+06	26,26
2418	0.404.825e+041.110e+04			0.09	3.573e+06	26,26	2419	0.282.893e+041.110e+04			0.11	3.573e+06	26,26
2420	0.292.893e+041.110e+04			0.11	3.573e+06	26,26	2421	0.322.893e+041.110e+04			0.12	3.573e+06	26,26
2422	0.342.893e+041.110e+04			0.13	3.573e+06	26,26	2431	0.334.825e+041.110e+04			0.08	3.573e+06	26,26
2432	0.334.825e+041.110e+04			0.08	3.573e+06	26,26	2433	0.344.825e+041.110e+04			0.08	3.573e+06	26,26
2434	0.344.825e+041.110e+04			0.08	3.573e+06	26,26	2435	0.334.825e+041.110e+04			0.08	3.573e+06	26,26
2436	0.334.825e+041.110e+04			0.08	3.573e+06	26,26	2437	0.344.825e+041.110e+04			0.08	3.573e+06	26,26
2438	0.344.825e+041.110e+04			0.08	3.573e+06	26,26	2439	0.404.825e+041.110e+04			0.09	3.573e+06	26,26
2440	0.282.893e+041.110e+04			0.11	3.573e+06	26,26	2441	0.292.893e+041.110e+04			0.11	3.573e+06	26,26
2442	0.322.893e+041.110e+04			0.12	3.573e+06	26,26	2443	0.342.893e+041.110e+04			0.13	3.573e+06	26,26

Nodo **Ver. V** **Ver. M**
 0.40 0.13

Fascia	Mat.	Spessore	Stato
		cm	
65	muratura E = 4.550e+04	40.0	ok L

Fascia	Mat.	Spessore	Stato
		cm	
66	muratura E = 4.550e+04	40.0	ok L

Fascia	Mat.	Spessore	Stato
		cm	
68	muratura E = 4.550e+04	40.0	ok L

Fascia	Mat.	Spessore	Stato
		cm	
69	muratura E = 4.550e+04	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
1140	0.101.073e+051.750e+04			0.02	3.971e+06	36,36
1142	0.151.073e+051.750e+04			0.02	3.971e+06	36,36
1293	0.121.073e+051.750e+04			0.02	3.971e+06	36,36
1301	0.101.073e+051.750e+04			0.02	3.971e+06	36,36
1303	0.151.073e+051.750e+04			0.02	3.971e+06	36,36

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
1141	0.121.073e+051.750e+04			0.02	3.971e+06	36,36
1292	0.101.073e+051.750e+04			0.02	3.971e+06	36,36
1294	0.151.073e+051.750e+04			0.02	3.971e+06	36,36
1302	0.121.073e+051.750e+04			0.02	3.971e+06	36,36

Nodo	Ver. V	Ver. M
	0.15	0.02

Fascia	Mat.	Spessore	Stato
		cm	
75	muratura E = 4.550e+04	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
34	0.115.515e+041.750e+04			0.03	3.971e+06	17,17	35	0.115.515e+041.750e+04			0.03	3.971e+06	17,17
200	0.115.515e+041.750e+04			0.03	3.971e+06	17,17	207	0.115.515e+041.750e+04			0.03	3.971e+06	17,17
1394	0.155.515e+041.750e+04			0.05	3.971e+06	17,17	1395	0.205.515e+041.750e+04			0.06	3.971e+06	17,17
1396	0.135.515e+041.750e+04			0.04	3.971e+06	17,17	1403	0.155.515e+041.750e+04			0.05	3.971e+06	17,17
1404	0.205.515e+041.750e+04			0.06	3.971e+06	17,17	1405	0.135.515e+041.750e+04			0.04	3.971e+06	17,17
1412	0.155.515e+041.750e+04			0.05	3.971e+06	17,17	1413	0.205.515e+041.750e+04			0.06	3.971e+06	17,17
1414	0.135.515e+041.750e+04			0.04	3.971e+06	17,17	1421	0.155.515e+041.750e+04			0.05	3.971e+06	17,17
1422	0.205.515e+041.750e+04			0.06	3.971e+06	17,17	1423	0.135.515e+041.750e+04			0.04	3.971e+06	17,17

Nodo	Ver. V	Ver. M
	0.20	0.06

Fascia	Mat.	Spessore	Stato
		cm	
76	muratura E = 4.550e+04	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
1399	0.165.515e+041.750e+04			0.05	3.971e+06	17,17	1400	0.175.515e+041.750e+04			0.05	3.971e+06	16,16
1401	0.195.515e+041.750e+04			0.06	3.971e+06	16,16	1402	0.125.515e+041.750e+04			0.04	3.971e+06	16,16
1408	0.165.515e+041.750e+04			0.05	3.971e+06	17,17	1409	0.175.515e+041.750e+04			0.05	3.971e+06	16,16
1410	0.195.515e+041.750e+04			0.06	3.971e+06	16,16	1411	0.125.515e+041.750e+04			0.04	3.971e+06	16,16
1417	0.165.515e+041.750e+04			0.05	3.971e+06	17,17	1418	0.175.515e+041.750e+04			0.05	3.971e+06	16,16
1419	0.195.515e+041.750e+04			0.06	3.971e+06	16,16	1420	0.125.515e+041.750e+04			0.04	3.971e+06	16,16
1426	0.165.515e+041.750e+04			0.05	3.971e+06	17,17	1427	0.175.515e+041.750e+04			0.05	3.971e+06	16,16
1428	0.195.515e+041.750e+04			0.06	3.971e+06	16,16	1429	0.125.515e+041.750e+04			0.04	3.971e+06	16,16

Nodo	Ver. V	Ver. M
	0.19	0.06

Fascia	Mat.	Spessore	Stato
		cm	
81	mattoni pieni e malta di calce	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
5	0.254.229e+041.110e+04			0.07	3.573e+06	17,17	6	0.254.229e+041.110e+04			0.07	3.573e+06	17,17
358	0.254.229e+041.110e+04			0.07	3.573e+06	17,17	379	0.254.229e+041.110e+04			0.07	3.573e+06	17,17
1448	0.204.229e+041.110e+04			0.05	3.573e+06	17,17	1449	0.174.229e+041.110e+04			0.04	3.573e+06	17,17
1457	0.204.229e+041.110e+04			0.05	3.573e+06	17,17	1458	0.174.229e+041.110e+04			0.04	3.573e+06	17,17
1466	0.204.229e+041.110e+04			0.05	3.573e+06	17,17	1467	0.254.229e+041.110e+04			0.07	3.573e+06	17,17
1468	0.174.229e+041.110e+04			0.04	3.573e+06	17,17	1476	0.204.229e+041.110e+04			0.05	3.573e+06	17,17
1477	0.254.229e+041.110e+04			0.07	3.573e+06	17,17	1478	0.174.229e+041.110e+04			0.04	3.573e+06	17,17
1486	0.204.229e+041.110e+04			0.05	3.573e+06	17,17	1487	0.174.229e+041.110e+04			0.04	3.573e+06	17,17
1495	0.204.229e+041.110e+04			0.05	3.573e+06	17,17	1496	0.174.229e+041.110e+04			0.04	3.573e+06	17,17

Nodo	Ver. V	Ver. M
	0.25	0.07

Fascia	Mat.	Spessore	Stato
		cm	
84	mattoni pieni e malta di calce	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
1455	0.324.229e+041.110e+04			0.08	3.573e+06	17,17	1456	0.674.229e+041.110e+04			0.17	3.573e+06	17,17
1464	0.324.229e+041.110e+04			0.08	3.573e+06	17,17	1465	0.674.229e+041.110e+04			0.17	3.573e+06	17,17
1474	0.324.229e+041.110e+04			0.08	3.573e+06	17,17	1475	0.674.229e+041.110e+04			0.17	3.573e+06	17,17
1484	0.324.229e+041.110e+04			0.08	3.573e+06	17,17	1485	0.674.229e+041.110e+04			0.17	3.573e+06	17,17
1493	0.324.229e+041.110e+04			0.08	3.573e+06	17,17	1494	0.674.229e+041.110e+04			0.17	3.573e+06	17,17
1502	0.324.229e+041.110e+04			0.08	3.573e+06	17,17	1503	0.674.229e+041.110e+04			0.17	3.573e+06	17,17
Nodo	Ver. V 0.67			Ver. M 0.17									

Fascia	Mat.	Spessore	Stato
		cm	
85	mattoni pieni e malta di calce	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
1151	0.034.229e+041.110e+047.26e-03			3.573e+06	16,16		1520	0.034.229e+041.110e+047.67e-03			3.573e+06	16,16	
1521	0.034.229e+041.110e+047.26e-03			3.573e+06	16,16		1529	0.034.229e+041.110e+047.67e-03			3.573e+06	16,16	
1530	0.034.229e+041.110e+047.26e-03			3.573e+06	16,16		1539	0.034.229e+041.110e+047.67e-03			3.573e+06	16,16	
1540	0.034.229e+041.110e+047.26e-03			3.573e+06	16,16		1549	0.034.229e+041.110e+047.67e-03			3.573e+06	16,16	
1550	0.034.229e+041.110e+047.26e-03			3.573e+06	16,16		1558	0.034.229e+041.110e+047.67e-03			3.573e+06	16,16	
1559	0.034.229e+041.110e+047.26e-03			3.573e+06	16,16		1567	0.034.229e+041.110e+047.67e-03			3.573e+06	16,16	
Nodo	Ver. V			Ver. M									
	0.03			7.67e-03									

Fascia	Mat.	Spessore	Stato
		cm	
87	mattoni pieni e malta di calce	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
1459	0.454.229e+041.110e+04			0.12	3.573e+06	15,15	1462	0.234.229e+041.110e+04			0.06	3.573e+06	15,15
1463	0.454.229e+041.110e+04			0.12	3.573e+06	15,15	1482	0.234.229e+041.110e+04			0.06	3.573e+06	15,15
1483	0.454.229e+041.110e+04			0.12	3.573e+06	15,15	1527	0.234.229e+041.110e+04			0.06	3.573e+06	15,15
1528	0.454.229e+041.110e+04			0.12	3.573e+06	15,15	1546	0.234.229e+041.110e+04			0.06	3.573e+06	15,15
1547	0.454.229e+041.110e+04			0.12	3.573e+06	15,15	1585	0.234.229e+041.110e+04			0.06	3.573e+06	15,15
1586	0.454.229e+041.110e+04			0.12	3.573e+06	15,15	1590	0.234.229e+041.110e+04			0.06	3.573e+06	15,15
Nodo	Ver. V 0.45			Ver. M 0.12									

Fascia	Mat.	Spessore	Stato
		cm	
88	mattoni pieni e malta di calce	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
9	0.304.229e+041.110e+04			0.08	3.573e+06	11,11	10	0.304.229e+041.110e+04			0.08	3.573e+06	11,11
12	0.304.229e+041.110e+04			0.08	3.573e+06	11,11	414	0.304.229e+041.110e+04			0.08	3.573e+06	11,11
1469	0.284.229e+041.110e+04			0.07	3.573e+06	11,11	1470	0.304.229e+041.110e+04			0.08	3.573e+06	11,11
1471	0.214.229e+041.110e+04			0.06	3.573e+06	11,11	1488	0.284.229e+041.110e+04			0.07	3.573e+06	11,11
1489	0.304.229e+041.110e+04			0.08	3.573e+06	11,11	1490	0.214.229e+041.110e+04			0.06	3.573e+06	11,11
1534	0.284.229e+041.110e+04			0.07	3.573e+06	11,11	1535	0.214.229e+041.110e+04			0.06	3.573e+06	11,11
1548	0.284.229e+041.110e+04			0.07	3.573e+06	11,11	1553	0.214.229e+041.110e+04			0.06	3.573e+06	11,11
1578	0.284.229e+041.110e+04			0.07	3.573e+06	11,11	1579	0.214.229e+041.110e+04			0.06	3.573e+06	11,11

1587 0.284.229e+041.110e+04 0.07 3.573e+06 11,11 1588 0.214.229e+041.110e+04 0.06 3.573e+06 11,11

Nodo Ver. V Ver. M
0.30 0.08

Fascia	Mat.	Spessore	Stato
		cm	
91	mattoni pieni e malta di calce	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
7	0.044.229e+041.110e+04			0.01	3.573e+06	17,17	8	0.044.229e+041.110e+04			0.01	3.573e+06	17,17
386	0.044.229e+041.110e+04			0.01	3.573e+06	17,17	407	0.044.229e+041.110e+04			0.01	3.573e+06	17,17
1513	0.114.229e+041.110e+04			0.03	3.573e+06	17,17	1514	0.044.229e+041.110e+04			0.01	3.573e+06	17,17
1522	0.114.229e+041.110e+04			0.03	3.573e+06	17,17	1523	0.044.229e+041.110e+04			0.01	3.573e+06	17,17
1531	0.114.229e+041.110e+04			0.03	3.573e+06	17,17	1532	0.044.229e+041.110e+04			0.01	3.573e+06	17,17
1533	0.044.229e+041.110e+04			0.01	3.573e+06	17,17	1541	0.114.229e+041.110e+04			0.03	3.573e+06	17,17
1542	0.044.229e+041.110e+04			0.01	3.573e+06	17,17	1543	0.044.229e+041.110e+04			0.01	3.573e+06	17,17
1551	0.114.229e+041.110e+04			0.03	3.573e+06	17,17	1552	0.044.229e+041.110e+04			0.01	3.573e+06	17,17
1560	0.114.229e+041.110e+04			0.03	3.573e+06	17,17	1561	0.044.229e+041.110e+04			0.01	3.573e+06	17,17

Nodo Ver. V Ver. M
0.11 0.03

Fascia	Mat.	Spessore	Stato
		cm	
94	muratura E = 4.550e+04	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
515	0.237.941e+041.750e+04			0.05	3.971e+06	30,30	533	0.237.941e+041.750e+04			0.05	3.971e+06	30,30
1591	0.287.941e+041.750e+04			0.06	3.971e+06	30,30	1592	0.297.941e+041.750e+04			0.06	3.971e+06	30,30
1593	0.327.941e+041.750e+04			0.07	3.971e+06	30,30	1594	0.377.941e+041.750e+04			0.08	3.971e+06	30,30
1595	0.417.941e+041.750e+04			0.09	3.971e+06	30,30	1596	0.467.941e+041.750e+04			0.10	3.971e+06	30,30
1597	0.517.941e+041.750e+04			0.11	3.971e+06	30,30	1600	0.287.941e+041.750e+04			0.06	3.971e+06	30,30
1601	0.237.941e+041.750e+04			0.05	3.971e+06	30,30	1602	0.297.941e+041.750e+04			0.06	3.971e+06	30,30
1603	0.327.941e+041.750e+04			0.07	3.971e+06	30,30	1604	0.377.941e+041.750e+04			0.08	3.971e+06	30,30
1605	0.417.941e+041.750e+04			0.09	3.971e+06	30,30	1606	0.467.941e+041.750e+04			0.10	3.971e+06	30,30
1607	0.517.941e+041.750e+04			0.11	3.971e+06	30,30	1610	0.287.941e+041.750e+04			0.06	3.971e+06	30,30
1611	0.297.941e+041.750e+04			0.06	3.971e+06	30,30	1612	0.327.941e+041.750e+04			0.07	3.971e+06	30,30
1613	0.377.941e+041.750e+04			0.08	3.971e+06	30,30	1614	0.417.941e+041.750e+04			0.09	3.971e+06	30,30
1615	0.467.941e+041.750e+04			0.10	3.971e+06	30,30	1616	0.517.941e+041.750e+04			0.11	3.971e+06	30,30

Nodo Ver. V Ver. M
0.51 0.11

Fascia	Mat.	Spessore	Stato
		cm	
95	muratura E = 4.550e+04	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
1597	0.507.941e+041.750e+04			0.11	3.971e+06	30,30	1598	0.557.941e+041.750e+04			0.12	3.971e+06	30,30
1599	0.506.404e+041.750e+04			0.14	3.971e+06	30,30	1607	0.507.941e+041.750e+04			0.11	3.971e+06	30,30
1608	0.557.941e+041.750e+04			0.12	3.971e+06	30,30	1609	0.506.404e+041.750e+04			0.14	3.971e+06	30,30
1616	0.507.941e+041.750e+04			0.11	3.971e+06	30,30	1617	0.557.941e+041.750e+04			0.12	3.971e+06	30,30
1618	0.506.404e+041.750e+04			0.14	3.971e+06	30,30							

Nodo Ver. V Ver. M
0.55 0.14

Fascia	Mat.	Spessore	Stato
		cm	
98	muratura E = 4.550e+04	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
473	0.117.941e+041.750e+04			0.02	3.971e+06	30,30	487	0.117.941e+041.750e+04			0.02	3.971e+06	30,30
1646	0.117.941e+041.750e+04			0.02	3.971e+06	30,30	1647	0.107.941e+041.750e+04			0.02	3.971e+06	30,30
1648	0.097.941e+041.750e+04			0.02	3.971e+06	30,30	1649	0.087.941e+041.750e+04			0.02	3.971e+06	30,30
1650	0.077.941e+041.750e+04			0.02	3.971e+06	30,30	1651	0.087.941e+041.750e+04			0.02	3.971e+06	27,27
1652	0.097.941e+041.750e+04			0.02	3.971e+06	27,27	1655	0.117.941e+041.750e+04			0.02	3.971e+06	30,30
1656	0.117.941e+041.750e+04			0.02	3.971e+06	30,30	1657	0.107.941e+041.750e+04			0.02	3.971e+06	30,30
1658	0.097.941e+041.750e+04			0.02	3.971e+06	30,30	1659	0.087.941e+041.750e+04			0.02	3.971e+06	30,30
1660	0.077.941e+041.750e+04			0.02	3.971e+06	30,30	1661	0.087.941e+041.750e+04			0.02	3.971e+06	27,27
1662	0.097.941e+041.750e+04			0.02	3.971e+06	27,27	1665	0.117.941e+041.750e+04			0.02	3.971e+06	30,30
1666	0.107.941e+041.750e+04			0.02	3.971e+06	30,30	1667	0.097.941e+041.750e+04			0.02	3.971e+06	30,30
1668	0.087.941e+041.750e+04			0.02	3.971e+06	30,30	1669	0.077.941e+041.750e+04			0.02	3.971e+06	30,30
1670	0.087.941e+041.750e+04			0.02	3.971e+06	27,27	1671	0.097.941e+041.750e+04			0.02	3.971e+06	27,27

Nodo	Ver. V	Ver. M
	0.11	0.02

Fascia	Mat.	Spessore	Stato
		cm	
99	muratura E = 4.550e+04	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
1652	0.097.941e+041.750e+04			0.02	3.971e+06	27,27	1653	0.117.941e+041.750e+04			0.02	3.971e+06	27,27
1654	0.086.404e+041.750e+04			0.02	3.971e+06	27,27	1662	0.097.941e+041.750e+04			0.02	3.971e+06	27,27
1663	0.117.941e+041.750e+04			0.02	3.971e+06	27,27	1664	0.086.404e+041.750e+04			0.02	3.971e+06	27,27
1671	0.097.941e+041.750e+04			0.02	3.971e+06	27,27	1672	0.117.941e+041.750e+04			0.02	3.971e+06	27,27
1673	0.086.404e+041.750e+04			0.02	3.971e+06	27,27							

Nodo	Ver. V	Ver. M
	0.11	0.02

Fascia	Mat.	Spessore	Stato
		cm	
104	mattoni pieni e malta di calce	40.0	NV L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
1456	1.374.229e+04	1.110e+04		0.36	3.573e+06	17,17	1465	2.202.643e+04	6937.50		0.58	2.233e+06	17,17
1475	2.202.643e+04	6937.50		0.58	2.233e+06	17,17	1485	2.202.643e+04	6937.50		0.58	2.233e+06	17,17
1494	2.202.643e+04	6937.50		0.58	2.233e+06	17,17	1503	1.374.229e+04	1.110e+04		0.36	3.573e+06	17,17
1742	1.374.229e+04	1.110e+04		0.36	3.573e+06	17,17	1743	0.694.229e+04	1.110e+04		0.18	3.573e+06	17,17
1744	0.312.687e+05	1.110e+04		0.01	3.573e+06	16,16	1745	0.042.687e+05	1.110e+04	1.58e-03		3.573e+06	16,16
1746	0.052.687e+05	1.110e+04	2.27e-03		3.573e+06	25,25	1747	0.072.687e+05	1.110e+04	2.96e-03		3.573e+06	25,25
1748	0.172.687e+05	1.110e+04	6.84e-03		3.573e+06	22,22	1749	1.242.687e+05	1.110e+04		0.05	3.573e+06	17,17
1750	0.864.229e+04	1.110e+04		0.23	3.573e+06	17,17	1751	2.182.643e+04	6937.50		0.57	2.233e+06	17,17
1752	1.102.643e+04	6937.50		0.29	2.233e+06	17,17	1753	0.312.687e+05	1.110e+04		0.01	3.573e+06	16,16
1754	0.042.687e+05	1.110e+04	1.58e-03		3.573e+06	16,16	1755	0.052.687e+05	1.110e+04	2.27e-03		3.573e+06	25,25
1756	0.072.687e+05	1.110e+04	2.96e-03		3.573e+06	25,25	1757	0.172.687e+05	1.110e+04	6.84e-03		3.573e+06	22,22
1758	1.242.687e+05	1.110e+04		0.05	3.573e+06	17,17	1759	0.864.229e+04	1.110e+04		0.23	3.573e+06	17,17
1760	2.182.643e+04	6937.50		0.57	2.233e+06	17,17	1761	1.102.643e+04	6937.50		0.29	2.233e+06	17,17
1767	1.242.687e+05	1.110e+04		0.05	3.573e+06	17,17	1768	0.864.229e+04	1.110e+04		0.23	3.573e+06	17,17
1769	2.182.643e+04	6937.50		0.57	2.233e+06	17,17	1770	1.102.643e+04	6937.50		0.29	2.233e+06	17,17
1776	1.242.687e+05	1.110e+04		0.05	3.573e+06	17,17	1777	0.864.229e+04	1.110e+04		0.23	3.573e+06	17,17
1778	2.182.643e+04	6937.50		0.57	2.233e+06	17,17	1779	1.102.643e+04	6937.50		0.29	2.233e+06	17,17

1780	0.312.687e+051.110e+04	0.01	3.573e+06	16,16	1781	0.042.687e+051.110e+041.58e-03	3.573e+06	16,16
1782	0.052.687e+051.110e+042.27e-03		3.573e+06	25,25	1783	0.072.687e+051.110e+042.96e-03	3.573e+06	25,25
1784	0.172.687e+051.110e+046.84e-03		3.573e+06	22,22	1785	1.242.687e+051.110e+04	0.05	3.573e+06
1786	0.864.229e+041.110e+04	0.23	3.573e+06	17,17	1787	1.374.229e+041.110e+04	0.36	3.573e+06
1788	0.694.229e+041.110e+04	0.18	3.573e+06	17,17	1789	0.312.687e+051.110e+04	0.01	3.573e+06
1790	0.042.687e+051.110e+041.58e-03		3.573e+06	16,16	1791	0.052.687e+051.110e+042.27e-03		3.573e+06
1792	0.072.687e+051.110e+042.96e-03		3.573e+06	25,25	1793	0.172.687e+051.110e+046.84e-03		3.573e+06
1794	1.242.687e+051.110e+04	0.05	3.573e+06	17,17	1795	0.864.229e+041.110e+04	0.23	3.573e+06

Nodo **Ver. V** **Ver. M**
 2.20 0.58

Fascia	Mat.	Spessore	Stato
		cm	
107	mattoni pieni e malta di calce	38.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2100	0.085.721e+041.055e+04			0.01	3.395e+06	37,37	2101	0.065.721e+041.055e+04			0.01	3.395e+06	37,37
2137	0.085.721e+041.055e+04			0.01	3.395e+06	37,37	2138	0.065.721e+041.055e+04			0.01	3.395e+06	37,37
2168	0.085.721e+041.055e+04			0.01	3.395e+06	37,37	2170	0.065.721e+041.055e+04			0.01	3.395e+06	37,37
2230	0.085.721e+041.055e+04			0.01	3.395e+06	37,37	2231	0.065.721e+041.055e+04			0.01	3.395e+06	37,37

Nodo **Ver. V** **Ver. M**
 0.08 0.01

Fascia	Mat.	Spessore	Stato
		cm	
108	mattoni pieni e malta di calce	38.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
1762	0.077.988e+041.055e+048.84e-03			3.395e+06		21,21	1766	0.047.988e+041.055e+045.25e-03			3.395e+06		21,21
1899	0.077.988e+041.055e+048.84e-03			3.395e+06		21,21	1900	0.047.988e+041.055e+045.25e-03			3.395e+06		21,21
2123	0.077.988e+041.055e+048.84e-03			3.395e+06		21,21	2133	0.047.988e+041.055e+045.25e-03			3.395e+06		21,21

Nodo **Ver. V** **Ver. M**
 0.07 8.84e-03

Fascia	Mat.	Spessore	Stato
		cm	
110	mattoni pieni e malta di calce	25.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
1773	0.065.255e+04	6937.50	7.38e-03	2.233e+06		20,20	1774	0.055.255e+04	6937.50	6.93e-03	2.233e+06		20,20
1775	0.045.255e+04	6937.50	5.36e-03	2.233e+06		20,20	1991	0.065.255e+04	6937.50	7.38e-03	2.233e+06		20,20
1992	0.045.255e+04	6937.50	5.36e-03	2.233e+06		20,20	2139	0.065.255e+04	6937.50	7.38e-03	2.233e+06		20,20
2140	0.045.255e+04	6937.50	5.36e-03	2.233e+06		20,20	2150	0.055.255e+04	6937.50	6.93e-03	2.233e+06		20,20
2151	0.055.255e+04	6937.50	6.93e-03	2.233e+06		20,20							

Nodo **Ver. V** **Ver. M**
 0.06 7.38e-03

Fascia	Mat.	Spessore	Stato
		cm	
111	mattoni pieni e malta di calce	25.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
2047	0.095.255e+04	6937.50		0.01	2.233e+06	20,20	2097	0.075.255e+04	6937.50	9.25e-03	2.233e+06	20,20	
2098	0.085.255e+04	6937.50		0.01	2.233e+06	20,20	2128	0.095.255e+04	6937.50		0.01	2.233e+06	20,20
2129	0.085.255e+04	6937.50		0.01	2.233e+06	20,20	2132	0.095.255e+04	6937.50		0.01	2.233e+06	20,20
2142	0.085.255e+04	6937.50		0.01	2.233e+06	20,20	2148	0.075.255e+04	6937.50	9.25e-03	2.233e+06	20,20	
2149	0.075.255e+04	6937.50	9.25e-03		2.233e+06	20,20							

Nodo	Ver. V	Ver. M
	0.09	0.01

Fascia	Mat.	Spessore	Stato
		cm	
113	mattoni pieni e malta di calce	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
1151	0.074.229e+041.110e+04			0.02	3.573e+06	17,17	1521	0.074.229e+041.110e+04			0.02	3.573e+06	17,17
1530	0.074.229e+041.110e+04			0.02	3.573e+06	17,17	1540	0.074.229e+041.110e+04			0.02	3.573e+06	17,17
1550	0.074.229e+041.110e+04			0.02	3.573e+06	17,17	1559	0.074.229e+041.110e+04			0.02	3.573e+06	17,17
1805	0.074.229e+041.110e+04			0.02	3.573e+06	17,17	1806	0.094.229e+041.110e+04			0.02	3.573e+06	17,17
1807	0.134.229e+041.110e+04			0.03	3.573e+06	17,17	1808	0.154.229e+041.110e+04			0.04	3.573e+06	14,14
1809	0.164.229e+041.110e+04			0.04	3.573e+06	17,17	1810	0.154.229e+041.110e+04			0.04	3.573e+06	14,14
1811	0.144.229e+041.110e+04			0.04	3.573e+06	14,14	1812	0.104.229e+041.110e+04			0.03	3.573e+06	17,17
1813	0.064.229e+041.110e+04			0.02	3.573e+06	17,17	1814	0.074.229e+041.110e+04			0.02	3.573e+06	17,17
1815	0.094.229e+041.110e+04			0.02	3.573e+06	17,17	1816	0.134.229e+041.110e+04			0.03	3.573e+06	17,17
1817	0.154.229e+041.110e+04			0.04	3.573e+06	14,14	1818	0.164.229e+041.110e+04			0.04	3.573e+06	17,17
1819	0.154.229e+041.110e+04			0.04	3.573e+06	14,14	1820	0.144.229e+041.110e+04			0.04	3.573e+06	14,14
1821	0.104.229e+041.110e+04			0.03	3.573e+06	17,17	1822	0.064.229e+041.110e+04			0.02	3.573e+06	17,17
1823	0.074.229e+041.110e+04			0.02	3.573e+06	17,17	1824	0.094.229e+041.110e+04			0.02	3.573e+06	17,17
1825	0.134.229e+041.110e+04			0.03	3.573e+06	17,17	1826	0.154.229e+041.110e+04			0.04	3.573e+06	14,14
1827	0.164.229e+041.110e+04			0.04	3.573e+06	17,17	1828	0.154.229e+041.110e+04			0.04	3.573e+06	14,14
1829	0.144.229e+041.110e+04			0.04	3.573e+06	14,14	1830	0.104.229e+041.110e+04			0.03	3.573e+06	17,17
1831	0.064.229e+041.110e+04			0.02	3.573e+06	17,17	1832	0.074.229e+041.110e+04			0.02	3.573e+06	17,17
1833	0.094.229e+041.110e+04			0.02	3.573e+06	17,17	1834	0.134.229e+041.110e+04			0.03	3.573e+06	17,17
1835	0.154.229e+041.110e+04			0.04	3.573e+06	14,14	1836	0.164.229e+041.110e+04			0.04	3.573e+06	17,17
1837	0.154.229e+041.110e+04			0.04	3.573e+06	14,14	1838	0.144.229e+041.110e+04			0.04	3.573e+06	14,14
1839	0.104.229e+041.110e+04			0.03	3.573e+06	17,17	1840	0.064.229e+041.110e+04			0.02	3.573e+06	17,17
1841	0.074.229e+041.110e+04			0.02	3.573e+06	17,17	1842	0.094.229e+041.110e+04			0.02	3.573e+06	17,17
1843	0.134.229e+041.110e+04			0.03	3.573e+06	17,17	1844	0.154.229e+041.110e+04			0.04	3.573e+06	14,14
1845	0.164.229e+041.110e+04			0.04	3.573e+06	17,17	1846	0.154.229e+041.110e+04			0.04	3.573e+06	14,14
1847	0.144.229e+041.110e+04			0.04	3.573e+06	14,14	1848	0.104.229e+041.110e+04			0.03	3.573e+06	17,17
1849	0.064.229e+041.110e+04			0.02	3.573e+06	17,17	1850	0.074.229e+041.110e+04			0.02	3.573e+06	17,17
1851	0.094.229e+041.110e+04			0.02	3.573e+06	17,17	1852	0.134.229e+041.110e+04			0.03	3.573e+06	17,17
1853	0.154.229e+041.110e+04			0.04	3.573e+06	14,14	1854	0.164.229e+041.110e+04			0.04	3.573e+06	17,17
1855	0.154.229e+041.110e+04			0.04	3.573e+06	14,14	1856	0.144.229e+041.110e+04			0.04	3.573e+06	14,14
1857	0.104.229e+041.110e+04			0.03	3.573e+06	17,17	1858	0.064.229e+041.110e+04			0.02	3.573e+06	17,17

Nodo	Ver. V	Ver. M
	0.16	0.04

Fascia	Mat.	Spessore	Stato
		cm	
115	mattoni pieni e malta di calce	40.0	NV L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
1459	0.994.229e+04	1.110e+04		0.26	3.573e+06	15,15	1463	1.592.643e+04	6937.50		0.42	2.233e+06	15,15
1483	1.592.643e+04	6937.50		0.42	2.233e+06	15,15	1528	1.592.643e+04	6937.50		0.42	2.233e+06	15,15
1547	1.592.643e+04	6937.50		0.42	2.233e+06	15,15	1586	0.994.229e+04	1.110e+04		0.26	3.573e+06	15,15
1868	1.044.229e+04	1.110e+04		0.27	3.573e+06	15,15	1869	0.584.229e+04	1.110e+04		0.15	3.573e+06	15,15
1870	0.252.687e+05	1.110e+04		0.01	3.573e+06	18,18	1871	0.062.687e+05	1.110e+04	2.41e-03		3.573e+06	39,39
1872	0.082.687e+05	1.110e+04	3.40e-03		3.573e+06	15,15	1873	0.092.687e+05	1.110e+04	3.54e-03		3.573e+06	11,11
1874	0.152.687e+05	1.110e+04	6.09e-03		3.573e+06	19,19	1875	1.042.687e+05	1.110e+04		0.04	3.573e+06	11,11

1876	0.694.229e+041.110e+04	0.18	3.573e+06	11,11	1877	1.672.643e+04	6937.50	0.44	2.233e+06	15,15	
1878	0.932.643e+04	6937.50	0.24	2.233e+06	15,15	1879	0.252.687e+051.110e+04	0.01	3.573e+06	18,18	
1880	0.062.687e+051.110e+042.41e-03		3.573e+06	39,39	1881	0.082.687e+051.110e+043.40e-03		3.573e+06	15,15		
1882	0.092.687e+051.110e+043.54e-03		3.573e+06	11,11	1883	0.152.687e+051.110e+046.09e-03		3.573e+06	19,19		
1884	1.042.687e+051.110e+04	0.04	3.573e+06	11,11	1885	0.694.229e+041.110e+04	0.18	3.573e+06	11,11		
1886	1.672.643e+04	6937.50	0.44	2.233e+06	15,15	1887	0.932.643e+04	6937.50	0.24	2.233e+06	15,15
1893	1.042.687e+051.110e+04	0.04	3.573e+06	11,11	1894	0.694.229e+041.110e+04	0.18	3.573e+06	11,11		
1895	1.672.643e+04	6937.50	0.44	2.233e+06	15,15	1896	0.932.643e+04	6937.50	0.24	2.233e+06	15,15
1902	1.042.687e+051.110e+04	0.04	3.573e+06	11,11	1903	0.694.229e+041.110e+04	0.18	3.573e+06	11,11		
1904	1.672.643e+04	6937.50	0.44	2.233e+06	15,15	1905	0.932.643e+04	6937.50	0.24	2.233e+06	15,15
1906	0.252.687e+051.110e+04	0.01	3.573e+06	18,18	1907	0.062.687e+051.110e+042.41e-03		3.573e+06	39,39		
1908	0.082.687e+051.110e+043.40e-03		3.573e+06	15,15	1909	0.092.687e+051.110e+043.54e-03		3.573e+06	11,11		
1910	0.152.687e+051.110e+046.09e-03		3.573e+06	19,19	1911	1.042.687e+051.110e+04	0.04	3.573e+06	11,11		
1912	0.694.229e+041.110e+04	0.18	3.573e+06	11,11	1913	1.044.229e+041.110e+04	0.27	3.573e+06	15,15		
1914	0.584.229e+041.110e+04	0.15	3.573e+06	15,15	1915	0.252.687e+051.110e+04	0.01	3.573e+06	18,18		
1916	0.062.687e+051.110e+042.41e-03		3.573e+06	39,39	1917	0.082.687e+051.110e+043.40e-03		3.573e+06	15,15		
1918	0.092.687e+051.110e+043.54e-03		3.573e+06	11,11	1919	0.152.687e+051.110e+046.09e-03		3.573e+06	19,19		
1920	1.042.687e+051.110e+04	0.04	3.573e+06	11,11	1921	0.694.229e+041.110e+04	0.18	3.573e+06	11,11		

Nodo **Ver. V** **Ver. M**
 1.67 0.44

Fascia	Mat.	Spessore	Stato
		cm	
116	mattoni pieni e malta di calce	38.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
1892	0.127.988e+041.055e+04		0.02	3.395e+06	20,20		1989	0.077.988e+041.055e+048.83e-03		3.395e+06	20,20		
2124	0.127.988e+041.055e+04		0.02	3.395e+06	20,20		2125	0.077.988e+041.055e+048.83e-03		3.395e+06	20,20		
2135	0.127.988e+041.055e+04		0.02	3.395e+06	20,20		2136	0.077.988e+041.055e+048.83e-03		3.395e+06	20,20		

Nodo **Ver. V** **Ver. M**
 0.12 0.02

Fascia	Mat.	Spessore	Stato
		cm	
117	mattoni pieni e malta di calce	25.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
1901	0.203.764e+04	6937.50	0.04	2.233e+06	37,37		1990	0.163.764e+04	6937.50	0.03	2.233e+06	37,37	
2043	0.173.764e+04	6937.50	0.03	2.233e+06	37,37		2044	0.203.764e+04	6937.50	0.04	2.233e+06	37,37	
2122	0.163.764e+04	6937.50	0.03	2.233e+06	37,37		2143	0.173.764e+04	6937.50	0.03	2.233e+06	37,37	
2158	0.203.764e+04	6937.50	0.04	2.233e+06	37,37		2160	0.173.764e+04	6937.50	0.03	2.233e+06	37,37	
2193	0.163.764e+04	6937.50	0.03	2.233e+06	37,37		2201	0.163.764e+04	6937.50	0.03	2.233e+06	37,37	
2202	0.203.764e+04	6937.50	0.04	2.233e+06	37,37		2210	0.173.764e+04	6937.50	0.03	2.233e+06	37,37	

Nodo **Ver. V** **Ver. M**
 0.20 0.04

Fascia	Mat.	Spessore	Stato
		cm	
119	muratura E = 4.550e+04	20.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
685	0.423.202e+04	8750.00	0.11	1.985e+06	27,27		1709	0.423.202e+04	8750.00	0.11	1.985e+06	27,27	
1718	0.423.202e+04	8750.00	0.11	1.985e+06	27,27		1778	0.383.202e+04	8750.00	0.10	1.985e+06	27,27	
1979	0.243.202e+04	8750.00	0.07	1.985e+06	27,27		1987	0.383.202e+04	8750.00	0.10	1.985e+06	27,27	
1988	0.243.202e+04	8750.00	0.07	1.985e+06	27,27		1996	0.383.202e+04	8750.00	0.10	1.985e+06	27,27	

1997 0.243.202e+04 8750.00 0.07 1.985e+06 27,27

Nodo Ver. V Ver. M
0.42 0.11

Fascia	Mat.	Spessore	Stato
		cm	
120	muratura E = 4.550e+04	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
1985	0.196.404e+04	1.750e+04		0.05	3.971e+06	15,15	1986	0.377.941e+04	1.750e+04		0.08	3.971e+06	15,15
1994	0.196.404e+04	1.750e+04		0.05	3.971e+06	15,15	1995	0.377.941e+04	1.750e+04		0.08	3.971e+06	15,15
2003	0.196.404e+04	1.750e+04		0.05	3.971e+06	15,15	2004	0.377.941e+04	1.750e+04		0.08	3.971e+06	15,15

Nodo Ver. V Ver. M
0.37 0.08

Fascia	Mat.	Spessore	Stato
		cm	
123	muratura E = 4.550e+04	20.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
1654	0.083.202e+04	8750.00		0.02	1.985e+06	27,27	1664	0.083.202e+04	8750.00		0.02	1.985e+06	27,27
1673	0.083.202e+04	8750.00		0.02	1.985e+06	27,27	2032	0.073.202e+04	8750.00		0.02	1.985e+06	30,30
2033	0.073.202e+04	8750.00		0.02	1.985e+06	30,30	2041	0.073.202e+04	8750.00		0.02	1.985e+06	30,30
2042	0.073.202e+04	8750.00		0.02	1.985e+06	30,30	2050	0.073.202e+04	8750.00		0.02	1.985e+06	30,30
2051	0.073.202e+04	8750.00		0.02	1.985e+06	30,30							

Nodo Ver. V Ver. M
0.08 0.02

Fascia	Mat.	Spessore	Stato
		cm	
125	muratura E = 4.550e+04	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2039	0.056.404e+04	1.750e+04		0.01	3.971e+06	30,30	2040	0.077.941e+04	1.750e+04		0.02	3.971e+06	30,30
2048	0.056.404e+04	1.750e+04		0.01	3.971e+06	30,30	2049	0.077.941e+04	1.750e+04		0.02	3.971e+06	30,30
2057	0.056.404e+04	1.750e+04		0.01	3.971e+06	30,30	2058	0.077.941e+04	1.750e+04		0.02	3.971e+06	30,30

Nodo Ver. V Ver. M
0.07 0.02

Fascia	Mat.	Spessore	Stato
		cm	
127	muratura E = 4.550e+04	20.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
1599	0.703.202e+04	8750.00		0.19	1.985e+06	32,32	1609	0.703.202e+04	8750.00		0.19	1.985e+06	32,32
1618	0.703.202e+04	8750.00		0.19	1.985e+06	32,32	2086	0.683.202e+04	8750.00		0.19	1.985e+06	32,32
2087	0.403.202e+04	8750.00		0.11	1.985e+06	32,32	2095	0.683.202e+04	8750.00		0.19	1.985e+06	32,32

2096	0.403.202e+04	8750.00	0.11	1.985e+06	32,32	2104	0.683.202e+04	8750.00	0.19	1.985e+06	32,32
2105	0.403.202e+04	8750.00	0.11	1.985e+06	32,32						

Nodo	Ver. V	Ver. M
	0.70	0.19

Fascia	Mat.	Spessore	Stato
		cm	
130	mattoni pieni e malta di calce	25.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb				
		daN	daN		daN cm				daN	daN		daN cm					
2153	0.185.255e+04	6937.50	0.02	2.233e+06	27,27	2154	0.185.255e+04	6937.50	0.02	2.233e+06	27,27	2154	0.185.255e+04	6937.50	0.02	2.233e+06	27,27
2175	0.235.255e+04	6937.50	0.03	2.233e+06	27,27	2176	0.225.255e+04	6937.50	0.03	2.233e+06	31,31	2176	0.225.255e+04	6937.50	0.03	2.233e+06	31,31
2184	0.235.255e+04	6937.50	0.03	2.233e+06	27,27	2185	0.185.255e+04	6937.50	0.02	2.233e+06	27,27	2185	0.185.255e+04	6937.50	0.02	2.233e+06	27,27
2186	0.225.255e+04	6937.50	0.03	2.233e+06	31,31	2194	0.235.255e+04	6937.50	0.03	2.233e+06	27,27	2194	0.235.255e+04	6937.50	0.03	2.233e+06	27,27
2195	0.225.255e+04	6937.50	0.03	2.233e+06	31,31												

Nodo	Ver. V	Ver. M
	0.23	0.03

Fascia	Mat.	Spessore	Stato
		cm	
131	mattoni pieni e malta di calce	38.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb				
		daN	daN		daN cm				daN	daN		daN cm					
2190	0.181.598e+05	1.055e+04	0.01	3.395e+06	27,27	2191	0.161.598e+05	1.055e+04	0.01	3.395e+06	27,27	2191	0.161.598e+05	1.055e+04	0.01	3.395e+06	27,27
2199	0.181.598e+05	1.055e+04	0.01	3.395e+06	27,27	2200	0.161.598e+05	1.055e+04	0.01	3.395e+06	27,27	2200	0.161.598e+05	1.055e+04	0.01	3.395e+06	27,27

Nodo	Ver. V	Ver. M
	0.18	0.01

Fascia	Mat.	Spessore	Stato
		cm	
135	mattoni pieni e malta di calce	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb				
		daN	daN		daN cm				daN	daN		daN cm					
935	0.475.956e+04	1.110e+04	0.09	3.573e+06	24,24	1039	0.475.956e+04	1.110e+04	0.09	3.573e+06	24,24	1039	0.475.956e+04	1.110e+04	0.09	3.573e+06	24,24
1041	0.475.956e+04	1.110e+04	0.09	3.573e+06	24,24	2287	0.505.956e+04	1.110e+04	0.09	3.573e+06	24,24	2287	0.505.956e+04	1.110e+04	0.09	3.573e+06	24,24
2288	0.515.956e+04	1.110e+04	0.10	3.573e+06	20,20	2289	0.495.956e+04	1.110e+04	0.09	3.573e+06	20,20	2289	0.495.956e+04	1.110e+04	0.09	3.573e+06	20,20
2290	0.475.956e+04	1.110e+04	0.09	3.573e+06	20,20	2291	0.425.956e+04	1.110e+04	0.08	3.573e+06	20,20	2291	0.425.956e+04	1.110e+04	0.08	3.573e+06	20,20
2292	0.395.956e+04	1.110e+04	0.07	3.573e+06	20,20	2293	0.375.956e+04	1.110e+04	0.07	3.573e+06	20,20	2293	0.375.956e+04	1.110e+04	0.07	3.573e+06	20,20
2294	0.355.956e+04	1.110e+04	0.06	3.573e+06	12,12	2295	0.305.810e+04	1.110e+04	0.06	3.573e+06	15,15	2295	0.305.810e+04	1.110e+04	0.06	3.573e+06	15,15
2296	0.505.956e+04	1.110e+04	0.09	3.573e+06	24,24	2297	0.515.956e+04	1.110e+04	0.10	3.573e+06	20,20	2297	0.515.956e+04	1.110e+04	0.10	3.573e+06	20,20
2298	0.495.956e+04	1.110e+04	0.09	3.573e+06	20,20	2299	0.475.956e+04	1.110e+04	0.09	3.573e+06	20,20	2299	0.475.956e+04	1.110e+04	0.09	3.573e+06	20,20
2300	0.425.956e+04	1.110e+04	0.08	3.573e+06	20,20	2301	0.395.956e+04	1.110e+04	0.07	3.573e+06	20,20	2301	0.395.956e+04	1.110e+04	0.07	3.573e+06	20,20
2302	0.375.956e+04	1.110e+04	0.07	3.573e+06	20,20	2303	0.355.956e+04	1.110e+04	0.06	3.573e+06	12,12	2303	0.355.956e+04	1.110e+04	0.06	3.573e+06	12,12
2304	0.305.810e+04	1.110e+04	0.06	3.573e+06	15,15	2305	0.505.956e+04	1.110e+04	0.09	3.573e+06	24,24	2305	0.505.956e+04	1.110e+04	0.09	3.573e+06	24,24
2306	0.515.956e+04	1.110e+04	0.10	3.573e+06	20,20	2307	0.495.956e+04	1.110e+04	0.09	3.573e+06	20,20	2307	0.495.956e+04	1.110e+04	0.09	3.573e+06	20,20
2308	0.475.956e+04	1.110e+04	0.09	3.573e+06	20,20	2309	0.425.956e+04	1.110e+04	0.08	3.573e+06	20,20	2309	0.425.956e+04	1.110e+04	0.08	3.573e+06	20,20
2310	0.395.956e+04	1.110e+04	0.07	3.573e+06	20,20	2311	0.375.956e+04	1.110e+04	0.07	3.573e+06	20,20	2311	0.375.956e+04	1.110e+04	0.07	3.573e+06	20,20
2312	0.355.956e+04	1.110e+04	0.06	3.573e+06	12,12	2313	0.305.810e+04	1.110e+04	0.06	3.573e+06	15,15	2313	0.305.810e+04	1.110e+04	0.06	3.573e+06	15,15

Nodo	Ver. V	Ver. M
	0.51	0.10

Fascia	Mat.	Spessore	Stato
		cm	
138	mattoni pieni e malta di calce	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2327	0.167.147e+041.110e+04			0.02	3.573e+06	20,20	2328	0.257.147e+041.110e+04			0.04	3.573e+06	20,20
2329	0.237.147e+041.110e+04			0.04	3.573e+06	20,20	2330	0.197.147e+041.110e+04			0.03	3.573e+06	20,20
2331	0.207.147e+041.110e+04			0.03	3.573e+06	23,23	2336	0.167.147e+041.110e+04			0.02	3.573e+06	20,20
2337	0.257.147e+041.110e+04			0.04	3.573e+06	20,20	2338	0.237.147e+041.110e+04			0.04	3.573e+06	20,20
2339	0.197.147e+041.110e+04			0.03	3.573e+06	20,20	2340	0.207.147e+041.110e+04			0.03	3.573e+06	23,23
2345	0.167.147e+041.110e+04			0.02	3.573e+06	20,20	2346	0.257.147e+041.110e+04			0.04	3.573e+06	20,20
2347	0.237.147e+041.110e+04			0.04	3.573e+06	20,20	2348	0.197.147e+041.110e+04			0.03	3.573e+06	20,20
2349	0.207.147e+041.110e+04			0.03	3.573e+06	23,23	2389	0.257.147e+041.110e+04			0.04	3.573e+06	20,20
2395	0.167.147e+041.110e+04			0.02	3.573e+06	20,20	2396	0.237.147e+041.110e+04			0.04	3.573e+06	20,20
2397	0.197.147e+041.110e+04			0.03	3.573e+06	20,20	2398	0.207.147e+041.110e+04			0.03	3.573e+06	23,23
Nodo	Ver. V 0.25			Ver. M 0.04									

Fascia	Mat.	Spessore	Stato
		cm	
141	mattoni pieni e malta di calce	25.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
761	0.193.746e+04	6937.50		0.04	2.233e+06	23,23	771	0.193.746e+04	6937.50		0.04	2.233e+06	23,23
839	0.193.746e+04	6937.50		0.04	2.233e+06	23,23	2445	0.133.746e+04	6937.50		0.02	2.233e+06	23,23
2454	0.133.746e+04	6937.50		0.02	2.233e+06	23,23	2459	0.133.746e+04	6937.50		0.02	2.233e+06	23,23
Nodo	Ver. V 0.19			Ver. M 0.04									

Fascia	Mat.	Spessore	Stato
		cm	
142	mattoni pieni e malta di calce	37.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2451	0.145.544e+041.027e+04			0.03	3.305e+06	23,23	2453	0.205.544e+041.027e+04			0.04	3.305e+06	23,23
2457	0.145.544e+041.027e+04			0.03	3.305e+06	23,23	2458	0.205.544e+041.027e+04			0.04	3.305e+06	23,23
2462	0.145.544e+041.027e+04			0.03	3.305e+06	23,23	2463	0.205.544e+041.027e+04			0.04	3.305e+06	23,23
Nodo	Ver. V 0.20			Ver. M 0.04									

Fascia	Mat.	Spessore	Stato
		cm	
143	mattoni pieni e malta di calce	25.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
810	0.203.179e+04	6937.50		0.04	2.233e+06	23,23	820	0.203.179e+04	6937.50		0.04	2.233e+06	23,23
829	0.203.179e+04	6937.50		0.04	2.233e+06	23,23	2504	0.193.179e+04	6937.50		0.04	2.233e+06	23,23
2505	0.103.179e+04	6937.50		0.02	2.233e+06	23,23	2513	0.193.179e+04	6937.50		0.04	2.233e+06	23,23
2514	0.103.179e+04	6937.50		0.02	2.233e+06	23,23	2522	0.193.179e+04	6937.50		0.04	2.233e+06	23,23
2523	0.103.179e+04	6937.50		0.02	2.233e+06	23,23							

Nodo **Ver. V** **Ver. M**
 0.20 0.04

Fascia	Mat.	Spessore	Stato
		cm	
145	mattoni pieni e malta di calce	37.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
2511	0.104.705e+041.027e+04			0.02	3.305e+06	21,21	2512	0.114.705e+041.027e+04			0.02	3.305e+06	21,21
2520	0.104.705e+041.027e+04			0.02	3.305e+06	21,21	2521	0.114.705e+041.027e+04			0.02	3.305e+06	21,21
2529	0.104.705e+041.027e+04			0.02	3.305e+06	21,21	2530	0.114.705e+041.027e+04			0.02	3.305e+06	21,21

Nodo **Ver. V** **Ver. M**
 0.11 0.02

Fascia	Mat.	Spessore	Stato
		cm	
148	mattoni pieni e malta di calce	25.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
1075	0.133.142e+04 6937.50			0.03	2.233e+06	21,21	1085	0.133.142e+04 6937.50			0.03	2.233e+06	21,21
1095	0.133.142e+04 6937.50			0.03	2.233e+06	21,21	2576	0.163.142e+04 6937.50			0.04	2.233e+06	21,21
2577	0.093.142e+04 6937.50			0.02	2.233e+06	21,21	2585	0.163.142e+04 6937.50			0.04	2.233e+06	21,21
2586	0.093.142e+04 6937.50			0.02	2.233e+06	21,21	2594	0.163.142e+04 6937.50			0.04	2.233e+06	21,21
2595	0.093.142e+04 6937.50			0.02	2.233e+06	21,21							

Nodo **Ver. V** **Ver. M**
 0.16 0.04

Fascia	Mat.	Spessore	Stato
		cm	
149	mattoni pieni e malta di calce	37.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
2583	0.054.650e+041.027e+04			0.01	3.305e+06	21,21	2584	0.084.650e+041.027e+04			0.02	3.305e+06	21,21
2592	0.054.650e+041.027e+04			0.01	3.305e+06	21,21	2593	0.084.650e+041.027e+04			0.02	3.305e+06	21,21
2601	0.054.650e+041.027e+04			0.01	3.305e+06	21,21	2602	0.084.650e+041.027e+04			0.02	3.305e+06	21,21

Nodo **Ver. V** **Ver. M**
 0.08 0.02

Fascia	Mat.	Spessore	Stato
		cm	
150	muratura E = 4.550e+04	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
2630	0.769.567e+041.750e+04			0.14	3.971e+06	42,42	2631	0.579.567e+041.750e+04			0.10	3.971e+06	42,42
2635	0.439.567e+041.750e+04			0.08	3.971e+06	42,42	2639	0.079.567e+041.750e+04			0.01	3.971e+06	42,42
2981	0.579.567e+041.750e+04			0.10	3.971e+06	42,42	2982	0.079.567e+041.750e+04			0.01	3.971e+06	42,42
2983	0.439.567e+041.750e+04			0.08	3.971e+06	42,42	2984	0.799.567e+041.750e+04			0.15	3.971e+06	42,42

2985	0.439.567e+041.750e+04	0.08	3.971e+06	42,42	2986	0.799.567e+041.750e+04	0.15	3.971e+06	42,42
2987	0.769.567e+041.750e+04	0.14	3.971e+06	42,42	2988	0.579.567e+041.750e+04	0.10	3.971e+06	42,42
2989	0.079.567e+041.750e+04	0.01	3.971e+06	42,42	2990	0.799.567e+041.750e+04	0.15	3.971e+06	42,42
2991	0.769.567e+041.750e+04	0.14	3.971e+06	42,42					

Nodo **Ver. V** **Ver. M**
 0.79 0.15

Fascia	Mat.	Spessore	Stato
		cm	
152	muratura E = 4.550e+04	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
2618	0.125.515e+041.750e+04			0.04	3.971e+06	17,17	2619	0.235.515e+041.750e+04			0.07	3.971e+06	17,17
2620	0.155.515e+041.750e+04			0.05	3.971e+06	17,17	2627	0.125.515e+041.750e+04			0.04	3.971e+06	17,17
2628	0.235.515e+041.750e+04			0.07	3.971e+06	17,17	2629	0.155.515e+041.750e+04			0.05	3.971e+06	17,17
2636	0.125.515e+041.750e+04			0.04	3.971e+06	17,17	2637	0.235.515e+041.750e+04			0.07	3.971e+06	17,17
2638	0.155.515e+041.750e+04			0.05	3.971e+06	17,17	2645	0.125.515e+041.750e+04			0.04	3.971e+06	17,17
2646	0.235.515e+041.750e+04			0.07	3.971e+06	17,17	2647	0.155.515e+041.750e+04			0.05	3.971e+06	17,17

Nodo **Ver. V** **Ver. M**
 0.23 0.07

Fascia	Mat.	Spessore	Stato
		cm	
153	muratura E = 4.550e+04	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
1142	0.171.073e+051.750e+04			0.03	3.971e+06	36,36	1294	0.171.073e+051.750e+04			0.03	3.971e+06	36,36
1303	0.171.073e+051.750e+04			0.03	3.971e+06	36,36	2841	0.221.073e+051.750e+04			0.04	3.971e+06	36,36
2842	0.271.073e+051.750e+04			0.04	3.971e+06	36,36	2843	0.331.073e+051.750e+04			0.05	3.971e+06	36,36
2844	0.281.073e+051.750e+04			0.05	3.971e+06	36,36	2850	0.051.073e+051.750e+047.35e-03			3.971e+06	36,36	
2851	0.061.073e+051.750e+04			0.01	3.971e+06	41,41	2852	0.171.073e+051.750e+04			0.03	3.971e+06	41,41
2853	0.291.073e+051.750e+04			0.05	3.971e+06	35,35	2886	0.211.073e+051.750e+04			0.03	3.971e+06	36,36
2963	0.211.073e+051.750e+04			0.03	3.971e+06	36,36	2964	0.221.073e+051.750e+04			0.04	3.971e+06	36,36
2965	0.271.073e+051.750e+04			0.04	3.971e+06	36,36	2966	0.331.073e+051.750e+04			0.05	3.971e+06	36,36
2967	0.281.073e+051.750e+04			0.05	3.971e+06	36,36	2968	0.051.073e+051.750e+047.35e-03			3.971e+06	36,36	
2969	0.061.073e+051.750e+04			0.01	3.971e+06	41,41	2970	0.171.073e+051.750e+04			0.03	3.971e+06	41,41
2971	0.291.073e+051.750e+04			0.05	3.971e+06	35,35	2972	0.211.073e+051.750e+04			0.03	3.971e+06	36,36
2973	0.221.073e+051.750e+04			0.04	3.971e+06	36,36	2974	0.271.073e+051.750e+04			0.04	3.971e+06	36,36
2975	0.331.073e+051.750e+04			0.05	3.971e+06	36,36	2976	0.281.073e+051.750e+04			0.05	3.971e+06	36,36
2977	0.051.073e+051.750e+047.35e-03			3.971e+06	36,36	2978	0.061.073e+051.750e+04			0.01	3.971e+06	41,41	
2979	0.171.073e+051.750e+04			0.03	3.971e+06	41,41	2980	0.291.073e+051.750e+04			0.05	3.971e+06	35,35

Nodo **Ver. V** **Ver. M**
 0.33 0.05

Fascia	Mat.	Spessore	Stato
		cm	
154	muratura E = 4.550e+04	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
2623	0.055.515e+041.750e+04			0.02	3.971e+06	17,17	2624	0.045.515e+041.750e+04			0.01	3.971e+06	17,17
2632	0.055.515e+041.750e+04			0.02	3.971e+06	17,17	2633	0.045.515e+041.750e+04			0.01	3.971e+06	17,17
2641	0.055.515e+041.750e+04			0.02	3.971e+06	17,17	2642	0.045.515e+041.750e+04			0.01	3.971e+06	17,17
2650	0.055.515e+041.750e+04			0.02	3.971e+06	17,17	2651	0.045.515e+041.750e+04			0.01	3.971e+06	17,17

Nodo **Ver. V** **Ver. M**

0.05

0.02

Fascia	Mat.	Spessore	Stato
		cm	
157	mattoni pieni e malta di calce	20.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2769	0.992.338e+04	5550.00		0.24	1.787e+06	36,36	2770	0.992.338e+04	5550.00		0.24	1.787e+06	36,36
2771	0.992.338e+04	5550.00		0.24	1.787e+06	36,36	2772	0.992.338e+04	5550.00		0.24	1.787e+06	36,36
2778	0.972.338e+04	5550.00		0.23	1.787e+06	36,36	2779	0.352.338e+04	5550.00		0.08	1.787e+06	36,36
2787	0.972.338e+04	5550.00		0.23	1.787e+06	36,36	2788	0.352.338e+04	5550.00		0.08	1.787e+06	36,36
2796	0.972.338e+04	5550.00		0.23	1.787e+06	36,36	2797	0.352.338e+04	5550.00		0.08	1.787e+06	36,36
2805	0.972.338e+04	5550.00		0.23	1.787e+06	36,36	2806	0.352.338e+04	5550.00		0.08	1.787e+06	36,36
Nodo	Ver. V 0.99			Ver. M 0.24									

Fascia	Mat.	Spessore	Stato
		cm	
158	mattoni pieni e malta di calce	20.0	NV L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2272	1.222.338e+04	5550.00		0.29	1.787e+06	37,37	2273	0.562.338e+04	5550.00		0.13	1.787e+06	37,37
2516	1.222.338e+04	5550.00		0.29	1.787e+06	37,37	2517	0.562.338e+04	5550.00		0.13	1.787e+06	37,37
2774	1.122.338e+04	5550.00		0.27	1.787e+06	37,37	2775	1.122.338e+04	5550.00		0.27	1.787e+06	37,37
2776	1.122.338e+04	5550.00		0.27	1.787e+06	37,37	2777	1.122.338e+04	5550.00		0.27	1.787e+06	37,37
2791	1.222.338e+04	5550.00		0.29	1.787e+06	37,37	2792	0.562.338e+04	5550.00		0.13	1.787e+06	37,37
2823	1.222.338e+04	5550.00		0.29	1.787e+06	37,37	2824	0.562.338e+04	5550.00		0.13	1.787e+06	37,37
Nodo	Ver. V 1.22			Ver. M 0.29									

Fascia	Mat.	Spessore	Stato
		cm	
160	mattoni pieni e malta di calce	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2785	0.194.676e+041.110e+04			0.05	3.573e+06	36,36	2786	0.464.676e+041.110e+04			0.11	3.573e+06	36,36
2794	0.194.676e+041.110e+04			0.05	3.573e+06	36,36	2795	0.464.676e+041.110e+04			0.11	3.573e+06	36,36
2803	0.194.676e+041.110e+04			0.05	3.573e+06	36,36	2804	0.464.676e+041.110e+04			0.11	3.573e+06	36,36
2812	0.194.676e+041.110e+04			0.05	3.573e+06	36,36	2813	0.464.676e+041.110e+04			0.11	3.573e+06	36,36
Nodo	Ver. V 0.46			Ver. M 0.11									

Fascia	Mat.	Spessore	Stato
		cm	
161	mattoni pieni e malta di calce	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2515	0.514.676e+041.110e+04			0.12	3.573e+06	37,37	2789	0.284.676e+041.110e+04			0.07	3.573e+06	37,37

2790	0.514.676e+041.110e+04	0.12	3.573e+06	37,37	2800	0.284.676e+041.110e+04	0.07	3.573e+06	37,37
2801	0.514.676e+041.110e+04	0.12	3.573e+06	37,37	2802	0.284.676e+041.110e+04	0.07	3.573e+06	37,37
2830	0.284.676e+041.110e+04	0.07	3.573e+06	37,37	2831	0.514.676e+041.110e+04	0.12	3.573e+06	37,37

Nodo **Ver. V** **Ver. M**
 0.51 0.12

Fascia	Mat.	Spessore	Stato
		cm	
164	muratura E = 4.550e+04	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2836	0.136.617e+041.750e+04			0.03	3.971e+06	23,23	2837	0.236.617e+041.750e+04			0.06	3.971e+06	23,23
2838	0.206.617e+041.750e+04			0.05	3.971e+06	23,23	2839	0.156.617e+041.750e+04			0.04	3.971e+06	23,23
2840	0.036.617e+041.750e+048.54e-03			0.03	3.971e+06	23,23	2845	0.136.617e+041.750e+04			0.03	3.971e+06	23,23
2846	0.236.617e+041.750e+04			0.06	3.971e+06	23,23	2847	0.206.617e+041.750e+04			0.05	3.971e+06	23,23
2848	0.156.617e+041.750e+04			0.04	3.971e+06	23,23	2849	0.036.617e+041.750e+048.54e-03			0.03	3.971e+06	23,23
2854	0.136.617e+041.750e+04			0.03	3.971e+06	23,23	2855	0.236.617e+041.750e+04			0.06	3.971e+06	23,23
2856	0.206.617e+041.750e+04			0.05	3.971e+06	23,23	2857	0.156.617e+041.750e+04			0.04	3.971e+06	23,23
2858	0.036.617e+041.750e+048.54e-03			0.03	3.971e+06	23,23	2863	0.136.617e+041.750e+04			0.03	3.971e+06	23,23
2864	0.236.617e+041.750e+04			0.06	3.971e+06	23,23	2865	0.206.617e+041.750e+04			0.05	3.971e+06	23,23
2866	0.156.617e+041.750e+04			0.04	3.971e+06	23,23	2867	0.036.617e+041.750e+048.54e-03			0.03	3.971e+06	23,23

Nodo **Ver. V** **Ver. M**
 0.23 0.06

Fascia	Mat.	Spessore	Stato
		cm	
169	mattoni pieni e malta di calce	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
1876	0.724.229e+041.110e+04			0.19	3.573e+06	15,15	1885	0.724.229e+041.110e+04			0.19	3.573e+06	15,15
1894	0.724.229e+041.110e+04			0.19	3.573e+06	15,15	1903	0.724.229e+041.110e+04			0.19	3.573e+06	15,15
1912	0.724.229e+041.110e+04			0.19	3.573e+06	15,15	1921	0.724.229e+041.110e+04			0.19	3.573e+06	15,15
3002	0.654.229e+041.110e+04			0.17	3.573e+06	15,15	3003	0.454.229e+041.110e+04			0.12	3.573e+06	15,15
3005	0.654.229e+041.110e+04			0.17	3.573e+06	15,15	3006	0.454.229e+041.110e+04			0.12	3.573e+06	15,15
3008	0.654.229e+041.110e+04			0.17	3.573e+06	15,15	3009	0.454.229e+041.110e+04			0.12	3.573e+06	15,15
3011	0.654.229e+041.110e+04			0.17	3.573e+06	15,15	3012	0.454.229e+041.110e+04			0.12	3.573e+06	15,15
3014	0.654.229e+041.110e+04			0.17	3.573e+06	15,15	3015	0.454.229e+041.110e+04			0.12	3.573e+06	15,15
3017	0.654.229e+041.110e+04			0.17	3.573e+06	15,15	3018	0.454.229e+041.110e+04			0.12	3.573e+06	15,15

Nodo **Ver. V** **Ver. M**
 0.72 0.19

Fascia	Mat.	Spessore	Stato
		cm	
170	mattoni pieni e malta di calce	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
3003	0.434.229e+041.110e+04			0.11	3.573e+06	15,15	3004	0.054.229e+041.110e+04			0.01	3.573e+06	15,15
3006	0.434.229e+041.110e+04			0.11	3.573e+06	15,15	3007	0.054.229e+041.110e+04			0.01	3.573e+06	15,15
3009	0.434.229e+041.110e+04			0.11	3.573e+06	15,15	3010	0.054.229e+041.110e+04			0.01	3.573e+06	15,15
3012	0.434.229e+041.110e+04			0.11	3.573e+06	15,15	3013	0.054.229e+041.110e+04			0.01	3.573e+06	15,15
3015	0.434.229e+041.110e+04			0.11	3.573e+06	15,15	3016	0.054.229e+041.110e+04			0.01	3.573e+06	15,15
3018	0.434.229e+041.110e+04			0.11	3.573e+06	15,15	3019	0.054.229e+041.110e+04			0.01	3.573e+06	15,15

Nodo **Ver. V** **Ver. M**
 0.43 0.11

Fascia	Mat.	Spessore	Stato
		cm	
173	mattoni pieni e malta di calce	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
1813	0.074.229e+041.110e+04			0.02	3.573e+06	11,11	1822	0.074.229e+041.110e+04			0.02	3.573e+06	11,11
1831	0.074.229e+041.110e+04			0.02	3.573e+06	11,11	1840	0.074.229e+041.110e+04			0.02	3.573e+06	11,11
1849	0.074.229e+041.110e+04			0.02	3.573e+06	11,11	1858	0.074.229e+041.110e+04			0.02	3.573e+06	11,11
3023	0.074.229e+041.110e+04			0.02	3.573e+06	11,11	3024	0.074.229e+041.110e+04			0.02	3.573e+06	11,11
3026	0.074.229e+041.110e+04			0.02	3.573e+06	11,11	3027	0.074.229e+041.110e+04			0.02	3.573e+06	11,11
3029	0.074.229e+041.110e+04			0.02	3.573e+06	11,11	3030	0.074.229e+041.110e+04			0.02	3.573e+06	11,11
3032	0.074.229e+041.110e+04			0.02	3.573e+06	11,11	3033	0.074.229e+041.110e+04			0.02	3.573e+06	11,11
3035	0.074.229e+041.110e+04			0.02	3.573e+06	11,11	3036	0.074.229e+041.110e+04			0.02	3.573e+06	11,11
3038	0.074.229e+041.110e+04			0.02	3.573e+06	11,11	3039	0.074.229e+041.110e+04			0.02	3.573e+06	11,11
Nodo	Ver. V 0.07			Ver. M 0.02									

Fascia	Mat.	Spessore	Stato
		cm	
174	mattoni pieni e malta di calce	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
3024	0.034.229e+041.110e+047.64e-03			3.573e+06		11,11	3025	0.024.229e+041.110e+046.26e-03			3.573e+06		11,11
3027	0.034.229e+041.110e+047.64e-03			3.573e+06		11,11	3028	0.024.229e+041.110e+046.26e-03			3.573e+06		11,11
3030	0.034.229e+041.110e+047.64e-03			3.573e+06		11,11	3031	0.024.229e+041.110e+046.26e-03			3.573e+06		11,11
3033	0.034.229e+041.110e+047.64e-03			3.573e+06		11,11	3034	0.024.229e+041.110e+046.26e-03			3.573e+06		11,11
3036	0.034.229e+041.110e+047.64e-03			3.573e+06		11,11	3037	0.024.229e+041.110e+046.26e-03			3.573e+06		11,11
3039	0.034.229e+041.110e+047.64e-03			3.573e+06		11,11	3040	0.024.229e+041.110e+046.26e-03			3.573e+06		11,11
Nodo	Ver. V 0.03			Ver. M 7.64e-03									

Fascia	Mat.	Spessore	Stato
		cm	
177	mattoni pieni e malta di calce	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
1750	0.934.229e+041.110e+04			0.24	3.573e+06	17,17	1759	0.934.229e+041.110e+04			0.24	3.573e+06	17,17
1768	0.934.229e+041.110e+04			0.24	3.573e+06	17,17	1777	0.934.229e+041.110e+04			0.24	3.573e+06	17,17
1786	0.934.229e+041.110e+04			0.24	3.573e+06	17,17	1795	0.934.229e+041.110e+04			0.24	3.573e+06	17,17
3044	0.854.229e+041.110e+04			0.22	3.573e+06	17,17	3045	0.604.229e+041.110e+04			0.16	3.573e+06	17,17
3047	0.854.229e+041.110e+04			0.22	3.573e+06	17,17	3048	0.604.229e+041.110e+04			0.16	3.573e+06	17,17
3050	0.854.229e+041.110e+04			0.22	3.573e+06	17,17	3051	0.604.229e+041.110e+04			0.16	3.573e+06	17,17
3053	0.854.229e+041.110e+04			0.22	3.573e+06	17,17	3054	0.604.229e+041.110e+04			0.16	3.573e+06	17,17
3056	0.854.229e+041.110e+04			0.22	3.573e+06	17,17	3057	0.604.229e+041.110e+04			0.16	3.573e+06	17,17
3059	0.854.229e+041.110e+04			0.22	3.573e+06	17,17	3060	0.604.229e+041.110e+04			0.16	3.573e+06	17,17
Nodo	Ver. V 0.93			Ver. M 0.24									

Fascia	Mat.	Spessore	Stato
		cm	
178	mattoni pieni e malta di calce	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2786	0.604.676e+041.110e+04			0.14	3.573e+06	36,36
2804	0.604.676e+041.110e+04			0.14	3.573e+06	36,36
3122	0.594.676e+041.110e+04			0.14	3.573e+06	36,36
3125	0.594.676e+041.110e+04			0.14	3.573e+06	36,36
3128	0.594.676e+041.110e+04			0.14	3.573e+06	36,36
3131	0.594.676e+041.110e+04			0.14	3.573e+06	36,36

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2795	0.604.676e+041.110e+04			0.14	3.573e+06	36,36
2813	0.604.676e+041.110e+04			0.14	3.573e+06	36,36
3123	0.434.676e+041.110e+04			0.10	3.573e+06	36,36
3126	0.434.676e+041.110e+04			0.10	3.573e+06	36,36
3129	0.434.676e+041.110e+04			0.10	3.573e+06	36,36
3132	0.434.676e+041.110e+04			0.10	3.573e+06	36,36

Nodo	Ver. V	Ver. M
	0.60	0.14

Fascia	Mat.	Spessore	Stato
		cm	
189	mattoni pieni e malta di calce	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
3123	0.414.676e+041.110e+04			0.10	3.573e+06	36,36	3124	0.044.676e+041.110e+04			0.01	3.573e+06	36,36
3126	0.414.676e+041.110e+04			0.10	3.573e+06	36,36	3127	0.044.676e+041.110e+04			0.01	3.573e+06	36,36
3129	0.414.676e+041.110e+04			0.10	3.573e+06	36,36	3130	0.044.676e+041.110e+04			0.01	3.573e+06	36,36
3132	0.414.676e+041.110e+04			0.10	3.573e+06	36,36	3133	0.044.676e+041.110e+04			0.01	3.573e+06	36,36

Nodo	Ver. V	Ver. M
	0.41	0.10

Fascia	Mat.	Spessore	Stato
		cm	
192	mattoni pieni e malta di calce	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2515	0.604.676e+041.110e+04			0.14	3.573e+06	37,37	2790	0.604.676e+041.110e+04			0.14	3.573e+06	37,37
2801	0.604.676e+041.110e+04			0.14	3.573e+06	37,37	2831	0.604.676e+041.110e+04			0.14	3.573e+06	37,37
3137	0.564.676e+041.110e+04			0.13	3.573e+06	37,37	3138	0.414.676e+041.110e+04			0.10	3.573e+06	37,37
3140	0.564.676e+041.110e+04			0.13	3.573e+06	37,37	3141	0.414.676e+041.110e+04			0.10	3.573e+06	37,37
3143	0.564.676e+041.110e+04			0.13	3.573e+06	37,37	3144	0.414.676e+041.110e+04			0.10	3.573e+06	37,37
3146	0.564.676e+041.110e+04			0.13	3.573e+06	37,37	3147	0.414.676e+041.110e+04			0.10	3.573e+06	37,37

Nodo	Ver. V	Ver. M
	0.60	0.14

Fascia	Mat.	Spessore	Stato
		cm	
193	mattoni pieni e malta di calce	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
3138	0.424.676e+041.110e+04			0.10	3.573e+06	37,37	3139	0.054.676e+041.110e+04			0.01	3.573e+06	37,37
3141	0.424.676e+041.110e+04			0.10	3.573e+06	37,37	3142	0.054.676e+041.110e+04			0.01	3.573e+06	37,37
3144	0.424.676e+041.110e+04			0.10	3.573e+06	37,37	3145	0.054.676e+041.110e+04			0.01	3.573e+06	37,37
3147	0.424.676e+041.110e+04			0.10	3.573e+06	37,37	3148	0.054.676e+041.110e+04			0.01	3.573e+06	37,37

Nodo	Ver. V	Ver. M
	0.42	0.10

Fascia	Mat.	Spessore	Stato
		cm	
198	mattoni pieni e malta di calce	37.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2584	0.124.650e+041.027e+04			0.03	3.305e+06	21,21	2593	0.124.650e+041.027e+04			0.03	3.305e+06	21,21
2602	0.124.650e+041.027e+04			0.03	3.305e+06	21,21	3155	0.144.650e+041.027e+04			0.03	3.305e+06	21,21
3156	0.124.650e+041.027e+04			0.03	3.305e+06	21,21	3158	0.144.650e+041.027e+04			0.03	3.305e+06	21,21
3160	0.124.650e+041.027e+04			0.03	3.305e+06	21,21	3162	0.144.650e+041.027e+04			0.03	3.305e+06	21,21
3163	0.124.650e+041.027e+04			0.03	3.305e+06	21,21							

Nodo	Ver. V	Ver. M
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0.14

0.03

Fascia	Mat.	Spessore	Stato
		cm	
199	mattoni pieni e malta di calce	37.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
3156	0.114.650e+041.027e+04			0.02	3.305e+06	21,21	3157	0.034.650e+041.027e+046.71e-03			3.305e+06	21,21	
3160	0.114.650e+041.027e+04			0.02	3.305e+06	21,21	3161	0.034.650e+041.027e+046.71e-03			3.305e+06	21,21	
3163	0.114.650e+041.027e+04			0.02	3.305e+06	21,21	3164	0.034.650e+041.027e+046.71e-03			3.305e+06	21,21	

Nodo	Ver. V	Ver. M
	0.11	0.02

Fascia	Mat.	Spessore	Stato
		cm	
202	mattoni pieni e malta di calce	37.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2512	0.064.705e+041.027e+04			0.01	3.305e+06	20,20	2521	0.064.705e+041.027e+04			0.01	3.305e+06	20,20
2530	0.064.705e+041.027e+04			0.01	3.305e+06	20,20	3177	0.074.705e+041.027e+04			0.01	3.305e+06	20,20
3178	0.064.705e+041.027e+04			0.01	3.305e+06	20,20	3180	0.074.705e+041.027e+04			0.01	3.305e+06	20,20
3181	0.064.705e+041.027e+04			0.01	3.305e+06	20,20	3183	0.074.705e+041.027e+04			0.01	3.305e+06	20,20
3184	0.064.705e+041.027e+04			0.01	3.305e+06	20,20							

Nodo	Ver. V	Ver. M
	0.07	0.01

Fascia	Mat.	Spessore	Stato
		cm	
203	mattoni pieni e malta di calce	37.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
3178	0.034.705e+041.027e+047.20e-03			3.305e+06	20,20		3179	0.024.705e+041.027e+044.53e-03			3.305e+06	20,20	
3181	0.034.705e+041.027e+047.20e-03			3.305e+06	20,20		3182	0.024.705e+041.027e+044.53e-03			3.305e+06	20,20	
3184	0.034.705e+041.027e+047.20e-03			3.305e+06	20,20		3185	0.024.705e+041.027e+044.53e-03			3.305e+06	20,20	

Nodo	Ver. V	Ver. M
	0.03	7.20e-03

Fascia	Mat.	Spessore	Stato
		cm	
208	muratura E = 4.550e+04	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2094	0.427.941e+041.750e+04			0.09	3.971e+06	32,32	2103	0.427.941e+041.750e+04			0.09	3.971e+06	32,32
2112	0.427.941e+041.750e+04			0.09	3.971e+06	32,32	3196	0.447.941e+041.750e+04			0.10	3.971e+06	32,32
3198	0.367.941e+041.750e+04			0.08	3.971e+06	32,32	3201	0.447.941e+041.750e+04			0.10	3.971e+06	32,32
3202	0.367.941e+041.750e+04			0.08	3.971e+06	32,32	3204	0.447.941e+041.750e+04			0.10	3.971e+06	32,32
3205	0.367.941e+041.750e+04			0.08	3.971e+06	32,32							

Nodo **Ver. V** **Ver. M**
 0.44 0.10

Fascia	Mat.	Spessore	Stato
		cm	
209	muratura E = 1.024e+05	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
3198	0.211.787e+053.150e+04			0.04	8.934e+06	32,32	3200	0.031.787e+053.150e+045.37e-03			8.934e+06	32,32	
3202	0.211.787e+053.150e+04			0.04	8.934e+06	32,32	3203	0.031.787e+053.150e+045.37e-03			8.934e+06	32,32	
3205	0.211.787e+053.150e+04			0.04	8.934e+06	32,32	3206	0.031.787e+053.150e+045.37e-03			8.934e+06	32,32	

Nodo **Ver. V** **Ver. M**
 0.21 0.04

Fascia	Mat.	Spessore	Stato
		cm	
212	muratura E = 4.550e+04	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2040	0.077.941e+041.750e+04			0.02	3.971e+06	30,30	2049	0.077.941e+041.750e+04			0.02	3.971e+06	30,30
2058	0.077.941e+041.750e+04			0.02	3.971e+06	30,30	3216	0.067.941e+041.750e+04			0.01	3.971e+06	30,30
3217	0.057.941e+041.750e+04			0.01	3.971e+06	30,30	3219	0.067.941e+041.750e+04			0.01	3.971e+06	30,30
3220	0.057.941e+041.750e+04			0.01	3.971e+06	30,30	3222	0.067.941e+041.750e+04			0.01	3.971e+06	30,30
3223	0.057.941e+041.750e+04			0.01	3.971e+06	30,30							

Nodo **Ver. V** **Ver. M**
 0.07 0.02

Fascia	Mat.	Spessore	Stato
		cm	
213	muratura E = 1.024e+05	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
3217	0.031.787e+053.150e+044.83e-03			8.934e+06	30,30		3218	0.011.787e+053.150e+042.34e-03			8.934e+06	30,30	
3220	0.031.787e+053.150e+044.83e-03			8.934e+06	30,30		3221	0.011.787e+053.150e+042.34e-03			8.934e+06	30,30	
3223	0.031.787e+053.150e+044.83e-03			8.934e+06	30,30		3224	0.011.787e+053.150e+042.34e-03			8.934e+06	30,30	

Nodo **Ver. V** **Ver. M**
 0.03 4.83e-03

Fascia	Mat.	Spessore	Stato
		cm	
216	muratura E = 4.550e+04	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
1986	0.427.941e+041.750e+04			0.09	3.971e+06	11,11	1995	0.427.941e+041.750e+04			0.09	3.971e+06	11,11
2004	0.427.941e+041.750e+04			0.09	3.971e+06	11,11	3234	0.427.941e+041.750e+04			0.09	3.971e+06	11,11
3235	0.337.941e+041.750e+04			0.07	3.971e+06	11,11	3237	0.427.941e+041.750e+04			0.09	3.971e+06	11,11
3238	0.337.941e+041.750e+04			0.07	3.971e+06	11,11	3240	0.427.941e+041.750e+04			0.09	3.971e+06	11,11
3241	0.337.941e+041.750e+04			0.07	3.971e+06	11,11							

Nodo **Ver. V** **Ver. M**
 0.42 0.09

Fascia	Mat.	Spessore	Stato
		cm	
217	muratura E = 1.024e+05	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
3235	0.191.787e+053.150e+04			0.03	8.934e+06	27,27	3236	0.011.787e+053.150e+042.50e-03			8.934e+06	27,27	
3238	0.191.787e+053.150e+04			0.03	8.934e+06	27,27	3239	0.011.787e+053.150e+042.50e-03			8.934e+06	27,27	
3241	0.191.787e+053.150e+04			0.03	8.934e+06	27,27	3242	0.011.787e+053.150e+042.50e-03			8.934e+06	27,27	

Nodo **Ver. V** **Ver. M**
 0.19 0.03

Fascia	Mat.	Spessore	Stato
		cm	
221	mattoni pieni e malta di calce	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
3275	0.197.147e+041.110e+04			0.03	3.573e+06	18,18	3322	0.147.147e+041.110e+04			0.02	3.573e+06	26,26
3340	0.147.147e+041.110e+04			0.02	3.573e+06	26,26	3341	0.197.147e+041.110e+04			0.03	3.573e+06	18,18
3343	0.147.147e+041.110e+04			0.02	3.573e+06	26,26	3344	0.197.147e+041.110e+04			0.03	3.573e+06	18,18
3346	0.147.147e+041.110e+04			0.02	3.573e+06	26,26	3347	0.197.147e+041.110e+04			0.03	3.573e+06	18,18

Nodo **Ver. V** **Ver. M**
 0.19 0.03

Fascia	Mat.	Spessore	Stato
		cm	
225	mattoni pieni e malta di calce	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
2295	0.085.810e+041.110e+04			0.02	3.573e+06	31,31	2304	0.085.810e+041.110e+04			0.02	3.573e+06	31,31
2313	0.085.810e+041.110e+04			0.02	3.573e+06	31,31	3323	0.045.810e+041.110e+048.59e-03			3.573e+06	31,31	
3325	0.045.810e+041.110e+047.06e-03			3.573e+06	31,31		3327	0.045.810e+041.110e+048.59e-03			3.573e+06	31,31	
3328	0.045.810e+041.110e+047.06e-03			3.573e+06	31,31		3330	0.045.810e+041.110e+048.59e-03			3.573e+06	31,31	
3331	0.045.810e+041.110e+047.06e-03			3.573e+06	31,31								

Nodo **Ver. V** **Ver. M**
 0.08 0.02

Fascia	Mat.	Spessore	Stato
		cm	
226	mattoni pieni e malta di calce	40.0	ok L

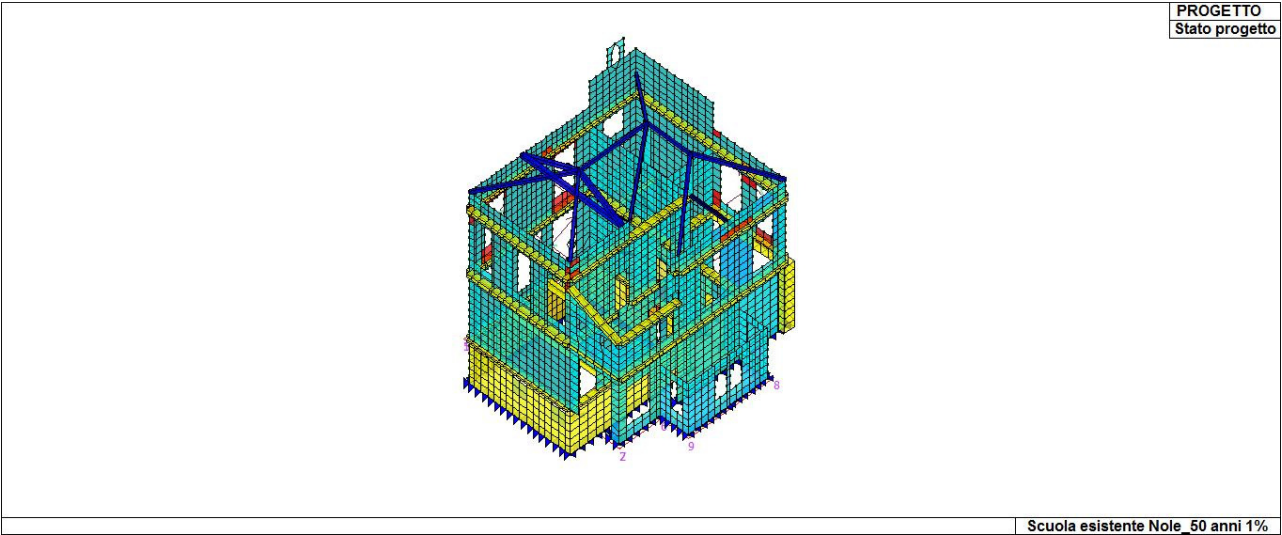
Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
3325	0.035.810e+041.110e+045.35e-03			3.573e+06	27,27		3326	0.025.810e+041.110e+044.51e-03			3.573e+06	27,27	
3328	0.035.810e+041.110e+045.35e-03			3.573e+06	27,27		3329	0.025.810e+041.110e+044.51e-03			3.573e+06	27,27	
3331	0.035.810e+041.110e+045.35e-03			3.573e+06	27,27		3332	0.025.810e+041.110e+044.51e-03			3.573e+06	27,27	

Nodo Ver. V Ver. M
 0.03 5.35e-03

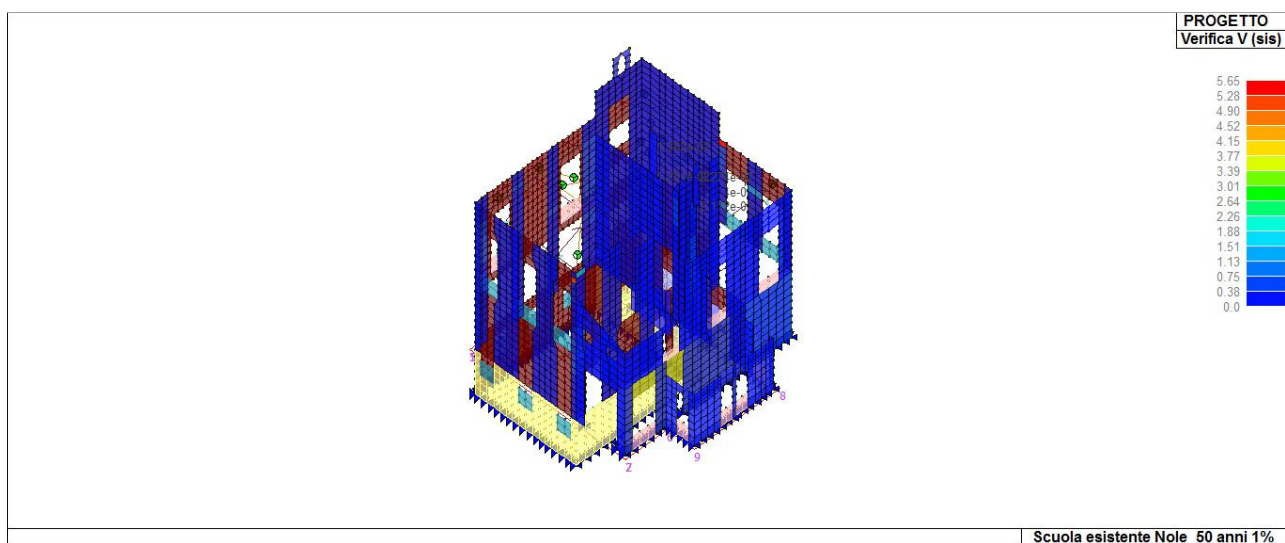
Fascia	Mat.	Spessore	Stato
		cm	
229	mattoni pieni e malta di calce	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
2331	0.217.147e+041.110e+04			0.03	3.573e+06	26,26	2340	0.217.147e+041.110e+04			0.03	3.573e+06	26,26
2349	0.217.147e+041.110e+04			0.03	3.573e+06	26,26	2398	0.217.147e+041.110e+04			0.03	3.573e+06	26,26
3322	0.077.147e+041.110e+04			0.01	3.573e+06	26,26	3339	0.117.147e+041.110e+04			0.02	3.573e+06	26,26
3340	0.077.147e+041.110e+04			0.01	3.573e+06	26,26	3342	0.117.147e+041.110e+04			0.02	3.573e+06	26,26
3343	0.077.147e+041.110e+04			0.01	3.573e+06	26,26	3345	0.117.147e+041.110e+04			0.02	3.573e+06	26,26
3346	0.077.147e+041.110e+04			0.01	3.573e+06	26,26	3348	0.117.147e+041.110e+04			0.02	3.573e+06	26,26

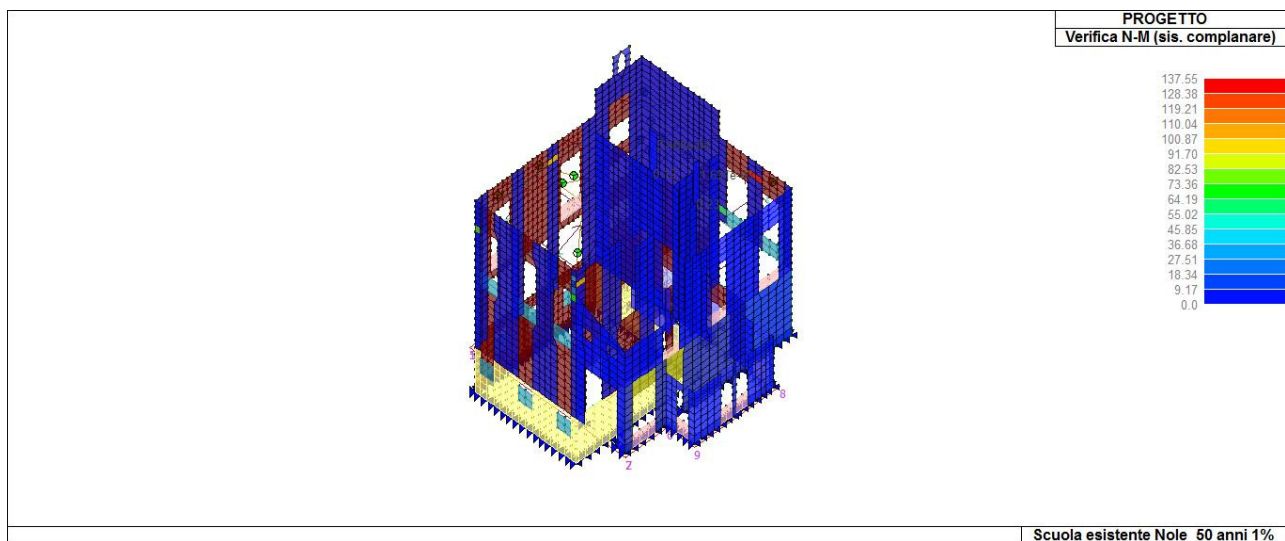
Nodo Ver. V Ver. M
 0.21 0.03



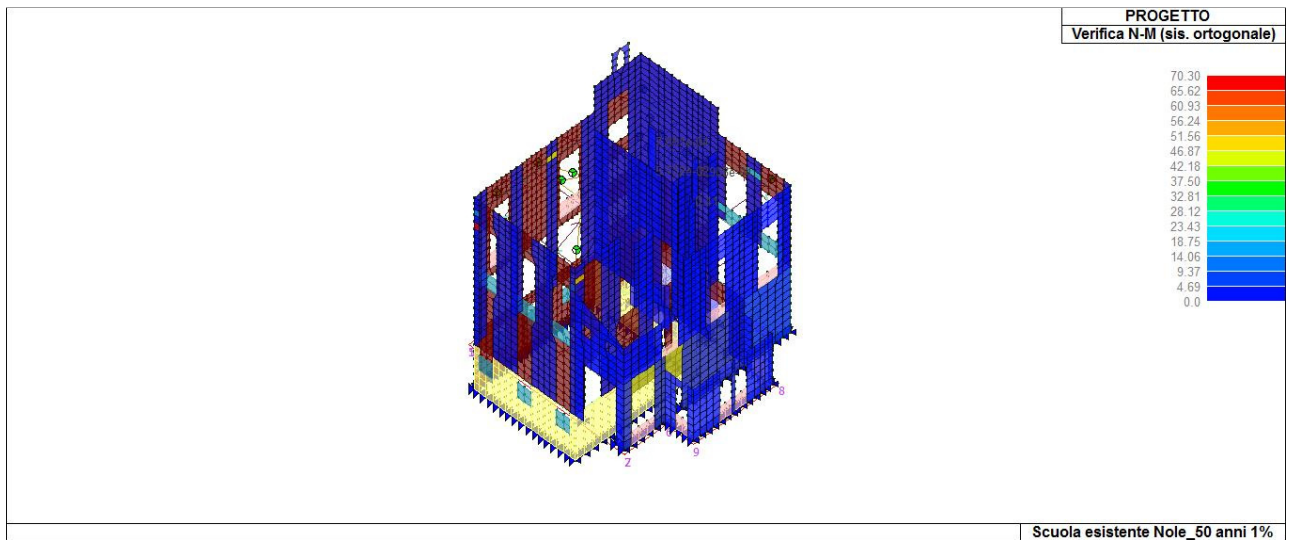
Verifiche sismiche murature (negative quelle in rosso) per un'accelerazione attesa al suolo pari a 1%



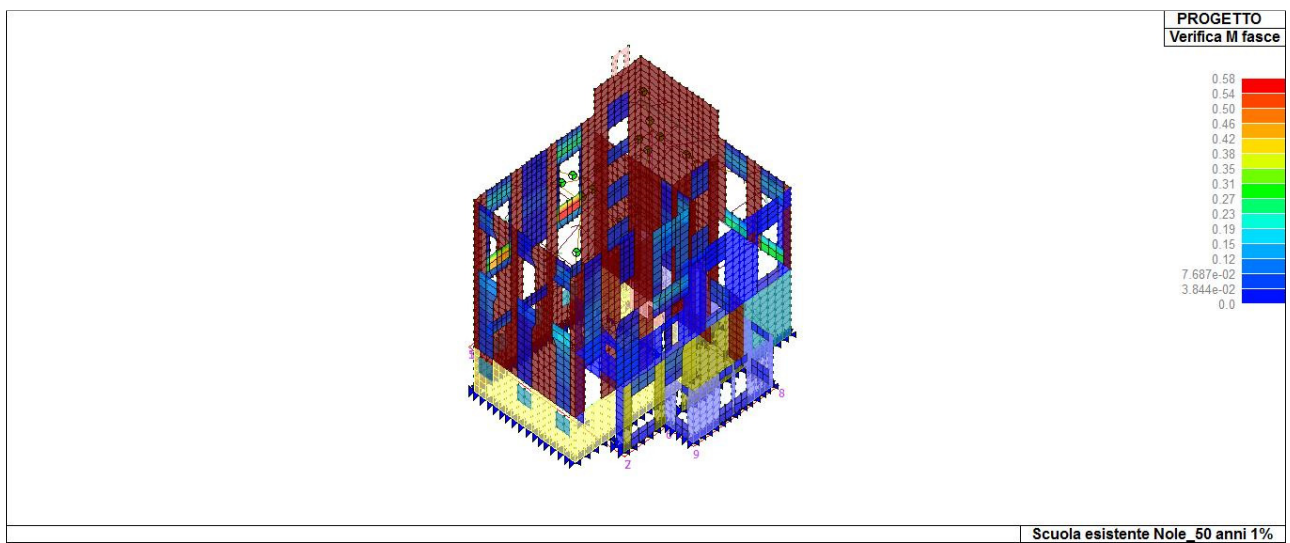
Verifica a taglio per un'accelerazione attesa al suolo pari a 1% (la verifica risulta negativa poiché > 1).



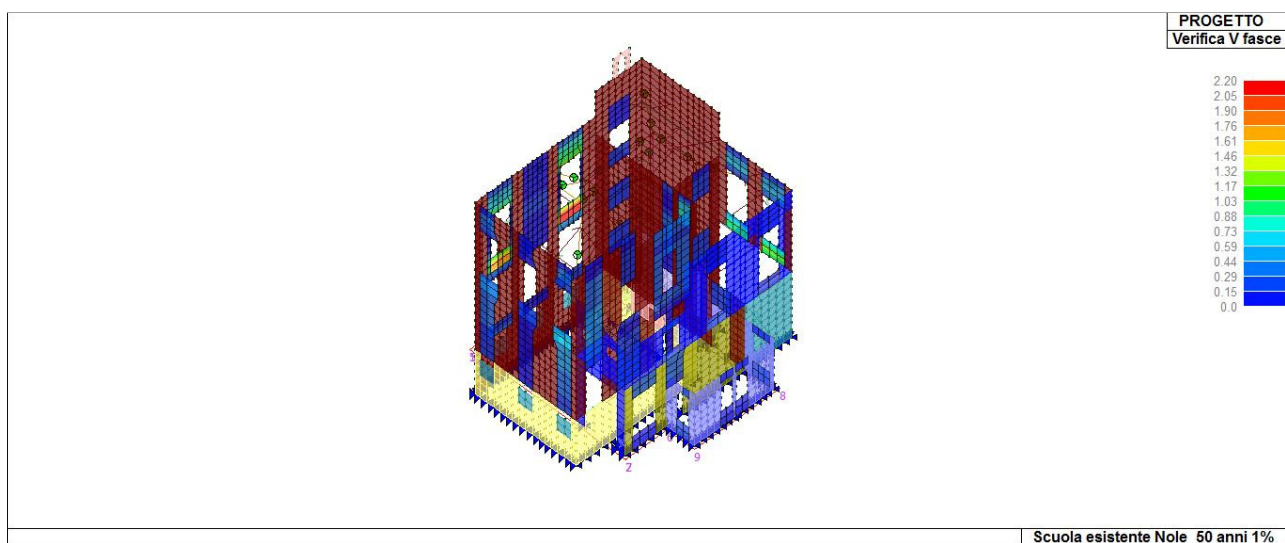
Verifica a pressoflessione nel piano per un'accelerazione attesa al suolo pari a 1% (la verifica risulta negativa poiché > 1).



Verifica a pressoflessione fuori dal piano per un'accelerazione attesa al suolo pari a 1% (la verifica risulta negativa poiché > 1).



Verifica a momentio flettente delle travi di muratura sottostanti e sopstanti le aperture (per un'accelerazione attesa al suolo pari a 1%). La verifica risulta positiva poiché < 1 .



Verifica a taglio delle travi di muratura sottostanti e soprastanti le aperture (per un'accelerazione attesa al suolo pari a 1%). La verifica risulta negativa poiché > 1 .



**VERIFICA STATICA E SISMICA DELL'EDIFICIO COMUNALE EX SCUOLE DI
VAUDA – VIA PONTE MASINO 1 - COMUNE DI NOLE (TO)**

MIGLIORAMENTO SISMICO 60%

**Relazione di calcolo strutturale impostata e redatta secondo le modalità
previste nel D.M. 17 Gennaio 2018 cap. 10 “Redazione dei progetti
strutturali esecutivi e delle relazioni di calcolo”.**

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D.M. 17/01/18 cap. 10.2 Affidabilità dei codici utilizzati

<https://www.2si.it/it/prodotti/affidabilita/>

INTESTAZIONE E CONTENUTI DELLA RELAZIONE

Progetto

La seguente relazione sintetizza i risultati della verifica statica e sismica dell'edificio in oggetto, attualmente non in uso ma nel passato sede di una scuola comunale. Nell'ottica di una futura riutilizzazione con la medesima destinazione di uso scolastico, è stata eseguita una analisi dinamica lineare ai sensi delle Norme Tecniche per le Costruzioni (NTC 2018) di cui al D.M. 17/01/2018 per valutare la sicurezza sismica della struttura quale edificio ad uso scolastico nella situazione di progetto di riuso. Pertanto è stata data all'edificio una destinazione d'uso a classe III ai sensi del par. 2.4.2 e vita nominale 50 anni ai sensi del 2.4.1 delle NTC 2018. L'edificio è sotto vincolo della Soprintendenza ai Beni Architettonici del Piemonte.

La verifica oggetto di questa relazione riguarda solamente la parte di edificio originario in muratura portante, poiché l'ampliamento con telaio in c.a. e tamponamenti sarà oggetto di demolizione e ricostruzione con nuova struttura in c.a., sismicamente indipendente. La parte originaria ha struttura portante in muratura con due diverse tessiture: in mattoni e malta cementizia di buona qualità per quanto riguarda l'ossatura portante, e con mattoni forati per le restanti parti (prevalentemente vano scale e parete di confine con ampliamento). I solai sono in laterocemento e la copertura con struttura lignea. In minima parte sono presenti anche travi a telaio in c.a.

Le strutture sono state oggetto di una campagna di prove su tutti i materiali, i cui risultati convergono con i valori medi delle tipologie murarie presenti nella tabella C8A.2.1. della Circolare di applicazione alle NTC 2008. L'estensione delle prove permette di quantificare il livello di conoscenza pari a LC2 (con fattore di confidenza = 1,2).

Per rendere nuovamente l'edificio utilizzabile per uso scolastico occorre che, ai sensi del par. 8.4.2 delle NTC 2018, esso abbia un miglioramento della sicurezza sismica pari almeno al 60%. Partendo da una verifica dello stato di fatto pari a 0% dell'accelerazione attesa al suolo, sono stati progettati interventi di rinforzo delle pareti murarie più carenti strutturalmente mediante utilizzo di intonaco armato (sistema "reticulatus" per zone con paramano a vista) e irrigidimento dei solai esistenti con soletta collaborante ancorata con i pioli al preesistente solaio in laterocemento. I risultati della verifica mediante analisi dinamica lineare sono stati positivi per un'accelerazione attesa al suolo pari al 60%.

Contenuti della relazione:

RELAZIONE DI CALCOLO STRUTTURALE

- Origine e Caratteristiche dei Codici di Calcolo
- Affidabilità dei codici utilizzati
- Validazione dei codici
- Tipo di analisi svolta
- Modalità di presentazione dei risultati
- Informazioni generali sull'elaborazione
- Giudizio motivato di accettabilità dei risultati

STAMPA DEI DATI DI INGRESSO

- Normative prese a riferimento
- Criteri adottati per le misure di sicurezza
- Criteri seguiti nella schematizzazione della struttura, dei vincoli e delle sconnessioni
- Interazione tra terreno e struttura
- Legami costitutivi adottati per la modellazione dei materiali e dei terreni
- Schematizzazione delle azioni, condizioni e combinazioni di carico
- Metodologie numeriche utilizzate per l'analisi strutturale
- Metodologie numeriche utilizzate per la progettazione e la verifica degli elementi strutturali

STAMPA DEI RISULTATI

Il Progettista:

Ing. Giovanni Data



17 December 2018

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RELAZIONE DI CALCOLO STRUTTURALE

Premessa

La presente relazione di calcolo strutturale, in conformità al §10.1 del DM 17/01/18, è comprensiva di una descrizione generale dell'opera e dei criteri generali di analisi e verifica. Segue inoltre le indicazioni fornite al §10.2 del DM stesso per quanto concerne analisi e verifiche svolte con l'ausilio di codici di calcolo.

Nella presente parte sono riportati i principali elementi di inquadramento del progetto esecutivo riguardante le strutture, in relazione agli strumenti urbanistici, al progetto architettonico, al progetto delle componenti tecnologiche in generale ed alle prestazioni attese dalla struttura.

Analisi storico-critica ed esito del rilievo geometrico-strutturale

Per edifici esistenti, in coerenza con il paragrafo 8.2 delle NTC-18, l'analisi storico-critica ed il rilievo geometrico-strutturale devono evidenziare i seguenti aspetti: (a) la costruzione riflette lo stato delle conoscenze al tempo della sua realizzazione; (b) possono essere insiti e non palesi difetti di impostazione e di realizzazione; (c) la costruzione può essere stata soggetta ad azioni, anche eccezionali, i cui effetti non siano completamente manifesti; (d) le strutture possono presentare degrado e/o modificazioni significative rispetto alla situazione originaria.

Analisi storico-critica

Per edifici esistenti, viene indicata la documentazione reperita e vengono esplicitate le informazioni desunte da ciascuno dei documenti esaminati per le finalità indicate al paragrafo 8.5.1 delle NTC-18.

Esito del rilievo geometrico-strutturale

Per edifici esistenti, vengono descritte le modalità con cui è stato effettuato il rilievo geometrico strutturale e gli esiti di quest'ultimo, anche con riferimenti espliciti e puntuali agli elaborati grafici che saranno riportati nella parte "4.1. Rilievo geometrico-strutturale". Il rilievo delle strutture deve essere eseguito e restituito secondo le modalità e con le finalità riportate nei paragrafi 8.5.2 e 8.7 delle NTC-18.

Descrizione generale dell'opera

La seguente relazione sintetizza i risultati della verifica statica e sismica dell'edificio in oggetto, attualmente non in uso ma nel passato sede di una scuola comunale. Nell'ottica di una futura riutilizzazione con la medesima destinazione di uso scolastico, è stata eseguita una analisi dinamica lineare ai sensi delle Norme Tecniche per le Costruzioni (NTC 2018) di cui al D.M. 17/01/2018 per valutare la sicurezza sismica della struttura quale edificio ad uso scolastico nella situazione di progetto di riuso. Pertanto è stata data all'edificio una destinazione d'uso a classe III ai sensi del par. 2.4.2 e vita nominale 50 anni ai sensi del 2.4.1 delle NTC 2018. L'edificio è sotto vincolo della Soprintendenza ai Beni Architettonici del Piemonte.

La verifica oggetto di questa relazione riguarda solamente la parte di edificio originario in muratura portante, poiché l'ampliamento con telaio in c.a. e tamponamenti sarà oggetto di demolizione e ricostruzione con nuova struttura in c.a., sismicamente indipendente. La parte originaria ha struttura portante in muratura con due diverse tessiture: in mattoni e malta cementizia di buona qualità per quanto riguarda l'ossatura portante, e con mattoni forati per le restanti parti (prevalentemente vano scale e parete di confine con ampliamento). I solai sono in laterocemento e la copertura con struttura lignea. In minima parte sono presenti anche travi a telaio in c.a.

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Per rendere nuovamente l'edificio utilizzabile per uso scolastico occorre che, ai sensi del par. 8.4.2 delle NTC 2018, esso abbia un miglioramento della sicurezza sismica pari almeno al 60%. Partendo da una verifica dello stato di fatto pari a 0% dell'accelerazione attesa al suolo, sono stati progettati interventi di rinforzo delle pareti murarie più carenti strutturalmente mediante utilizzo di intonaco armato (sistema "reticulatus" per zone con paramano a vista) e irrigidimento dei solai esistenti con soletta collaborante ancorata con i pioli al preesistente solaio in laterocemento. I risultati della verifica mediante analisi dinamica lineare sono stati positivi per un'accelerazione attesa al suolo pari al 60%.

Descrizione generale dell'opera

Fabbricato ad uso	Scuola
Ubicazione	Comune di NOLE (TO) (Regione PIEMONTE)
	Località NOLE (TO)
	Longitudine 7.572, Latitudine 45.244
Numero di piani	Fuori terra: 2
	Interrati: 1
	le dimensioni dell'opera in pianta sono racchiuse in un rettangolo di 11 x 12 m
Numero vani scale	1
Numero vani ascensore	0
Tipo di fondazione	Pareti in c.a.

Principali caratteristiche della struttura

Struttura regolare in pianta	SI
Struttura regolare in altezza	SI
Classe di duttilità	BD
Travi: ricalate o in spessore	ricalcate
Pilastrati	SI
Pilastrati in falso	NO
Tipo di fondazione	Pareti in c.a.

Condizioni per cui è necessario considerare la componente verticale del sisma	NO
---	----

Parametri della struttura			
Classe d'uso	Vita Vn [anni]	Coeff. Uso	Periodo Vr [anni]
III	50.0	1.5	75.0

Fattore di struttura
Ai sensi del par. 7.2.1. delle NTC 2018 l'edificio in oggetto può essere classificato come regolare sia in pianta che in altezza, e pertanto il fattore di struttura $q=3,4$.

Quadro normativo di riferimento adottato

Le norme ed i documenti assunti quale riferimento per la progettazione strutturale vengono indicati di seguito. Nel capitolo "normativa di riferimento" è comunque presente l'elenco completo delle normative disponibili.

Progetto-verifica degli elementi	
Progetto cemento armato	D.M. 09-01-1996
Progetto acciaio	D.M. 14-01-2008
Progetto legno	D.M. 14-01-2008
Progetto muratura	D.M. 20-11-1987
Azione sismica	
Norma applicata per l'azione sismica	D.M. 17-01-2018

Livelli di conoscenza e fattori di confidenza

Il livello di conoscenza, per edifici esistenti è LC2
Pertanto il fattore di confidenza è 1,2

Azioni di progetto sulla costruzione

Nei capitoli "modellazione delle azioni" e "schematizzazione dei casi di carico" sono indicate le azioni sulla costruzioni.

Nel prosieguo si indicano tipo di analisi strutturale condotta (statico,dinamico, lineare o non lineare) e il metodo adottato per la risoluzione del problema strutturale nonché le metodologie seguite per la verifica o per il progetto-verifica delle sezioni. Si riportano le combinazioni di carico adottate e, nel caso di calcoli non lineari, i percorsi di carico seguiti; le configurazioni studiate per la struttura in esame *sono risultate effettivamente esaustive per la progettazione-verifica*.

La verifica della sicurezza degli elementi strutturali avviene con i metodi della scienza delle costruzioni. L'analisi strutturale è condotta con il metodo degli spostamenti per la valutazione dello stato tensodeformativo indotto da carichi statici. L'analisi strutturale è condotta con il metodo dell'analisi modale e dello spettro di risposta in termini di accelerazione per la valutazione dello stato tensodeformativo indotto da carichi dinamici (tra cui quelli di tipo sismico).

L'analisi strutturale viene effettuata con il metodo degli elementi finiti. Il metodo sopraindicato si basa sulla schematizzazione della struttura in elementi connessi solo in corrispondenza di un numero prefissato di punti denominati nodi. I nodi sono definiti dalle tre coordinate cartesiane in un sistema di riferimento globale. Le incognite del problema (nell'ambito del metodo degli spostamenti) sono le componenti di spostamento dei nodi riferite al sistema di riferimento globale (traslazioni secondo X, Y, Z, rotazioni attorno X, Y, Z). La soluzione del problema si ottiene con un sistema di equazioni algebriche lineari i cui termini noti sono costituiti dai carichi agenti sulla struttura opportunamente concentrati ai nodi:

$$\mathbf{K} \cdot \mathbf{u} = \mathbf{F} \text{ dove}$$

\mathbf{K} = matrice di rigidezza
 \mathbf{u} = vettore spostamenti nodali
 \mathbf{F} = vettore forze nodali

Dagli spostamenti ottenuti con la risoluzione del sistema vengono quindi dedotte le sollecitazioni e/o le tensioni di ogni elemento, riferite generalmente ad una terna locale all'elemento stesso.

Il sistema di riferimento utilizzato è costituito da una terna cartesiana destrorsa XYZ. Si assume l'asse Z verticale ed orientato verso l'alto.

Gli elementi utilizzati per la modellazione dello schema statico della struttura sono i seguenti:

Elemento tipo TRUSS	(biella-D2)
Elemento tipo BEAM	(trave-D2)
Elemento tipo MEMBRANE	(membrana-D3)
Elemento tipo PLATE	(piastra-guscio-D3)
Elemento tipo BOUNDARY	(molla)
Elemento tipo STIFFNESS	(matrice di rigidezza)
Elemento tipo BRICK	(elemento solido)
Elemento tipo SOLAIO	(macro elemento composto da più membrane)

Modello numerico

In questa parte viene descritto il modello numerico utilizzato (o i modelli numerici utilizzati) per l'analisi della struttura. La presentazione delle informazioni deve essere, coerentemente con le prescrizioni del paragrafo 10.2 e relativi sottoparagrafi delle NTC-18, tale da garantirne la leggibilità, la corretta interpretazione e la riproducibilità

Tipo di analisi strutturale	
Statica lineare	SI
Statica non lineare	NO
Sismica statica lineare	NO
Sismica dinamica lineare	SI
Sismica statica non lineare (prop. masse)	NO
Sismica statica non lineare (prop. modo)	NO
Sismica statica non lineare (triangolare)	NO
Non linearità geometriche (fattore P delta)	NO

Di seguito si indicano l'origine e le caratteristiche dei codici di calcolo utilizzati riportando titolo, produttore e distributore, versione, estremi della licenza d'uso:

Informazioni sul codice di calcolo	
Titolo:	PRO SAP PROfessional Structural Analysis Program
Versione:	PROFESSIONAL (build 2018-07-183)
Produttore-Distributore:	2S.I. Software e Servizi per l'Ingegneria s.r.l., Ferrara
Dati utente finale:	In.Ar.Te. Torino S.r.l.
Codice Utente:	
Codice Licenza:	Licenza dsi4017

Un attento esame preliminare della documentazione a corredo del software **ha consentito di valutarne l'affidabilità e soprattutto l'idoneità al caso specifico**. La documentazione, fornita dal produttore e distributore del software, contiene una esauriente descrizione delle basi teoriche e degli algoritmi impiegati, l'individuazione dei campi d'impiego, nonché casi prova interamente risolti e commentati, corredati dei file di input necessari a riprodurre l'elaborazione:

Affidabilità dei codici utilizzati	
2S.I. ha verificato l'affidabilità e la robustezza del codice di calcolo attraverso un numero significativo di casi prova in cui i risultati dell'analisi numerica sono stati confrontati con soluzioni teoriche. E' possibile reperire la documentazione contenente alcuni dei più significativi casi trattati al seguente link: http://www.2si.it/Software/Affidabilità.htm	

Modellazione della geometria e proprietà meccaniche:	
nodi	3382
elementi D2 (per aste, travi, pilastri...)	353
elementi D3 (per pareti, platee, gusci...)	2978
elementi solaio	36
elementi solidi	0
Dimensione del modello strutturale [cm]:	
X min =	-636.36
Xmax =	528.64

Ymin =	-334.97
Ymax =	903.53
Zmin =	-315.00
Zmax =	1340.00
Strutture verticali:	
Elementi di tipo asta	NO
Pilastri	SI
Pareti	SI
Setti (a comportamento membranale)	NO
Strutture non verticali:	
Elementi di tipo asta	SI
Travi	SI
Gusci	NO
Membrane	NO
Orizzontamenti:	
Solai con la proprietà piano rigido	SI
Solai senza la proprietà piano rigido	SI
Tipo di vincoli:	
Nodi vincolati rigidamente	SI
Nodi vincolati elasticamente	NO
Nodi con isolatori sismici	NO
Fondazioni puntuali (plinti/plinti su palo)	NO
Fondazioni di tipo trave	NO
Fondazioni di tipo platea	NO
Fondazioni con elementi solidi	NO

Modellazione delle azioni

Si veda il capitolo **“Schematizzazione dei casi di carico”** per le informazioni necessarie alla comprensione ed alla ricostruzione delle azioni applicate al modello numerico, coerentemente con quanto indicato nella parte *“2.6. Azioni di progetto sulla costruzione”*.

Combinazioni e/o percorsi di carico

Si veda il capitolo **“Definizione delle combinazioni”** in cui sono indicate le combinazioni di carico adottate e, nel caso di calcoli non lineari, i percorsi di carico seguiti.

Combinazioni dei casi di carico	
APPROCCIO PROGETTUALE	Approccio 2
Tensioni ammissibili	NO
SLU	SI
SLV (SLU con sisma)	SI
SLC	NO
SLD	SI
SLO	NO
SLU GEO A2 (per approccio 1)	NO
SLU EQU	NO
Combinazione caratteristica (rara)	NO
Combinazione frequente	NO
Combinazione quasi permanente (SLE)	NO
SLA (accidentale quale incendio)	NO

Principali risultati

I risultati devono costituire una sintesi completa ed efficace, presentata in modo da riassumere il comportamento della struttura, per ogni

tipo di analisi svolta.

2.8.1. Risultati dell'analisi modale

Viene riportato il tipo di analisi modale condotta, restituiti i risultati della stessa e valutate le informazioni desumibili in merito al comportamento della struttura.

2.8.2. Deformate e sollecitazioni per condizioni di carico

Vengono riportati i principali risultati atti a descrivere il comportamento della struttura, in termini di stati di sollecitazione e di deformazione generalizzata, distinti per condizione elementare di carico o per combinazioni omogenee delle stesse.

2.8.3. Involuppo delle sollecitazioni maggiormente significative. L'analisi e la restituzione degli involuppi (nelle combinazioni considerate agli SLU e agli SLE) delle caratteristiche di sollecitazione devono essere finalizzate alla valutazione dello stato di sollecitazione nei diversi elementi della struttura.

2.8.4. Reazioni vincolari

Vengono riportate le reazioni dei vincoli nelle singole condizioni di carico e/o nelle combinazioni considerate.

2.8.5. Altri risultati significativi

Nella presente parte vengono riportati tutti gli altri risultati che il progettista ritiene di interesse per la descrizione e la comprensione del/i modello/i e del comportamento della struttura.

La presente relazione, oltre ad illustrare in modo esaustivo i dati in ingresso ed i risultati delle analisi in forma tabellare, riporta una serie di immagini:

per i dati in ingresso:

- modello solido della struttura
- numerazione di nodi e ed elementi
- configurazioni di carico statiche
- configurazioni di carico sismiche con baricentri delle masse e eccentricità

per le combinazioni più significative (statisticamente più gravose per la struttura):

- configurazioni deformate
- diagrammi e involuppi delle azioni interne
- mappe delle tensioni
- reazioni vincolari
- mappe delle pressioni sul terreno

per il progetto-verifica degli elementi:

- diagrammi di armatura
- percentuali di sfruttamento
- mappe delle verifiche più significative per i vari stati limite

Informazioni generali sull'elaborazione e giudizio motivato di accettabilità dei risultati.

Il programma prevede una serie di controlli automatici (check) che consentono l'individuazione di errori di modellazione. Al termine dell'analisi un controllo automatico identifica la presenza di spostamenti o rotazioni abnormi. Si può pertanto asserire che l'elaborazione sia corretta e completa. I risultati delle elaborazioni sono stati sottoposti a controlli che ne comprovano l'attendibilità. Tale valutazione ha compreso il confronto con i risultati di semplici calcoli, eseguiti con metodi tradizionali e adottati, anche in fase di primo proporzionamento della struttura. Inoltre, sulla base di considerazioni riguardanti gli stati tensionali e deformativi determinati, si è valutata la validità delle scelte operate in sede di schematizzazione e di modellazione della struttura e delle azioni. Si allega al termine della presente relazione elenco sintetico dei controlli svolti (verifiche di equilibrio tra reazioni vincolari e carichi applicati, comparazioni tra i risultati delle analisi e quelli di valutazioni semplificate, etc.) .

Verifiche agli stati limite ultimi

Nel capitolo relativo alla progettazione degli elementi strutturali agli SLU vengono indicate, con riferimento alla normativa adottata, le modalità ed i criteri seguiti per valutare la sicurezza della struttura nei confronti delle possibili situazioni di crisi ed i risultati delle valutazioni svolte. In via generale, oltre alle verifiche di resistenza e di spostamento, devono essere prese in considerazione verifiche nei confronti dei fenomeni di instabilità, locale e globale, di fatica, di duttilità, di degrado.

Verifiche agli stati limite di esercizio

Nel capitolo relativo alla progettazione degli elementi strutturali agli SLU vengono indicate, con riferimento alla normativa adottata, le modalità seguite per valutare l'affidabilità della struttura nei confronti delle possibili situazioni di perdita di funzionalità (per eccessive deformazioni, fessurazioni, vibrazioni, etc.) ed i risultati delle valutazioni svolte.

RELAZIONE SUI MATERIALI

Il capitolo Materiali riporta informazioni esaustive relative all'elenco dei materiali impiegati e loro modalità di posa in opera e ai valori di calcolo.

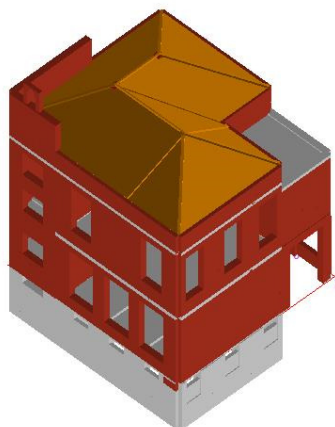
NORMATIVA DI RIFERIMENTO

1. D.Min. Infrastrutture Min. Interni e Prot. Civile 17 Gennaio 2018 e allegate "Norme tecniche per le costruzioni".
2. D.Min. Infrastrutture Min. Interni e Prot. Civile 14 Gennaio 2008 e allegate "Norme tecniche per le costruzioni".
3. D.Min. Infrastrutture e trasporti 14 Settembre 2005 e allegate "Norme tecniche per le costruzioni".
4. D.M. LL.PP. 9 Gennaio 1996 "Norme tecniche per il calcolo, l'esecuzione ed il collaudo delle strutture in cemento armato, normale e precompresso e per le strutture metalliche".
5. D.M. LL.PP. 16 Gennaio 1996 "Norme tecniche relative ai <<Criteri generali per la verifica di sicurezza delle costruzioni e dei carichi e sovraccarichi>>".
6. D.M. LL.PP. 16 Gennaio 1996 "Norme tecniche per le costruzioni in zone sismiche".
7. Circolare 4/07/96, n.156AA.GG./STC. istruzioni per l'applicazione delle "Norme tecniche relative ai <<Criteri generali per la verifica di sicurezza delle costruzioni e dei carichi e sovraccarichi>>" di cui al D.M. 16/01/96.
8. Circolare 10/04/97, n.65AA.GG. istruzioni per l'applicazione delle "Norme tecniche per le costruzioni in zone sismiche" di cui al D.M. 16/01/96.
9. D.M. LL.PP. 20 Novembre 1987 "Norme tecniche per la progettazione, esecuzione e collaudo degli edifici in muratura e per il loro consolidamento".
10. Circolare 4 Gennaio 1989 n. 30787 "Istruzioni in merito alle norme tecniche per la progettazione, esecuzione e collaudo degli edifici in muratura e per il loro consolidamento".
11. D.M. LL.PP. 11 Marzo 1988 "Norme tecniche riguardanti le indagini sui terreni e sulle rocce, la stabilità dei pendii naturali e delle scarpate, i criteri generali e le prescrizioni per la progettazione, l'esecuzione e il collaudo delle opere di sostegno delle terre e delle opere di fondazione".
12. D.M. LL.PP. 3 Dicembre 1987 "Norme tecniche per la progettazione, esecuzione e collaudo delle costruzioni prefabbricate".
13. UNI 9502 - Procedimento analitico per valutare la resistenza al fuoco degli elementi costruttivi di conglomerato cementizio armato, normale e precompresso - edizione maggio 2001
14. Ordinanza del Presidente del Consiglio dei Ministri n. 3274 del 20 marzo 2003 "Primi elementi in materia di criteri generali per la classificazione sismica del territorio nazionale e di normative tecniche per le costruzioni in zona sismica" e successive modificazioni e integrazioni.
15. UNI EN 1990:2006 13/04/2006 Eurocodice 0 - Criteri generali di progettazione strutturale.
16. UNI EN 1991-1-1:2004 01/08/2004 Eurocodice 1 - Azioni sulle strutture - Parte 1-1: Azioni in generale - Pesi per unità di volume, pesi propri e sovraccarichi per gli edifici.
17. UNI EN 1991-2:2005 01/03/2005 Eurocodice 1 - Azioni sulle strutture - Parte 2: Carichi da traffico sui ponti.
18. UNI EN 1991-1-3:2004 01/10/2004 Eurocodice 1 - Azioni sulle strutture - Parte 1-3: Azioni in generale - Carichi da neve.
19. UNI EN 1991-1-4:2005 01/07/2005 Eurocodice 1 - Azioni sulle strutture - Parte 1-4: Azioni in generale - Azioni del vento.
20. UNI EN 1991-1-5:2004 01/10/2004 Eurocodice 1 - Azioni sulle strutture - Parte 1-5: Azioni in generale - Azioni termiche.
21. UNI EN 1992-1-1:2005 24/11/2005 Eurocodice 2 - Progettazione delle strutture di calcestruzzo - Parte 1-1: Regole generali e regole per gli edifici.
22. UNI EN 1992-1-2:2005 01/04/2005 Eurocodice 2 - Progettazione delle strutture di calcestruzzo - Parte 1-2: Regole generali - Progettazione strutturale contro l'incendio.
23. UNI EN 1993-1-1:2005 01/08/2005 Eurocodice 3 - Progettazione delle strutture di acciaio - Parte 1-1: Regole generali e regole per gli edifici.
24. UNI EN 1993-1-8:2005 01/08/2005 Eurocodice 3 - Progettazione delle strutture di acciaio - Parte 1-8: Progettazione dei collegamenti.
25. UNI EN 1994-1-1:2005 01/03/2005 Eurocodice 4 - Progettazione delle strutture composte acciaio-calcestruzzo - Parte 1-1: Regole generali e regole per gli edifici.
26. UNI EN 1994-2:2006 12/01/2006 Eurocodice 4 - Progettazione delle strutture composte acciaio-calcestruzzo - Parte 2: Regole generali e regole per i ponti.
27. UNI EN 1995-1-1:2005 01/02/2005 Eurocodice 5 - Progettazione delle strutture di legno - Parte 1-1: Regole generali - Regole comuni e regole per gli edifici.
28. UNI EN 1995-2:2005 01/01/2005 Eurocodice 5 - Progettazione delle strutture di legno - Parte 2: Ponti.
29. UNI EN 1996-1-1:2006 26/01/2006 Eurocodice 6 - Progettazione delle strutture di muratura - Parte 1-1: Regole generali per strutture di muratura armata e non armata.
30. UNI EN 1996-3:2006 09/03/2006 Eurocodice 6 - Progettazione delle strutture di muratura - Parte 3: Metodi di calcolo semplificato per strutture di muratura non armata.
31. UNI EN 1997-1:2005 01/02/2005 Eurocodice 7 - Progettazione geotecnica - Parte 1: Regole generali.
32. UNI EN 1998-1:2005 01/03/2005 Eurocodice 8 - Progettazione delle strutture per la resistenza sismica - Parte 1: Regole generali, azioni sismiche e regole per gli edifici.
33. UNI EN 1998-3:2005 01/08/2005 Eurocodice 8 - Progettazione delle strutture per la resistenza sismica - Parte 3: Valutazione e adeguamento degli edifici.
34. UNI EN 1998-5:2005 01/01/2005 Eurocodice 8 - Progettazione delle strutture per la resistenza sismica - Parte 5: Fondazioni, strutture di contenimento ed aspetti geotecnici.

NOTA sul capitolo "normativa di riferimento": riporta l'elenco delle normative implementate nel software. Le norme utilizzate per la struttura oggetto della presente relazione sono indicate nel precedente capitolo "RELAZIONE DI CALCOLO STRUTTURALE" "ANALISI E VERIFICHE SVOLTE CON L'AUSILIO DI CODICI DI CALCOLO". Laddove nei capitoli successivi vengano richiamate norme antecedenti al DM 17.01.08 è dovuto o a progettazione simulata di edificio esistente.

In attesa della pubblicazione della circolare di istruzione per l'applicazione delle Norme Tecniche delle Costruzioni del 17 gennaio 2018 viene utilizzata la CIRCOLARE esplicativa n. 617 del 2 febbraio 2009, "Istruzioni per l'applicazione delle «Nuove norme tecniche per le costruzioni» di cui al decreto ministeriale 14 gennaio 2008".

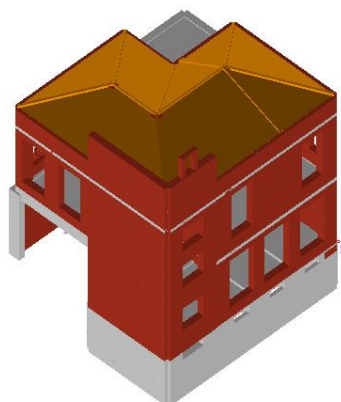
MODELLO



Scuola Nole_rinforzi 50 anni (3) 60% Regolare

Vista 3D

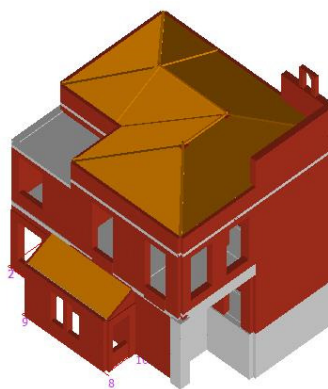
MODELLO



Scuola Nole_rinforzi 50 anni (3) 60% Regolare

Vista 3D

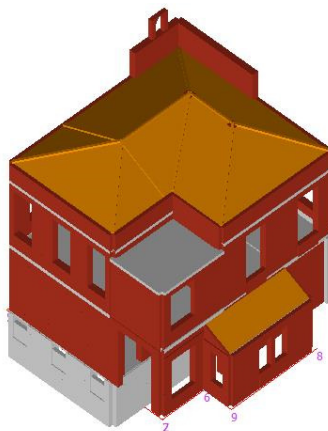
MODELLO



Scuola Nole_rinforzi 50 anni (3) 60% Regolare

Vista 3D

MODELLO



Scuola Nole_rinforzi 50 anni (3) 60% Regolare

Vista 3D

CARATTERISTICHE MATERIALI UTILIZZATI

LEGENDA TABELLA DATI MATERIALI

Il programma consente l'uso di materiali diversi. Sono previsti i seguenti tipi di materiale:

1	materiale tipo cemento armato
2	materiale tipo acciaio
3	materiale tipo muratura
4	materiale tipo legno
5	materiale tipo generico

I materiali utilizzati nella modellazione sono individuati da una sigla identificativa ed un codice numerico (gli elementi strutturali richiamano quest'ultimo nella propria descrizione). Per ogni materiale vengono riportati in tabella i seguenti dati:

Young	modulo di elasticità normale
Poisson	coefficiente di contrazione trasversale
G	modulo di elasticità tangenziale
Gamma	peso specifico
Alfa	coefficiente di dilatazione termica

I dati soprariportati vengono utilizzati per la modellazione dello schema statico e per la determinazione dei carichi inerziali e termici. In relazione al tipo di materiale vengono riportati inoltre:

1	cemento armato	Rck Fctm	resistenza caratteristica cubica resistenza media a trazione semplice
2	acciaio	Ft Fy Fd Fdt Sadm Sadmt	tensione di rottura a trazione tensione di snervamento resistenza di calcolo resistenza di calcolo per spess. t>40 mm tensione ammissibile tensione ammissibile per spess. t>40 mm
3	muratura	Resist. Fk Resist. Fvko	resistenza caratteristica a compressione resistenza caratteristica a taglio
4	legno	Resist. fc0k Resist. ft0k Resist. fmk Resist. fvk Modulo E0,05 Lamellare	Resistenza caratteristica (tensione amm. per REGLES) per compressione Resistenza caratteristica (tensione amm. per REGLES) per trazione Resistenza caratteristica (tensione amm. per REGLES) per flessione Resistenza caratteristica (tensione amm. per REGLES) per taglio Modulo elastico parallelo caratteristico lamellare o massiccio

Vengono inoltre riportate le tabelle contenenti il riassunto delle informazioni assegnate nei criteri di progetto in uso.

Con riferimento al **Documento di Affidabilità** "Test di validazione del software di calcolo PRO_SAP e dei moduli aggiuntivi PRO_SAP Modulo Geotecnico, PRO_CAD nodi acciaio e PRO_MST" - versione Maggio 2011, disponibile per il download sul sito www.2si.it, si segnalano i seguenti esempi applicativi:

Modellazione di strutture in c.a.

Test N°	Titolo
41	GERARCHIA DELLE RESISTENZE PER TRAVI IN C.A.
42	GERARCHIA DELLE RESISTENZE PER PILASTRI IN C.A.
43	VERIFICA ALLE T.A. DI STRUTTURE IN C.A.
44	VERIFICA AGLI SLU DI STRUTTURE IN C.A.
45	VERIFICA A PUNZONAMENTO ALLO SLU DI PIASTRE IN C.A.
46	VERIFICA A PUNZONAMENTO ALLO SLU DI TRAVI IN C.A.
47	PROGETTAZIONE A TAGLIO DI STRUTTURE IN C.A. SECONDO IL D.M. 9/1/96
48	PROGETTAZIONE A TAGLIO DI STRUTTURE IN C.A. SECONDO IL D.M. 14/1/2008
49	VERIFICA ALLO SLE (TENSIONI E FESSURAZIONE) DI STRUTTURE IN C.A.
50	VERIFICA ALLO SLE (DEFORMAZIONE) DI STRUTTURE IN C.A.
51	FATTORE DI STRUTTURA
52	SOVRARESISTENZE
53	DETTAGLI COSTRUTTIVI C.A.: LIMITI D'ARMATURA PILASTRI E NODI TRAVE-PILASTRO
54	PARETI IN C.A. SNELLE IN ZONA SISMICA
80	ANALISI PUSHOVER DI UN EDIFICIO IN C.A.
120	PROGETTO E VERIFICA DI TRAVI PREM

Modellazione di strutture in acciaio

Test N°	Titolo
55	VERIFICA DI STABILITA' DI ASTE COMPRESSE IN ACCIAIO – METODO OMEGA
56	LUCE LIBERA DI TRAVI E ASTE IN ACCIAIO
57	LUCE LIBERA DI COLONNE IN ACCIAIO
58	SVERGOLAMENTO DI TRAVI IN ACCIAIO
59	FATTORE DI STRUTTURA
60	ACCIAIO D.M.2008
61	ACCIAIO EC3
62	GERARCHIA RESISTENZE STRUTTURE IN ACCIAIO
63	STABILITA' DI ASTE COMPOSTE IN ACCIAIO
73	COLLEGAMENTI IN ACCIAIO: NODO TRAVE COLONNA FLANGIATO CON PRESENZA IRRIGIDIMENTI TRASVERSALI
74	COLLEGAMENTI IN ACCIAIO: NODO TRAVE COLONNA FLANGIATO CON PRESENZA DI UN PIATTO DI RINFORZO SALDATO ALL'ANIMA DELLA COLONNA
75	COLLEGAMENTI IN ACCIAIO: NODO TRAVE COLONNA FLANGIATO CON PRESENZA DI DUE PIATTI DI RINFORZO SALDATI ALL'ANIMA DELLA COLONNA
76	COLLEGAMENTI IN ACCIAIO: NODO TRAVE COLONNA FLANGIATO A DUE VIE SU ALI COLONNA
77	COLLEGAMENTI IN ACCIAIO: NODO TRAVE COLONNA FLANGIATO A UNA VIA CON DUE COMBINAZIONI DI CARICO
78	COLLEGAMENTI IN ACCIAIO: NODO TRAVE COLONNA FLANGIATO SU ANIMA SENZA RINFORZI A QUATTRO FILE DI BULLONI DI CUI UNA SU PIASTRA INFERIORE E UNA SU PIASTRA SUPERIORE
79	VERIFICA DELLA PIASTRA NODO TRAVE COLONNA
85	TELAIO ACCIAIO: CONTROVENTI CONCENTRICI

Modellazione di strutture in muratura

Test N°	Titolo
81	ANALISI PUSHOVER DI UNA STRUTTURA IN MURATURA
84	ANALISI ELASTO PLASTICA INCREMENTALE, PARETE IN MURATURA

86	VERIFICA NON SISMICA DELLE MURATURE (D.M. 87 TA)
87	VERIFICA NON SISMICA DELLE MURATURE (D.M. 2005 SL)
88	FATTORE DI STRUTTURA

Modellazione di strutture in legno

Test N°	Titolo
17	SOLAIO: MISTO LEGNO-CALCESTRUZZO
89	VERIFICA ALLO SLU DI STRUTTURE IN LEGNO SECONDO EC5
90	VERIFICA ALLO SLE DI STRUTTURE IN LEGNO SECONDO EC5
91	FATTORE DI STRUTTURA
92	VERIFICHE EC5
93	SNELLEZZE EC5
94	VERIFICA AL FUOCO DI STRUTTURE IN LEGNO SECONDO EC5
117	PROGETTO E VERIFICA DI GUSCI IN MATERIALE XLAM
118	PROGETTO E VERIFICA DI PARETI IN MATERIALE XLAM E RELATIVI COLLEGAMENTI
119	PROGETTO E VERIFICA DI SOLAI IN MATERIALE XLAM

id	Tipo / Note		Young	Poisson	G	Gamma	Alfa
		daN/cm2	daN/cm2		daN/cm2	daN/cm3	
1	Calcestruzzo Classe C25/30		3.145e+05	0.20	1.310e+05	2.50e-03	1.00e-05
	Rck	300.0					
	fctm	25.6					
10	acciaio Fe360 - S235		2.100e+06	0.30	8.077e+05	7.80e-03	1.20e-05
	ft	3600.0					
	fy	2350.0					
	fd	2350.0					
	fdt	2100.0					
	sadm	1600.0					
	sadmt	1400.0					
13	Tamponatura 1100 daN/mc per elemento pannello		4.500e+04	0.0	1.800e+04	1.10e-03	1.00e-05
	Resist. fk	59.0					
	Resist. fvko	4.1					
31	Muratura in pietre a spacco con buona tessitura E = 1.740e+04		1.740e+04	0.0	5800.0	2.10e-03	1.00e-05
	Resist. fk	26.0					
	Resist. fvko	0.6					
34	mattoni pieni e malta di calce		3.375e+04	0.0	1.125e+04	1.80e-03	1.00e-05
	Resist. fk	93.6					
	Resist. fvko	2.2					
36	muratura (consolidata) E = 6.825e+04		6.825e+04	0.0	1.706e+04	1.50e-03	1.00e-05
	Resist. fk	97.5					
	Resist. fvko	5.3					
40	muratura E = 2.000e+04 mattoni in argilla espansa e cls con malta M2		2.000e+04	0.20	8300.0	1.40e-03	1.00e-05
	Resist. fk	60.0					
	Resist. fvko	2.0					
42	Legno massiccio C24		1.000e+05	0.0	6300.0	3.50e-04	0.0
	Modulo E0,05		6.727e+04				
	LamellareMateriale non massiccio e pertanto da considerare come lamellareNo						
	Resist. fc0k	210.0					
	Resist. ft0k	140.0					
	Resist. fmk	240.0					
	Resist. fvk	40.0					
54	Calcestruzzo C 8/10		2.533e+05	0.20	1.520e+05	2.50e-03	1.00e-05
	Rck	100.0					
	fctm	10.0					
55	mattoni pieni e malta di calce INTONACO ARMATO		5.063e+04	0.0	1.688e+04	1.80e-03	1.00e-05
	Resist. fk	140.4					
	Resist. fvko	3.3					
56	mattoni pieni e malta di calce INTONACO ARMATO		5.063e+04	0.0	1.688e+04	1.80e-03	1.00e-05
	Resist. fk	140.4					
	Resist. fvko	3.3					
57	muratura (consolidata) E = 1.536e+05		1.536e+05	0.0	3.839e+04	1.50e-03	1.00e-05

Id	Tipo / Note		Young	Poisson	G	Gamma	Alfa
	Resist. fk	219.4					
	Resist. fvko	9.4					
58	mattoni pieni e malta di calce		3.375e+04	0.0	1.125e+04	1.80e-03	1.00e-05
	Resist. fk	72.0					
	Resist. fvko	1.7					
59	muratura E = 1.024e+05		1.024e+05	0.0	2.559e+04	1.50e-03	1.00e-05
	Resist. fk	146.3					
	Resist. fvko	6.3					

Aste acc.	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Generalità						
Beta assegnato	0.80	0.80	0.80			
Verifica come controvento	No	No	No			
Usa condizioni I e II	Si	Si	Si			
Coefficiente gamma M0	1.05	1.05	1.05			
Coefficiente gamma M1	1.05	1.05	1.05			
Coefficiente gamma M2	1.25	1.25	1.25			

Pilastrini acc.	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Lunghezze libere						
Metodo di calcolo 2-2	Assegnato	Assegnato	Assegnato			
2-2 Beta assegnato	2.00	2.00	2.00			
2-2 Beta * L assegnato [cm]	0.0	0.0	0.0			
Metodo di calcolo 3-3	Assegnato	Assegnato	Assegnato			
3-3 Beta assegnato	2.00	2.00	2.00			
3-3 Beta * L assegnato [cm]	0.0	0.0	0.0			
1-1 Beta assegnato	1.00	1.00	1.00			
1-1 Beta * L assegnato [cm]	0.0	0.0	0.0			
Generalità						
Coefficiente gamma M0	1.05	1.05	1.05			
Coefficiente gamma M1	1.05	1.05	1.05			
Coefficiente gamma M2	1.25	1.25	1.25			
Effetti del 2 ordine	Si	Si	No			
Momenti equivalenti	Si	Si	Si			
Usa condizioni I e II	Si	Si	Si			

Travi acc.	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Lunghezze libere						
3-3 Beta * L automatico	Si	Si	Si			
3-3 Beta assegnato	1.00	1.00	1.00			
3-3 Beta assegnato [cm]	0.0	0.0	0.0			
2-2 Beta * L automatico	Si	Si	Si			
2-2 Beta assegnato	1.00	1.00	1.00			
2-2 Beta * L assegnato [cm]	0.0	0.0	0.0			
1-1 Beta * L automatico	Si	Si	Si			
1-1 Beta assegnato	1.00	1.00	1.00			
1-1 Beta * L assegnato [cm]	0.0	0.0	0.0			
Generalità						
Coefficiente gamma M0	1.05	1.05	1.05			
Coefficiente gamma M1	1.05	1.05	1.05			
Coefficiente gamma M2	1.25	1.25	1.25			
Luce di taglio per GR [cm]	1.00	1.00	1.00			
Usa condizioni I e II	Si	Si	Si			
Momenti equivalenti	Si	Si	Si			

Pareti c.a.	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Generalità						
Progetto armatura	Parete sismica	Parete sismica	Singolo elemento			
Armatura						

Pareti c.a.	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Inclinazione Av [gradi]	90.00	90.00	90.00			
Angolo Av-Ao [gradi]	90.00	90.00	90.00			
Minima tesa	0.25	0.25	0.25			
Massima tesa	4.00	4.00	4.00			
Maglia unica centrale	No	No	No			
Unico strato verticale	No	No	No			
Unico strato orizzontale	No	No	No			
Copriferro [cm]	2.00	2.00	2.00			
Maglia V						
diametro	10	10	10			
passo	25	25	25			
diametro aggiuntivi	12	12	12			
Maglia O						
diametro	8	8	8			
passo	25	25	25			
diametro aggiuntivi	8	8	8			
Stati limite ultimi						
Tensione fy [daN/cm2]	4500.00	4500.00	4300.00			
Tipo acciaio	tipo C	tipo C	tipo C			
Coefficiente gamma s	1.15	1.15	1.15			
Coefficiente gamma c	1.50	1.50	1.50			
Fattore di confidenza FC	0.0	0.0	0.0			
Verifiche con N costante	Si	Si	Si			
Tensioni ammissibili						
Tensione amm. cls [daN/cm2]	97.50	97.50	97.50			
Tensione amm. acciaio [daN/cm2]	2600.00	2600.00	2600.00			
Rapporto omogeneizzazione N	15.00	15.00	15.00			
Massimo rapporto area compressa/tesa	1.00	1.00	1.00			
Parete estesa debolmente armata						
Fattore amplificazione taglio V	1.50	1.50	1.50			
Hcrit. par. 7.4.4.5.1 [cm]	0.0	0.0	0.0			
Hcrit. par. 7.4.6.1.4 [cm]	0.0	0.0	0.0			
Diagramma involuppo taglio	Si	No	No			
Vincolo lati	nessun lato	nessun lato	nessun lato			
Verifica come fascia	No	No	No			
Diametro di estremità	0	0	0			
Zona confinata						
Minima tesa	1.00	1.00	1.00			
Massima tesa	4.00	4.00	4.00			
Distanza barre [cm]	2.00	2.00	2.00			
Interferro	2	2	2			
Armatura inclinata						
Area barre [cm2]	0.0	0.0	0.0			
Angolo orizzontale [gradi]	0.0	0.0	0.0			
Distanza di base [cm]	0.0	0.0	0.0			
Resistenza al fuoco						
3- intradosso	No	No	No			
3+ estradosso	No	No	No			
Tempo di esposizione R	15	15	120			

Gusci c.a.	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Armatura						
Inclinazione Ax [gradi]	0.0	0.0	0.0			
Angolo Ax-Ay [gradi]	90.00	90.00	90.00			
Minima tesa	0.31	0.31	0.33			
Massima tesa	0.78	0.78	0.81			
Maglia unica centrale	No	No	No			
Copriferro [cm]	2.00	2.00	2.00			
Maglia x						
diametro	10	10	10			
passo	20	20	20			
diametro aggiuntivi	12	12	12			
Maglia y						
diametro	10	10	10			
passo	20	20	20			
diametro aggiuntivi	12	12	12			
Stati limite ultimi						
Tensione fy [daN/cm2]	4500.00	4500.00	4300.00			
Tipo acciaio	tipo C	tipo C	tipo C			
Coefficiente gamma s	1.15	1.15	1.15			

Gusci c.a.	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Coefficiente gamma c	1.50	1.50	1.50			
Fattore di confidenza FC	0.0	0.0	0.0			
Verifiche con N costante	Si	Si	Si			
Applica SLU da DIN	No	No	No			
Tensioni ammissibili						
Tensione amm. cls [daN/cm2]	97.50	97.50	97.50			
Tensione amm. acciaio [daN/cm2]	2600.00	2600.00	2600.00			
Rapporto omogeneizzazione N	15.00	15.00	15.00			
Massimo rapporto area compressa/tesa	1.00	1.00	1.00			
Resistenza al fuoco						
3- intradosso	No	No	No			
3+ estradosso	No	No	No			
Tempo di esposizione R	15	15	120			

Travi c.a.	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Generalità						
Progetta a filo	No	No	No			
Af inf: da q*L*L /	0.0	0.0	0.0			
Armatura						
Minima tesa	0.31	0.31	0.33			
Minima compressa	0.31	0.31	0.33			
Massima tesa	0.78	0.78	0.81			
Da sezione	Si	Si	No			
Usa armatura teorica	No	No	No			
Stati limite ultimi						
Tensione fy [daN/cm2]	4500.00	4500.00	4300.00			
Tensione fy staffe [daN/cm2]	4500.00	4500.00	4300.00			
Tipo acciaio	tipo C	tipo C	tipo C			
Coefficiente gamma s	1.15	1.15	1.15			
Coefficiente gamma c	1.50	1.50	1.50			
Fattore di confidenza FC	0.0	0.0	0.0			
Verifiche con N costante	Si	Si	Si			
Fattore di ridistribuzione	0.0	0.0	0.0			
Modello per il confinamento						
Relazione tensio-deformativa	Mander	Mander	Mander			
Incrudimento acciaio	5.000e-03	5.000e-03	5.000e-03			
Fattore lambda	1.00	1.00	1.00			
epsilon max,s	4.000e-02	4.000e-02	4.000e-02			
epsilon cu2	4.500e-03	4.500e-03	4.500e-03			
epsilon c2	0.0	0.0	0.0			
epsilon cy	0.0	0.0	0.0			
Tensioni ammissibili						
Tensione amm. cls [daN/cm2]	97.50	97.50	97.50			
Tensione amm. acciaio [daN/cm2]	2600.00	2600.00	2600.00			
Rapporto omogeneizzazione N	15.00	15.00	15.00			
Massimo rapporto area compressa/tesa	1.00	1.00	1.00			
Staffe						
Diametro staffe	0.0	0.0	0.0			
Passo minimo [cm]	4.00	5.00	5.00			
Passo massimo [cm]	30.00	30.00	30.00			
Passo raffittito [cm]	15.00	15.00	15.00			
Lunghezza zona raffittita [cm]	50.00	50.00	50.00			
Ctg(Teta) Max	2.50	2.50	2.50			
Percentuale sagomati	0.0	0.0	0.0			
Luce di taglio per GR [cm]	1.00	1.00	1.00			
Adotta scorrimento medio	No	No	Si			
Torsione non essenziale inclusa	Si	Si	Si			

Pilastrì c.a.	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Generalità						
Progetto armatura	Privilegia lati	Privilegia lati	Disponi come da sezione			
Progetta a filo	No	No	No			
Effetti del 2 ordine	Si	Si	No			
Beta per 2-2	1.00	1.00	1.00			
Beta per 3-3	1.00	1.00	1.00			
Armatura						

Pilastrici c.a.	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Massima tesa	4.00	4.00	4.00			
Minima tesa	1.00	1.00	1.00			
Stati limite ultimi						
Tensione fy [daN/cm2]	4500.00	4500.00	4300.00			
Tensione fy staffe [daN/cm2]	4500.00	4500.00	4300.00			
Tipo acciaio	tipo C	tipo C	tipo C			
Coefficiente gamma s	1.15	1.15	1.15			
Coefficiente gamma c	1.50	1.50	1.50			
Fattore di confidenza FC	0.0	0.0	0.0			
Verifiche con N costante	Si	Si	Si			
Modello per il confinamento						
Relazione tensio-deformativa	Mander	Mander	Mander			
Incrudimento acciaio	5.000e-03	5.000e-03	5.000e-03			
Fattore lambda	1.00	1.00	1.00			
epsilon max.s	4.000e-02	4.000e-02	4.000e-02			
epsilon cu2	4.500e-03	4.500e-03	4.500e-03			
epsilon c2	0.0	0.0	0.0			
epsilon cy	0.0	0.0	0.0			
Tensioni ammissibili						
Tensione amm. cls [daN/cm2]	97.50	97.50	97.50			
Tensione amm. acciaio [daN/cm2]	2600.00	2600.00	2600.00			
Rapporto omogeneizzazione N	15.00	15.00	15.00			
Staffe						
Diametro staffe	0.0	0.0	0.0			
Passo minimo [cm]	5.00	5.00	5.00			
Passo massimo [cm]	25.00	25.00	25.00			
Passo raffittito [cm]	15.00	15.00	15.00			
Lunghezza zona raffittita [cm]	45.00	45.00	45.00			
Ctg(Teta) Max	2.50	2.50	2.50			
Luce di taglio per GR [cm]	1.00	1.00	1.00			
Massimizza gerarchia	Si	Si	Si			

Muratura	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Lunghezze libere						
Altezza interpiano [cm]	0.0	0.0	300.00			
Rho	0.85	0.85	1.00			
Snellezza limite	20.00	20.00	0.0			
Generalità						
Gamma non sismico	3.00	3.00	0.0			
Gamma sismico	2.00	2.00	0.0			
Fattore di confidenza FC	0.0	0.0	0.0			
Tolleranza azioni [daN/cm2]	0.0	0.0	0.0			
Media valori per quota	Si	Si	Si			
Media valori per elemento	Si	Si	No			
Verifica come fascia	No	No	Si			
Usa formula [7.8.3]	Si	Si	No			

Solai e pannelli	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Generalità						
Usa tensioni ammissibili	No	No	No			
Af inf: da traliccio	Si	Si	Si			
Consenti armatura a taglio	No	No	No			
Incrementa armatura longitudinale per taglio	Si	Si	Si			
Af inf: da q*L*L /	20.00	20.00	16.00			
Incremento fascia piena [cm]	5.00	5.00	5.00			
Armatura						
Minima tesa	0.15	0.15	0.15			
Massima tesa	3.00	3.00	3.00			
Minima compressa	0.0	0.0	0.0			
Af/h [cm]	7.000e-02	7.000e-02	7.000e-02			
Stati limite ultimi						
Tensione fy [daN/cm2]	4500.00	4500.00	4300.00			
Tipo acciaio	tipo C	tipo C	tipo C			
Coefficiente gamma s	1.15	1.15	1.15			
Coefficiente gamma c	1.50	1.50	1.50			
Fattore di redistribuzione	0.0	0.0	0.0			

Solai e pannelli	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Tensioni ammissibili						
Tensione amm. cls [daN/cm2]	85.00	85.00	97.50			
Tensione amm. acciaio [daN/cm2]	2600.00	2600.00	2600.00			
Rapporto omogeneizzazione N	15.00	15.00	15.00			
Massimo rapporto area compressa/tesa	1.00	1.00	1.00			
Verifica freccia						
Infinita	250.00	500.00	500.00			
Istantanea	500.00	1000.00	1000.00			
Fattore viscosità	3.00	3.00	3.00			
Usa J non fessurato	No	No	No			
Elementi non strutturali						
Tamponatura antiespulsione	No	Si	Si			
Tamponatura con armatura	No	No	Si			
Fattore di struttura/comportamento	2.00	2.00	2.00			
Coefficiente gamma m	0.0	0.0	0.0			
Periodo Ta	0.0	0.0	0.0			
Altezza pannello	0.0	0.0	0.0			

Legno	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Lunghezze libere						
aste						
Beta assegnato	0.80	0.80	0.80			
travi						
3-3 Beta * L automatico	Si	Si	Si			
3-3 Beta assegnato	1.00	1.00	1.00			
3-3 Beta * L assegnato [cm]	0.0	0.0	0.0			
2-2 Beta * L automatico	Si	Si	Si			
2-2 Beta assegnato	1.00	1.00	1.00			
2-2 Beta * L assegnato [cm]	0.0	0.0	0.0			
1-1 Beta * L automatico	Si	Si	Si			
1-1 Beta assegnato	1.00	1.00	1.00			
1-1 Beta * L assegnato [cm]	0.0	0.0	0.0			
pilastrì						
Metodo di calcolo 3-3	Assegnato	Assegnato	Assegnato			
3-3 Beta assegnato	2.00	2.00	2.00			
3-3 Beta * L assegnato [cm]	0.0	0.0	0.0			
Metodo di calcolo 2-2	Assegnato	Assegnato	Assegnato			
2-2 Beta assegnato	2.00	2.00	2.00			
2-2 Beta * L assegnato [cm]	0.0	0.0	0.0			
1-1 Beta assegnato	1.00	1.00	1.00			
1-1 Beta * L assegnato [cm]	0.0	0.0	0.0			
Generalità						
Gamma non sismico	1.50	1.50	1.50			
Gamma sismico	1.50	1.50	1.50			
Fattore di confidenza FC	0.0	0.0	0.0			
Classificazione						
Classe di servizio	1 (bassa umidità)	1 (bassa umidità)	1 (bassa umidità)			
Per classe di servizio 1						
Kmod permanente	0.60	0.60	0.60			
Kmod lunga	0.70	0.70	0.70			
Kmod media	0.80	0.80	0.80			
Kmod breve	0.90	0.90	0.90			
Kmod istantanea	1.00	1.00	1.10			
Kdef	0.60	0.60	0.60			
Per classe di servizio 2						
Kmod permanente	0.60	0.60	0.60			
Kmod lunga	0.70	0.70	0.70			
Kmod media	0.80	0.80	0.80			
Kmod breve	0.90	0.90	0.90			
Kmod istantanea	1.00	1.00	1.10			
Kdef	0.80	0.80	0.80			
Per classe di servizio 3						
Kmod permanente	0.50	0.50	0.50			
Kmod lunga	0.55	0.55	0.55			
Kmod media	0.65	0.65	0.65			
Kmod breve	0.70	0.70	0.70			
Kmod istantanea	0.90	0.90	0.90			
Kdef	2.00	2.00	2.00			

XLAM	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Generalità						
L direzione 1 [*] [cm]	1.00	1.00	0.0			
L direzione 2 [cm]	0.0	0.0	0.0			
Verifica V da D.38	No	No	No			
Verifica M da M.5-45	No	No	No			
Media valori elementi	Si	Si	Si			
Connessioni pareti						
rvpk [daN/cm]	50.00	50.00	50.00			
rvtk [daN/cm]	50.00	50.00	50.00			
rvlk [daN/cm]	50.00	50.00	50.00			
RHk [daN]	5000.00	5000.00	5000.00			
dH [cm]	25.00	25.00	25.00			
fcH90k [daN/cm2]	20.00	20.00	20.00			
Pannelli solaio						
f ist<L/	500.00	500.00	500.00			
f inf<L/	350.00	350.00	350.00			
Verifica vibrazioni (EC5 7.3)	No	No	No			
E massetto collaborante [daN/cm2]	200000.00	200000.00	200000.00			
t massetto collaborante [cm]	4.00	4.00	4.00			
Smorzamento percentuale	0.0	0.0	0.0			
Resistenza al fuoco						
Spessore carbonizzazione [cm]	0.0	0.0	0.0			
3- intradosso	No	No	No			
3+ estradosso	No	No	No			

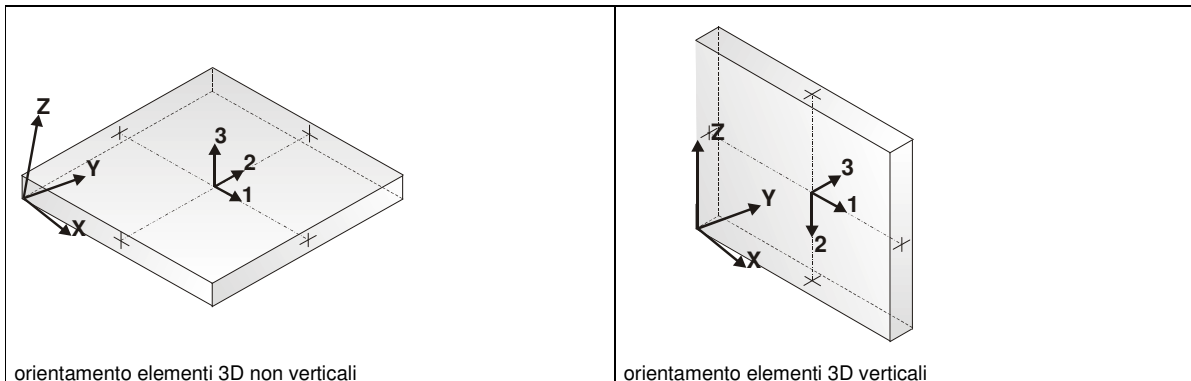
MODELLAZIONE STRUTTURA: ELEMENTI SHELL

LEGENDA TABELLA DATI SHELL

Il programma utilizza per la modellazione elementi a tre o quattro nodi denominati in generale shell.

Ogni elemento shell è individuato dai nodi I, J, K, L (L=I per gli elementi a tre nodi).

Ogni elemento è caratterizzato da un insieme di proprietà riportate in tabella che ne completano la modellazione.



In particolare per ogni elemento viene indicato in tabella:

Elem.	numero dell'elemento
Note	codice di comportamento: <i>Guscio</i> (elemento guscio in elevazione non verticale) <i>Guscio fond.</i> (elemento guscio su suolo elastico) <i>Setto</i> (elemento guscio in elevazione verticale) <i>Membrana</i> (elemento guscio con comportamento membranale)
Nodo I (J, K, L)	numero del nodo I (J, K, L)
Mat.	codice del materiale assegnato all'elemento
Spessore	spessore dell'elemento (costante)
Wink V	costante di sottofondo (coefficiente di Winkler) per la modellazione del suolo elastico verticale
Wink O	costante di sottofondo (coefficiente di Winkler) per la modellazione del suolo elastico orizzontale

Con riferimento al **Documento di Affidabilità** “*Test di validazione del software di calcolo PRO_SAP e dei moduli aggiuntivi PRO_SAP Modulo Geotecnico, PRO_CAD nodi acciaio e PRO_MST*” - versione Maggio 2011, disponibile per il download sul sito www.2si.it, si segnalano i seguenti esempi applicativi:

Test N°	Titolo
8	MENSOLE CON ELEMENTI PLATE E MATERIALE ORTOTROPO
10	PIASTRA CON ELEMENTI PLATE E MATERIALE ORTOTROPO
21	DRILLING
25	TENSIONI DI ELEMENTI PLATE
31	REALIZZAZIONE DI MESH PIANA SU GEOMETRIA CON PUNTI FISSI IMPORTATA DA FILE .DXF
32	REALIZZAZIONE DI MESH PIANA SU GEOMETRIA CON SEGMENTI E FORI INTERNI IMPORTATA DA FILE .DXF
33	REALIZZAZIONE DI MESH PIANE SU GEOMETRIE COSTRUITE IN PRO_SAP
34	ANALISI DI BUCKLING DI PIASTRA ISOTROPA
35	ANALISI DI BUCKLING DI UN CILINDRO COMPRESSO INCASTRATO ALLA BASE
36	ANALISI DI PARETI FORATE
37	BIMETALLIC STRIP (NAFEMS EXERCISE 6)
38	ANALISI ELASTICA DI PIASTRA CON INTAGLIO CIRCOLARE (FLAT BAR WITH EDGE NOTCHES-NAFEMS EXERCISE 9)
39	PLATEA NERVATA
45	VERIFICA A PUNZONAMENTO ALLO SLU DI PIASTRE IN C.A.
117	PROGETTO E VERIFICA DI GUSCI IN MATERIALE XLAM
118	PROGETTO E VERIFICA DI PARETI IN MATERIALE XLAM E RELATIVI COLLEGAMENTI

Elem.	Note	Nodo I	Nodo J	Nodo K	Nodo L	Mat.	Spessore cm	Wink V daN/cm3	Wink O daN/cm3
1	Setto	62	68	67	66	54	30.0		
2	Setto	66	67	70	69	54	30.0		
3	Setto	69	70	72	71	54	30.0		
4	Setto	71	72	74	73	54	30.0		
5	Setto	73	74	76	75	54	30.0		
6	Setto	75	76	77	36	54	30.0		
7	Setto	68	79	78	67	54	30.0		
8	Setto	67	78	80	70	54	30.0		
9	Setto	70	80	81	72	54	30.0		
10	Setto	72	81	82	74	54	30.0		
11	Setto	74	82	83	76	54	30.0		
12	Setto	76	83	84	77	54	30.0		
13	Setto	79	86	85	78	54	30.0		
14	Setto	78	85	87	80	54	30.0		
15	Setto	80	87	88	81	54	30.0		

16	Setto	81	88	89	82	54	30.0
17	Setto	82	89	90	83	54	30.0
18	Setto	83	90	91	84	54	30.0
19	Setto	86	93	92	85	54	30.0
20	Setto	85	92	94	87	54	30.0
21	Setto	87	94	95	88	54	30.0
22	Setto	88	95	96	89	54	30.0
23	Setto	89	96	97	90	54	30.0
24	Setto	90	97	98	91	54	30.0
25	Setto	93	100	99	92	54	30.0
26	Setto	92	99	101	94	54	30.0
27	Setto	94	101	102	95	54	30.0
28	Setto	95	102	103	96	54	30.0
29	Setto	96	103	104	97	54	30.0
30	Setto	97	104	105	98	54	30.0
31	Setto	100	107	106	99	54	30.0
32	Setto	99	106	108	101	54	30.0
33	Setto	101	108	109	102	54	30.0
34	Setto	102	109	110	103	54	30.0
35	Setto	103	110	111	104	54	30.0
36	Setto	104	111	112	105	54	30.0
42	Setto	1921	1930	1929	1920	55	40.0
43	Setto	114	121	120	113	54	30.0
44	Setto	113	120	122	115	54	30.0
45	Setto	115	122	123	116	54	30.0
46	Setto	116	123	124	117	54	30.0
47	Setto	117	124	125	118	54	30.0
48	Setto	118	125	126	119	54	30.0
49	Setto	121	128	127	120	54	30.0
50	Setto	120	127	129	122	54	30.0
51	Setto	122	129	130	123	54	30.0
52	Setto	123	130	131	124	54	30.0
53	Setto	124	131	132	125	54	30.0
54	Setto	125	132	133	126	54	30.0
55	Setto	128	63	134	127	54	30.0
56	Setto	127	134	135	129	54	30.0
57	Setto	129	135	136	130	54	30.0
58	Setto	130	136	137	131	54	30.0
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203	Setto	220	289	290	40	54	40.0
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464	Setto	579	572	573	580	54	50.0
465	Setto	581	574	572	579	54	50.0
466	Setto	582	575	574	581	54	50.0
467	Setto	583	576	575	582	54	50.0
468	Setto	584	577	576	583	54	50.0
469	Setto	585	578	577	584	54	50.0
470	Setto	586	579	580	587	54	50.0
471	Setto	588	581	579	586	54	50.0
472	Setto	589	582	581	588	54	50.0
473	Setto	590	583	582	589	54	50.0
474	Setto	591	584	583	590	54	50.0
475	Setto	592	585	584	591	54	50.0
476	Setto	593	586	587	55	54	50.0
477	Setto	594	588	586	593	54	50.0
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479	Setto	596	590	589	595	54	50.0
480	Setto	597	591	590	596	54	50.0
481	Setto	19	592	591	597	54	50.0
482	Setto	598	593	55	599	54	50.0

483	Setto	600	594	593	598	54	50.0
484	Setto	601	595	594	600	54	50.0
485	Setto	602	596	595	601	54	50.0
486	Setto	603	597	596	602	54	50.0
487	Setto	604	19	597	603	54	50.0
488	Setto	605	598	599	54	54	50.0
489	Setto	606	600	598	605	54	50.0
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491	Setto	608	602	601	607	54	50.0
492	Setto	609	603	602	608	54	50.0
493	Setto	18	604	603	609	54	50.0
494	Setto	610	605	54	53	54	50.0
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496	Setto	612	607	606	611	54	50.0
497	Setto	613	608	607	612	54	50.0
498	Setto	614	609	608	613	54	50.0
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512	Setto	627	622	52	41	54	50.0
513	Setto	628	623	622	627	54	50.0
514	Setto	629	624	623	628	54	50.0
515	Setto	630	625	624	629	54	50.0
516	Setto	631	626	625	630	54	50.0
517	Setto	2	16	626	631	54	50.0
518	Setto	58	633	632	139	54	50.0
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527	Setto	635	642	643	636	54	50.0
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536	Setto	647	41	627	646	54	50.0
537	Setto	646	627	628	648	54	50.0
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539	Setto	649	629	630	650	54	50.0
540	Setto	650	630	631	651	54	50.0
541	Setto	651	631	2	652	54	50.0
542	Setto	3	655	654	653	34	37.0
543	Setto	653	654	657	656	34	37.0
544	Setto	656	657	659	658	34	37.0
545	Setto	658	659	661	660	34	37.0
546	Setto	660	661	663	662	34	37.0
547	Setto	662	663	665	664	34	37.0
548	Setto	664	665	667	666	34	37.0
549	Setto	666	667	669	668	34	37.0
550	Setto	668	669	671	670	34	37.0
558	Setto	1949	1239	1240	1950	36	40.0
559	Setto	669	679	680	671	34	37.0
560	Setto	700	710	711	702	34	37.0
561	Setto	702	711	712	703	34	37.0
562	Setto	703	712	713	704	34	37.0
563	Setto	704	713	714	705	34	37.0
564	Setto	1722	1707	1708	1723	36	40.0
566	Setto	1720	452	1701	693	36	40.0
568	Setto	679	689	690	680	34	37.0

569	Setto	705	714	681	706	34	37.0
570	Setto	706	681	682	707	34	37.0
571	Setto	707	682	683	708	34	37.0
572	Setto	708	683	684	709	34	37.0
573	Setto	1723	1708	1709	685	36	40.0
574	Setto	693	1701	1702	694	36	40.0
575	Setto	694	1702	1703	695	36	40.0
577	Setto	689	698	699	690	34	37.0
578	Setto	695	1703	1704	696	36	40.0
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580	Setto	432	1720	693	1710	36	40.0
581	Setto	1710	693	694	1711	36	40.0
582	Setto	1711	694	695	1712	36	40.0
583	Setto	1712	695	696	1713	36	40.0
584	Setto	1713	696	1719	1714	36	40.0
586	Setto	698	708	709	699	34	37.0
587	Setto	701	15	710	700	34	37.0
588	Setto	715	710	15	22	34	42.0
589	Setto	716	711	710	715	34	42.0
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594	Setto	721	682	681	720	34	42.0
595	Setto	722	683	682	721	34	42.0
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598	Setto	726	716	715	724	34	25.0
599	Setto	853	844	843	852	34	42.0
600	Setto	854	845	844	853	34	42.0
601	Setto	762	846	845	854	34	42.0
602	Setto	763	847	846	762	34	42.0
603	Setto	764	848	847	763	34	42.0
604	Setto	732	722	721	731	34	42.0
605	Setto	733	723	722	732	40	30.0
606	Setto	734	724	725	735	34	25.0
607	Setto	736	726	724	734	34	25.0
608	Setto	765	849	848	764	34	42.0
609	Setto	766	850	27	28	34	42.0
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612	Setto	729	853	852	728	34	42.0
613	Setto	742	732	731	741	34	42.0
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618	Setto	737	762	854	730	34	42.0
619	Setto	738	763	762	737	34	42.0
620	Setto	739	764	763	738	34	42.0
621	Setto	740	765	764	739	34	42.0
622	Setto	751	742	741	750	34	42.0
623	Setto	752	743	742	751	40	30.0
624	Setto	821	811	812	26	34	42.0
625	Setto	822	813	811	821	34	42.0
626	Setto	823	814	813	822	34	42.0
627	Setto	824	815	814	823	34	42.0
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633	Setto	843	823	822	842	34	42.0
634	Setto	844	824	823	843	34	42.0
635	Setto	845	825	824	844	34	42.0
636	Setto	846	826	825	845	34	42.0
637	Setto	847	827	826	846	34	42.0
638	Setto	768	758	757	767	34	42.0
639	Setto	769	759	758	768	34	42.0
640	Setto	770	760	759	769	34	42.0
641	Setto	771	761	760	770	40	30.0
642	Setto	848	828	827	847	34	42.0
643	Setto	849	829	828	848	34	42.0
644	Setto	850	840	841	27	34	42.0
645	Setto	851	842	840	850	34	42.0
646	Setto	852	843	842	851	34	42.0
647	Setto	777	768	767	776	34	42.0

648	Setto	778	769	768	777	34	42.0
649	Setto	779	770	769	778	34	42.0
650	Setto	780	771	770	779	40	30.0
651	Setto	781	772	25	782	34	42.0
652	Setto	783	773	772	781	34	42.0
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657	Setto	788	778	777	787	34	42.0
658	Setto	789	779	778	788	34	42.0
659	Setto	790	780	779	789	34	42.0
660	Setto	791	781	782	792	34	42.0
661	Setto	793	783	781	791	34	42.0
662	Setto	794	784	783	793	34	42.0
663	Setto	795	785	784	794	34	42.0
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665	Setto	797	787	786	796	34	42.0
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669	Setto	801	791	792	802	34	42.0
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672	Setto	805	795	794	804	34	42.0
673	Setto	806	796	795	805	34	42.0
674	Setto	807	797	796	806	34	42.0
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676	Setto	809	799	798	808	34	42.0
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678	Setto	811	801	802	812	34	42.0
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680	Setto	814	804	803	813	34	42.0
681	Setto	815	805	804	814	34	42.0
682	Setto	816	806	805	815	34	42.0
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686	Setto	820	810	809	819	34	42.0
687	Setto	830	744	23	831	34	42.0
688	Setto	832	745	744	830	34	42.0
689	Setto	833	746	745	832	34	42.0
690	Setto	834	747	746	833	34	42.0
691	Setto	835	748	747	834	34	42.0
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695	Setto	839	752	751	838	40	30.0
696	Setto	2093	2102	2103	2094	36	40.0
697	Setto	754	832	830	753	34	42.0
698	Setto	755	833	832	754	34	42.0
699	Setto	756	834	833	755	34	42.0
700	Setto	757	835	834	756	34	42.0
701	Setto	758	836	835	757	34	42.0
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703	Setto	760	838	837	759	34	42.0
704	Setto	761	839	838	760	40	30.0
705	Setto	840	821	26	841	34	42.0
706	Setto	842	822	821	840	34	42.0
707	Setto	30	857	856	855	59	40.0
708	Setto	855	856	859	858	59	40.0
709	Setto	858	859	861	860	59	40.0
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711	Setto	862	863	865	864	59	40.0
712	Setto	864	865	867	866	59	40.0
713	Setto	866	867	869	868	59	40.0
714	Setto	868	869	871	870	59	40.0
715	Setto	870	871	873	872	59	40.0
716	Setto	857	28	766	856	59	40.0
717	Setto	856	766	727	859	59	40.0
718	Setto	859	727	728	861	59	40.0
719	Setto	861	728	729	863	59	40.0
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721	Setto	865	730	737	867	59	40.0
722	Setto	867	737	738	869	59	40.0
723	Setto	869	738	739	871	59	40.0
724	Setto	871	739	740	873	59	40.0

725	Setto	905	880	878	904	59	40.0
726	Setto	904	878	882	907	59	40.0
727	Setto	907	882	884	909	59	40.0
728	Setto	909	884	893	911	59	40.0
729	Setto	911	893	894	913	59	40.0
730	Setto	913	894	895	915	59	40.0
731	Setto	885	886	888	887	59	40.0
732	Setto	887	888	890	889	59	40.0
733	Setto	889	890	892	891	59	40.0
734	Setto	915	895	896	917	59	40.0
735	Setto	917	896	897	919	59	40.0
736	Setto	919	897	898	876	59	40.0
737	Setto	880	31	874	878	59	40.0
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739	Setto	882	877	879	884	59	40.0
740	Setto	886	899	900	888	59	40.0
741	Setto	888	900	901	890	59	40.0
742	Setto	890	901	902	892	59	40.0
743	Setto	884	879	881	893	59	40.0
744	Setto	893	881	883	894	59	40.0
745	Setto	894	883	885	895	59	40.0
746	Setto	895	885	887	896	59	40.0
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750	Setto	900	868	870	901	59	40.0
751	Setto	901	870	872	902	59	40.0
752	Setto	2	905	904	903	59	40.0
753	Setto	903	904	907	906	59	40.0
754	Setto	906	907	909	908	59	40.0
755	Setto	908	909	911	910	59	40.0
756	Setto	910	911	913	912	59	40.0
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761	Setto	903	920	16	2	55	40.0
762	Setto	906	922	920	903	55	40.0
763	Setto	908	923	922	906	55	40.0
764	Setto	910	924	923	908	55	40.0
765	Setto	912	925	924	910	55	40.0
766	Setto	914	926	925	912	55	40.0
767	Setto	916	927	926	914	55	40.0
768	Setto	918	928	927	916	55	40.0
769	Setto	875	929	928	918	55	40.0
770	Setto	1046	933	932	1045	55	40.0
771	Setto	1040	934	933	1046	55	40.0
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773	Setto	1042	653	3	21	55	40.0
774	Setto	1043	656	653	1042	55	40.0
775	Setto	1044	658	656	1043	55	40.0
776	Setto	927	937	936	926	55	40.0
777	Setto	928	938	937	927	55	40.0
778	Setto	2456	2264	2283	2455	40	30.0
779	Setto	930	660	658	1044	55	40.0
780	Setto	931	662	660	930	55	40.0
781	Setto	932	664	662	931	55	40.0
782	Setto	933	666	664	932	55	40.0
783	Setto	934	668	666	933	55	40.0
784	Setto	935	670	668	934	55	40.0
785	Setto	937	946	945	936	55	40.0
786	Setto	938	947	946	937	55	40.0
787	Setto	939	948	947	938	55	40.0
788	Setto	940	949	18	17	55	40.0
789	Setto	941	950	949	940	55	40.0
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792	Setto	944	953	952	943	55	40.0
793	Setto	945	954	953	944	55	40.0
794	Setto	946	955	954	945	55	40.0
795	Setto	947	956	955	946	55	40.0
796	Setto	948	957	956	947	55	40.0
797	Setto	107	1289	1288	106	54	30.0
798	Setto	106	1288	1290	108	54	30.0
799	Setto	108	1290	958	109	54	30.0
800	Setto	109	958	959	110	54	30.0
801	Setto	110	959	960	111	54	30.0

802	Setto	111	960	1942	112	54	30.0
803	Setto	955	964	963	954	55	40.0
804	Setto	956	965	964	955	55	40.0
805	Setto	957	966	965	956	55	40.0
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807	Setto	1288	113	115	1290	54	30.0
808	Setto	1290	115	116	958	54	30.0
809	Setto	958	116	117	959	54	30.0
810	Setto	959	117	118	960	54	30.0
811	Setto	960	118	119	1942	54	30.0
812	Setto	964	973	972	963	55	40.0
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815	Setto	967	976	592	19	55	40.0
816	Setto	968	977	976	967	55	40.0
817	Setto	969	978	977	968	55	40.0
818	Setto	970	979	978	969	55	40.0
819	Setto	971	980	979	970	55	40.0
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821	Setto	973	982	981	972	55	40.0
822	Setto	974	983	982	973	55	40.0
823	Setto	975	984	983	974	55	40.0
824	Setto	976	985	585	592	55	40.0
825	Setto	977	986	985	976	55	40.0
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829	Setto	981	990	989	980	55	40.0
830	Setto	982	991	990	981	55	40.0
831	Setto	983	992	991	982	55	40.0
832	Setto	984	993	992	983	55	40.0
833	Setto	985	994	578	585	55	40.0
834	Setto	986	995	994	985	55	40.0
835	Setto	987	996	995	986	55	40.0
836	Setto	988	997	996	987	55	40.0
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842	Setto	994	1003	571	578	55	40.0
843	Setto	995	1004	1003	994	55	40.0
844	Setto	996	1005	1004	995	55	40.0
845	Setto	997	1006	1005	996	55	40.0
846	Setto	998	1007	1006	997	55	40.0
847	Setto	999	1008	1007	998	55	40.0
848	Setto	1000	1009	1008	999	55	40.0
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850	Setto	1002	1011	1010	1001	55	40.0
851	Setto	1003	1012	564	571	55	40.0
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853	Setto	1005	1014	1013	1004	55	40.0
854	Setto	1006	1015	1014	1005	55	40.0
855	Setto	1007	1016	1015	1006	55	40.0
856	Setto	1008	1017	1016	1007	55	40.0
857	Setto	1009	1018	1017	1008	55	40.0
858	Setto	1010	1019	1018	1009	55	40.0
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860	Setto	1012	1021	557	564	55	40.0
861	Setto	1013	1023	1021	1012	55	40.0
862	Setto	1014	1024	1023	1013	55	40.0
863	Setto	1015	1025	1024	1014	55	40.0
864	Setto	1016	1026	1025	1015	55	40.0
865	Setto	1017	1027	1026	1016	55	40.0
866	Setto	1018	1028	1027	1017	55	40.0
867	Setto	1019	1029	1028	1018	55	40.0
868	Setto	2412	2402	2401	2411	55	40.0
869	Setto	1021	1031	20	557	55	40.0
870	Setto	1023	1032	1031	1021	55	40.0
871	Setto	1024	1033	1032	1023	55	40.0
872	Setto	1025	1034	1033	1024	55	40.0
873	Setto	1026	1035	1034	1025	55	40.0
874	Setto	1027	1036	1035	1026	55	40.0
875	Setto	1028	1037	1036	1027	55	40.0
876	Setto	1029	1038	1037	1028	55	40.0
877	Setto	1030	1039	1038	1029	55	40.0
878	Setto	1037	1046	1045	1036	55	40.0

879	Setto	1038	1040	1046	1037	55	40.0
880	Setto	1039	1041	1040	1038	55	40.0
881	Setto	1047	1048	1049	29	13	20.0
882	Setto	1050	1051	1048	1047	13	20.0
883	Setto	1052	1053	1051	1050	13	20.0
884	Setto	1054	1055	1053	1052	13	20.0
885	Setto	1056	1057	1055	1054	13	20.0
886	Setto	1058	1059	1057	1056	13	20.0
887	Setto	1060	1061	1059	1058	13	20.0
888	Setto	1062	1063	1061	1060	13	20.0
889	Setto	1064	1065	1063	1062	13	20.0
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891	Setto	1051	1068	1066	1048	13	20.0
892	Setto	1053	1069	1068	1051	13	20.0
893	Setto	1055	1070	1069	1053	13	20.0
894	Setto	1057	1071	1070	1055	13	20.0
895	Setto	1059	1072	1071	1057	13	20.0
896	Setto	1061	1073	1072	1059	13	20.0
897	Setto	1063	1074	1073	1061	13	20.0
898	Setto	1065	1075	1074	1063	13	20.0
899	Setto	1066	1076	1077	1067	13	20.0
900	Setto	1068	1078	1076	1066	13	20.0
901	Setto	1069	1079	1078	1068	13	20.0
902	Setto	1070	1080	1079	1069	13	20.0
903	Setto	1071	1081	1080	1070	13	20.0
904	Setto	1072	1082	1081	1071	13	20.0
905	Setto	1073	1083	1082	1072	13	20.0
906	Setto	1074	1084	1083	1073	13	20.0
907	Setto	1075	1085	1084	1074	13	20.0
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909	Setto	1078	1088	1086	1076	13	20.0
910	Setto	1079	1089	1088	1078	13	20.0
911	Setto	1080	1090	1089	1079	13	20.0
912	Setto	1081	1091	1090	1080	13	20.0
913	Setto	1082	1092	1091	1081	13	20.0
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915	Setto	1084	1094	1093	1083	13	20.0
916	Setto	1085	1095	1094	1084	13	20.0
917	Setto	1086	1096	1097	1087	13	20.0
918	Setto	1088	1098	1096	1086	13	20.0
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921	Setto	1091	1101	1100	1090	13	20.0
922	Setto	1092	1102	1101	1091	13	20.0
923	Setto	1093	481	1102	1092	13	20.0
924	Setto	1094	921	481	1093	13	20.0
925	Setto	1095	1022	921	1094	13	20.0
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928	Setto	1099	728	727	1098	13	20.0
929	Setto	1100	729	728	1099	13	20.0
930	Setto	1101	730	729	1100	13	20.0
931	Setto	1102	737	730	1101	13	20.0
932	Setto	481	738	737	1102	13	20.0
933	Setto	921	739	738	481	13	20.0
934	Setto	1022	740	739	921	13	20.0
935	Setto	1103	1104	38	37	59	40.0
936	Setto	1105	1106	1104	1103	59	40.0
937	Setto	1107	1108	1106	1105	59	40.0
938	Setto	1109	1110	1108	1107	59	40.0
939	Setto	1111	1112	1110	1109	59	40.0
940	Setto	1113	1114	1112	1111	59	40.0
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942	Setto	1117	1118	1116	1115	59	40.0
943	Setto	1119	1120	1118	1117	59	40.0
944	Setto	1157	1162	1160	1155	59	40.0
945	Setto	1159	1164	1162	1157	59	40.0
946	Setto	1161	1166	1164	1159	59	40.0
947	Setto	1163	1121	1166	1161	59	40.0
948	Setto	1165	1122	1121	1163	59	40.0
949	Setto	1114	1126	1125	1112	59	40.0
950	Setto	1116	1127	1126	1114	59	40.0
951	Setto	1118	1128	1127	1116	59	40.0
952	Setto	1120	1129	1128	1118	59	40.0
953	Setto	1167	1123	1122	1165	59	40.0
954	Setto	1168	1124	32	150	59	40.0
955	Setto	1158	1130	1124	1168	59	40.0

956	Setto	1160	1131	1130	1158	59	40.0
957	Setto	1162	1132	1131	1160	59	40.0
958	Setto	1126	1135	1134	1125	59	40.0
959	Setto	1127	1136	1135	1126	59	40.0
960	Setto	1128	1137	1136	1127	59	40.0
961	Setto	1129	1138	1137	1128	59	40.0
962	Setto	1164	1133	1132	1162	59	40.0
963	Setto	1166	1139	1133	1164	59	40.0
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965	Setto	1122	1141	1140	1121	59	40.0
966	Setto	1123	1142	1141	1122	59	40.0
967	Setto	1135	1144	1143	1134	59	40.0
968	Setto	1136	1145	1144	1135	59	40.0
969	Setto	1137	1146	1145	1136	59	40.0
970	Setto	1138	1147	1146	1137	59	40.0
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972	Setto	1152	1153	1150	1149	59	40.0
973	Setto	1154	1155	1153	1152	59	40.0
974	Setto	1156	1157	1155	1154	59	40.0
975	Setto	1143	1159	1157	1156	59	40.0
976	Setto	1144	1161	1159	1143	59	40.0
977	Setto	1145	1163	1161	1144	59	40.0
978	Setto	1146	1165	1163	1145	59	40.0
979	Setto	1147	1167	1165	1146	59	40.0
980	Setto	1150	1168	150	157	59	40.0
981	Setto	1153	1158	1168	1150	59	40.0
982	Setto	1155	1160	1158	1153	59	40.0
983	Setto	36	77	1170	1169	36	40.0
984	Setto	1169	1170	1172	1171	36	40.0
985	Setto	1171	1172	1174	1173	36	40.0
986	Setto	1173	1174	1176	1175	36	40.0
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988	Setto	1177	1178	1180	1179	36	40.0
989	Setto	1179	1180	1182	1181	36	40.0
990	Setto	1181	1182	1184	1183	36	40.0
991	Setto	1183	1184	1186	1185	36	40.0
992	Setto	77	84	1187	1170	36	40.0
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994	Setto	1172	1188	1189	1174	36	40.0
995	Setto	1174	1189	1190	1176	36	40.0
996	Setto	1176	1190	1191	1178	36	40.0
997	Setto	1178	1191	1192	1180	36	40.0
998	Setto	1180	1192	1193	1182	36	40.0
999	Setto	1182	1193	1194	1184	36	40.0
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1002	Setto	1187	1196	1197	1188	36	40.0
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1005	Setto	1190	1199	1200	1191	36	40.0
1006	Setto	1191	1200	1201	1192	36	40.0
1007	Setto	1192	1201	1202	1193	36	40.0
1008	Setto	1193	1202	1203	1194	36	40.0
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1015	Setto	1200	1209	1210	1201	36	40.0
1016	Setto	1201	1210	1211	1202	36	40.0
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1018	Setto	1203	1212	1213	1204	36	40.0
1019	Setto	98	105	1214	1205	36	40.0
1020	Setto	1205	1214	1215	1206	36	40.0
1021	Setto	1206	1215	1216	1207	36	40.0
1022	Setto	1207	1216	1217	1208	36	40.0
1023	Setto	1208	1217	1218	1209	36	40.0
1024	Setto	1209	1218	1219	1210	36	40.0
1025	Setto	1210	1219	1220	1211	36	40.0
1026	Setto	1211	1220	1221	1212	36	40.0
1027	Setto	1212	1221	1222	1213	36	40.0
1028	Setto	105	112	1223	1214	36	40.0
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1031	Setto	1216	1225	1226	1217	36	40.0
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1033	Setto	1218	1227	1228	1219	36	40.0
1034	Setto	1219	1228	1229	1220	36	40.0
1035	Setto	1220	1229	1230	1221	36	40.0
1036	Setto	1221	1230	1231	1222	36	40.0
1037	Setto	1922	1931	1576	1492	55	40.0
1038	Setto	1923	1932	1931	1922	55	40.0
1039	Setto	1924	1933	1932	1923	55	40.0
1040	Setto	1925	1934	1933	1924	55	40.0
1041	Setto	1926	1935	1934	1925	55	40.0
1042	Setto	1927	1936	1935	1926	55	40.0
1043	Setto	1928	1937	1936	1927	55	40.0
1044	Setto	1929	1938	1937	1928	55	40.0
1045	Setto	1930	1939	1938	1929	55	40.0
1046	Setto	119	126	1241	1232	36	40.0
1047	Setto	1232	1241	1242	1233	36	40.0
1048	Setto	1233	1242	1243	1234	36	40.0
1049	Setto	1234	1243	1244	1235	36	40.0
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1062	Setto	1247	1256	1257	1248	36	40.0
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1064	Setto	133	37	1103	1250	36	40.0
1065	Setto	1250	1103	1105	1251	36	40.0
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1067	Setto	1252	1107	1109	1253	36	40.0
1068	Setto	1253	1109	1111	1254	36	40.0
1069	Setto	1254	1111	1113	1255	36	40.0
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1072	Setto	1257	1117	1119	1258	36	40.0
1073	Setto	32	638	1259	1124	59	40.0
1074	Setto	1124	1259	1260	1130	59	40.0
1075	Setto	1130	1260	1261	1131	59	40.0
1076	Setto	1131	1261	1262	1132	59	40.0
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1079	Setto	1139	1264	1265	1140	59	40.0
1080	Setto	1140	1265	1266	1141	59	40.0
1081	Setto	1141	1266	1267	1142	59	40.0
1082	Setto	638	645	1268	1259	59	40.0
1083	Setto	1259	1268	1269	1260	59	40.0
1084	Setto	1260	1269	1270	1261	59	40.0
1085	Setto	1261	1270	1271	1262	59	40.0
1086	Setto	1262	1271	1272	1263	59	40.0
1087	Setto	1263	1272	1273	1264	59	40.0
1088	Setto	1264	1273	1274	1265	59	40.0
1089	Setto	1265	1274	1275	1266	59	40.0
1090	Setto	1266	1275	1276	1267	59	40.0
1091	Setto	645	652	1277	1268	59	40.0
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1093	Setto	1269	1278	1279	1270	59	40.0
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1100	Setto	652	2	903	1277	59	40.0
1101	Setto	1277	903	906	1278	59	40.0
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1103	Setto	1279	908	910	1280	59	40.0
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1115	Setto	1291	1139	1140	1292	59	40.0

1116	Setto	1292	1140	1141	1293	59	40.0
1117	Setto	1293	1141	1142	1294	59	40.0
1124	Setto	1300	1291	1292	1301	59	40.0
1125	Setto	1301	1292	1293	1302	59	40.0
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1127	Setto	280	33	1295	1304	59	40.0
1128	Setto	1304	1295	1296	1305	59	40.0
1129	Setto	1305	1296	1297	1306	59	40.0
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1131	Setto	1307	1298	1299	1308	59	40.0
1132	Setto	1308	1299	1300	1309	59	40.0
1133	Setto	1309	1300	1301	1310	59	40.0
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1136	Setto	273	280	1304	1313	59	40.0
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1142	Setto	1318	1309	1310	1319	59	40.0
1143	Setto	1319	1310	1311	1320	59	40.0
1144	Setto	1320	1311	1312	1321	59	40.0
1145	Setto	266	273	1313	1322	59	40.0
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1159	Setto	1335	1326	1327	1336	59	40.0
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1171	Setto	1347	1338	1339	1348	59	40.0
1172	Setto	245	252	1340	1349	59	40.0
1173	Setto	1349	1340	1341	1350	59	40.0
1174	Setto	1350	1341	1342	1351	59	40.0
1175	Setto	1351	1342	1343	1352	59	40.0
1176	Setto	1352	1343	1344	1353	59	40.0
1177	Setto	1353	1344	1345	1354	59	40.0
1178	Setto	1354	1345	1346	1355	59	40.0
1179	Setto	1355	1346	1347	1356	59	40.0
1180	Setto	1356	1347	1348	1357	59	40.0
1181	Setto	238	245	1349	1358	59	40.0
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1184	Setto	1360	1351	1352	1361	59	40.0
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1189	Setto	1365	1356	1357	1366	59	40.0
1190	Setto	231	238	1358	1367	59	40.0
1191	Setto	1367	1358	1359	1368	59	40.0
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1193	Setto	1369	1360	1361	1370	59	40.0
1194	Setto	1370	1361	1362	1371	59	40.0
1195	Setto	1371	1362	1363	1372	59	40.0
1196	Setto	1372	1363	1364	1373	59	40.0
1197	Setto	1373	1364	1365	1374	59	40.0
1198	Setto	1374	1365	1366	1375	59	40.0

1199	Setto	1	231	1367	1376	59	40.0
1200	Setto	1376	1367	1368	1377	59	40.0
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1202	Setto	1378	1369	1370	1379	59	40.0
1203	Setto	1379	1370	1371	1380	59	40.0
1204	Setto	1380	1371	1372	1381	59	40.0
1205	Setto	1381	1372	1373	1382	59	40.0
1206	Setto	1382	1373	1374	1383	59	40.0
1207	Setto	1383	1374	1375	1384	59	40.0
1208	Setto	1169	1385	188	36	36	40.0
1209	Setto	1171	1386	1385	1169	36	40.0
1210	Setto	1173	1387	1386	1171	36	40.0
1211	Setto	1175	1388	1387	1173	36	40.0
1212	Setto	1177	1389	1388	1175	36	40.0
1213	Setto	1179	1390	1389	1177	36	40.0
1214	Setto	1181	1391	1390	1179	36	40.0
1215	Setto	1183	1392	1391	1181	36	40.0
1216	Setto	1185	1393	1392	1183	36	40.0
1217	Setto	1385	1394	35	188	36	40.0
1218	Setto	1386	1395	1394	1385	36	40.0
1219	Setto	1387	1396	1395	1386	36	40.0
1220	Setto	1388	1397	1396	1387	36	40.0
1221	Setto	1389	1398	1397	1388	36	40.0
1222	Setto	1390	1399	1398	1389	36	40.0
1223	Setto	1391	1400	1399	1390	36	40.0
1224	Setto	1392	1401	1400	1391	36	40.0
1225	Setto	1393	1402	1401	1392	36	40.0
1226	Setto	1394	1403	200	35	36	40.0
1227	Setto	1395	1404	1403	1394	36	40.0
1228	Setto	1396	1405	1404	1395	36	40.0
1229	Setto	1227	1946	1947	1228	36	40.0
1230	Setto	1228	1947	1948	1229	36	40.0
1231	Setto	1229	1948	1949	1230	36	40.0
1232	Setto	1400	1409	1408	1399	36	40.0
1233	Setto	1401	1410	1409	1400	36	40.0
1234	Setto	1402	1411	1410	1401	36	40.0
1235	Setto	1403	1412	207	200	36	40.0
1236	Setto	1404	1413	1412	1403	36	40.0
1237	Setto	1405	1414	1413	1404	36	40.0
1238	Setto	1230	1949	1950	1231	36	40.0
1239	Setto	1942	119	1232	1941	36	40.0
1240	Setto	1941	1232	1233	1943	36	40.0
1241	Setto	1409	1418	1417	1408	36	40.0
1242	Setto	1410	1419	1418	1409	36	40.0
1243	Setto	1411	1420	1419	1410	36	40.0
1244	Setto	1412	1421	34	207	36	40.0
1245	Setto	1413	1422	1421	1412	36	40.0
1246	Setto	1414	1423	1422	1413	36	40.0
1247	Setto	1943	1233	1234	1944	36	40.0
1248	Setto	1944	1234	1235	1945	36	40.0
1249	Setto	1945	1235	1236	1946	36	40.0
1250	Setto	1418	1427	1426	1417	36	40.0
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1252	Setto	1420	1429	1428	1419	36	40.0
1253	Setto	1421	1430	219	34	36	40.0
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1255	Setto	1423	1432	1431	1422	36	40.0
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1261	Setto	1429	1438	1437	1428	36	40.0
1262	Setto	1430	1376	1	219	36	40.0
1263	Setto	1431	1377	1376	1430	36	40.0
1264	Setto	1432	1378	1377	1431	36	40.0
1265	Setto	1433	1379	1378	1432	36	40.0
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1267	Setto	1435	1381	1380	1434	36	40.0
1268	Setto	1436	1382	1381	1435	36	40.0
1269	Setto	1437	1383	1382	1436	36	40.0
1270	Setto	1438	1384	1383	1437	36	40.0
1271	Setto	1376	1439	295	1	34	40.0
1272	Setto	1377	1440	1439	1376	34	40.0
1273	Setto	1378	1441	1440	1377	34	40.0
1274	Setto	1379	1442	1441	1378	34	40.0
1275	Setto	1380	1443	1442	1379	34	40.0

1276	Setto	1381	1444	1443	1380	34	40.0
1277	Setto	1382	1445	1444	1381	34	40.0
1278	Setto	1383	1446	1445	1382	34	40.0
1279	Setto	1384	1447	1446	1383	34	40.0
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1281	Setto	1440	1449	1448	1439	34	40.0
1282	Setto	1441	1450	1449	1440	34	40.0
1283	Setto	1442	1451	1450	1441	34	40.0
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1288	Setto	1447	1456	1455	1446	34	40.0
1289	Setto	1448	1457	358	5	34	40.0
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1291	Setto	1567	1526	1544	1566	34	40.0
1292	Setto	1151	1148	1526	1567	34	40.0
1293	Setto	1577	1536	320		34	40.0
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1295	Setto	1538	1579	1578	1536	34	40.0
1296	Setto	1545	1580	1579	1538	34	40.0
1297	Setto	1456	1465	1464	1455	34	40.0
1298	Setto	1457	1466	1467	358	34	40.0
1299	Setto	1458	1468	1466	1457	34	40.0
1300	Setto	1559	1151	1567	1558	34	40.0
1301	Setto	1460	1524	4	307	55	40.0
1302	Setto	1461	1569	1524	1460	55	40.0
1303	Setto	1472	1570	1569	1461	55	40.0
1304	Setto	1473	1571	1570	1472	55	40.0
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1306	Setto	1465	1475	1474	1464	34	40.0
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1308	Setto	1468	1478	1476	1466	34	40.0
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1310	Setto	1481	1574	1573	1480	55	40.0
1311	Setto	1491	1575	1574	1481	55	40.0
1312	Setto	1492	1576	1575	1491	55	40.0
1313	Setto	1547	1459	1590	1546	34	40.0
1314	Setto	1548	1460	307	10	55	40.0
1315	Setto	1475	1485	1484	1474	34	40.0
1316	Setto	1476	1486	379	1477	34	40.0
1317	Setto	1478	1487	1486	1476	34	40.0
1318	Setto	1553	1461	1460	1548	55	40.0
1319	Setto	1554	1472	1461	1553	55	40.0
1320	Setto	1555	1473	1472	1554	55	40.0
1321	Setto	1556	1479	1473	1555	55	40.0
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1324	Setto	1485	1494	1493	1484	34	40.0
1325	Setto	1486	1495	6	379	34	40.0
1326	Setto	1487	1496	1495	1486	34	40.0
1327	Setto	1590	1491	1481	1589	55	40.0
1328	Setto	1578	1587	414	9	34	40.0
1329	Setto	1579	1588	1587	1578	34	40.0
1330	Setto	1528	1547	1546	1527	34	40.0
1331	Setto	1534	1548	10	12	34	40.0
1332	Setto	1535	1553	1548	1534	34	40.0
1333	Setto	1494	1503	1502	1493	34	40.0
1334	Setto	1495	1504	333	6	34	40.0
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1339	Setto	1500	1509	1508	1499	34	40.0
1340	Setto	1501	1510	1509	1500	34	40.0
1341	Setto	1502	1511	1510	1501	34	40.0
1342	Setto	1503	1512	1511	1502	34	40.0
1343	Setto	1504	1513	7	333	34	40.0
1344	Setto	1505	1514	1513	1504	34	40.0
1345	Setto	1506	1515	1514	1505	34	40.0
1346	Setto	1507	1516	1515	1506	34	40.0
1347	Setto	1508	1517	1516	1507	34	40.0
1348	Setto	1509	1518	1517	1508	34	40.0
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1350	Setto	1511	1520	1519	1510	34	40.0
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1354	Setto	1525	1581	1580	1545	34	40.0
1355	Setto	1537	1582	1581	1525	34	40.0
1356	Setto	1568	1583	1582	1537	34	40.0
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1359	Setto	1588	1471	1469	1587	34	40.0
1360	Setto	1521	1530	1529	1520	34	40.0
1361	Setto	1522	1531	1532	386	34	40.0
1362	Setto	1523	1533	1531	1522	34	40.0
1363	Setto	1544	1584	1583	1568	34	40.0
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1366	Setto	1577	320	319		54	40.0
1367	Setto	8	1577	319	313	54	40.0
1368	Setto	1560	1536	1577	8	34	40.0
1369	Setto	1530	1540	1539	1529	34	40.0
1370	Setto	1531	1541	1542	1532	34	40.0
1371	Setto	1533	1543	1541	1531	34	40.0
1372	Setto	1463	1483	1482	1462	34	40.0
1373	Setto	1469	1488	1489	1470	34	40.0
1374	Setto	1471	1490	1488	1469	34	40.0
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1377	Setto	1563	1525	1545	1562	34	40.0
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1379	Setto	1541	1551	407	1542	34	40.0
1380	Setto	1543	1552	1551	1541	34	40.0
1381	Setto	1564	1537	1525	1563	34	40.0
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1387	Setto	1550	1559	1558	1549	34	40.0
1388	Setto	1551	1560	8	407	34	40.0
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1390	Setto	533	3	653	1591	36	40.0
1391	Setto	1591	653	656	1592	36	40.0
1392	Setto	1592	656	658	1593	36	40.0
1393	Setto	1593	658	660	1594	36	40.0
1394	Setto	1594	660	662	1595	36	40.0
1395	Setto	1595	662	664	1596	36	40.0
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1397	Setto	1597	666	668	1598	36	40.0
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1399	Setto	1601	533	1591	1600	36	40.0
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1433	Setto	1634	1625	1626	1635	36	40.0
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1471	Setto	467	473	1665	1674	36	40.0
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1474	Setto	1676	1667	1668	1677	36	40.0
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1537	Setto	1737	1748	1747	1735	55	40.0
1538	Setto	1739	1749	1748	1737	55	40.0
1539	Setto	1741	1750	1749	1739	55	40.0
1542	Setto	1744	1753	1752	1743	55	40.0
1543	Setto	1745	1754	1753	1744	55	40.0
1544	Setto	1746	1755	1754	1745	55	40.0
1545	Setto	1747	1756	1755	1746	55	40.0
1546	Setto	1748	1757	1756	1747	55	40.0
1548	Setto	1750	1759	1758	1749	55	40.0
1551	Setto	2157	2187	1898	2212	34	38.0
1552	Setto	1892	1763	2247	1891	34	38.0
1553	Setto	1989	1889	1763	1892	34	38.0
1554	Setto	2218	2161	2159	2213	34	38.0
1555	Setto	2137	2230	2231	2138	34	38.0
1556	Setto	1900	1766	1762	1899	34	38.0
1557	Setto	1759	1768	1767	1758	55	40.0
1560	Setto	758	1772	2126	759	34	38.0
1561	Setto	2100	2137	2138	2101	34	38.0
1562	Setto	1991	1773	1774	2151	34	25.0
1563	Setto	2132	2242	2243	2148	34	38.0
1564	Setto	2127	2175	2176	2192	34	38.0
1565	Setto	2047	2132	2148	2097	34	25.0
1566	Setto	1768	1777	1776	1767	55	40.0
1569	Setto	1992	1775	1773	1991	34	25.0
1570	Setto	2220	2163	2161	2218	34	38.0
1571	Setto	2222	2165	2163	2220	34	38.0
1572	Setto	2224	2167	2165	2222	34	38.0
1573	Setto	2226	2169	2167	2224	34	38.0
1574	Setto	2133	1900	1899	2123	34	38.0
1575	Setto	1777	1786	1785	1776	55	40.0
1578	Setto	1780	1789	1788	1779	55	40.0
1579	Setto	1781	1790	1789	1780	55	40.0
1580	Setto	1782	1791	1790	1781	55	40.0
1581	Setto	1783	1792	1791	1782	55	40.0
1582	Setto	1784	1793	1792	1783	55	40.0
1584	Setto	1786	1795	1794	1785	55	40.0
1585	Setto	1787	1796	1512	1503	55	40.0
1586	Setto	1788	1797	1796	1787	55	40.0
1587	Setto	1789	1798	1797	1788	55	40.0
1588	Setto	1790	1799	1798	1789	55	40.0
1589	Setto	1791	1800	1799	1790	55	40.0
1590	Setto	1792	1801	1800	1791	55	40.0
1591	Setto	1793	1802	1801	1792	55	40.0
1594	Setto	1796	1805	1521	1512	55	40.0
1595	Setto	1797	1806	1805	1796	55	40.0
1596	Setto	1798	1807	1806	1797	55	40.0
1597	Setto	1799	1808	1807	1798	55	40.0
1598	Setto	1800	1809	1808	1799	55	40.0
1599	Setto	1801	1810	1809	1800	55	40.0
1600	Setto	1802	1811	1810	1801	55	40.0
1603	Setto	1805	1814	1530	1521	55	40.0

1604	Setto	1806	1815	1814	1805	55	40.0
1605	Setto	1807	1816	1815	1806	55	40.0
1606	Setto	1808	1817	1816	1807	55	40.0
1607	Setto	1809	1818	1817	1808	55	40.0
1608	Setto	1810	1819	1818	1809	55	40.0
1609	Setto	1811	1820	1819	1810	55	40.0
1610	Setto	1812	1821	1820	1811	55	40.0
1611	Setto	1813	1822	1821	1812	55	40.0
1612	Setto	1814	1823	1540	1530	55	40.0
1613	Setto	1815	1824	1823	1814	55	40.0
1614	Setto	1816	1825	1824	1815	55	40.0
1615	Setto	1817	1826	1825	1816	55	40.0
1616	Setto	1818	1827	1826	1817	55	40.0
1617	Setto	1819	1828	1827	1818	55	40.0
1618	Setto	1820	1829	1828	1819	55	40.0
1619	Setto	1821	1830	1829	1820	55	40.0
1620	Setto	1822	1831	1830	1821	55	40.0
1621	Setto	1823	1832	1550	1540	55	40.0
1622	Setto	1824	1833	1832	1823	55	40.0
1623	Setto	1825	1834	1833	1824	55	40.0
1624	Setto	1826	1835	1834	1825	55	40.0
1625	Setto	1827	1836	1835	1826	55	40.0
1626	Setto	1828	1837	1836	1827	55	40.0
1627	Setto	1829	1838	1837	1828	55	40.0
1628	Setto	1830	1839	1838	1829	55	40.0
1629	Setto	1831	1840	1839	1830	55	40.0
1630	Setto	1832	1841	1559	1550	55	40.0
1631	Setto	1833	1842	1841	1832	55	40.0
1632	Setto	1834	1843	1842	1833	55	40.0
1633	Setto	1835	1844	1843	1834	55	40.0
1634	Setto	1836	1845	1844	1835	55	40.0
1635	Setto	1837	1846	1845	1836	55	40.0
1636	Setto	1838	1847	1846	1837	55	40.0
1637	Setto	1839	1848	1847	1838	55	40.0
1638	Setto	1840	1849	1848	1839	55	40.0
1639	Setto	1841	1850	1151	1559	55	40.0
1640	Setto	1842	1851	1850	1841	55	40.0
1641	Setto	1843	1852	1851	1842	55	40.0
1642	Setto	1844	1853	1852	1843	55	40.0
1643	Setto	1845	1854	1853	1844	55	40.0
1644	Setto	1846	1855	1854	1845	55	40.0
1645	Setto	1847	1856	1855	1846	55	40.0
1646	Setto	1848	1857	1856	1847	55	40.0
1647	Setto	1849	1858	1857	1848	55	40.0
1648	Setto	1850	1859	1148	1151	55	40.0
1649	Setto	1851	1860	1859	1850	55	40.0
1650	Setto	1852	1861	1860	1851	55	40.0
1651	Setto	1853	1862	1861	1852	55	40.0
1652	Setto	1854	1863	1862	1853	55	40.0
1653	Setto	1855	1864	1863	1854	55	40.0
1654	Setto	1856	1865	1864	1855	55	40.0
1655	Setto	1857	1866	1865	1856	55	40.0
1656	Setto	1858	1867	1866	1857	55	40.0
1657	Setto	1859	1868	1586	1148	55	40.0
1658	Setto	1860	1869	1868	1859	55	40.0
1659	Setto	1861	1870	1869	1860	55	40.0
1660	Setto	1862	1871	1870	1861	55	40.0
1661	Setto	1863	1872	1871	1862	55	40.0
1662	Setto	1864	1873	1872	1863	55	40.0
1663	Setto	1865	1874	1873	1864	55	40.0
1664	Setto	1866	1875	1874	1865	55	40.0
1665	Setto	1867	1876	1875	1866	55	40.0
1666	Setto	1868	1877	1463	1586	55	40.0
1667	Setto	1869	1878	1877	1868	55	40.0
1668	Setto	1870	1879	1878	1869	55	40.0
1669	Setto	1871	1880	1879	1870	55	40.0
1670	Setto	1872	1881	1880	1871	55	40.0
1671	Setto	1873	1882	1881	1872	55	40.0
1672	Setto	1874	1883	1882	1873	55	40.0
1673	Setto	1875	1884	1883	1874	55	40.0
1674	Setto	1876	1885	1884	1875	55	40.0
1675	Setto	1877	1886	1483	1463	55	40.0
1676	Setto	1878	1887	1886	1877	55	40.0
1677	Setto	2142	2244	2242	2132	34	38.0
1678	Setto	2098	2142	2132	2047	34	25.0
1679	Setto	2241	2178	2179	1771	34	38.0
1680	Setto	2159	1991	2151	2155	34	38.0

1681	Setto	2161	1992	1991	2159	34	38.0
1682	Setto	2240	2177	2178	2241	34	38.0
1683	Setto	1885	1894	1893	1884	55	40.0
1684	Setto	1886	1895	1528	1483	55	40.0
1685	Setto	1887	1896	1895	1886	55	40.0
1686	Setto	1775	2140	2139	1773	34	25.0
1687	Setto	2163	1993	1992	2161	34	38.0
1688	Setto	2125	1989	1892	2124	34	38.0
1689	Setto	1764	2245	2244	2142	34	38.0
1690	Setto	2192	2176	2177	2240	34	38.0
1691	Setto	1990	2122	2044	1901	34	25.0
1692	Setto	1894	1903	1902	1893	55	40.0
1693	Setto	1895	1904	1547	1528	55	40.0
1694	Setto	1896	1905	1904	1895	55	40.0
1695	Setto	2128	2047	2097	2149	34	25.0
1696	Setto	2129	2098	2047	2128	34	25.0
1697	Setto	2165	1890	1993	2163	34	38.0
1698	Setto	2167	2045	1890	2165	34	38.0
1699	Setto	2169	2123	2045	2167	34	38.0
1700	Setto	2171	2133	2123	2169	34	38.0
1701	Setto	1903	1912	1911	1902	55	40.0
1702	Setto	1904	1913	1459	1547	55	40.0
1703	Setto	1905	1914	1913	1904	55	40.0
1704	Setto	1906	1915	1914	1905	55	40.0
1705	Setto	1907	1916	1915	1906	55	40.0
1706	Setto	1908	1917	1916	1907	55	40.0
1707	Setto	1909	1918	1917	1908	55	40.0
1708	Setto	1910	1919	1918	1909	55	40.0
1709	Setto	1911	1920	1919	1910	55	40.0
1710	Setto	1912	1921	1920	1911	55	40.0
1711	Setto	1913	1922	1492	1459	55	40.0
1712	Setto	1914	1923	1922	1913	55	40.0
1713	Setto	1915	1924	1923	1914	55	40.0
1714	Setto	1916	1925	1924	1915	55	40.0
1715	Setto	1917	1926	1925	1916	55	40.0
1716	Setto	1918	1927	1926	1917	55	40.0
1717	Setto	1919	1928	1927	1918	55	40.0
1718	Setto	1920	1929	1928	1919	55	40.0
1719	Setto	112	1942	1941	1223	36	40.0
1720	Setto	1223	1941	1943	1224	36	40.0
1721	Setto	1224	1943	1944	1225	36	40.0
1722	Setto	1225	1944	1945	1226	36	40.0
1723	Setto	1226	1945	1946	1227	36	40.0
1724	Setto	1576	1718	1978	1931	36	40.0
1725	Setto	1931	1978	1979	1932	36	40.0
1726	Setto	1932	1979	1980	1933	36	40.0
1727	Setto	1933	1980	1981	1934	36	40.0
1728	Setto	1934	1981	1982	1935	36	40.0
1729	Setto	1935	1982	1983	1936	36	40.0
1730	Setto	1936	1983	1984	1937	36	40.0
1733	Setto	1718	685	1987	1978	36	40.0
1734	Setto	1978	1987	1988	1979	36	40.0
1735	Setto	2136	2125	2124	2135	34	38.0
1736	Setto	24	2183	2127	753	34	38.0
1737	Setto	753	2127	2192	754	34	38.0
1738	Setto	1765	2246	2245	1764	34	38.0
1739	Setto	1901	2044	2043	2143	34	25.0
1740	Setto	2172	2188	2187	2157	34	38.0
1741	Setto	1985	1994	1995	1986	36	40.0
1742	Setto	685	1709	1996	1987	36	40.0
1743	Setto	1987	1996	1997	1988	36	40.0
1744	Setto	2139	2128	2149	2150	34	38.0
1745	Setto	2140	2129	2128	2139	34	38.0
1746	Setto	2141	2130	2129	2140	34	38.0
1747	Setto	2144	2131	2130	2141	34	38.0
1748	Setto	2213	2159	2155	2216	34	38.0
1749	Setto	2145	2134	2131	2144	34	38.0
1750	Setto	1994	2003	2004	1995	36	40.0
1751	Setto	1709	1700	2005	1996	36	40.0
1752	Setto	1996	2005	2006	1997	36	40.0
1753	Setto	1997	2006	2007	1998	36	40.0
1754	Setto	1998	2007	2008	1999	36	40.0
1755	Setto	1999	2008	2009	2000	36	40.0
1756	Setto	2000	2009	2010	2001	36	40.0
1757	Setto	2001	2010	2011	2002	36	40.0
1758	Setto	2002	2011	2012	2003	36	40.0
1759	Setto	2003	2012	2013	2004	36	40.0

1760	Setto	1700	1691	2014	2005	36	40.0
1761	Setto	2005	2014	2015	2006	36	40.0
1762	Setto	2006	2015	2016	2007	36	40.0
1763	Setto	2007	2016	2017	2008	36	40.0
1764	Setto	2008	2017	2018	2009	36	40.0
1765	Setto	2009	2018	2019	2010	36	40.0
1766	Setto	2010	2019	2020	2011	36	40.0
1767	Setto	2011	2020	2021	2012	36	40.0
1768	Setto	2012	2021	2022	2013	36	40.0
1769	Setto	1691	1682	2023	2014	36	40.0
1770	Setto	2014	2023	2024	2015	36	40.0
1771	Setto	2015	2024	2025	2016	36	40.0
1772	Setto	2016	2025	2026	2017	36	40.0
1773	Setto	2017	2026	2027	2018	36	40.0
1774	Setto	2018	2027	2028	2019	36	40.0
1775	Setto	2019	2028	2029	2020	36	40.0
1776	Setto	2020	2029	2030	2021	36	40.0
1777	Setto	2021	2030	2031	2022	36	40.0
1778	Setto	1682	1673	2032	2023	36	40.0
1779	Setto	2023	2032	2033	2024	36	40.0
1780	Setto	2024	2033	2034	2025	36	40.0
1781	Setto	2025	2034	2035	2026	36	40.0
1782	Setto	2026	2035	2036	2027	36	40.0
1783	Setto	2027	2036	2037	2028	36	40.0
1784	Setto	2028	2037	2038	2029	36	40.0
1785	Setto	2029	2038	2039	2030	36	40.0
1786	Setto	2030	2039	2040	2031	36	40.0
1787	Setto	1673	1664	2041	2032	36	40.0
1788	Setto	2032	2041	2042	2033	36	40.0
1789	Setto	2106	2115	2116	2107	36	40.0
1790	Setto	2107	2116	2117	2108	36	40.0
1791	Setto	2108	2117	2118	2109	36	40.0
1792	Setto	2109	2118	2119	2110	36	40.0
1795	Setto	2039	2048	2049	2040	36	40.0
1796	Setto	1664	1654	2050	2041	36	40.0
1797	Setto	2041	2050	2051	2042	36	40.0
1798	Setto	1891	2247	2246	1765	34	38.0
1799	Setto	1762	2135	2134	2145	34	38.0
1800	Setto	1766	2136	2135	1762	34	38.0
1801	Setto	2174	2189	2188	2172	34	38.0
1802	Setto	2182	2046	2189	2174	34	38.0
1803	Setto	1773	2139	2150	1774	34	25.0
1804	Setto	2048	2057	2058	2049	36	40.0
1805	Setto	1654	1645	2059	2050	36	40.0
1806	Setto	2050	2059	2060	2051	36	40.0
1807	Setto	2051	2060	2061	2052	36	40.0
1808	Setto	2052	2061	2062	2053	36	40.0
1809	Setto	2053	2062	2063	2054	36	40.0
1810	Setto	2054	2063	2064	2055	36	40.0
1811	Setto	2055	2064	2065	2056	36	40.0
1812	Setto	2056	2065	2066	2057	36	40.0
1813	Setto	2057	2066	2067	2058	36	40.0
1814	Setto	1645	1636	2068	2059	36	40.0
1815	Setto	2059	2068	2069	2060	36	40.0
1816	Setto	2060	2069	2070	2061	36	40.0
1817	Setto	2061	2070	2071	2062	36	40.0
1818	Setto	2062	2071	2072	2063	36	40.0
1819	Setto	2063	2072	2073	2064	36	40.0
1820	Setto	2064	2073	2074	2065	36	40.0
1821	Setto	2065	2074	2075	2066	36	40.0
1822	Setto	2066	2075	2076	2067	36	40.0
1823	Setto	1636	1627	2077	2068	36	40.0
1824	Setto	2068	2077	2078	2069	36	40.0
1825	Setto	2069	2078	2079	2070	36	40.0
1826	Setto	2070	2079	2080	2071	36	40.0
1827	Setto	2071	2080	2081	2072	36	40.0
1828	Setto	2072	2081	2082	2073	36	40.0
1829	Setto	2073	2082	2083	2074	36	40.0
1830	Setto	2074	2083	2084	2075	36	40.0
1831	Setto	2075	2084	2085	2076	36	40.0
1832	Setto	1627	1618	2086	2077	36	40.0
1833	Setto	2077	2086	2087	2078	36	40.0
1834	Setto	2078	2087	2088	2079	36	40.0
1835	Setto	2079	2088	2089	2080	36	40.0
1836	Setto	2080	2089	2090	2081	36	40.0
1837	Setto	2081	2090	2091	2082	36	40.0
1838	Setto	2082	2091	2092	2083	36	40.0

1839	Setto	2083	2092	2093	2084	36	40.0
1840	Setto	2084	2093	2094	2085	36	40.0
1841	Setto	1618	1609	2095	2086	36	40.0
1842	Setto	2086	2095	2096	2087	36	40.0
1843	Setto	1609	1599	2104	2095	36	40.0
1844	Setto	2095	2104	2105	2096	36	40.0
1845	Setto	2104	2113	2114	2105	36	40.0
1846	Setto	2105	2114	2115	2106	36	40.0
1847	Setto	2102	2111	2112	2103	36	40.0
1848	Setto	1599	670	2113	2104	36	40.0
1849	Setto	753	830	831	24	34	42.0
1850	Setto	2201	1990	1901	2158	34	25.0
1851	Setto	2158	1901	2143	2160	34	25.0
1852	Setto	2189	2226	2224	2188	34	38.0
1853	Setto	2046	2099	2226	2189	34	38.0
1854	Setto	756	2241	1771	757	34	38.0
1855	Setto	757	1771	1772	758	34	38.0
1856	Setto	2168	2100	2101	2170	34	38.0
1857	Setto	1771	2179	2180	1772	34	38.0
1858	Setto	2202	2146	2152	2193	34	38.0
1859	Setto	28	2201	2158	766	34	38.0
1860	Setto	766	2158	2160	727	34	38.0
1861	Setto	727	2160	2162	728	34	38.0
1862	Setto	728	2162	2164	729	34	38.0
1863	Setto	729	2164	2166	730	34	38.0
1864	Setto	730	2166	2168	737	34	38.0
1865	Setto	737	2168	2170	738	34	38.0
1866	Setto	2210	2173	2146	2202	34	38.0
1867	Setto	2211	2212	2173	2210	34	38.0
1868	Setto	2154	2185	2184	2175	34	25.0
1869	Setto	2175	2184	2186	2176	34	25.0
1870	Setto	2099	2171	2169	2226	34	38.0
1871	Setto	754	2192	2240	755	34	38.0
1872	Setto	755	2240	2241	756	34	38.0
1873	Setto	1888	2213	2216	2156	34	38.0
1874	Setto	2180	2190	2191	2181	34	38.0
1875	Setto	2228	2157	2212	2211	34	38.0
1876	Setto	2229	2172	2157	2228	34	38.0
1877	Setto	2185	2153	2194	2184	34	25.0
1878	Setto	2184	2194	2195	2186	34	25.0
1879	Setto	1897	2218	2213	1888	34	38.0
1880	Setto	1898	2220	2218	1897	34	38.0
1881	Setto	2187	2222	2220	1898	34	38.0
1882	Setto	2188	2224	2222	2187	34	38.0
1883	Setto	2190	2199	2200	2191	34	38.0
1884	Setto	2230	2174	2172	2229	34	38.0
1885	Setto	2231	2182	2174	2230	34	38.0
1886	Setto	2153	2147	2203	2194	34	38.0
1887	Setto	2194	2203	2204	2195	34	38.0
1888	Setto	2195	2204	2205	2196	34	38.0
1889	Setto	2196	2205	2206	2197	34	38.0
1890	Setto	2197	2206	2207	2198	34	38.0
1891	Setto	2198	2207	2208	2199	34	38.0
1892	Setto	2199	2208	2209	2200	34	38.0
1893	Setto	1772	2180	2181	2126	34	38.0
1894	Setto	2183	2154	2175	2127	34	38.0
1895	Setto	2214	2203	2147	2215	34	38.0
1896	Setto	2217	2204	2203	2214	34	38.0
1897	Setto	2219	2205	2204	2217	34	38.0
1898	Setto	2221	2206	2205	2219	34	38.0
1899	Setto	2223	2207	2206	2221	34	38.0
1900	Setto	2225	2208	2207	2223	34	38.0
1901	Setto	2227	2209	2208	2225	34	38.0
1902	Setto	2122	2193	2202	2044	34	25.0
1903	Setto	2044	2202	2210	2043	34	25.0
1904	Setto	2232	2214	2215	2233	34	38.0
1905	Setto	2234	2217	2214	2232	34	38.0
1906	Setto	2235	2219	2217	2234	34	38.0
1907	Setto	2236	2221	2219	2235	34	38.0
1908	Setto	2237	2223	2221	2236	34	38.0
1909	Setto	2238	2225	2223	2237	34	38.0
1910	Setto	2239	2227	2225	2238	34	38.0
1911	Setto	2146	1888	2156	2152	34	38.0
1912	Setto	2173	1897	1888	2146	34	38.0
1913	Setto	2242	2232	2233	2243	34	38.0
1914	Setto	2244	2234	2232	2242	34	38.0
1915	Setto	2245	2235	2234	2244	34	38.0

1916	Setto	2246	2236	2235	2245	34	38.0
1917	Setto	2247	2237	2236	2246	34	38.0
1918	Setto	1763	2238	2237	2247	34	38.0
1919	Setto	1889	2239	2238	1763	34	38.0
1920	Setto	2212	1898	1897	2173	34	38.0
1921	Setto	670	671	2248	2113	40	30.0
1922	Setto	2113	2248	2249	2114	40	30.0
1923	Setto	3328	3325	3323	3327	55	40.0
1924	Setto	3329	3326	3325	3328	56	40.0
1925	Setto	3330	3327	2304	2313	55	40.0
1926	Setto	3331	3328	3327	3330	55	40.0
1927	Setto	3332	3329	3328	3331	56	40.0
1928	Setto	3333	3330	2313	2322	55	40.0
1929	Setto	3334	3331	3330	3333	55	40.0
1930	Setto	671	680	2257	2248	40	30.0
1931	Setto	2248	2257	2258	2249	40	30.0
1932	Setto	2250	3332	3331	3334	56	40.0
1933	Setto	929	2405	938	928	55	40.0
1934	Setto	2251	3333	2322	2407	55	40.0
1935	Setto	2252	3334	3333	2251	55	40.0
1936	Setto	2253	2250	3334	2252	56	40.0
1937	Setto	2455	2283	2282	2481	40	30.0
1938	Setto	709	684	2274	2284	40	30.0
1939	Setto	680	690	2266	2257	40	30.0
1940	Setto	2257	2266	2267	2258	40	30.0
1941	Setto	2254	2251	2407	2331	55	40.0
1942	Setto	2255	2252	2251	2254	55	40.0
1943	Setto	2256	2253	2252	2255	56	40.0
1944	Setto	2259	2254	2331	2340	55	40.0
1945	Setto	2284	2274	2281	2285	40	30.0
1946	Setto	2260	2255	2254	2259	55	40.0
1947	Setto	2261	2256	2255	2260	56	40.0
1948	Setto	690	699	2275	2266	40	30.0
1949	Setto	2266	2275	2276	2267	40	30.0
1950	Setto	2262	2259	2340	2398	55	40.0
1951	Setto	2263	2260	2259	2262	55	40.0
1952	Setto	2265	2261	2260	2263	56	40.0
1953	Setto	2268	2262	2398	2349	55	40.0
1954	Setto	3322	2263	2262	2268	55	40.0
1955	Setto	2278	2279	2270	3246	55	25.0
1956	Setto	2481	2282	2281	2480	40	30.0
1957	Setto	699	709	2284	2275	40	30.0
1958	Setto	2275	2284	2285	2276	40	30.0
1959	Setto	286	287	3319	3315	55	25.0
1960	Setto	2405	939	938		55	40.0
1961	Setto	288	3324	287	286	55	25.0
1962	Setto	2277	3159	3324	288	55	25.0
1963	Setto	2287	2113	670	935	55	40.0
1964	Setto	2288	2114	2113	2287	55	40.0
1965	Setto	2289	2115	2114	2288	55	40.0
1966	Setto	2290	2116	2115	2289	55	40.0
1967	Setto	2291	2117	2116	2290	55	40.0
1968	Setto	2292	2118	2117	2291	55	40.0
1969	Setto	2293	2119	2118	2292	55	40.0
1970	Setto	2294	2120	2119	2293	55	40.0
1971	Setto	2295	2121	2120	2294	55	40.0
1972	Setto	2296	2287	935	1041	55	40.0
1973	Setto	2297	2288	2287	2296	55	40.0
1974	Setto	2298	2289	2288	2297	55	40.0
1975	Setto	2299	2290	2289	2298	55	40.0
1976	Setto	2300	2291	2290	2299	55	40.0
1977	Setto	2301	2292	2291	2300	55	40.0
1978	Setto	2302	2293	2292	2301	55	40.0
1979	Setto	2303	2294	2293	2302	55	40.0
1980	Setto	2304	2295	2294	2303	55	40.0
1981	Setto	2305	2296	1041	1039	55	40.0
1982	Setto	2306	2297	2296	2305	55	40.0
1983	Setto	2307	2298	2297	2306	55	40.0
1984	Setto	2308	2299	2298	2307	55	40.0
1985	Setto	2309	2300	2299	2308	55	40.0
1986	Setto	2310	2301	2300	2309	55	40.0
1987	Setto	2311	2302	2301	2310	55	40.0
1988	Setto	2312	2303	2302	2311	55	40.0
1989	Setto	2313	2304	2303	2312	55	40.0
1990	Setto	2314	2305	1039	1030	55	40.0
1991	Setto	2315	2306	2305	2314	55	40.0
1992	Setto	2316	2307	2306	2315	55	40.0

1993	Setto	2317	2308	2307	2316	55	40.0
1994	Setto	2318	2309	2308	2317	55	40.0
1995	Setto	2319	2310	2309	2318	55	40.0
1996	Setto	2320	2311	2310	2319	55	40.0
1997	Setto	2321	2312	2311	2320	55	40.0
1998	Setto	2322	2313	2312	2321	55	40.0
1999	Setto	2413	2403	2402	2412	55	40.0
2000	Setto	2424	2314	1030	2425	55	40.0
2001	Setto	2426	2315	2314	2424	55	40.0
2002	Setto	2427	2316	2315	2426	55	40.0
2003	Setto	2428	2317	2316	2427	55	40.0
2004	Setto	2429	2318	2317	2428	55	40.0
2005	Setto	2430	2319	2318	2429	55	40.0
2006	Setto	2404	2320	2319	2430	55	40.0
2007	Setto	2406	2321	2320	2404	55	40.0
2008	Setto	2407	2322	2321	2406	55	40.0
2009	Setto	2423	2414	929	875	55	40.0
2010	Setto	2323	2415	2414	2423	55	40.0
2011	Setto	2324	2416	2415	2323	55	40.0
2012	Setto	2325	2417	2416	2324	55	40.0
2013	Setto	2337	2328	2327	2336	55	40.0
2014	Setto	2338	2329	2328	2337	55	40.0
2015	Setto	2339	2330	2329	2338	55	40.0
2016	Setto	2340	2331	2330	2339	55	40.0
2017	Setto	2326	2418	2417	2325	55	40.0
2018	Setto	2332	2419	2418	2326	55	40.0
2019	Setto	2333	2420	2419	2332	55	40.0
2020	Setto	2334	2421	2420	2333	55	40.0
2021	Setto	2335	2422	2421	2334	55	40.0
2022	Setto	2330	2406	2404	2329	55	40.0
2023	Setto	2331	2407	2406	2330	55	40.0
2024	Setto	1020	2425	1019		55	40.0
2025	Setto	2425	1030	1029	1019	55	40.0
2026	Setto	2350	2341	1002	993	55	40.0
2027	Setto	2351	2342	2341	2350	55	40.0
2028	Setto	2352	2343	2342	2351	55	40.0
2029	Setto	2353	2344	2343	2352	55	40.0
2030	Setto	2354	2345	2344	2353	55	40.0
2031	Setto	2355	2346	2345	2354	55	40.0
2032	Setto	2356	2347	2346	2355	55	40.0
2033	Setto	2357	2348	2347	2356	55	40.0
2034	Setto	2358	2349	2348	2357	55	40.0
2035	Setto	2359	2350	993	984	55	40.0
2036	Setto	2360	2351	2350	2359	55	40.0
2037	Setto	2361	2352	2351	2360	55	40.0
2038	Setto	2362	2353	2352	2361	55	40.0
2039	Setto	2363	2354	2353	2362	55	40.0
2040	Setto	2364	2355	2354	2363	55	40.0
2041	Setto	2365	2356	2355	2364	55	40.0
2042	Setto	2366	2357	2356	2365	55	40.0
2043	Setto	2367	2358	2357	2366	55	40.0
2044	Setto	2368	2359	984	975	55	40.0
2045	Setto	2369	2360	2359	2368	55	40.0
2046	Setto	2370	2361	2360	2369	55	40.0
2047	Setto	2371	2362	2361	2370	55	40.0
2048	Setto	2372	2363	2362	2371	55	40.0
2049	Setto	2373	2364	2363	2372	55	40.0
2050	Setto	2374	2365	2364	2373	55	40.0
2051	Setto	2375	2366	2365	2374	55	40.0
2052	Setto	2376	2367	2366	2375	55	40.0
2053	Setto	2377	2368	975	966	55	40.0
2054	Setto	2378	2369	2368	2377	55	40.0
2055	Setto	2379	2370	2369	2378	55	40.0
2056	Setto	2380	2371	2370	2379	55	40.0
2057	Setto	2381	2372	2371	2380	55	40.0
2058	Setto	2382	2373	2372	2381	55	40.0
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2060	Setto	2384	2375	2374	2383	55	40.0
2061	Setto	2385	2376	2375	2384	55	40.0
2062	Setto	2408	2424	2425	1020	55	40.0
2063	Setto	2386	2426	2424	2408	55	40.0
2064	Setto	2387	2427	2426	2386	55	40.0
2065	Setto	2388	2428	2427	2387	55	40.0
2066	Setto	2327	2429	2428	2388	55	40.0
2067	Setto	2391	2382	2381	2390	55	40.0
2068	Setto	2392	2383	2382	2391	55	40.0
2069	Setto	2393	2384	2383	2392	55	40.0

2070	Setto	2394	2385	2384	2393	55	40.0
2071	Setto	2328	2430	2429	2327	55	40.0
2072	Setto	2329	2404	2430	2328	55	40.0
2073	Setto	2346	2389	2395	2345	55	40.0
2074	Setto	2347	2396	2389	2346	55	40.0
2075	Setto	2348	2397	2396	2347	55	40.0
2076	Setto	2400	2391	2390	2399	55	40.0
2077	Setto	2401	2392	2391	2400	55	40.0
2078	Setto	2402	2393	2392	2401	55	40.0
2079	Setto	2403	2394	2393	2402	55	40.0
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2081	Setto	2389	2337	2336	2395	55	40.0
2082	Setto	2396	2338	2337	2389	55	40.0
2083	Setto	2397	2339	2338	2396	55	40.0
2084	Setto	2398	2340	2339	2397	55	40.0
2085	Setto	2410	2400	2399	2409	55	40.0
2086	Setto	2411	2401	2400	2410	55	40.0
2087	Setto	2432	2431	939	2405	55	40.0
2088	Setto	2434	2433	2431	2432	55	40.0
2089	Setto	2436	2435	2433	2434	55	40.0
2090	Setto	2438	2437	2435	2436	55	40.0
2091	Setto	2439	2409	2437	2438	55	40.0
2092	Setto	2440	2410	2409	2439	55	40.0
2093	Setto	2441	2411	2410	2440	55	40.0
2094	Setto	2442	2412	2411	2441	55	40.0
2095	Setto	2443	2413	2412	2442	55	40.0
2096	Setto	2414	2432	2405	929	55	40.0
2097	Setto	2415	2434	2432	2414	55	40.0
2098	Setto	2416	2436	2434	2415	55	40.0
2099	Setto	2417	2438	2436	2416	55	40.0
2100	Setto	2418	2439	2438	2417	55	40.0
2101	Setto	2419	2440	2439	2418	55	40.0
2102	Setto	2420	2441	2440	2419	55	40.0
2103	Setto	2421	2442	2441	2420	55	40.0
2104	Setto	2422	2443	2442	2421	55	40.0
2105	Setto	2444	2445	771	780	40	30.0
2106	Setto	2446	2447	2445	2444	40	30.0
2107	Setto	2448	2449	2447	2446	40	30.0
2108	Setto	2450	2451	2449	2448	40	30.0
2109	Setto	2452	2453	2451	2450	40	30.0
2110	Setto	2445	2454	761	771	40	30.0
2111	Setto	2475	2480	2479	2474	40	30.0
2112	Setto	3381	3374	3375	3382	40	30.0
2113	Setto	3382	3375	3376	2471	40	30.0
2114	Setto	2453	2458	2457	2451	40	30.0
2115	Setto	2454	2459	839	761	40	30.0
2116	Setto	2471	3376	3377	2472	40	30.0
2117	Setto	2479	2274	684	723	40	30.0
2118	Setto	2480	2281	2274	2479	40	30.0
2119	Setto	2458	2463	2462	2457	40	30.0
2120	Setto	2459	2464	752	839	40	30.0
2121	Setto	2460	2465	2464	2459	40	30.0
2122	Setto	2461	2466	2465	2460	40	30.0
2123	Setto	2462	2467	2466	2461	40	30.0
2124	Setto	2463	2468	2467	2462	40	30.0
2125	Setto	2464	2469	743	752	40	30.0
2126	Setto	2465	2470	2469	2464	40	30.0
2127	Setto	3348	3364	3371	3352	40	30.0
2128	Setto	2258	2267	3379	2476	40	30.0
2129	Setto	2476	3379	3380	2477	40	30.0
2130	Setto	2469	2474	733	743	40	30.0
2131	Setto	2470	2475	2474	2469	40	30.0
2132	Setto	2477	3380	3381	3360	40	30.0
2133	Setto	3360	3381	3382	3364	40	30.0
2134	Setto	3364	3382	2471	3371	40	30.0
2135	Setto	2474	2479	723	733	40	30.0
2136	Setto	2482	2444	780	790	34	37.0
2137	Setto	2483	2446	2444	2482	34	37.0
2138	Setto	2484	2448	2446	2483	34	37.0
2139	Setto	2485	2450	2448	2484	34	37.0
2140	Setto	2486	2452	2450	2485	34	37.0
2141	Setto	2488	2487	2452	2486	34	37.0
2142	Setto	2490	2489	2487	2488	34	37.0
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2144	Setto	2494	2493	2491	2492	34	37.0
2145	Setto	2495	2482	790	800	34	37.0
2146	Setto	2496	2483	2482	2495	34	37.0

2147	Setto	2497	2484	2483	2496	34	37.0
2148	Setto	2498	2485	2484	2497	34	37.0
2149	Setto	2499	2486	2485	2498	34	37.0
2150	Setto	2500	2488	2486	2499	34	37.0
2151	Setto	2501	2490	2488	2500	34	37.0
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2153	Setto	2503	2494	2492	2502	34	37.0
2154	Setto	2504	2495	800	810	34	37.0
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2156	Setto	2506	2497	2496	2505	34	37.0
2157	Setto	2507	2498	2497	2506	34	37.0
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2159	Setto	2509	2500	2499	2508	34	37.0
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2161	Setto	2511	2502	2501	2510	34	37.0
2162	Setto	2512	2503	2502	2511	34	37.0
2163	Setto	2513	2504	810	820	34	25.0
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2165	Setto	2810	2819	2820	2811	55	40.0
2166	Setto	2811	2820	2821	2812	55	40.0
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2169	Setto	2814	2823	2824	2815	55	40.0
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2171	Setto	2521	2512	2511	2520	34	37.0
2172	Setto	2522	2513	820	829	34	25.0
2173	Setto	2523	2514	2513	2522	34	25.0
2174	Setto	2816	2825	2826	2817	55	40.0
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2176	Setto	2818	2827	2828	2819	55	40.0
2177	Setto	2819	2828	2829	2820	55	40.0
2178	Setto	2820	2829	2830	2821	55	40.0
2179	Setto	2821	2830	2831	2822	55	40.0
2180	Setto	2530	2521	2520	2529	34	37.0
2181	Setto	2531	2522	829	849	34	37.0
2182	Setto	2532	2523	2522	2531	34	37.0
2183	Setto	2533	2524	2523	2532	34	37.0
2184	Setto	2534	2525	2524	2533	34	37.0
2185	Setto	2535	2526	2525	2534	34	37.0
2186	Setto	2536	2527	2526	2535	34	37.0
2187	Setto	2537	2528	2527	2536	34	37.0
2188	Setto	2538	2529	2528	2537	34	37.0
2189	Setto	2539	2530	2529	2538	34	37.0
2190	Setto	2540	2531	849	765	34	37.0
2191	Setto	2541	2532	2531	2540	34	37.0
2192	Setto	2542	2533	2532	2541	34	37.0
2193	Setto	2543	2534	2533	2542	34	37.0
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2195	Setto	2545	2536	2535	2544	34	37.0
2196	Setto	2546	2537	2536	2545	34	37.0
2197	Setto	2547	2538	2537	2546	34	37.0
2198	Setto	2548	2539	2538	2547	34	37.0
2199	Setto	2549	2540	765	740	34	37.0
2200	Setto	2550	2541	2540	2549	34	37.0
2201	Setto	2551	2542	2541	2550	34	37.0
2202	Setto	2552	2543	2542	2551	34	37.0
2203	Setto	2553	2544	2543	2552	34	37.0
2204	Setto	2554	2545	2544	2553	34	37.0
2205	Setto	2555	2546	2545	2554	34	37.0
2206	Setto	2556	2547	2546	2555	34	37.0
2207	Setto	2557	2548	2547	2556	34	37.0
2208	Setto	2558	2559	1065	1064	34	37.0
2209	Setto	2560	2561	2559	2558	34	37.0
2210	Setto	2562	2563	2561	2560	34	37.0
2211	Setto	2564	2565	2563	2562	34	37.0
2212	Setto	2566	2567	2565	2564	34	37.0
2213	Setto	2568	2569	2567	2566	34	37.0
2214	Setto	2570	2571	2569	2568	34	37.0
2215	Setto	2572	2573	2571	2570	34	37.0
2216	Setto	2574	2575	2573	2572	34	37.0
2217	Setto	2559	2576	1075	1065	34	37.0
2218	Setto	2561	2577	2576	2559	34	37.0
2219	Setto	2563	2578	2577	2561	34	37.0
2220	Setto	2565	2579	2578	2563	34	37.0
2221	Setto	2567	2580	2579	2565	34	37.0
2222	Setto	2569	2581	2580	2567	34	37.0
2223	Setto	2571	2582	2581	2569	34	37.0
2224	Setto	2573	2583	2582	2571	34	37.0

2225	Setto	2575	2584	2583	2573	34	37.0
2226	Setto	2576	2585	1085	1075	34	25.0
2227	Setto	2577	2586	2585	2576	34	25.0
2228	Setto	2600	2589	2588	2599	34	37.0
2229	Setto	2601	2590	2589	2600	34	37.0
2230	Setto	2602	2591	2590	2601	34	37.0
2231	Setto	2603	2549	740	1022	34	37.0
2232	Setto	2604	2550	2549	2603	34	37.0
2233	Setto	2605	2551	2550	2604	34	37.0
2234	Setto	2584	2593	2592	2583	34	37.0
2235	Setto	2585	2594	1095	1085	34	25.0
2236	Setto	2586	2595	2594	2585	34	25.0
2237	Setto	2606	2552	2551	2605	34	37.0
2238	Setto	2587	2553	2552	2606	34	37.0
2239	Setto	2588	2554	2553	2587	34	37.0
2240	Setto	2589	2555	2554	2588	34	37.0
2241	Setto	2590	2556	2555	2589	34	37.0
2242	Setto	2591	2557	2556	2590	34	37.0
2243	Setto	2593	2602	2601	2592	34	37.0
2244	Setto	2594	2603	1022	1095	34	37.0
2245	Setto	2595	2604	2603	2594	34	37.0
2246	Setto	2596	2605	2604	2595	34	37.0
2247	Setto	2597	2606	2605	2596	34	37.0
2248	Setto	2598	2587	2606	2597	34	37.0
2249	Setto	2599	2588	2587	2598	34	37.0
2250	Setto	2607	1724	1384	1438	36	40.0
2251	Setto	2608	1726	1724	2607	36	40.0
2252	Setto	2609	1728	1726	2608	36	40.0
2253	Setto	2610	1730	1728	2609	36	40.0
2254	Setto	2611	1732	1730	2610	36	40.0
2255	Setto	2612	1734	1732	2611	36	40.0
2256	Setto	2613	1736	1734	2612	36	40.0
2257	Setto	2614	1738	1736	2613	36	40.0
2258	Setto	2615	1740	1738	2614	36	40.0
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2260	Setto	2617	2608	2607	2616	36	40.0
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2264	Setto	2621	2612	2611	2620	36	40.0
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2266	Setto	2623	2614	2613	2622	36	40.0
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2268	Setto	2988	2631	2639	2989	59	40.0
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2270	Setto	2635	2326	2332	2990	59	40.0
2271	Setto	2628	2619	2618	2627	36	40.0
2272	Setto	2629	2620	2619	2628	36	40.0
2273	Setto	2970	2979	2980	2971	59	40.0
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2275	Setto	1285	875	2423	2640	59	40.0
2276	Setto	2633	2624	2623	2632	36	40.0
2277	Setto	2990	2332	2333	2991	59	40.0
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2279	Setto	2981	2334	2335	2982	59	40.0
2280	Setto	2637	2628	2627	2636	36	40.0
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2286	Setto	2983	2635	2990	2984	59	40.0
2287	Setto	2984	2990	2991	2630	59	40.0
2288	Setto	2630	2991	2981	2631	59	40.0
2289	Setto	2646	2637	2636	2645	36	40.0
2290	Setto	2647	2638	2637	2646	36	40.0
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2293	Setto	2987	2630	2631	2988	59	40.0
2294	Setto	2651	2642	2641	2650	36	40.0
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2297	Setto	2654	2645	2644	2653	36	40.0
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2299	Setto	2656	2647	2646	2655	36	40.0
2300	Setto	2657	2648	2647	2656	36	40.0
2301	Setto	2658	2649	2648	2657	36	40.0

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2304	Setto	2661	2652	1393	1185	36	40.0
2305	Setto	2662	2653	2652	2661	36	40.0
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2345	Setto	2692	2701	2702	2693	36	40.0
2346	Setto	2693	2702	2703	2694	36	40.0
2347	Setto	2694	2703	2704	2695	36	40.0
2348	Setto	2695	2704	2705	2696	36	40.0
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2366	Setto	2713	2722	2723	2714	36	40.0
2367	Setto	1231	1950	2724	2715	36	40.0
2368	Setto	2715	2724	2725	2716	36	40.0
2369	Setto	2716	2725	2726	2717	36	40.0
2370	Setto	2717	2726	2727	2718	36	40.0
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2376	Setto	1950	1240	2733	2724	36	40.0
2377	Setto	2724	2733	2734	2725	36	40.0
2378	Setto	2725	2734	2735	2726	36	40.0

2379	Setto	2726	2735	2736	2727	36	40.0
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2381	Setto	2728	2737	2738	2729	36	40.0
2382	Setto	2729	2738	2739	2730	36	40.0
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2427	Setto	2518	2562	2564	2519	55	40.0
2428	Setto	2519	2564	2566	2793	55	40.0
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2431	Setto	2787	2796	2797	2788	55	40.0
2432	Setto	2793	2566	2568	2798	55	40.0
2433	Setto	2798	2568	2570	2799	55	40.0
2434	Setto	2830	2789	2790	2831	55	40.0
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2437	Setto	2799	2570	2572	2800	55	40.0
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2600	Setto	1294	1142	2886	2972	59	40.0
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2611	Setto	3001	3000	2998	2999	55	40.0
2612	Setto	3002	2997	1930	1921	55	40.0
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2615	Setto	3005	3002	1921	1912	55	40.0
2616	Setto	3006	3003	3002	3005	55	40.0
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2618	Setto	3008	3005	1912	1903	55	40.0
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2621	Setto	3011	3008	1903	1894	55	40.0
2622	Setto	3012	3009	3008	3011	55	40.0
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2628	Setto	3018	3015	3014	3017	55	40.0
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2676	Setto	3066	3063	3062	3065	55	40.0
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2692	Setto	3082	3079	3078	3081	57	40.0
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2704	Setto	3090	3093	3094	3091	57	40.0
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2732	Setto	2768	2786	3122	3119	55	40.0
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2735	Setto	2786	2795	3125	3122	55	40.0
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2739	Setto	3125	3128	3129	3126	55	40.0
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2750	Setto	2831	2790	3140	3137	55	40.0
2751	Setto	3137	3140	3141	3138	55	40.0
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2756	Setto	2515	2801	3146	3143	55	40.0
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2762	Setto	3149	3152	2575	2574	34	37.0
2763	Setto	3150	3153	3152	3149	34	37.0
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2766	Setto	3153	3156	3155	3152	34	37.0
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2768	Setto	3155	3158	2593	2584	34	37.0
2769	Setto	3156	3160	3158	3155	34	37.0
2770	Setto	3157	3161	3160	3156	58	37.0
2771	Setto	3158	3162	2602	2593	34	37.0

2772	Setto	3160	3163	3162	3158	34	37.0
2773	Setto	3161	3164	3163	3160	58	37.0
2775	Setto	3163	3166	3165	3162	34	37.0
2776	Setto	3164	3167	3166	3163	58	37.0
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2779	Setto	3167	3170	3169	3166	58	37.0
2781	Setto	3169	3172	3171	3168	34	37.0
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2789	Setto	3177	3180	2521	2530	34	37.0
2790	Setto	3178	3181	3180	3177	34	37.0
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2792	Setto	3180	3183	2512	2521	34	37.0
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2827	Setto	3220	3217	3218	3221	57	40.0
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2831	Setto	2031	2040	3222	3225	36	40.0
2832	Setto	3225	3222	3223	3226	36	40.0
2833	Setto	3226	3223	3224	3227	57	40.0
2834	Setto	2022	2031	3225	3228	36	40.0
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2836	Setto	3229	3226	3227	3230	57	40.0
2837	Setto	2013	2022	3228	3231	36	40.0
2838	Setto	3231	3228	3229	3232	36	40.0
2839	Setto	3232	3229	3230	3233	57	40.0
2840	Setto	2004	2013	3231	3234	36	40.0
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2842	Setto	3235	3232	3233	3236	57	40.0
2843	Setto	1995	2004	3234	3237	36	40.0
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2845	Setto	3238	3235	3236	3239	57	40.0
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2892	Setto	3278	3282	3283	3279	36	40.0
2893	Setto	3109	3112	3284	3280	36	40.0
2894	Setto	3280	3284	3285	3281	36	40.0
2895	Setto	3281	3285	3286	3282	36	40.0
2896	Setto	3282	3286	3287	3283	36	40.0
2897	Setto	3112	3115	3288	3284	36	40.0
2898	Setto	3284	3288	3289	3285	36	40.0
2899	Setto	3285	3289	3290	3286	36	40.0
2900	Setto	3286	3290	3291	3287	36	40.0
2901	Setto	3115	3118	3292	3288	36	40.0
2902	Setto	3288	3292	3293	3289	36	40.0
2903	Setto	3289	3293	3294	3290	36	40.0
2904	Setto	3290	3294	3295	3291	36	40.0
2905	Setto	3118	3121	3296	3292	36	40.0
2906	Setto	3292	3296	3297	3293	36	40.0
2907	Setto	3293	3297	3298	3294	36	40.0
2908	Setto	3294	3298	3299	3295	36	40.0
2909	Setto	3301	3300	3067	3070	36	40.0
2910	Setto	3303	3302	3300	3301	36	40.0
2911	Setto	3305	3304	3302	3303	36	40.0
2912	Setto	3307	3306	3304	3305	36	40.0
2913	Setto	3308	3301	3070	3073	36	40.0
2914	Setto	3309	3303	3301	3308	36	40.0
2915	Setto	3310	3305	3303	3309	36	40.0
2916	Setto	3311	3307	3305	3310	36	40.0
2917	Setto	3312	3308	3073	3076	36	40.0
2918	Setto	3313	3309	3308	3312	36	40.0
2919	Setto	3314	3310	3309	3313	36	40.0
2920	Setto	2280	2286	2279	2278	55	25.0
2921	Setto	3316	3312	3076	3079	36	40.0
2922	Setto	3317	3313	3312	3316	36	40.0
2923	Setto	3318	3314	3313	3317	36	40.0
2927	Setto	3327	3323	2295	2304	55	40.0
2928	Setto	2487	3335	2453	2452	40	30.0
2929	Setto	2489	3336	3335	2487	40	30.0
2930	Setto	2491	3337	3336	2489	40	30.0
2931	Setto	2114	2249	2473	2115	40	30.0
2932	Setto	3339	2460	2459	2454	40	30.0
2933	Setto	3340	2461	2460	3339	40	30.0
2934	Setto	2457	2462	2461	3340	40	30.0
2935	Setto	2447	3339	2454	2445	40	30.0
2936	Setto	2449	3340	3339	2447	40	30.0
2937	Setto	2451	2457	3340	2449	40	30.0
2938	Setto	3371	2471	2472	3378	40	30.0
2939	Setto	3352	3371	3378	3356	40	30.0

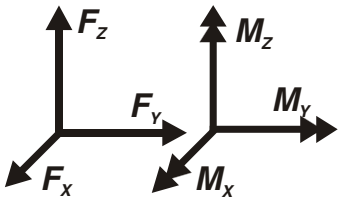
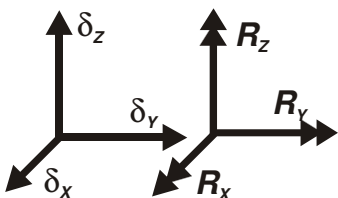
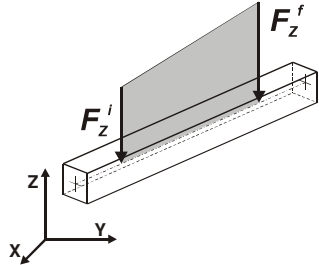
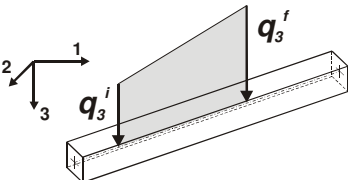
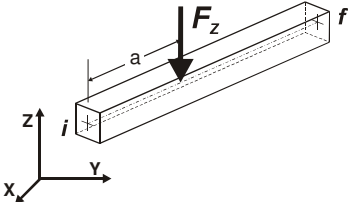
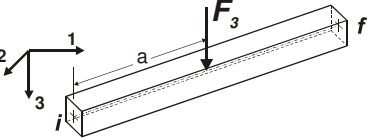
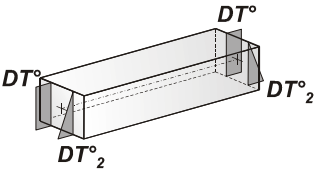
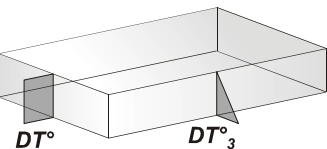
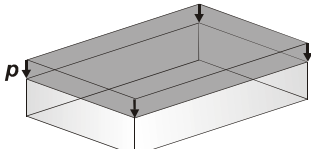
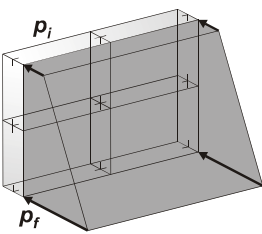
2940	Setto	2249	2258	2476	2473	40	30.0
2941	Setto	2115	2473	3338	2116	40	30.0
2942	Setto	3341	3345	2468	2463	40	30.0
2943	Setto	3342	3346	3345	3341	40	30.0
2944	Setto	3343	3347	3346	3342	40	30.0
2945	Setto	2116	3338	3344	2117	40	30.0
2946	Setto	3335	2478	2458	2453	40	30.0
2947	Setto	3336	3349	2478	3335	40	30.0
2948	Setto	3347	3351	3350	3346	40	30.0
2949	Setto	2117	3344	3348	2118	40	30.0
2950	Setto	3337	3353	3349	3336	40	30.0
2951	Setto	2478	3341	2463	2458	40	30.0
2952	Setto	3351	3355	3354	3350	40	30.0
2953	Setto	2118	3348	3352	2119	40	30.0
2954	Setto	3349	3342	3341	2478	40	30.0
2955	Setto	3353	3343	3342	3349	40	30.0
2956	Setto	3355	3359	3358	3354	40	30.0
2957	Setto	2119	3352	3356	2120	40	30.0
2958	Setto	3357	3361	2264	2456	40	30.0
2959	Setto	3358	3362	3361	3357	40	30.0
2960	Setto	3359	3363	3362	3358	40	30.0
2961	Setto	2473	2476	2477	3338	40	30.0
2962	Setto	2285	2281	2282	3365	40	30.0
2963	Setto	3365	2282	2283	3366	40	30.0
2964	Setto	3366	2283	2264	3367	40	30.0
2965	Setto	3367	2264	3361	3368	40	30.0
2966	Setto	3368	3361	3362	3369	40	30.0
2967	Setto	3369	3362	3363	3370	40	30.0
2968	Setto	3338	2477	3360	3344	40	30.0
2969	Setto	2276	2285	3365	3372	40	30.0
2970	Setto	3372	3365	3366	3373	40	30.0
2971	Setto	3373	3366	3367	3374	40	30.0
2972	Setto	3374	3367	3368	3375	40	30.0
2973	Setto	3375	3368	3369	3376	40	30.0
2974	Setto	3376	3369	3370	3377	40	30.0
2975	Setto	3344	3360	3364	3348	40	30.0
2976	Setto	2267	2276	3372	3379	40	30.0
2977	Setto	3379	3372	3373	3380	40	30.0
2978	Setto	3380	3373	3374	3381	40	30.0

MODELLAZIONE DELLE AZIONI

LEGENDA TABELLA DATI AZIONI

Il programma consente l'uso di diverse tipologie di carico (azioni). Le azioni utilizzate nella modellazione sono individuate da una sigla identificativa ed un codice numerico (gli elementi strutturali richiamano quest'ultimo nella propria descrizione). Per ogni azione applicata alla struttura viene di riportato il codice, il tipo e la sigla identificativa. Le tabelle successive dettagliano i valori caratteristici di ogni azione in relazione al tipo. Le tabelle riportano infatti i seguenti dati in relazione al tipo:

1	carico concentrato nodale 6 dati (forza F_x , F_y , F_z , momento M_x , M_y , M_z)
2	spostamento nodale impresso 6 dati (spostamento T_x , T_y , T_z , rotazione R_x , R_y , R_z)
3	carico distribuito globale su elemento tipo trave 7 dati (f_x , f_y , f_z , m_x , m_y , m_z , ascissa di inizio carico) 7 dati (f_x , f_y , f_z , m_x , m_y , m_z , ascissa di fine carico)
4	carico distribuito locale su elemento tipo trave 7 dati (f_1 , f_2 , f_3 , m_1 , m_2 , m_3 , ascissa di inizio carico) 7 dati (f_1 , f_2 , f_3 , m_1 , m_2 , m_3 , ascissa di fine carico)
5	carico concentrato globale su elemento tipo trave 7 dati (F_x , F_y , F_z , M_x , M_y , M_z , ascissa di carico)
6	carico concentrato locale su elemento tipo trave 7 dati (F_1 , F_2 , F_3 , M_1 , M_2 , M_3 , ascissa di carico)
7	variazione termica applicata ad elemento tipo trave 7 dati (variazioni termiche: uniforme, media e differenza in altezza e larghezza al nodo iniziale e finale)
8	carico di pressione uniforme su elemento tipo piastra 1 dato (pressione)
9	carico di pressione variabile su elemento tipo piastra 4 dati (pressione, quota, pressione, quota)
10	variazione termica applicata ad elemento tipo piastra 2 dati (variazioni termiche: media e differenza nello spessore)
11	carico variabile generale su elementi tipo trave e piastra 1 dato descrizione della tipologia 4 dati per segmento (posizione, valore, posizione, valore) la tipologia precisa l'ascissa di definizione, la direzione del carico, la modalità di carico e la larghezza d'influenza per gli elementi tipo trave
12	gruppo di carichi con impronta su piastra 9 dati (numero di ripetizioni in direzione X e Y, valore di ciascun carico, posizione centrale del primo, dimensioni dell'impronta, interasse tra i carichi)

 <p>Carico nodale</p>	concentrato	 <p>Spostamento impresso</p>
 <p>Carico distribuito globale</p>		 <p>Carico distribuito locale</p>
 <p>Carico globale</p>	concentrato	 <p>Carico concentrato locale</p>
 <p>Carico termico 2D</p>		 <p>Carico termico 3D</p>
 <p>Carico uniforme</p>	pressione	 <p>Carico pressione variabile</p>

SCHEMATIZZAZIONE DEI CASI DI CARICO

LEGENDA TABELLA CASI DI CARICO

Il programma consente l'applicazione di diverse tipologie di casi di carico.

Sono previsti i seguenti 11 tipi di casi di carico:

	Sigla	Tipo	Descrizione
1	Ggk	A	caso di carico comprensivo del peso proprio struttura
2	Gk	NA	caso di carico con azioni permanenti
3	Qk	NA	caso di carico con azioni variabili
4	Gsk	A	caso di carico comprensivo dei carichi permanenti sui solai e sulle coperture
5	Qsk	A	caso di carico comprensivo dei carichi variabili sui solai
6	Qnk	A	caso di carico comprensivo dei carichi di neve sulle coperture
7	Qtk	SA	caso di carico comprensivo di una variazione termica agente sulla struttura
8	Qvk	NA	caso di carico comprensivo di azioni da vento sulla struttura
9	Esk	SA	caso di carico sismico con analisi statica equivalente
10	Edk	SA	caso di carico sismico con analisi dinamica
11	Etik	NA	caso di carico comprensivo di azioni derivanti dall' incremento di spinta delle terre in condizione sismica
12	Pk	NA	caso di carico comprensivo di azioni derivanti da coazioni, cedimenti e precompressioni

Sono di tipo automatico A (ossia non prevedono introduzione dati da parte dell'utente) i seguenti casi di carico: 1-Ggk; 4-Gsk; 5-Qsk; 6-Qnk.

Sono di tipo semi-automatico SA (ossia prevedono una minima introduzione dati da parte dell'utente) i seguenti casi di carico:

7-Qtk, in quanto richiede solo il valore della variazione termica;

9-Esk e 10-Edk, in quanto richiedono il valore dell'angolo di ingresso del sisma e l'individuazione dei casi di carico partecipanti alla definizione delle masse.

Sono di tipo non automatico NA ossia prevedono la diretta applicazione di carichi generici agli elementi strutturali (si veda il precedente punto Modellazione delle Azioni) i restanti casi di carico.

Nella tabella successiva vengono riportati i casi di carico agenti sulla struttura, con l'indicazione dei dati relativi al caso di carico stesso: Numero Tipo e Sigla identificativa, Valore di riferimento del caso di carico (se previsto).

In successione, per i casi di carico non automatici, viene riportato l'elenco di nodi ed elementi direttamente caricati con la sigla identificativa del carico.

Per i casi di carico di tipo sismico (9-Esk e 10-Edk), viene riportata la tabella di definizione delle masse: per ogni caso di carico partecipante alla definizione delle masse viene indicata la relativa aliquota (partecipazione) considerata. Si precisa che per i caso di carico 5-Qsk e 6-Qnk la partecipazione è prevista localmente per ogni elemento solaio o copertura presente nel modello (si confronti il valore Sksol nel capitolo relativo agli elementi solaio) e pertanto la loro partecipazione è di norma pari a uno.

CDC	Tipo	Sigla Id	Note
1	Ggk	CDC=Ggk (peso proprio della struttura)	
2	Gsk	CDC=G1sk (permanente solai-coperture)	
3	Gsk	CDC=G2sk (permanente solai-coperture n.c.d.)	
4	Gsk	CDC=G2pk (permanente pannelli n.c.d.)	
5	Qsk	CDC=Qsk (variabile solai)	
6	Qnk	CDC=Qnk (carico da neve)	
7	Edk	CDC=Ed (dinamico SLU) alfa=0.0 (ecc. +)	partecipazione:1.00 per 1 CDC=Ggk (peso proprio della struttura)
			partecipazione:1.00 per 2 CDC=G1sk (permanente solai-coperture)
			partecipazione:1.00 per 3 CDC=G2sk (permanente solai-coperture n.c.d.)
			partecipazione:1.00 per 4 CDC=G2pk (permanente pannelli n.c.d.)
			partecipazione:1.00 per 5 CDC=Qsk (variabile solai)
			partecipazione:1.00 per 6 CDC=Qnk (carico da neve)
8	Edk	CDC=Ed (dinamico SLU) alfa=0.0 (ecc. -)	come precedente CDC sismico
9	Edk	CDC=Ed (dinamico SLU) alfa=90.00 (ecc. +)	come precedente CDC sismico
10	Edk	CDC=Ed (dinamico SLU) alfa=90.00 (ecc. -)	come precedente CDC sismico
11	Edk	CDC=Ed (dinamico SLD) alfa=0.0 (ecc. +)	come precedente CDC sismico
12	Edk	CDC=Ed (dinamico SLD) alfa=0.0 (ecc. -)	come precedente CDC sismico
13	Edk	CDC=Ed (dinamico SLD) alfa=90.00 (ecc. +)	come precedente CDC sismico
14	Edk	CDC=Ed (dinamico SLD) alfa=90.00 (ecc. -)	come precedente CDC sismico

DEFINIZIONE DELLE COMBINAZIONI

LEGENDA TABELLA COMBINAZIONI DI CARICO

Il programma combina i diversi tipi di casi di carico (CDC) secondo le regole previste dalla normativa vigente. Le combinazioni previste sono destinate al controllo di sicurezza della struttura ed alla verifica degli spostamenti e delle sollecitazioni.

La prima tabella delle combinazioni riportata di seguito comprende le seguenti informazioni: Numero, Tipo, Sigla identificativa. Una seconda tabella riporta il peso nella combinazione assunto per ogni caso di carico.

Ai fini delle verifiche degli stati limite si definiscono le seguenti combinazioni delle azioni:

Combinazione fondamentale SLU

$\gamma_{G1} \cdot G_1 + \gamma_{G2} \cdot G_2 + \gamma_P \cdot P + \gamma_{Q1} \cdot Q_{k1} + \gamma_{Q2} \cdot \psi_{02} \cdot Q_{k2} + \gamma_{Q3} \cdot \psi_{03} \cdot Q_{k3} + \dots$

Combinazione caratteristica (rara) SLE

$G_1 + G_2 + P + Q_{k1} + \psi_{02} \cdot Q_{k2} + \psi_{03} \cdot Q_{k3} + \dots$

Combinazione frequente SLE

$G_1 + G_2 + P + \psi_{11} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \psi_{23} \cdot Q_{k3} + \dots$

Combinazione quasi permanente SLE

$G_1 + G_2 + P + \psi_{21} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \psi_{23} \cdot Q_{k3} + \dots$

Combinazione sismica, impiegata per gli stati limite ultimi e di esercizio connessi all'azione sismica E

$E + G_1 + G_2 + P + \psi_{21} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \dots$

Combinazione eccezionale, impiegata per gli stati limite connessi alle azioni eccezionali

$G_1 + G_2 + A_d + P + \psi_{21} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \dots$

Dove:

NTC 2018 Tabella 2.5.I

Destinazione d'uso/azione	ψ_0	ψ_1	ψ_2
Categoria A residenziali	0,70	0,50	0,30
Categoria B uffici	0,70	0,50	0,30
Categoria C ambienti suscettibili di affollamento	0,70	0,70	0,60
Categoria D ambienti ad uso commerciale	0,70	0,70	0,60
Categoria E biblioteche, archivi, magazzini,...	1,00	0,90	0,80
Categoria F Rimesse e parcheggi (autoveicoli ≤ 30 kN)	0,70	0,70	0,60
Categoria G Rimesse e parcheggi (autoveicoli > 30 kN)	0,70	0,50	0,30
Categoria H Coperture	0,00	0,00	0,00
Vento	0,60	0,20	0,00
Neve a quota ≤ 1000 m	0,50	0,20	0,00
Neve a quota > 1000 m	0,70	0,50	0,20
Variazioni Termiche	0,60	0,50	0,00

Nelle verifiche possono essere adottati in alternativa due diversi approcci progettuali:

- per l'approccio 1 si considerano due diverse combinazioni di gruppi di coefficienti di sicurezza parziali per le azioni, per i materiali e per la resistenza globale (combinazione 1 con coefficienti A1 e combinazione 2 con coefficienti A2),
- per l'approccio 2 si definisce un'unica combinazione per le azioni, per la resistenza dei materiali e per la resistenza globale (con coefficienti A1).

NTC 2018 Tabella 2.6.I

		Coefficiente γ_f	EQU	A1	A2
Carichi permanenti	Favorevoli	γ_{G1}	0,9	1,0	1,0
	Sfavorevoli		1,1	1,3	1,0
Carichi permanenti non strutturali (Non compiutamente definiti)	Favorevoli	γ_{G2}	0,8	0,8	0,8
	Sfavorevoli		1,5	1,5	1,3
Carichi variabili	Favorevoli	γ_{Qi}	0,0	0,0	0,0
	Sfavorevoli		1,5	1,5	1,3

Cmb	Tipo	Sigla Id	effetto P-delta
1	SLU	Comb. SLU A1 1	
2	SLU	Comb. SLU A1 2	
3	SLU	Comb. SLU A1 3	
4	SLU	Comb. SLU A1 4	
5	SLU	Comb. SLU A1 5	
6	SLU	Comb. SLU A1 6	
7	SLU	Comb. SLU A1 7	
8	SLU	Comb. SLU A1 8	

Cmb	Typo	Sigla Id	effetto P-delta
9	SLU	Comb. SLU A1 9	
10	SLU	Comb. SLU A1 10	
11	SLU	Comb. SLU A1 (SLV sism.) 11	
12	SLU	Comb. SLU A1 (SLV sism.) 12	
13	SLU	Comb. SLU A1 (SLV sism.) 13	
14	SLU	Comb. SLU A1 (SLV sism.) 14	
15	SLU	Comb. SLU A1 (SLV sism.) 15	
16	SLU	Comb. SLU A1 (SLV sism.) 16	
17	SLU	Comb. SLU A1 (SLV sism.) 17	
18	SLU	Comb. SLU A1 (SLV sism.) 18	
19	SLU	Comb. SLU A1 (SLV sism.) 19	
20	SLU	Comb. SLU A1 (SLV sism.) 20	
21	SLU	Comb. SLU A1 (SLV sism.) 21	
22	SLU	Comb. SLU A1 (SLV sism.) 22	
23	SLU	Comb. SLU A1 (SLV sism.) 23	
24	SLU	Comb. SLU A1 (SLV sism.) 24	
25	SLU	Comb. SLU A1 (SLV sism.) 25	
26	SLU	Comb. SLU A1 (SLV sism.) 26	
27	SLU	Comb. SLU A1 (SLV sism.) 27	
28	SLU	Comb. SLU A1 (SLV sism.) 28	
29	SLU	Comb. SLU A1 (SLV sism.) 29	
30	SLU	Comb. SLU A1 (SLV sism.) 30	
31	SLU	Comb. SLU A1 (SLV sism.) 31	
32	SLU	Comb. SLU A1 (SLV sism.) 32	
33	SLU	Comb. SLU A1 (SLV sism.) 33	
34	SLU	Comb. SLU A1 (SLV sism.) 34	
35	SLU	Comb. SLU A1 (SLV sism.) 35	
36	SLU	Comb. SLU A1 (SLV sism.) 36	
37	SLU	Comb. SLU A1 (SLV sism.) 37	
38	SLU	Comb. SLU A1 (SLV sism.) 38	
39	SLU	Comb. SLU A1 (SLV sism.) 39	
40	SLU	Comb. SLU A1 (SLV sism.) 40	
41	SLU	Comb. SLU A1 (SLV sism.) 41	
42	SLU	Comb. SLU A1 (SLV sism.) 42	
43	SLD(sis)	Comb. SLE (SLD Danno sism.) 43	
44	SLD(sis)	Comb. SLE (SLD Danno sism.) 44	
45	SLD(sis)	Comb. SLE (SLD Danno sism.) 45	
46	SLD(sis)	Comb. SLE (SLD Danno sism.) 46	
47	SLD(sis)	Comb. SLE (SLD Danno sism.) 47	
48	SLD(sis)	Comb. SLE (SLD Danno sism.) 48	
49	SLD(sis)	Comb. SLE (SLD Danno sism.) 49	
50	SLD(sis)	Comb. SLE (SLD Danno sism.) 50	
51	SLD(sis)	Comb. SLE (SLD Danno sism.) 51	
52	SLD(sis)	Comb. SLE (SLD Danno sism.) 52	
53	SLD(sis)	Comb. SLE (SLD Danno sism.) 53	
54	SLD(sis)	Comb. SLE (SLD Danno sism.) 54	
55	SLD(sis)	Comb. SLE (SLD Danno sism.) 55	
56	SLD(sis)	Comb. SLE (SLD Danno sism.) 56	
57	SLD(sis)	Comb. SLE (SLD Danno sism.) 57	
58	SLD(sis)	Comb. SLE (SLD Danno sism.) 58	
59	SLD(sis)	Comb. SLE (SLD Danno sism.) 59	
60	SLD(sis)	Comb. SLE (SLD Danno sism.) 60	
61	SLD(sis)	Comb. SLE (SLD Danno sism.) 61	
62	SLD(sis)	Comb. SLE (SLD Danno sism.) 62	
63	SLD(sis)	Comb. SLE (SLD Danno sism.) 63	
64	SLD(sis)	Comb. SLE (SLD Danno sism.) 64	
65	SLD(sis)	Comb. SLE (SLD Danno sism.) 65	
66	SLD(sis)	Comb. SLE (SLD Danno sism.) 66	
67	SLD(sis)	Comb. SLE (SLD Danno sism.) 67	
68	SLD(sis)	Comb. SLE (SLD Danno sism.) 68	
69	SLD(sis)	Comb. SLE (SLD Danno sism.) 69	
70	SLD(sis)	Comb. SLE (SLD Danno sism.) 70	
71	SLD(sis)	Comb. SLE (SLD Danno sism.) 71	
72	SLD(sis)	Comb. SLE (SLD Danno sism.) 72	
73	SLD(sis)	Comb. SLE (SLD Danno sism.) 73	
74	SLD(sis)	Comb. SLE (SLD Danno sism.) 74	

[illegible]

	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
2	1.30	1.30	1.50	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3	1.00	1.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4	1.00	1.00	0.0	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5	1.30	1.30	1.50	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
6	1.30	1.30	1.50	1.50	1.05	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
7	1.30	1.30	1.50	1.50	1.05	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
8	1.00	1.00	0.0	0.0	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
9	1.00	1.00	0.0	0.0	1.05	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
10	1.00	1.00	0.0	0.0	1.05	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
11	1.00	1.00	1.00	1.00	0.60	0.0	-1.00	0.0	-0.30	0.0	0.0	0.0	0.0	0.0
12	1.00	1.00	1.00	1.00	0.60	0.0	-1.00	0.0	0.30	0.0	0.0	0.0	0.0	0.0
13	1.00	1.00	1.00	1.00	0.60	0.0	1.00	0.0	-0.30	0.0	0.0	0.0	0.0	0.0
14	1.00	1.00	1.00	1.00	0.60	0.0	1.00	0.0	0.30	0.0	0.0	0.0	0.0	0.0
15	1.00	1.00	1.00	1.00	0.60	0.0	-1.00	0.0	0.0	-0.30	0.0	0.0	0.0	0.0
16	1.00	1.00	1.00	1.00	0.60	0.0	-1.00	0.0	0.0	0.30	0.0	0.0	0.0	0.0
17	1.00	1.00	1.00	1.00	0.60	0.0	1.00	0.0	0.0	-0.30	0.0	0.0	0.0	0.0
18	1.00	1.00	1.00	1.00	0.60	0.0	1.00	0.0	0.0	0.30	0.0	0.0	0.0	0.0
19	1.00	1.00	1.00	1.00	0.60	0.0	0.0	-1.00	-0.30	0.0	0.0	0.0	0.0	0.0
20	1.00	1.00	1.00	1.00	0.60	0.0	0.0	-1.00	0.30	0.0	0.0	0.0	0.0	0.0
21	1.00	1.00	1.00	1.00	0.60	0.0	0.0	1.00	-0.30	0.0	0.0	0.0	0.0	0.0
22	1.00	1.00	1.00	1.00	0.60	0.0	0.0	1.00	0.30	0.0	0.0	0.0	0.0	0.0
23	1.00	1.00	1.00	1.00	0.60	0.0	0.0	-1.00	0.0	-0.30	0.0	0.0	0.0	0.0
24	1.00	1.00	1.00	1.00	0.60	0.0	0.0	-1.00	0.0	0.30	0.0	0.0	0.0	0.0
25	1.00	1.00	1.00	1.00	0.60	0.0	0.0	1.00	0.0	-0.30	0.0	0.0	0.0	0.0
26	1.00	1.00	1.00	1.00	0.60	0.0	0.0	1.00	0.0	0.30	0.0	0.0	0.0	0.0
27	1.00	1.00	1.00	1.00	0.60	0.0	-0.30	0.0	-1.00	0.0	0.0	0.0	0.0	0.0
28	1.00	1.00	1.00	1.00	0.60	0.0	-0.30	0.0	1.00	0.0	0.0	0.0	0.0	0.0
29	1.00	1.00	1.00	1.00	0.60	0.0	0.30	0.0	-1.00	0.0	0.0	0.0	0.0	0.0
30	1.00	1.00	1.00	1.00	0.60	0.0	0.30	0.0	1.00	0.0	0.0	0.0	0.0	0.0
31	1.00	1.00	1.00	1.00	0.60	0.0	0.0	-0.30	-1.00	0.0	0.0	0.0	0.0	0.0
32	1.00	1.00	1.00	1.00	0.60	0.0	0.0	-0.30	1.00	0.0	0.0	0.0	0.0	0.0
33	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.30	-1.00	0.0	0.0	0.0	0.0	0.0
34	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.30	1.00	0.0	0.0	0.0	0.0	0.0
35	1.00	1.00	1.00	1.00	0.60	0.0	-0.30	0.0	0.0	-1.00	0.0	0.0	0.0	0.0
36	1.00	1.00	1.00	1.00	0.60	0.0	-0.30	0.0	0.0	1.00	0.0	0.0	0.0	0.0
37	1.00	1.00	1.00	1.00	0.60	0.0	0.30	0.0	0.0	-1.00	0.0	0.0	0.0	0.0
38	1.00	1.00	1.00	1.00	0.60	0.0	0.30	0.0	0.0	1.00	0.0	0.0	0.0	0.0
39	1.00	1.00	1.00	1.00	0.60	0.0	0.0	-0.30	0.0	-1.00	0.0	0.0	0.0	0.0
40	1.00	1.00	1.00	1.00	0.60	0.0	0.0	-0.30	0.0	1.00	0.0	0.0	0.0	0.0
41	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.30	0.0	-1.00	0.0	0.0	0.0	0.0
42	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.30	0.0	1.00	0.0	0.0	0.0	0.0
43	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	-0.30	0.0
44	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	0.30	0.0
45	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	1.00	0.0	-0.30	0.0
46	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	1.00	0.0	0.30	0.0
47	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	0.0	-0.30
48	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	0.0	0.30
49	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	1.00	0.0	0.0	-0.30
50	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	1.00	0.0	0.0	0.30
51	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	-0.30	0.0
52	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	0.30	0.0
53	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.0	1.00	-0.30	0.0
54	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.30	0.0
55	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	-0.30
56	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	0.30
57	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.0	-0.30
58	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.0	0.30
59	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	-1.00	0.0
60	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	1.00	0.0
61	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.30	0.0	-1.00	0.0
62	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.30	0.0	1.00	0.0
63	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.0	-0.30	-1.00	0.0
64	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.0	-0.30	1.00	0.0
65	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.0	0.30	-1.00	0.0
66	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.0	0.30	1.00	0.0
67	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	0.0	-1.00
68	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	0.0	1.00
69	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.30	0.0	0.0	-1.00
70	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.30	0.0	0.0	1.00
71	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	-1.00
72	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	1.00
73	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.0	0.30	0.0	-1.00
74	1.00	1.00	1.00	1.00	0.60	0.0	0.0	0.0	0.0	0.0	0.0	0.30	0.0	1.00

AZIONE SISMICA

VALUTAZIONE DELL' AZIONE SISMICA

L'azione sismica sulle costruzioni è valutata a partire dalla "pericolosità sismica di base", in condizioni ideali di sito di riferimento rigido con superficie topografica orizzontale.

Allo stato attuale, la pericolosità sismica su reticolo di riferimento nell'intervallo di riferimento è fornita dai dati pubblicati sul sito <http://esse1.mi.ingv.it/>. Per punti non coincidenti con il reticolo di riferimento e periodi di ritorno non contemplati direttamente si opera come indicato nell' allegato alle NTC (rispettivamente media pesata e interpolazione).

L' azione sismica viene definita in relazione ad un periodo di riferimento V_r che si ricava, per ciascun tipo di costruzione, moltiplicandone la vita nominale per il coefficiente d'uso (vedi tabella Parametri della struttura). Fissato il periodo di riferimento V_r e la probabilità di superamento P_{ver} associata a ciascuno degli stati limite considerati, si ottiene il periodo di ritorno T_r e i relativi parametri di pericolosità sismica (vedi tabella successiva):

ag: accelerazione orizzontale massima del terreno;

Fo: valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale;

T*c: periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale;

Parametri della struttura

Classe d'uso	Vita V_n [anni]	Coeff. Uso	Periodo V_r [anni]	Tipo di suolo	Categoria topografica
III	50.0	1.5	75.0	B	T1

Individuati su reticolo di riferimento i parametri di pericolosità sismica si valutano i parametri spettrali riportati in tabella:

S è il coefficiente che tiene conto della categoria di sottosuolo e delle condizioni topografiche mediante la relazione seguente $S = S_s \cdot S_t$ (3.2.3)

Fo è il fattore che quantifica l'amplificazione spettrale massima, su sito di riferimento rigido orizzontale

Fv è il fattore che quantifica l'amplificazione spettrale massima verticale, in termini di accelerazione orizzontale massima del terreno ag su sito di riferimento rigido orizzontale

Tb è il periodo corrispondente all'inizio del tratto dello spettro ad accelerazione costante.

Tc è il periodo corrispondente all'inizio del tratto dello spettro a velocità costante.

Td è il periodo corrispondente all'inizio del tratto dello spettro a spostamento costante.

Id nodo	Longitudine	Latitudine	Distanza
			Km
Loc.	7.572	45.244	
12903	7.528	45.237	3.520
12904	7.599	45.241	2.133
12682	7.594	45.291	5.484
12681	7.523	45.287	6.109

SL	P _{ver}	T _r	ag	Fo	T*c
		Anni	g		sec
SLO	92.0	30.0	0.024	2.570	0.180
SLD	92.0	30.0	0.024	2.570	0.180
SLV	50.0	108.0	0.039	2.640	0.220
SLC	33.0	187.0	0.046	2.670	0.240

SL	ag	S	Fo	Fv	Tb	Tc	Td
	g				sec	sec	sec
SLO	0.024	1.200	2.570	0.541	0.093	0.279	1.697
SLD	0.024	1.200	2.570	0.541	0.093	0.279	1.697
SLV	0.039	1.200	2.640	0.702	0.109	0.328	1.755
SLC	0.046	1.200	2.670	0.772	0.117	0.351	1.784

RISULTATI ANALISI SISMICHE

LEGENDA TABELLA ANALISI SISMICHE

Il programma consente l'analisi di diverse configurazioni sismiche.

Sono previsti, infatti, i seguenti casi di carico:

9. Esk caso di carico sismico con analisi statica equivalente

10. Edk caso di carico sismico con analisi dinamica

Ciascun caso di carico è caratterizzato da un angolo di ingresso e da una configurazione di masse determinante la forza sismica complessiva (si rimanda al capitolo relativo ai casi di carico per chiarimenti inerenti questo aspetto).

Nella colonna Note, in funzione della norma in uso sono riportati i parametri fondamentali che caratterizzano l'azione sismica: in particolare possono essere presenti i seguenti valori:

Angolo di ingresso	Angolo di ingresso dell'azione sismica orizzontale
Fattore di importanza	Fattore di importanza dell'edificio, in base alla categoria di appartenenza
Zona sismica	Zona sismica
Accelerazione ag	Accelerazione orizzontale massima sul suolo
Categoria suolo	Categoria di profilo stratigrafico del suolo di fondazione
Fattore q	Fattore di struttura/di comportamento. Dipendente dalla tipologia strutturale
Fattore di sito S	Fattore dipendente dalla stratigrafia e dal profilo topografico
Classe di duttilità CD	Classe di duttilità della struttura – "A" duttilità alta, "B" duttilità bassa
Fattore riduz. SLD	Fattore di riduzione dello spettro elastico per lo stato limite di danno
Periodo proprio T1	Periodo proprio di vibrazione della struttura
Coefficiente Lambda	Coefficiente dipendente dal periodo proprio T1 e dal numero di piani della struttura
Ordinata spettro Sd(T1)	Valore delle ordinate dello spettro di progetto per lo stato limite ultimo, componente orizzontale (verticale Svd)
Ordinata spettro Se(T1)	Valore delle ordinate dello spettro elastico ridotta del fattore SLD per lo stato limite di danno, componente orizzontale (verticale Sve)
Ordinata spettro S (Tb-Tc)	Valore dell' ordinata dello spettro in uso nel tratto costante
numero di modi considerati	Numero di modi di vibrare della struttura considerati nell'analisi dinamica

Per ciascun caso di carico sismico viene riportato l'insieme di dati sotto riportati (le masse sono espresse in unità di forza):

- a) analisi sismica statica equivalente:
 - quota, posizione del centro di applicazione e azione orizzontale risultante, posizione del baricentro delle rigidezze, rapporto r/L_s (per strutture a nucleo), indici di regolarità e/r secondo EC8 4.2.3.2
 - azione sismica complessiva
- b) analisi sismica dinamica con spettro di risposta:
 - quota, posizione del centro di massa e massa risultante, posizione del baricentro delle rigidezze, rapporto r/L_s (per strutture a nucleo) , indici di regolarità e/r secondo EC8 4.2.3.2
 - frequenza, periodo, accelerazione spettrale, massa eccitata nelle tre direzioni globali per tutti i modi
 - massa complessiva ed aliquota di massa complessiva eccitata.

Per ciascuna combinazione sismica definita SLD o SLO viene riportato il livello di deformazione η_T (dr) degli elementi strutturali verticali. Per semplicità di consultazione il livello è espresso anche in unità $1000 \cdot \eta_T/h$ da confrontare direttamente con i valori forniti nella norma (es. 5 per edifici con tamponamenti collegati rigidamente alla struttura, 10.0 per edifici con tamponamenti collegati elasticamente, 3 per edifici in muratura ordinaria, 4 per edifici in muratura armata).

Qualora si applichi il D.M. 96 (vedi NOTA sul capitolo "normativa di riferimento") l'analisi sismica dinamica può essere comprensiva di sollecitazione verticale contemporanea a quella orizzontale, nel qual caso è effettuata una sovrapposizione degli effetti in ragione della radice dei quadrati degli effetti stessi. Per ciascuna combinazione sismica - analisi effettuate con il D.M. 96 (vedi NOTA sul capitolo "normativa di riferimento") - viene riportato il livello di deformazione η_T , η_P e η_D degli elementi strutturali verticali. Per semplicità di consultazione il livello è espresso in unità $1000 \cdot \eta_T/h$ da confrontare direttamente con il valore 2 o 4 per la verifica.

Per gli edifici sismicamente isolati si riportano di seguito le verifiche condotte sui dispositivi di isolamento. Le verifiche sono effettuate secondo la circolare 619/2009 del C.S.LL.PP nelle combinazioni in SLC come previsto dal DM 17-01-2018. Per ogni combinazione è riportato il codice di verifica ed i valori utilizzati per la verifica: spostamento dE, area ridotta e dimensione A2, azione verticale, deformazioni di taglio dell'elastomero e tensioni nell'acciaio.

Qualora si applichi l'Ordinanza 3274 e s.m.i. le verifiche sono eseguite in accordo con l'allegato 10.A.

In particolare la tabella, per ogni combinazione di calcolo, riporta:

Nodo	Nodo di appoggio dell' isolatore
Cmb	Combinazione oggetto della verifica
Verif.	Codice di verifica ok – verifica positiva , NV – verifica negativa, ND – verifica non completata
dE	Spostamento relativo tra le due facce (amplificato del 20% per Ordinanza 3274 e smi) combinato con la regola del 30%
Ang fi	Angolo utilizzato per il calcolo dell' area ridotta Ar (per dispositivi circolari)
V	Azione verticale agente
Ar	Area ridotta efficace
Dim A2	Dimensione utile per il calcolo della deformazione per rotazione
Sig s	Tensione nell' inserto in acciaio

Gam c(a,s,t)	Deformazioni di taglio dell' elastomero
Vcr	Carico critico per instabilità

Affinché la verifica sia positiva deve essere:

- 1) $V > 0$
- 2) $\text{Sig } s < f_{yk}$
- 3) $\text{Gam } t < 5$
- 4) $\text{Gam } s < \text{Gam } *$ (caratteristica dell' elastomero)
- 5) $\text{Gam } s < 2$
- 6) $V < 0.5 V_{cr}$

Con riferimento al **Documento di Affidabilità** "Test di validazione del software di calcolo PRO_SAP e dei moduli aggiuntivi PRO_SAP Modulo Geotecnico, PRO_CAD nodi acciaio e PRO_MST" - versione Maggio 2011, disponibile per il download sul sito www.2si.it, si segnalano i seguenti esempi applicativi:

Test N°	Titolo
23	DM 2008: SPETTRO
29	SISMICA 1000/H, SOMMA V, EFFETTO P-δ
30	ANALISI DI UN EDIFICIO CON ISOLATORI SISMICI
70	MASSE SISMICHE
75	PROGETTO DI ISOLATORI ELASTOMERICI
76	VERIFICA DI ISOLATORI ELASTOMERICI
77	VERIFICA DI ISOLATORI FRICTION PENDULUM

La costruzione, esistente, è caratterizzata da regolarità sia in pianta sia in altezza ed è progettata in classe di duttilità media (CD"B").

Sistema costruttivo: muratura

Definizione rapporto α_1/α_1 :	valore come da normativa
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Riferimento normativo α_1/α_2 : costruzioni di muratura ordinaria

Valore rapporto	$\alpha_u/\alpha_1 =$	1.700
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Fattore dissipativo $q_p = 2.000 \alpha_1/\alpha_1 = 3.400$

Dissipativi Verifiche fragili

q SLU x	3.400	1.000
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q SLU y	3.400	1.000
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q SLU z	1.500	1.000
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Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
cm	daN	cm	cm	cm	cm	cm	cm			
1340.00	96.19	-491.36	-334.97	0.0	0.0	-491.36	-334.97	0.155	0.0	0.0
1295.00	116.44	-491.36	-334.97	0.0	0.0	-491.36	-334.97	1.791	0.0	0.0
1250.00	101.25	-491.36	-334.97	0.0	0.0	-491.36	-334.97	1.791	0.0	0.0
1205.00	1203.52	-572.28	-173.84	0.0	-26.80	-635.82	-328.32	0.015	2.913	3.350
1195.00	7848.27	-175.90	173.40	0.0	-15.15	-313.36	198.69	0.654	1.046	0.168
1160.00	2326.05	-575.55	-168.23	0.0	-26.80	-635.82	-328.32	0.015	2.763	3.471
1115.00	2319.30	-575.63	-167.75	0.0	-26.80	-635.82	-328.32	0.015	2.759	3.482
1070.00	2319.30	-575.63	-167.75	0.0	-26.80	-635.82	-328.32	0.015	2.759	3.482
1025.00	1.465e+04	-128.29	99.57	0.0	-52.28	-544.49	-95.81	0.601	1.188	0.224
985.00	1.083e+04	-102.23	128.80	0.0	-52.28	-542.49	-74.78	0.744	1.130	0.289
945.00	1.083e+04	-102.21	128.80	0.0	-52.28	-542.49	-74.78	0.744	1.130	0.289
905.00	6.437e+04	-130.89	142.36	0.0	-52.28	-436.66	166.12	0.443	1.017	0.032
855.00	2.344e+04	10.15	277.19	0.0	-52.28	-430.77	347.85	0.460	1.438	0.099
805.00	1.496e+04	-105.98	181.79	0.0	-52.28	-430.86	314.26	0.449	1.073	0.180
755.00	1.478e+04	-111.83	175.63	0.0	-52.28	-430.86	314.26	0.449	1.054	0.189
705.00	1.434e+04	-113.81	161.90	0.0	-52.28	-431.46	281.46	0.467	1.028	0.157
655.00	1.389e+04	-115.92	147.28	0.0	-52.28	-431.46	281.46	0.467	1.022	0.177
605.00	1.373e+04	-110.92	157.10	0.0	-52.28	-431.43	318.26	0.449	1.058	0.210
555.00	1.499e+04	-84.11	147.58	0.0	-52.28	-417.55	263.67	0.542	1.003	0.142
535.00	462.89	-284.62	710.53	0.0	0.0	-295.19	710.53	0.049	0.058	0.0
505.00	1.751e+04	-80.04	167.93	0.0	-52.28	-417.49	314.16	0.560	0.998	0.187
455.00	1.393e+05	-28.92	228.10	0.0	-52.28	-380.74	478.92	0.654	0.963	0.374
404.44	1.813e+04	-50.00	221.17	0.0	-52.28	-389.48	517.14	0.548	1.015	0.444
378.89	7112.79	-473.91	-262.63	0.0	-6.20	-445.72	-328.72	2.380	0.183	0.414
353.89	2.196e+04	-32.62	456.21	0.0	-61.93	-349.91	587.97	0.556	0.867	0.279
303.33	1.928e+04	-91.51	295.05	0.0	-61.93	-423.33	593.38	0.329	1.179	0.506
252.78	2.190e+04	-176.89	242.77	0.0	-61.93	-426.16	607.02	0.312	0.909	0.621
202.22	1.592e+04	-73.92	284.63	0.0	-61.93	-426.16	607.02	0.312	1.284	0.549
151.67	1.601e+04	-65.56	283.49	0.0	-61.93	-426.19	571.76	0.342	1.256	0.478
122.00	7167.74	-473.02	-262.23	0.0	-6.20	-445.72	-328.72	2.380	0.177	0.416
101.11	1.343e+04	-59.25	403.57	0.0	-61.93	-361.56	648.71	0.484	0.885	0.510
88.00	511.85	445.72	710.53	0.0	0.0	459.84	710.53	0.039	0.268	0.0
80.00	1592.11	106.62	-334.97	0.0	0.0	112.14	-334.97	0.080	0.025	0.0
50.56	1.912e+04	-72.11	249.76	0.0	-61.93	-425.00	501.84	0.409	1.124	0.402
Risulta	5.465e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	5.029	0.199	0.036	1866.06	0.3	2.721e+04	5.0	6.52e-03	1.19e-06	0.0	0.0
2	5.128	0.195	0.036	2457.01	0.4	1.427e+05	26.1	0.04	6.64e-06	0.0	0.0
3	7.049	0.142	0.036	3.504e+05	64.1	811.79	0.1	11.65	2.13e-03	0.0	0.0
4	7.913	0.126	0.036	7448.91	1.4	1.226e+05	22.4	16.77	3.07e-03	0.0	0.0
5	8.299	0.120	0.036	2104.23	0.4	1.244e+04	2.3	10.80	1.98e-03	0.0	0.0
6	8.598	0.116	0.036	1063.31	0.2	1.583e+04	2.9	7.32e-04	0.0	0.0	0.0
7	9.293	0.108	0.036	3202.37	0.6	311.55	5.70e-02	9.08	1.66e-03	0.0	0.0
8	9.483	0.105	0.036	1.194e+04	2.2	2.259e+04	4.1	111.32	2.04e-02	0.0	0.0
9	9.789	0.102	0.037	1549.68	0.3	2453.61	0.4	27.74	5.08e-03	0.0	0.0
10	10.492	0.095	0.037	2.455e+04	4.5	2429.66	0.4	4.84	8.86e-04	0.0	0.0
11	11.063	0.090	0.038	1.567e+04	2.9	9207.29	1.7	2.10	3.85e-04	0.0	0.0
12	11.694	0.086	0.038	4143.31	0.8	4.202e+04	7.7	0.71	1.30e-04	0.0	0.0
13	12.282	0.081	0.039	6449.23	1.2	9552.64	1.7	17.71	3.24e-03	0.0	0.0
14	13.117	0.076	0.039	7860.57	1.4	3774.59	0.7	0.18	3.25e-05	0.0	0.0
15	13.350	0.075	0.039	5.82	1.07e-03	18.48	3.38e-03	1.34	2.44e-04	0.0	0.0
16	13.449	0.074	0.039	1193.18	0.2	5209.81	1.0	69.37	1.27e-02	0.0	0.0
17	14.421	0.069	0.040	9784.36	1.8	36.87	6.75e-03	57.59	1.05e-02	0.0	0.0
18	14.733	0.068	0.040	597.10	0.1	1662.48	0.3	36.05	6.60e-03	0.0	0.0
19	15.311	0.065	0.040	766.40	0.1	9393.06	1.7	87.09	1.59e-02	0.0	0.0
20	15.578	0.064	0.040	4461.95	0.8	3.62	6.63e-04	6.32	1.16e-03	0.0	0.0
21	15.965	0.063	0.041	4954.49	0.9	471.24	8.62e-02	45.17	8.26e-03	0.0	0.0
22	16.516	0.061	0.041	5935.85	1.1	0.32	5.91e-05	286.98	5.25e-02	0.0	0.0
23	16.661	0.060	0.041	218.14	3.99e-02	4005.87	0.7	93.58	1.71e-02	0.0	0.0
24	17.136	0.058	0.041	571.36	0.1	5254.29	1.0	21.87	4.00e-03	0.0	0.0
25	17.517	0.057	0.041	8.80	1.61e-03	958.34	0.2	20.59	3.77e-03	0.0	0.0
26	17.774	0.056	0.041	43.74	8.00e-03	8140.53	1.5	0.39	7.09e-05	0.0	0.0
27	18.243	0.055	0.041	42.95	7.86e-03	1147.99	0.2	870.37	0.2	0.0	0.0
28	18.742	0.053	0.041	1565.71	0.3	2297.54	0.4	4110.75	0.8	0.0	0.0
29	19.555	0.051	0.042	44.84	8.20e-03	3926.25	0.7	2688.58	0.5	0.0	0.0
30	19.803	0.050	0.042	1933.85	0.4	188.46	3.45e-02	5886.35	1.1	0.0	0.0
31	20.171	0.050	0.042	11.93	2.18e-03	24.46	4.48e-03	7155.39	1.3	0.0	0.0
32	20.287	0.049	0.042	1775.31	0.3	342.01	6.26e-02	4494.37	0.8	0.0	0.0
33	20.629	0.048	0.042	626.28	0.1	0.04	8.22e-06	0.55	1.01e-04	0.0	0.0
34	21.018	0.048	0.042	1817.64	0.3	2454.77	0.4	868.55	0.2	0.0	0.0
35	21.224	0.047	0.042	334.59	6.12e-02	6.50	1.19e-03	2229.28	0.4	0.0	0.0
36	21.654	0.046	0.042	1.344e+04	2.5	452.70	8.28e-02	5786.46	1.1	0.0	0.0
37	22.114	0.045	0.042	161.20	2.95e-02	190.73	3.49e-02	1686.09	0.3	0.0	0.0
38	22.421	0.045	0.042	0.26	4.73e-05	0.36	6.57e-05	9816.41	1.8	0.0	0.0
39	22.627	0.044	0.042	90.47	1.66e-02	1908.54	0.3	829.52	0.2	0.0	0.0
40	22.751	0.044	0.042	75.68	1.38e-02	401.91	7.35e-02	4594.39	0.8	0.0	0.0
41	23.049	0.043	0.042	321.89	5.89e-02	2102.15	0.4	4813.82	0.9	0.0	0.0
42	23.539	0.042	0.043	888.20	0.2	34.39	6.29e-03	3.223e+04	5.9	0.0	0.0
43	23.974	0.042	0.043	457.57	8.37e-02	13.94	2.55e-03	1852.67	0.3	0.0	0.0
44	24.123	0.041	0.043	1451.64	0.3	5334.36	1.0	2931.76	0.5	0.0	0.0
45	24.382	0.041	0.043	1235.36	0.2	392.28	7.18e-02	828.08	0.2	0.0	0.0
46	24.532	0.041	0.043	445.78	8.16e-02	2527.54	0.5	39.78	7.28e-03	0.0	0.0
47	25.030	0.040	0.043	146.18	2.67e-02	31.56	5.77e-03	718.13	0.1	0.0	0.0
48	25.338	0.039	0.043	677.58	0.1	113.32	2.07e-02	1.458e+04	2.7	0.0	0.0
49	25.666	0.039	0.043	127.75	2.34e-02	4323.97	0.8	9786.24	1.8	0.0	0.0
50	26.072	0.038	0.043	8.11	1.48e-03	1351.54	0.2	2091.99	0.4	0.0	0.0
51	26.381	0.038	0.043	2003.93	0.4	69.73	1.28e-02	2260.63	0.4	0.0	0.0
52	26.843	0.037	0.043	0.29	5.23e-05	515.08	9.43e-02	1.679e+04	3.1	0.0	0.0
53	27.165	0.037	0.043	226.68	4.15e-02	5249.68	1.0	8.039e+04	14.7	0.0	0.0
54	27.258	0.037	0.043	301.40	5.52e-02	970.77	0.2	5.532e+04	10.1	0.0	0.0
55	27.582	0.036	0.043	0.12	2.19e-05	3460.28	0.6	1549.98	0.3	0.0	0.0
56	27.725	0.036	0.043	33.58	6.14e-03	446.25	8.17e-02	2.098e+04	3.8	0.0	0.0
57	27.928	0.036	0.043	0.02	3.66e-06	3712.23	0.7	47.98	8.78e-03	0.0	0.0
58	28.101	0.036	0.043	62.23	1.14e-02	19.55	3.58e-03	2055.82	0.4	0.0	0.0
59	28.433	0.035	0.043	161.28	2.95e-02	2626.03	0.5	3334.77	0.6	0.0	0.0
60	29.327	0.034	0.043	568.95	0.1	3178.03	0.6	676.29	0.1	0.0	0.0
61	29.912	0.033	0.043	5.35	9.78e-04	1821.28	0.3	3314.28	0.6	0.0	0.0
62	30.051	0.033	0.043	6.42	1.17e-03	452.14	8.27e-02	2547.75	0.5	0.0	0.0
63	30.373	0.033	0.043	3.38	6.18e-04	750.86	0.1	2053.86	0.4	0.0	0.0
64	30.647	0.033	0.043	6.00	1.10e-03	131.20	2.40e-02	1.144e+04	2.1	0.0	0.0
65	30.980	0.032	0.043	23.72	4.34e-03	1077.83	0.2	3.662e+04	6.7	0.0	0.0
66	31.224	0.032	0.044	0.52	9.54e-05	0.06	1.07e-05	1657.24	0.3	0.0	0.0
67	31.780	0.031	0.044	441.89	8.09e-02	434.61	7.95e-02	1047.37	0.2	0.0	0.0
68	32.538	0.031	0.044	755.40	0.1	92.41	1.69e-02	2130.28	0.4	0.0	0.0
69	32.677	0.031	0.044	78.63	1.44e-02	2915.48	0.5	1138.55	0.2	0.0	0.0
70	32.999	0.030	0.044	195.39	3.58e-02	227.44	4.16e-02	2206.08	0.4	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	Z %	Energia	Energia x v
71	33.219	0.030	0.044	74.00	1.35e-02	56.85	1.04e-02	1670.70	0.3	0.0	0.0
72	33.458	0.030	0.044	131.91	2.41e-02	589.71	0.1	4375.01	0.8	0.0	0.0
73	33.818	0.030	0.044	47.67	8.72e-03	172.34	3.15e-02	187.57	3.43e-02	0.0	0.0
74	33.924	0.029	0.044	252.64	4.62e-02	299.67	5.48e-02	1544.79	0.3	0.0	0.0
75	34.309	0.029	0.044	1625.37	0.3	26.57	4.86e-03	2031.61	0.4	0.0	0.0
76	34.786	0.029	0.044	85.19	1.56e-02	106.44	1.95e-02	97.05	1.78e-02	0.0	0.0
77	34.861	0.029	0.044	443.68	8.12e-02	211.03	3.86e-02	381.86	6.99e-02	0.0	0.0
78	35.161	0.028	0.044	2.38	4.35e-04	838.98	0.2	532.69	9.75e-02	0.0	0.0
79	35.340	0.028	0.044	91.88	1.68e-02	463.41	8.48e-02	66.93	1.22e-02	0.0	0.0
80	35.803	0.028	0.044	136.18	2.49e-02	715.52	0.1	3554.20	0.7	0.0	0.0
81	36.292	0.028	0.044	1017.12	0.2	24.16	4.42e-03	1734.44	0.3	0.0	0.0
82	36.426	0.027	0.044	69.34	1.27e-02	1203.31	0.2	7139.08	1.3	0.0	0.0
83	36.628	0.027	0.044	10.21	1.87e-03	435.47	7.97e-02	11.71	2.14e-03	0.0	0.0
84	37.020	0.027	0.044	507.80	9.29e-02	206.50	3.78e-02	622.70	0.1	0.0	0.0
85	37.554	0.027	0.044	0.06	1.11e-05	37.73	6.90e-03	179.27	3.28e-02	0.0	0.0
86	37.627	0.027	0.044	211.99	3.88e-02	368.92	6.75e-02	453.52	8.30e-02	0.0	0.0
87	38.110	0.026	0.044	138.53	2.53e-02	109.06	2.00e-02	616.40	0.1	0.0	0.0
88	38.390	0.026	0.044	34.51	6.31e-03	615.97	0.1	8863.21	1.6	0.0	0.0
89	38.841	0.026	0.044	180.91	3.31e-02	40.62	7.43e-03	65.45	1.20e-02	0.0	0.0
90	39.181	0.026	0.044	1113.60	0.2	452.61	8.28e-02	1511.85	0.3	0.0	0.0
91	39.461	0.025	0.044	1174.30	0.2	553.26	0.1	693.65	0.1	0.0	0.0
92	39.516	0.025	0.044	1806.71	0.3	99.03	1.81e-02	143.58	2.63e-02	0.0	0.0
93	39.944	0.025	0.044	22.99	4.21e-03	372.74	6.82e-02	34.62	6.33e-03	0.0	0.0
94	40.359	0.025	0.044	58.82	1.08e-02	0.11	1.98e-05	554.52	0.1	0.0	0.0
95	40.411	0.025	0.044	1.29	2.36e-04	5.09	9.31e-04	51.79	9.48e-03	0.0	0.0
96	40.473	0.025	0.044	55.00	1.01e-02	892.60	0.2	1076.89	0.2	0.0	0.0
97	40.604	0.025	0.044	25.68	4.70e-03	3.95	7.22e-04	1312.79	0.2	0.0	0.0
98	41.081	0.024	0.044	203.92	3.73e-02	96.97	1.77e-02	2693.53	0.5	0.0	0.0
99	41.492	0.024	0.044	2.35	4.30e-04	14.12	2.58e-03	2101.25	0.4	0.0	0.0
100	41.909	0.024	0.044	94.85	1.74e-02	361.57	6.62e-02	464.84	8.51e-02	0.0	0.0
101	42.212	0.024	0.044	19.90	3.64e-03	254.44	4.66e-02	451.84	8.27e-02	0.0	0.0
102	42.335	0.024	0.044	68.59	1.26e-02	250.08	4.58e-02	1.024e+04	1.9	0.0	0.0
103	42.388	0.024	0.044	59.95	1.10e-02	592.68	0.1	824.69	0.2	0.0	0.0
104	43.370	0.023	0.044	70.70	1.29e-02	28.11	5.14e-03	1129.51	0.2	0.0	0.0
105	43.971	0.023	0.044	79.10	1.45e-02	112.26	2.05e-02	95.07	1.74e-02	0.0	0.0
106	44.262	0.023	0.044	51.99	9.51e-03	20.33	3.72e-03	107.96	1.98e-02	0.0	0.0
107	44.407	0.023	0.044	45.26	8.28e-03	18.08	3.31e-03	659.75	0.1	0.0	0.0
108	44.917	0.022	0.044	262.82	4.81e-02	173.12	3.17e-02	2645.65	0.5	0.0	0.0
109	45.185	0.022	0.044	155.46	2.84e-02	312.72	5.72e-02	486.17	8.90e-02	0.0	0.0
110	45.342	0.022	0.044	93.91	1.72e-02	268.88	4.92e-02	238.59	4.37e-02	0.0	0.0
111	45.683	0.022	0.044	345.09	6.31e-02	89.87	1.64e-02	1.11	2.04e-04	0.0	0.0
112	46.567	0.021	0.045	132.77	2.43e-02	227.78	4.17e-02	0.14	2.52e-05	0.0	0.0
113	46.864	0.021	0.045	18.54	3.39e-03	348.71	6.38e-02	624.22	0.1	0.0	0.0
114	46.895	0.021	0.045	0.09	1.58e-05	12.94	2.37e-03	4399.06	0.8	0.0	0.0
115	47.173	0.021	0.045	0.02	4.54e-06	10.40	1.90e-03	1000.13	0.2	0.0	0.0
116	47.543	0.021	0.045	35.76	6.54e-03	105.02	1.92e-02	7058.63	1.3	0.0	0.0
117	47.801	0.021	0.045	67.17	1.23e-02	122.65	2.24e-02	186.55	3.41e-02	0.0	0.0
118	48.130	0.021	0.045	56.75	1.04e-02	140.37	2.57e-02	65.81	1.20e-02	0.0	0.0
119	48.786	0.020	0.045	7.83	1.43e-03	21.21	3.88e-03	217.17	3.97e-02	0.0	0.0
120	49.200	0.020	0.045	58.87	1.08e-02	138.10	2.53e-02	1280.56	0.2	0.0	0.0
121	49.448	0.020	0.045	0.11	2.10e-05	498.09	9.11e-02	214.81	3.93e-02	0.0	0.0
122	49.689	0.020	0.045	44.85	8.21e-03	61.25	1.12e-02	307.53	5.63e-02	0.0	0.0
123	49.838	0.020	0.045	80.88	1.48e-02	86.49	1.58e-02	289.39	5.30e-02	0.0	0.0
124	50.011	0.020	0.045	52.99	9.70e-03	70.93	1.30e-02	111.32	2.04e-02	0.0	0.0
125	50.349	0.020	0.045	202.66	3.71e-02	40.40	7.39e-03	43.67	7.99e-03	0.0	0.0
126	50.537	0.020	0.045	70.14	1.28e-02	0.57	1.04e-04	568.44	0.1	0.0	0.0
127	51.257	0.020	0.045	1560.24	0.3	3.77	6.90e-04	1363.64	0.2	0.0	0.0
128	51.687	0.019	0.045	152.46	2.79e-02	0.95	1.73e-04	641.58	0.1	0.0	0.0
129	51.800	0.019	0.045	415.52	7.60e-02	0.10	1.80e-05	5.29e-03	0.0	0.0	0.0
130	52.229	0.019	0.045	0.42	7.70e-05	36.46	6.67e-03	177.91	3.26e-02	0.0	0.0
131	52.479	0.019	0.045	201.60	3.69e-02	3.37	6.17e-04	176.92	3.24e-02	0.0	0.0
132	52.818	0.019	0.045	72.79	1.33e-02	14.65	2.68e-03	724.86	0.1	0.0	0.0
133	52.861	0.019	0.045	128.54	2.35e-02	103.69	1.90e-02	379.23	6.94e-02	0.0	0.0
134	53.184	0.019	0.045	1136.73	0.2	104.51	1.91e-02	438.94	8.03e-02	0.0	0.0
135	53.368	0.019	0.045	217.07	3.97e-02	40.71	7.45e-03	554.60	0.1	0.0	0.0
136	53.713	0.019	0.045	417.61	7.64e-02	58.80	1.08e-02	4.35	7.97e-04	0.0	0.0
137	53.778	0.019	0.045	19.43	3.56e-03	320.75	5.87e-02	4.62	8.46e-04	0.0	0.0
138	53.856	0.019	0.045	354.56	6.49e-02	156.39	2.86e-02	491.22	8.99e-02	0.0	0.0
139	54.241	0.018	0.045	0.78	1.42e-04	5.97	1.09e-03	1161.84	0.2	0.0	0.0
140	54.498	0.018	0.045	1307.27	0.2	247.13	4.52e-02	58.59	1.07e-02	0.0	0.0
141	54.531	0.018	0.045	0.07	1.24e-05	234.33	4.29e-02	1866.35	0.3	0.0	0.0
142	54.855	0.018	0.045	21.97	4.02e-03	47.15	8.63e-03	521.36	9.54e-02	0.0	0.0
143	55.194	0.018	0.045	7.95	1.46e-03	29.57	5.41e-03	479.28	8.77e-02	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
144	55.309	0.018	0.045	8.41	1.54e-03	68.65	1.26e-02	442.08	8.09e-02	0.0	0.0
145	55.603	0.018	0.045	0.05	9.52e-06	24.48	4.48e-03	30.68	5.61e-03	0.0	0.0
146	56.036	0.018	0.045	77.54	1.42e-02	163.27	2.99e-02	170.59	3.12e-02	0.0	0.0
147	56.297	0.018	0.045	55.83	1.02e-02	756.33	0.1	29.32	5.36e-03	0.0	0.0
148	56.457	0.018	0.045	69.96	1.28e-02	35.70	6.53e-03	0.51	9.27e-05	0.0	0.0
149	56.989	0.018	0.045	57.48	1.05e-02	10.66	1.95e-03	724.04	0.1	0.0	0.0
150	57.211	0.017	0.045	363.78	6.66e-02	4.22	7.73e-04	90.82	1.66e-02	0.0	0.0
151	57.636	0.017	0.045	68.76	1.26e-02	0.31	5.68e-05	38.63	7.07e-03	0.0	0.0
152	57.991	0.017	0.045	69.37	1.27e-02	40.60	7.43e-03	18.67	3.42e-03	0.0	0.0
153	58.025	0.017	0.045	251.99	4.61e-02	242.66	4.44e-02	110.23	2.02e-02	0.0	0.0
154	58.262	0.017	0.045	987.84	0.2	92.84	1.70e-02	168.55	3.08e-02	0.0	0.0
155	58.550	0.017	0.045	307.47	5.63e-02	15.83	2.90e-03	160.81	2.94e-02	0.0	0.0
156	58.696	0.017	0.045	158.86	2.91e-02	17.32	3.17e-03	1.07	1.95e-04	0.0	0.0
157	58.957	0.017	0.045	204.22	3.74e-02	538.37	9.85e-02	63.36	1.16e-02	0.0	0.0
158	59.088	0.017	0.045	0.07	1.36e-05	136.48	2.50e-02	166.69	3.05e-02	0.0	0.0
159	59.626	0.017	0.045	0.38	7.03e-05	3.68	6.73e-04	0.18	3.35e-05	0.0	0.0
160	59.749	0.017	0.045	2.17	3.96e-04	96.29	1.76e-02	3.37	6.17e-04	0.0	0.0
161	60.317	0.017	0.045	70.72	1.29e-02	48.19	8.82e-03	49.37	9.03e-03	0.0	0.0
162	60.507	0.017	0.045	13.66	2.50e-03	177.96	3.26e-02	30.41	5.56e-03	0.0	0.0
163	60.978	0.016	0.045	20.60	3.77e-03	14.77	2.70e-03	1.06	1.94e-04	0.0	0.0
164	61.146	0.016	0.045	149.86	2.74e-02	6.81	1.25e-03	12.19	2.23e-03	0.0	0.0
165	61.557	0.016	0.045	21.30	3.90e-03	3.51	6.43e-04	2.23	4.08e-04	0.0	0.0
166	61.919	0.016	0.045	451.98	8.27e-02	215.33	3.94e-02	324.18	5.93e-02	0.0	0.0
167	61.982	0.016	0.045	136.33	2.49e-02	0.12	2.26e-05	84.99	1.56e-02	0.0	0.0
168	62.451	0.016	0.045	192.17	3.52e-02	186.96	3.42e-02	176.73	3.23e-02	0.0	0.0
169	62.786	0.016	0.045	139.10	2.55e-02	30.12	5.51e-03	714.80	0.1	0.0	0.0
170	62.898	0.016	0.045	173.26	3.17e-02	21.85	4.00e-03	30.32	5.55e-03	0.0	0.0
171	63.280	0.016	0.045	120.99	2.21e-02	246.12	4.50e-02	3.92	7.17e-04	0.0	0.0
172	63.473	0.016	0.045	45.97	8.41e-03	0.77	1.40e-04	0.04	6.53e-06	0.0	0.0
173	63.624	0.016	0.045	150.75	2.76e-02	409.01	7.48e-02	231.54	4.24e-02	0.0	0.0
174	63.713	0.016	0.045	182.19	3.33e-02	42.75	7.82e-03	1.51e-03	0.0	0.0	0.0
175	63.980	0.016	0.045	7.18	1.31e-03	5.50	1.01e-03	1079.01	0.2	0.0	0.0
176	64.013	0.016	0.045	136.29	2.49e-02	18.59	3.40e-03	37.69	6.90e-03	0.0	0.0
177	64.183	0.016	0.045	8.74	1.60e-03	331.76	6.07e-02	139.32	2.55e-02	0.0	0.0
178	64.519	0.015	0.045	188.47	3.45e-02	214.92	3.93e-02	402.35	7.36e-02	0.0	0.0
179	64.668	0.015	0.045	89.13	1.63e-02	30.31	5.55e-03	2.15	3.94e-04	0.0	0.0
180	65.065	0.015	0.045	61.36	1.12e-02	484.11	8.86e-02	437.74	8.01e-02	0.0	0.0
181	65.425	0.015	0.045	8.69	1.59e-03	367.03	6.72e-02	14.72	2.69e-03	0.0	0.0
182	65.739	0.015	0.045	0.56	1.02e-04	475.09	8.69e-02	144.24	2.64e-02	0.0	0.0
183	66.044	0.015	0.045	3.55	6.50e-04	45.75	8.37e-03	163.76	3.00e-02	0.0	0.0
184	66.069	0.015	0.045	124.24	2.27e-02	65.61	1.20e-02	152.65	2.79e-02	0.0	0.0
185	66.353	0.015	0.045	7.28	1.33e-03	16.16	2.96e-03	57.33	1.05e-02	0.0	0.0
186	66.621	0.015	0.045	4.09	7.49e-04	81.21	1.49e-02	418.56	7.66e-02	0.0	0.0
187	66.903	0.015	0.045	17.80	3.26e-03	66.70	1.22e-02	7.14	1.31e-03	0.0	0.0
188	67.062	0.015	0.045	23.05	4.22e-03	112.66	2.06e-02	94.17	1.72e-02	0.0	0.0
189	67.147	0.015	0.045	6.40	1.17e-03	24.81	4.54e-03	6897.78	1.3	0.0	0.0
190	67.279	0.015	0.045	10.87	1.99e-03	57.75	1.06e-02	4.75	8.69e-04	0.0	0.0
191	67.622	0.015	0.045	150.17	2.75e-02	1.09	1.99e-04	99.68	1.82e-02	0.0	0.0
192	67.821	0.015	0.045	11.02	2.02e-03	26.49	4.85e-03	17.86	3.27e-03	0.0	0.0
193	68.042	0.015	0.045	5.76	1.05e-03	252.67	4.62e-02	1.68	3.07e-04	0.0	0.0
194	68.381	0.015	0.045	2.62	4.79e-04	150.90	2.76e-02	104.19	1.91e-02	0.0	0.0
195	68.452	0.015	0.045	72.38	1.32e-02	9.39	1.72e-03	277.84	5.08e-02	0.0	0.0
196	68.748	0.015	0.045	7.31	1.34e-03	2.07	3.79e-04	712.77	0.1	0.0	0.0
197	69.446	0.014	0.045	56.26	1.03e-02	0.88	1.61e-04	277.44	5.08e-02	0.0	0.0
198	69.579	0.014	0.045	5.93	1.08e-03	121.71	2.23e-02	865.33	0.2	0.0	0.0
199	69.683	0.014	0.045	1.82	3.33e-04	266.31	4.87e-02	60.14	1.10e-02	0.0	0.0
200	70.109	0.014	0.045	30.14	5.51e-03	345.11	6.31e-02	1.73	3.17e-04	0.0	0.0
201	70.486	0.014	0.045	59.23	1.08e-02	36.24	6.63e-03	143.19	2.62e-02	0.0	0.0
202	70.538	0.014	0.045	0.60	1.09e-04	0.92	1.68e-04	4.39	8.04e-04	0.0	0.0
203	70.853	0.014	0.045	4.72	8.64e-04	44.23	8.09e-03	0.02	4.17e-06	0.0	0.0
204	70.942	0.014	0.045	33.03	6.04e-03	84.26	1.54e-02	247.15	4.52e-02	0.0	0.0
205	71.037	0.014	0.045	38.82	7.10e-03	41.66	7.62e-03	510.66	9.34e-02	0.0	0.0
206	71.253	0.014	0.045	41.73	7.64e-03	2.37	4.33e-04	9.25	1.69e-03	0.0	0.0
207	71.542	0.014	0.045	56.11	1.03e-02	21.13	3.87e-03	119.62	2.19e-02	0.0	0.0
208	71.632	0.014	0.045	136.70	2.50e-02	1.50	2.74e-04	508.80	9.31e-02	0.0	0.0
209	72.194	0.014	0.045	56.97	1.04e-02	7.22	1.32e-03	13.12	2.40e-03	0.0	0.0
210	72.358	0.014	0.045	2.05e-06	0.0	4.58	8.38e-04	6.92	1.27e-03	0.0	0.0
211	72.464	0.014	0.045	173.29	3.17e-02	6.39	1.17e-03	112.01	2.05e-02	0.0	0.0
212	72.587	0.014	0.045	0.60	1.11e-04	2.15	3.94e-04	347.42	6.36e-02	0.0	0.0
213	73.035	0.014	0.045	0.75	1.37e-04	60.28	1.10e-02	297.78	5.45e-02	0.0	0.0
214	73.078	0.014	0.045	14.70	2.69e-03	146.72	2.68e-02	315.29	5.77e-02	0.0	0.0
215	73.518	0.014	0.045	0.57	1.04e-04	0.05	9.98e-06	126.14	2.31e-02	0.0	0.0
216	73.686	0.014	0.045	14.58	2.67e-03	24.25	4.44e-03	194.86	3.57e-02	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spetttrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
217	74.012	0.014	0.045	5.89	1.08e-03	29.80	5.45e-03	467.24	8.55e-02	0.0	0.0
218	74.306	0.013	0.045	6.72	1.23e-03	8.93	1.63e-03	1103.83	0.2	0.0	0.0
219	74.431	0.013	0.045	235.87	4.32e-02	25.10	4.59e-03	211.63	3.87e-02	0.0	0.0
220	75.017	0.013	0.045	0.02	4.52e-06	47.20	8.64e-03	461.64	8.45e-02	0.0	0.0
Risulta				5.260e+05		5.295e+05		4.780e+05			
In percentuale				96.25		96.88		87.47			

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
cm	daN	cm	cm	cm	cm	cm	cm			
1340.00	96.19	-491.36	-334.97	0.0	0.0	-491.36	-334.97	0.155	0.0	0.0
1295.00	116.44	-491.36	-334.97	0.0	0.0	-491.36	-334.97	1.791	0.0	0.0
1250.00	101.25	-491.36	-334.97	0.0	0.0	-491.36	-334.97	1.791	0.0	0.0
1205.00	1203.52	-572.28	-173.84	0.0	26.80	-635.82	-328.32	0.015	2.913	3.350
1195.00	7848.27	-175.90	173.40	0.0	15.15	-313.36	198.69	0.654	1.046	0.168
1160.00	2326.05	-575.55	-168.23	0.0	26.80	-635.82	-328.32	0.015	2.763	3.471
1115.00	2319.30	-575.63	-167.75	0.0	26.80	-635.82	-328.32	0.015	2.759	3.482
1070.00	2319.30	-575.63	-167.75	0.0	26.80	-635.82	-328.32	0.015	2.759	3.482
1025.00	1.465e+04	-128.29	99.57	0.0	52.28	-544.49	-95.81	0.601	1.188	0.224
985.00	1.083e+04	-102.23	128.80	0.0	52.28	-542.49	-74.78	0.744	1.130	0.289
945.00	1.083e+04	-102.21	128.80	0.0	52.28	-542.49	-74.78	0.744	1.130	0.289
905.00	6.437e+04	-130.89	142.36	0.0	52.28	-436.66	166.12	0.443	1.017	0.032
855.00	2.344e+04	10.15	277.19	0.0	52.28	-430.77	347.85	0.460	1.438	0.099
805.00	1.496e+04	-105.98	181.79	0.0	52.28	-430.86	314.26	0.449	1.073	0.180
755.00	1.478e+04	-111.83	175.63	0.0	52.28	-430.86	314.26	0.449	1.054	0.189
705.00	1.434e+04	-113.81	161.90	0.0	52.28	-431.46	281.46	0.467	1.028	0.157
655.00	1.389e+04	-115.92	147.28	0.0	52.28	-431.46	281.46	0.467	1.022	0.177
605.00	1.373e+04	-110.92	157.10	0.0	52.28	-431.43	318.26	0.449	1.058	0.210
555.00	1.499e+04	-84.11	147.58	0.0	52.28	-417.55	263.67	0.542	1.003	0.142
535.00	462.89	-284.62	710.53	0.0	0.0	-295.19	710.53	0.049	0.058	0.0
505.00	1.751e+04	-80.04	167.93	0.0	52.28	-417.49	314.16	0.560	0.998	0.187
455.00	1.393e+05	-28.92	228.10	0.0	52.28	-380.74	478.92	0.654	0.963	0.374
404.44	1.813e+04	-50.00	221.17	0.0	52.28	-389.48	517.14	0.548	1.015	0.444
378.89	7112.79	-473.91	-262.63	0.0	6.20	-445.72	-328.72	2.380	0.183	0.414
353.89	2.196e+04	-32.62	456.21	0.0	61.93	-349.91	587.97	0.556	0.867	0.279
303.33	1.928e+04	-91.51	295.05	0.0	61.93	-423.33	593.38	0.329	1.179	0.506
252.78	2.190e+04	-176.89	242.77	0.0	61.93	-426.16	607.02	0.312	0.909	0.621
202.22	1.592e+04	-73.92	284.63	0.0	61.93	-426.16	607.02	0.312	1.284	0.549
151.67	1.601e+04	-65.56	283.49	0.0	61.93	-426.19	571.76	0.342	1.256	0.478
122.00	7167.74	-473.02	-262.23	0.0	6.20	-445.72	-328.72	2.380	0.177	0.416
101.11	1.343e+04	-59.25	403.57	0.0	61.93	-361.56	648.71	0.484	0.885	0.510
88.00	511.85	445.72	710.53	0.0	0.0	459.84	710.53	0.039	0.268	0.0
80.00	1592.11	106.62	-334.97	0.0	0.0	112.14	-334.97	0.080	0.025	0.0
50.56	1.912e+04	-72.11	249.76	0.0	61.93	-425.00	501.84	0.409	1.124	0.402
Risulta	5.465e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	5.038	0.198	0.036	1031.38	0.2	3.924e+04	7.2	6.76e-03	1.24e-06	0.0	0.0
2	5.138	0.195	0.036	1002.63	0.2	1.313e+05	24.0	0.06	1.16e-05	0.0	0.0
3	7.421	0.135	0.036	3.605e+05	66.0	98.65	1.81e-02	14.96	2.74e-03	0.0	0.0
4	7.895	0.127	0.036	9359.96	1.7	1.163e+05	21.3	18.27	3.34e-03	0.0	0.0
5	8.269	0.121	0.036	703.38	0.1	1.132e+04	2.1	12.44	2.28e-03	0.0	0.0
6	8.569	0.117	0.036	838.44	0.2	2.047e+04	3.7	0.08	1.45e-05	0.0	0.0
7	9.390	0.106	0.036	1.100e+04	2.0	2.650e+04	4.8	92.94	1.70e-02	0.0	0.0
8	9.508	0.105	0.037	3652.96	0.7	7.65	1.40e-03	17.29	3.16e-03	0.0	0.0
9	9.789	0.102	0.037	1463.78	0.3	2047.23	0.4	14.11	2.58e-03	0.0	0.0
10	10.334	0.097	0.037	2.182e+04	4.0	6159.24	1.1	0.88	1.61e-04	0.0	0.0
11	10.972	0.091	0.038	721.82	0.1	3265.21	0.6	14.43	2.64e-03	0.0	0.0
12	11.701	0.085	0.038	4956.24	0.9	3.773e+04	6.9	1.07	1.96e-04	0.0	0.0
13	12.259	0.082	0.039	1.497e+04	2.7	1.796e+04	3.3	5.25	9.61e-04	0.0	0.0
14	12.323	0.081	0.039	2134.29	0.4	2570.06	0.5	5.08	9.30e-04	0.0	0.0
15	13.284	0.075	0.039	1.183e+04	2.2	193.66	3.54e-02	1.75	3.20e-04	0.0	0.0
16	13.575	0.074	0.040	5179.70	0.9	1528.01	0.3	120.02	2.20e-02	0.0	0.0
17	14.077	0.071	0.040	2033.63	0.4	1424.85	0.3	6.91	1.26e-03	0.0	0.0
18	14.578	0.069	0.040	733.68	0.1	2426.54	0.4	101.92	1.86e-02	0.0	0.0
19	15.097	0.066	0.040	2775.07	0.5	5957.55	1.1	54.25	9.93e-03	0.0	0.0
20	15.386	0.065	0.040	1192.69	0.2	147.10	2.69e-02	1.98	3.62e-04	0.0	0.0
21	15.793	0.063	0.041	4087.57	0.7	2569.01	0.5	13.72	2.51e-03	0.0	0.0
22	15.900	0.063	0.041	372.23	6.81e-02	1214.19	0.2	189.41	3.47e-02	0.0	0.0
23	16.229	0.062	0.041	1099.24	0.2	1104.65	0.2	27.01	4.94e-03	0.0	0.0
24	16.655	0.060	0.041	0.03	6.23e-06	4731.47	0.9	46.50	8.51e-03	0.0	0.0
25	17.220	0.058	0.041	405.71	7.42e-02	128.03	2.34e-02	37.88	6.93e-03	0.0	0.0
26	17.519	0.057	0.041	323.66	5.92e-02	1.330e+04	2.4	1.09	2.00e-04	0.0	0.0
27	18.154	0.055	0.041	248.58	4.55e-02	1101.79	0.2	140.45	2.57e-02	0.0	0.0
28	18.519	0.054	0.041	516.26	9.45e-02	626.82	0.1	2911.68	0.5	0.0	0.0
29	18.967	0.053	0.042	33.63	6.15e-03	1399.27	0.3	3012.41	0.6	0.0	0.0
30	20.162	0.050	0.042	0.56	1.02e-04	145.58	2.66e-02	8108.48	1.5	0.0	0.0
31	20.197	0.050	0.042	231.53	4.24e-02	20.36	3.73e-03	1.130e+04	2.1	0.0	0.0
32	20.398	0.049	0.042	3080.17	0.6	6734.00	1.2	92.21	1.69e-02	0.0	0.0
33	20.878	0.048	0.042	7819.42	1.4	134.24	2.46e-02	2695.67	0.5	0.0	0.0
34	21.298	0.047	0.042	1.11	2.03e-04	33.19	6.07e-03	749.08	0.1	0.0	0.0
35	21.783	0.046	0.042	5383.10	1.0	102.89	1.88e-02	121.43	2.22e-02	0.0	0.0
36	22.131	0.045	0.042	3716.30	0.7	1683.67	0.3	7541.06	1.4	0.0	0.0
37	22.509	0.044	0.042	288.70	5.28e-02	256.42	4.69e-02	1.847e+04	3.4	0.0	0.0
38	22.746	0.044	0.042	331.50	6.07e-02	1111.37	0.2	1088.79	0.2	0.0	0.0
39	22.777	0.044	0.042	476.61	8.72e-02	248.90	4.55e-02	1725.91	0.3	0.0	0.0
40	23.012	0.043	0.042	3825.44	0.7	1011.29	0.2	4756.89	0.9	0.0	0.0
41	23.342	0.043	0.042	7.36	1.35e-03	107.13	1.96e-02	5451.15	1.0	0.0	0.0
42	23.452	0.043	0.042	99.93	1.83e-02	78.96	1.44e-02	1095.61	0.2	0.0	0.0
43	23.599	0.042	0.043	3861.18	0.7	1356.11	0.2	1.154e+04	2.1	0.0	0.0
44	23.965	0.042	0.043	0.15	2.83e-05	380.15	6.96e-02	4896.62	0.9	0.0	0.0
45	24.290	0.041	0.043	206.19	3.77e-02	369.02	6.75e-02	1.209e+04	2.2	0.0	0.0
46	24.482	0.041	0.043	223.17	4.08e-02	7170.25	1.3	3252.28	0.6	0.0	0.0
47	25.015	0.040	0.043	173.74	3.18e-02	48.14	8.81e-03	1.13	2.06e-04	0.0	0.0
48	25.114	0.040	0.043	4.17	7.62e-04	21.18	3.88e-03	5023.07	0.9	0.0	0.0
49	25.486	0.039	0.043	1107.81	0.2	888.73	0.2	0.82	1.50e-04	0.0	0.0
50	25.611	0.039	0.043	0.11	2.01e-05	396.00	7.25e-02	1.286e+04	2.4	0.0	0.0
51	26.142	0.038	0.043	75.42	1.38e-02	4096.96	0.7	1893.26	0.3	0.0	0.0
52	26.460	0.038	0.043	387.58	7.09e-02	79.17	1.45e-02	1769.07	0.3	0.0	0.0
53	26.993	0.037	0.043	159.10	2.91e-02	0.10	1.83e-05	3.785e+04	6.9	0.0	0.0
54	27.270	0.037	0.043	156.58	2.87e-02	9824.57	1.8	1.079e+05	19.8	0.0	0.0
55	27.569	0.036	0.043	797.70	0.1	13.46	2.46e-03	8053.38	1.5	0.0	0.0
56	27.688	0.036	0.043	97.53	1.78e-02	1580.26	0.3	7950.85	1.5	0.0	0.0
57	27.856	0.036	0.043	46.65	8.54e-03	1955.00	0.4	7254.71	1.3	0.0	0.0
58	28.030	0.036	0.043	138.77	2.54e-02	467.76	8.56e-02	1.196e+04	2.2	0.0	0.0
59	28.252	0.035	0.043	884.70	0.2	22.77	4.17e-03	1736.74	0.3	0.0	0.0
60	28.831	0.035	0.043	308.32	5.64e-02	240.44	4.40e-02	823.24	0.2	0.0	0.0
61	29.279	0.034	0.043	363.04	6.64e-02	4914.34	0.9	1368.46	0.3	0.0	0.0
62	29.467	0.034	0.043	623.62	0.1	2776.30	0.5	2016.70	0.4	0.0	0.0
63	30.331	0.033	0.043	147.92	2.71e-02	34.42	6.30e-03	4092.02	0.7	0.0	0.0
64	30.522	0.033	0.043	537.48	9.83e-02	845.07	0.2	8752.60	1.6	0.0	0.0
65	30.700	0.033	0.043	130.95	2.40e-02	898.10	0.2	200.53	3.67e-02	0.0	0.0
66	30.850	0.032	0.043	27.98	5.12e-03	79.20	1.45e-02	3.349e+04	6.1	0.0	0.0
67	30.999	0.032	0.043	316.15	5.78e-02	139.02	2.54e-02	1703.11	0.3	0.0	0.0
68	31.984	0.031	0.044	32.65	5.97e-03	590.07	0.1	401.84	7.35e-02	0.0	0.0
69	32.235	0.031	0.044	734.59	0.1	640.10	0.1	1.105e+04	2.0	0.0	0.0
70	32.386	0.031	0.044	126.31	2.31e-02	1387.35	0.3	1743.22	0.3	0.0	0.0
71	32.939	0.030	0.044	554.45	0.1	19.14	3.50e-03	295.62	5.41e-02	0.0	0.0
72	33.467	0.030	0.044	1338.78	0.2	1181.20	0.2	1247.64	0.2	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	Z %	Energia	Energia x v
73	33.708	0.030	0.044	1101.61	0.2	254.62	4.66e-02	613.15	0.1	0.0	0.0
74	33.901	0.029	0.044	726.11	0.1	104.57	1.91e-02	1075.71	0.2	0.0	0.0
75	34.398	0.029	0.044	325.37	5.95e-02	947.88	0.2	825.99	0.2	0.0	0.0
76	34.632	0.029	0.044	117.39	2.15e-02	40.97	7.50e-03	5.33	9.75e-04	0.0	0.0
77	35.053	0.029	0.044	373.03	6.83e-02	2.12	3.87e-04	1063.48	0.2	0.0	0.0
78	35.607	0.028	0.044	49.16	8.99e-03	207.44	3.80e-02	431.12	7.89e-02	0.0	0.0
79	35.871	0.028	0.044	27.91	5.11e-03	1064.32	0.2	7069.67	1.3	0.0	0.0
80	36.027	0.028	0.044	625.93	0.1	1105.93	0.2	751.97	0.1	0.0	0.0
81	36.212	0.028	0.044	25.54	4.67e-03	472.99	8.65e-02	1582.38	0.3	0.0	0.0
82	36.551	0.027	0.044	344.03	6.30e-02	1872.52	0.3	3036.60	0.6	0.0	0.0
83	36.749	0.027	0.044	202.98	3.71e-02	102.12	1.87e-02	28.96	5.30e-03	0.0	0.0
84	37.330	0.027	0.044	468.66	8.58e-02	4.74	8.68e-04	174.30	3.19e-02	0.0	0.0
85	37.405	0.027	0.044	20.49	3.75e-03	8.08	1.48e-03	3533.85	0.6	0.0	0.0
86	37.589	0.027	0.044	76.77	1.40e-02	96.01	1.76e-02	2708.93	0.5	0.0	0.0
87	37.898	0.026	0.044	350.87	6.42e-02	170.60	3.12e-02	121.98	2.23e-02	0.0	0.0
88	38.141	0.026	0.044	95.68	1.75e-02	6.89	1.26e-03	149.64	2.74e-02	0.0	0.0
89	38.540	0.026	0.044	41.06	7.51e-03	39.74	7.27e-03	1237.83	0.2	0.0	0.0
90	38.694	0.026	0.044	0.78	1.43e-04	405.29	7.42e-02	5399.72	1.0	0.0	0.0
91	39.142	0.026	0.044	51.44	9.41e-03	43.14	7.89e-03	3249.71	0.6	0.0	0.0
92	39.783	0.025	0.044	18.80	3.44e-03	634.98	0.1	18.79	3.44e-03	0.0	0.0
93	40.230	0.025	0.044	40.87	7.48e-03	515.40	9.43e-02	1527.65	0.3	0.0	0.0
94	40.428	0.025	0.044	16.18	2.96e-03	242.67	4.44e-02	91.54	1.68e-02	0.0	0.0
95	40.610	0.025	0.044	10.33	1.89e-03	1.73	3.17e-04	3751.71	0.7	0.0	0.0
96	40.670	0.025	0.044	35.45	6.49e-03	77.90	1.43e-02	3086.62	0.6	0.0	0.0
97	41.077	0.024	0.044	452.49	8.28e-02	1138.82	0.2	1371.67	0.3	0.0	0.0
98	41.214	0.024	0.044	293.19	5.36e-02	2.78	5.09e-04	1356.56	0.2	0.0	0.0
99	41.700	0.024	0.044	204.62	3.74e-02	52.00	9.52e-03	33.51	6.13e-03	0.0	0.0
100	41.763	0.024	0.044	44.43	8.13e-03	60.12	1.10e-02	223.22	4.08e-02	0.0	0.0
101	42.111	0.024	0.044	224.03	4.10e-02	15.45	2.83e-03	4167.74	0.8	0.0	0.0
102	42.251	0.024	0.044	108.94	1.99e-02	34.71	6.35e-03	128.39	2.35e-02	0.0	0.0
103	42.555	0.023	0.044	659.46	0.1	611.49	0.1	1095.81	0.2	0.0	0.0
104	42.587	0.023	0.044	418.35	7.66e-02	44.70	8.18e-03	68.09	1.25e-02	0.0	0.0
105	43.022	0.023	0.044	3.02	5.53e-04	6.58	1.20e-03	446.30	8.17e-02	0.0	0.0
106	43.236	0.023	0.044	89.27	1.63e-02	474.71	8.69e-02	4087.88	0.7	0.0	0.0
107	43.703	0.023	0.044	383.94	7.03e-02	20.42	3.74e-03	218.97	4.01e-02	0.0	0.0
108	44.165	0.023	0.044	20.83	3.81e-03	38.69	7.08e-03	403.85	7.39e-02	0.0	0.0
109	44.449	0.022	0.044	53.39	9.77e-03	4.53	8.29e-04	400.13	7.32e-02	0.0	0.0
110	44.809	0.022	0.044	83.23	1.52e-02	1.45	2.65e-04	22.24	4.07e-03	0.0	0.0
111	44.957	0.022	0.044	0.03	4.90e-06	103.75	1.90e-02	996.82	0.2	0.0	0.0
112	45.392	0.022	0.044	40.20	7.36e-03	165.00	3.02e-02	0.27	4.90e-05	0.0	0.0
113	46.246	0.022	0.044	9.96	1.82e-03	208.51	3.82e-02	4.66	8.52e-04	0.0	0.0
114	46.412	0.022	0.045	28.33	5.18e-03	250.77	4.59e-02	69.93	1.28e-02	0.0	0.0
115	46.582	0.021	0.045	36.68	6.71e-03	233.85	4.28e-02	858.65	0.2	0.0	0.0
116	46.792	0.021	0.045	2.54	4.64e-04	11.67	2.14e-03	20.77	3.80e-03	0.0	0.0
117	47.215	0.021	0.045	20.02	3.66e-03	257.30	4.71e-02	274.08	5.02e-02	0.0	0.0
118	47.324	0.021	0.045	53.23	9.74e-03	8.78	1.61e-03	2598.23	0.5	0.0	0.0
119	48.128	0.021	0.045	7.10	1.30e-03	42.37	7.75e-03	1.282e+04	2.3	0.0	0.0
120	48.414	0.021	0.045	79.39	1.45e-02	4.76	8.71e-04	79.18	1.45e-02	0.0	0.0
121	48.861	0.020	0.045	17.56	3.21e-03	1.01	1.85e-04	46.43	8.50e-03	0.0	0.0
122	49.219	0.020	0.045	130.27	2.38e-02	475.84	8.71e-02	146.89	2.69e-02	0.0	0.0
123	49.459	0.020	0.045	43.38	7.94e-03	56.60	1.04e-02	0.63	1.15e-04	0.0	0.0
124	49.676	0.020	0.045	57.92	1.06e-02	80.61	1.48e-02	54.76	1.00e-02	0.0	0.0
125	49.905	0.020	0.045	35.85	6.56e-03	3.31	6.06e-04	24.78	4.53e-03	0.0	0.0
126	50.097	0.020	0.045	7.13	1.30e-03	320.10	5.86e-02	1934.96	0.4	0.0	0.0
127	50.239	0.020	0.045	38.55	7.05e-03	4.60	8.42e-04	25.70	4.70e-03	0.0	0.0
128	50.501	0.020	0.045	9.70	1.78e-03	165.93	3.04e-02	82.35	1.51e-02	0.0	0.0
129	51.064	0.020	0.045	178.74	3.27e-02	206.05	3.77e-02	680.04	0.1	0.0	0.0
130	51.318	0.019	0.045	69.04	1.26e-02	3.35	6.12e-04	297.33	5.44e-02	0.0	0.0
131	51.558	0.019	0.045	15.82	2.89e-03	17.65	3.23e-03	2.48	4.54e-04	0.0	0.0
132	52.080	0.019	0.045	88.51	1.62e-02	24.95	4.57e-03	28.26	5.17e-03	0.0	0.0
133	52.361	0.019	0.045	25.47	4.66e-03	6.69	1.22e-03	926.30	0.2	0.0	0.0
134	53.113	0.019	0.045	216.69	3.97e-02	0.33	5.98e-05	1.56	2.86e-04	0.0	0.0
135	53.332	0.019	0.045	1.54	2.81e-04	36.75	6.72e-03	34.91	6.39e-03	0.0	0.0
136	53.433	0.019	0.045	6.08	1.11e-03	155.94	2.85e-02	1996.62	0.4	0.0	0.0
137	53.534	0.019	0.045	1.35	2.46e-04	647.86	0.1	5.38	9.84e-04	0.0	0.0
138	53.952	0.019	0.045	212.46	3.89e-02	9.10	1.67e-03	1645.02	0.3	0.0	0.0
139	54.074	0.018	0.045	1.26	2.31e-04	42.69	7.81e-03	478.91	8.76e-02	0.0	0.0
140	54.357	0.018	0.045	238.99	4.37e-02	299.42	5.48e-02	200.92	3.68e-02	0.0	0.0
141	54.659	0.018	0.045	11.51	2.11e-03	13.68	2.50e-03	225.17	4.12e-02	0.0	0.0
142	55.059	0.018	0.045	21.48	3.93e-03	29.05	5.32e-03	289.55	5.30e-02	0.0	0.0
143	55.394	0.018	0.045	214.73	3.93e-02	2.56	4.68e-04	1223.81	0.2	0.0	0.0
144	55.683	0.018	0.045	196.74	3.60e-02	18.64	3.41e-03	39.44	7.22e-03	0.0	0.0
145	55.973	0.018	0.045	484.26	8.86e-02	182.49	3.34e-02	81.32	1.49e-02	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	Z %	Energia	Energia x v
146	56.335	0.018	0.045	170.53	3.12e-02	0.02	2.81e-06	143.31	2.62e-02	0.0	0.0
147	56.502	0.018	0.045	2.15	3.93e-04	27.19	4.98e-03	9.77	1.79e-03	0.0	0.0
148	57.103	0.018	0.045	1826.88	0.3	152.85	2.80e-02	69.90	1.28e-02	0.0	0.0
149	57.150	0.017	0.045	409.73	7.50e-02	40.12	7.34e-03	471.91	8.64e-02	0.0	0.0
150	57.485	0.017	0.045	22.74	4.16e-03	14.66	2.68e-03	29.12	5.33e-03	0.0	0.0
151	57.751	0.017	0.045	81.65	1.49e-02	166.43	3.05e-02	25.50	4.67e-03	0.0	0.0
152	57.797	0.017	0.045	426.31	7.80e-02	51.08	9.35e-03	0.27	4.97e-05	0.0	0.0
153	58.195	0.017	0.045	8.09	1.48e-03	87.16	1.59e-02	356.89	6.53e-02	0.0	0.0
154	58.311	0.017	0.045	6.46	1.18e-03	157.10	2.87e-02	20.31	3.72e-03	0.0	0.0
155	58.625	0.017	0.045	629.65	0.1	231.57	4.24e-02	45.34	8.30e-03	0.0	0.0
156	58.763	0.017	0.045	5.86	1.07e-03	370.89	6.79e-02	66.54	1.22e-02	0.0	0.0
157	58.828	0.017	0.045	158.49	2.90e-02	355.76	6.51e-02	3.75	6.86e-04	0.0	0.0
158	59.463	0.017	0.045	10.55	1.93e-03	22.55	4.13e-03	156.23	2.86e-02	0.0	0.0
159	59.792	0.017	0.045	240.28	4.40e-02	78.46	1.44e-02	0.04	7.46e-06	0.0	0.0
160	60.163	0.017	0.045	25.54	4.67e-03	207.95	3.81e-02	318.18	5.82e-02	0.0	0.0
161	60.374	0.017	0.045	927.39	0.2	8.53	1.56e-03	95.79	1.75e-02	0.0	0.0
162	60.479	0.017	0.045	57.31	1.05e-02	81.20	1.49e-02	34.88	6.38e-03	0.0	0.0
163	60.670	0.016	0.045	4.22	7.72e-04	73.99	1.35e-02	2.67	4.88e-04	0.0	0.0
164	61.226	0.016	0.045	54.91	1.00e-02	1.11e-03	0.0	0.30	5.54e-05	0.0	0.0
165	61.512	0.016	0.045	87.73	1.61e-02	0.24	4.38e-05	35.13	6.43e-03	0.0	0.0
166	61.635	0.016	0.045	132.69	2.43e-02	431.92	7.90e-02	394.72	7.22e-02	0.0	0.0
167	61.769	0.016	0.045	213.29	3.90e-02	73.46	1.34e-02	195.94	3.59e-02	0.0	0.0
168	62.278	0.016	0.045	185.70	3.40e-02	84.00	1.54e-02	1.35	2.47e-04	0.0	0.0
169	62.558	0.016	0.045	11.02	2.02e-03	49.09	8.98e-03	94.86	1.74e-02	0.0	0.0
170	62.886	0.016	0.045	0.28	5.11e-05	29.74	5.44e-03	195.36	3.57e-02	0.0	0.0
171	63.101	0.016	0.045	3.54	6.49e-04	35.26	6.45e-03	1104.78	0.2	0.0	0.0
172	63.214	0.016	0.045	63.51	1.16e-02	22.78	4.17e-03	108.22	1.98e-02	0.0	0.0
173	63.640	0.016	0.045	34.85	6.38e-03	128.04	2.34e-02	131.04	2.40e-02	0.0	0.0
174	63.792	0.016	0.045	69.54	1.27e-02	2.76	5.05e-04	128.64	2.35e-02	0.0	0.0
175	63.995	0.016	0.045	80.70	1.48e-02	57.45	1.05e-02	68.44	1.25e-02	0.0	0.0
176	64.176	0.016	0.045	0.64	1.16e-04	591.65	0.1	84.09	1.54e-02	0.0	0.0
177	64.249	0.016	0.045	0.82	1.50e-04	263.04	4.81e-02	45.14	8.26e-03	0.0	0.0
178	64.602	0.015	0.045	189.85	3.47e-02	427.05	7.81e-02	130.57	2.39e-02	0.0	0.0
179	64.771	0.015	0.045	15.18	2.78e-03	24.49	4.48e-03	541.48	9.91e-02	0.0	0.0
180	65.045	0.015	0.045	5.03	9.20e-04	87.56	1.60e-02	209.79	3.84e-02	0.0	0.0
181	65.405	0.015	0.045	37.74	6.91e-03	5.83	1.07e-03	10.61	1.94e-03	0.0	0.0
182	65.577	0.015	0.045	73.95	1.35e-02	38.24	7.00e-03	430.80	7.88e-02	0.0	0.0
183	65.823	0.015	0.045	6.83	1.25e-03	97.37	1.78e-02	297.34	5.44e-02	0.0	0.0
184	66.052	0.015	0.045	0.10	1.84e-05	956.93	0.2	409.51	7.49e-02	0.0	0.0
185	66.222	0.015	0.045	54.56	9.98e-03	13.38	2.45e-03	3041.81	0.6	0.0	0.0
186	66.463	0.015	0.045	7.46	1.36e-03	39.65	7.26e-03	3.58	6.56e-04	0.0	0.0
187	66.583	0.015	0.045	153.60	2.81e-02	70.78	1.30e-02	2405.91	0.4	0.0	0.0
188	66.736	0.015	0.045	71.59	1.31e-02	23.25	4.26e-03	218.18	3.99e-02	0.0	0.0
189	66.879	0.015	0.045	1.14	2.08e-04	55.39	1.01e-02	221.72	4.06e-02	0.0	0.0
190	67.233	0.015	0.045	114.51	2.10e-02	152.53	2.79e-02	14.62	2.68e-03	0.0	0.0
191	67.439	0.015	0.045	23.74	4.34e-03	109.89	2.01e-02	8.60	1.57e-03	0.0	0.0
192	67.534	0.015	0.045	43.33	7.93e-03	275.71	5.05e-02	78.02	1.43e-02	0.0	0.0
193	67.992	0.015	0.045	191.09	3.50e-02	4.69	8.59e-04	0.07	1.26e-05	0.0	0.0
194	68.312	0.015	0.045	51.90	9.50e-03	5.52	1.01e-03	185.18	3.39e-02	0.0	0.0
195	68.420	0.015	0.045	332.52	6.08e-02	58.35	1.07e-02	67.21	1.23e-02	0.0	0.0
196	68.686	0.015	0.045	349.12	6.39e-02	16.91	3.09e-03	29.59	5.41e-03	0.0	0.0
197	68.886	0.015	0.045	67.14	1.23e-02	18.95	3.47e-03	343.46	6.28e-02	0.0	0.0
198	69.183	0.014	0.045	221.05	4.04e-02	2.68	4.91e-04	127.16	2.33e-02	0.0	0.0
199	69.381	0.014	0.045	32.78	6.00e-03	49.35	9.03e-03	371.15	6.79e-02	0.0	0.0
200	69.558	0.014	0.045	7.14	1.31e-03	340.44	6.23e-02	152.32	2.79e-02	0.0	0.0
201	69.989	0.014	0.045	3.53	6.46e-04	118.26	2.16e-02	11.12	2.03e-03	0.0	0.0
202	70.284	0.014	0.045	39.71	7.27e-03	0.23	4.26e-05	6.79	1.24e-03	0.0	0.0
203	70.502	0.014	0.045	66.62	1.22e-02	78.48	1.44e-02	161.60	2.96e-02	0.0	0.0
204	70.890	0.014	0.045	116.78	2.14e-02	68.68	1.26e-02	150.46	2.75e-02	0.0	0.0
205	71.258	0.014	0.045	44.47	8.14e-03	11.55	2.11e-03	12.58	2.30e-03	0.0	0.0
206	71.344	0.014	0.045	90.66	1.66e-02	156.82	2.87e-02	204.47	3.74e-02	0.0	0.0
207	71.698	0.014	0.045	2.38	4.36e-04	1.31	2.40e-04	13.14	2.40e-03	0.0	0.0
208	71.759	0.014	0.045	23.07	4.22e-03	28.75	5.26e-03	59.94	1.10e-02	0.0	0.0
209	72.090	0.014	0.045	0.02	4.07e-06	58.42	1.07e-02	19.11	3.50e-03	0.0	0.0
210	72.279	0.014	0.045	84.60	1.55e-02	1.52	2.78e-04	172.84	3.16e-02	0.0	0.0
211	72.403	0.014	0.045	47.13	8.62e-03	6.18	1.13e-03	216.09	3.95e-02	0.0	0.0
212	72.759	0.014	0.045	19.69	3.60e-03	4.32	7.90e-04	277.34	5.07e-02	0.0	0.0
213	73.310	0.014	0.045	172.43	3.16e-02	135.45	2.48e-02	17.83	3.26e-03	0.0	0.0
214	73.454	0.014	0.045	423.70	7.75e-02	47.31	8.66e-03	50.61	9.26e-03	0.0	0.0
215	73.633	0.014	0.045	114.67	2.10e-02	3.97	7.27e-04	18.57	3.40e-03	0.0	0.0
216	73.691	0.014	0.045	8.50	1.56e-03	26.62	4.87e-03	15.45	2.83e-03	0.0	0.0
217	73.851	0.014	0.045	8.26	1.51e-03	29.81	5.45e-03	9.47	1.73e-03	0.0	0.0
218	74.267	0.013	0.045	79.24	1.45e-02	45.40	8.31e-03	290.82	5.32e-02	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
219	74.553	0.013	0.045	263.68	4.82e-02	14.34	2.62e-03	1.50e-03	0.0	0.0	0.0
220	74.756	0.013	0.045	309.02	5.65e-02	1.21	2.22e-04	1032.60	0.2	0.0	0.0
Risulta				5.245e+05		5.295e+05		4.736e+05			
In percentuale				95.98		96.89		86.65			

CDC	Tipo	Sigla Id	Note
9	Edk	CDC=Ed (dinamico SLU) alfa=90.00 (ecc. +)	
			verifica esistenti: fattore FC 1.200
			categoria suolo: B
			fattore di sito S = 1.200
			ordinata spettro (tratto Tb-Tc) = 0.036 g
			angolo di ingresso:90.00
			eccentricità aggiuntiva: positiva
			periodo proprio T1: 0.202 sec.
			fattore q: 3.400
			fattore per spost. mu d: 4.899
			classe di duttilità CD: B
			numero di modi considerati:220
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
cm	daN	cm	cm	cm	cm	cm	cm			
1340.00	96.19	-491.36	-334.97	5.50	0.0	-491.36	-334.97	0.155	0.0	0.0
1295.00	116.44	-491.36	-334.97	5.50	0.0	-491.36	-334.97	1.791	0.0	0.0
1250.00	101.25	-491.36	-334.97	5.50	0.0	-491.36	-334.97	1.791	0.0	0.0
1205.00	1203.52	-572.28	-173.84	16.15	0.0	-635.82	-328.32	0.015	2.913	3.350
1195.00	7848.27	-175.90	173.40	23.73	0.0	-313.36	198.69	0.654	1.046	0.168
1160.00	2326.05	-575.55	-168.23	16.15	0.0	-635.82	-328.32	0.015	2.763	3.471
1115.00	2319.30	-575.63	-167.75	16.15	0.0	-635.82	-328.32	0.015	2.759	3.482
1070.00	2319.30	-575.63	-167.75	16.15	0.0	-635.82	-328.32	0.015	2.759	3.482
1025.00	1.465e+04	-128.29	99.57	58.25	0.0	-544.49	-95.81	0.601	1.188	0.224
985.00	1.083e+04	-102.23	128.80	58.25	0.0	-542.49	-74.78	0.744	1.130	0.289
945.00	1.083e+04	-102.21	128.80	58.25	0.0	-542.49	-74.78	0.744	1.130	0.289
905.00	6.437e+04	-130.89	142.36	58.25	0.0	-436.66	166.12	0.443	1.017	0.032
855.00	2.344e+04	10.15	277.19	58.25	0.0	-430.77	347.85	0.460	1.438	0.099
805.00	1.496e+04	-105.98	181.79	58.25	0.0	-430.86	314.26	0.449	1.073	0.180
755.00	1.478e+04	-111.83	175.63	58.25	0.0	-430.86	314.26	0.449	1.054	0.189
705.00	1.434e+04	-113.81	161.90	58.25	0.0	-431.46	281.46	0.467	1.028	0.157
655.00	1.389e+04	-115.92	147.28	58.25	0.0	-431.46	281.46	0.467	1.022	0.177
605.00	1.373e+04	-110.92	157.10	58.25	0.0	-431.43	318.26	0.449	1.058	0.210
555.00	1.499e+04	-84.11	147.58	58.25	0.0	-417.55	263.67	0.542	1.003	0.142
535.00	462.89	-284.62	710.53	25.37	0.0	-295.19	710.53	0.049	0.058	0.0
505.00	1.751e+04	-80.04	167.93	58.25	0.0	-417.49	314.16	0.560	0.998	0.187
455.00	1.393e+05	-28.92	228.10	58.25	0.0	-380.74	478.92	0.654	0.963	0.374
404.44	1.813e+04	-50.00	221.17	58.25	0.0	-389.48	517.14	0.548	1.015	0.444
378.89	7112.79	-473.91	-262.63	16.15	0.0	-445.72	-328.72	2.380	0.183	0.414
353.89	2.196e+04	-32.62	456.21	58.25	0.0	-349.91	587.97	0.556	0.867	0.279
303.33	1.928e+04	-91.51	295.05	58.25	0.0	-423.33	593.38	0.329	1.179	0.506
252.78	2.190e+04	-176.89	242.77	58.25	0.0	-426.16	607.02	0.312	0.909	0.621
202.22	1.592e+04	-73.92	284.63	58.25	0.0	-426.16	607.02	0.312	1.284	0.549
151.67	1.601e+04	-65.56	283.49	58.25	0.0	-426.19	571.76	0.342	1.256	0.478
122.00	7167.74	-473.02	-262.23	16.15	0.0	-445.72	-328.72	2.380	0.177	0.416
101.11	1.343e+04	-59.25	403.57	58.25	0.0	-361.56	648.71	0.484	0.885	0.510
88.00	511.85	445.72	710.53	10.71	0.0	459.84	710.53	0.039	0.268	0.0
80.00	1592.11	106.62	-334.97	37.58	0.0	112.14	-334.97	0.080	0.025	0.0
50.56	1.912e+04	-72.11	249.76	58.25	0.0	-425.00	501.84	0.409	1.124	0.402
Risulta	5.465e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
1	4.866	0.206	0.036	1238.75	0.2	2.719e+04	5.0	1.59e-03	0.0	0.0	0.0
2	4.953	0.202	0.036	1359.25	0.2	1.534e+05	28.1	0.05	9.52e-06	0.0	0.0
3	7.211	0.139	0.036	3.135e+05	57.4	3884.05	0.7	9.18	1.68e-03	0.0	0.0
4	7.657	0.131	0.036	4.807e+04	8.8	9.780e+04	17.9	19.44	3.56e-03	0.0	0.0
5	8.056	0.124	0.036	5115.54	0.9	1969.52	0.4	9.10	1.66e-03	0.0	0.0
6	8.239	0.121	0.036	347.97	6.37e-02	2.846e+04	5.2	1.58	2.89e-04	0.0	0.0
7	9.235	0.108	0.036	4172.92	0.8	145.69	2.67e-02	17.31	3.17e-03	0.0	0.0
8	9.445	0.106	0.036	7750.63	1.4	2.828e+04	5.2	88.49	1.62e-02	0.0	0.0
9	9.740	0.103	0.037	1998.59	0.4	4970.84	0.9	35.75	6.54e-03	0.0	0.0
10	10.324	0.097	0.037	2.745e+04	5.0	812.28	0.1	2.84	5.19e-04	0.0	0.0
11	10.833	0.092	0.038	5049.62	0.9	199.44	3.65e-02	3.03	5.54e-04	0.0	0.0
12	11.554	0.087	0.038	9123.27	1.7	3.848e+04	7.0	0.96	1.75e-04	0.0	0.0
13	12.144	0.082	0.039	861.14	0.2	9787.16	1.8	11.37	2.08e-03	0.0	0.0
14	12.674	0.079	0.039	1.035e+04	1.9	1.419e+04	2.6	1.61	2.94e-04	0.0	0.0
15	13.262	0.075	0.039	4473.95	0.8	789.92	0.1	12.85	2.35e-03	0.0	0.0
16	13.365	0.075	0.039	187.56	3.43e-02	909.95	0.2	52.00	9.52e-03	0.0	0.0
17	14.089	0.071	0.040	7030.54	1.3	323.59	5.92e-02	130.79	2.39e-02	0.0	0.0
18	14.204	0.070	0.040	1559.10	0.3	3678.30	0.7	5.90	1.08e-03	0.0	0.0
19	15.016	0.067	0.040	8193.14	1.5	5426.01	1.0	89.77	1.64e-02	0.0	0.0
20	15.065	0.066	0.040	896.77	0.2	2656.27	0.5	26.62	4.87e-03	0.0	0.0
21	15.618	0.064	0.040	3613.52	0.7	3862.02	0.7	62.80	1.15e-02	0.0	0.0
22	16.284	0.061	0.041	3397.29	0.6	121.57	2.22e-02	116.53	2.13e-02	0.0	0.0
23	16.568	0.060	0.041	0.02	3.74e-06	3962.62	0.7	134.25	2.46e-02	0.0	0.0
24	16.852	0.059	0.041	15.83	2.90e-03	2822.65	0.5	7.81e-04	0.0	0.0	0.0
25	17.050	0.059	0.041	41.16	7.53e-03	9897.50	1.8	50.93	9.32e-03	0.0	0.0
26	17.256	0.058	0.041	167.26	3.06e-02	2919.22	0.5	44.67	8.17e-03	0.0	0.0
27	17.679	0.057	0.041	23.61	4.32e-03	3347.60	0.6	0.42	7.77e-05	0.0	0.0
28	18.121	0.055	0.041	1450.82	0.3	538.56	9.85e-02	1540.11	0.3	0.0	0.0
29	19.146	0.052	0.042	1.77	3.24e-04	4048.95	0.7	1397.28	0.3	0.0	0.0
30	19.704	0.051	0.042	67.11	1.23e-02	462.87	8.47e-02	1.362e+04	2.5	0.0	0.0
31	20.012	0.050	0.042	699.58	0.1	4609.05	0.8	1907.61	0.3	0.0	0.0
32	20.198	0.050	0.042	237.87	4.35e-02	266.16	4.87e-02	4945.11	0.9	0.0	0.0
33	20.530	0.049	0.042	4501.72	0.8	303.55	5.55e-02	217.79	3.99e-02	0.0	0.0
34	20.855	0.048	0.042	1791.93	0.3	169.89	3.11e-02	1252.25	0.2	0.0	0.0
35	21.417	0.047	0.042	5852.89	1.1	266.88	4.88e-02	781.09	0.1	0.0	0.0
36	21.745	0.046	0.042	410.70	7.52e-02	698.50	0.1	9279.53	1.7	0.0	0.0
37	22.122	0.045	0.042	7414.14	1.4	385.64	7.06e-02	1239.18	0.2	0.0	0.0
38	22.357	0.045	0.042	88.92	1.63e-02	1399.21	0.3	784.67	0.1	0.0	0.0
39	22.470	0.045	0.042	124.39	2.28e-02	0.16	2.85e-05	1.376e+04	2.5	0.0	0.0
40	22.715	0.044	0.042	101.31	1.85e-02	519.34	9.50e-02	2955.65	0.5	0.0	0.0
41	22.844	0.044	0.042	550.88	0.1	236.74	4.33e-02	2507.25	0.5	0.0	0.0
42	23.347	0.043	0.042	2044.37	0.4	340.61	6.23e-02	7320.79	1.3	0.0	0.0
43	23.559	0.042	0.043	0.19	3.48e-05	658.55	0.1	1.684e+04	3.1	0.0	0.0
44	23.608	0.042	0.043	2558.50	0.5	10.39	1.90e-03	1.025e+04	1.9	0.0	0.0
45	23.984	0.042	0.043	1047.10	0.2	5969.61	1.1	2743.68	0.5	0.0	0.0
46	24.215	0.041	0.043	939.44	0.2	552.43	0.1	155.26	2.84e-02	0.0	0.0
47	24.520	0.041	0.043	135.60	2.48e-02	6.73	1.23e-03	2683.27	0.5	0.0	0.0
48	24.938	0.040	0.043	463.11	8.47e-02	2301.98	0.4	8127.91	1.5	0.0	0.0
49	25.118	0.040	0.043	52.01	9.52e-03	252.64	4.62e-02	1359.47	0.2	0.0	0.0
50	25.564	0.039	0.043	289.37	5.30e-02	4050.74	0.7	1964.48	0.4	0.0	0.0
51	26.011	0.038	0.043	815.58	0.1	109.51	2.00e-02	338.38	6.19e-02	0.0	0.0
52	26.329	0.038	0.043	10.26	1.88e-03	9.31	1.70e-03	9054.70	1.7	0.0	0.0
53	26.885	0.037	0.043	208.98	3.82e-02	500.22	9.15e-02	482.03	8.82e-02	0.0	0.0
54	27.091	0.037	0.043	0.51	9.26e-05	3473.74	0.6	9.563e+04	17.5	0.0	0.0
55	27.212	0.037	0.043	20.10	3.68e-03	1.68	3.07e-04	2.222e+04	4.1	0.0	0.0
56	27.438	0.036	0.043	266.40	4.87e-02	1139.12	0.2	2068.31	0.4	0.0	0.0
57	27.479	0.036	0.043	28.46	5.21e-03	859.39	0.2	6.590e+04	12.1	0.0	0.0
58	27.714	0.036	0.043	2.41	4.42e-04	2223.94	0.4	28.43	5.20e-03	0.0	0.0
59	28.023	0.036	0.043	199.03	3.64e-02	5680.42	1.0	609.51	0.1	0.0	0.0
60	28.863	0.035	0.043	516.85	9.46e-02	76.05	1.39e-02	1323.58	0.2	0.0	0.0
61	29.320	0.034	0.043	62.58	1.15e-02	3276.13	0.6	6467.18	1.2	0.0	0.0
62	29.532	0.034	0.043	99.84	1.83e-02	3307.30	0.6	1390.32	0.3	0.0	0.0
63	29.829	0.034	0.043	35.13	6.43e-03	484.69	8.87e-02	3735.29	0.7	0.0	0.0
64	30.162	0.033	0.043	315.57	5.77e-02	1705.15	0.3	2123.77	0.4	0.0	0.0
65	30.751	0.033	0.043	623.28	0.1	142.62	2.61e-02	1.400e+04	2.6	0.0	0.0
66	30.972	0.032	0.043	42.26	7.73e-03	284.26	5.20e-02	1.520e+04	2.8	0.0	0.0
67	31.129	0.032	0.043	194.17	3.55e-02	986.45	0.2	3311.81	0.6	0.0	0.0
68	31.346	0.032	0.044	832.08	0.2	74.73	1.37e-02	6621.95	1.2	0.0	0.0
69	31.796	0.031	0.044	111.40	2.04e-02	1007.05	0.2	64.53	1.18e-02	0.0	0.0
70	32.367	0.031	0.044	16.21	2.97e-03	8.18	1.50e-03	177.45	3.25e-02	0.0	0.0
71	32.675	0.031	0.044	235.19	4.30e-02	151.98	2.78e-02	6542.47	1.2	0.0	0.0
72	32.873	0.030	0.044	228.91	4.19e-02	5.30	9.69e-04	3210.39	0.6	0.0	0.0
73	33.015	0.030	0.044	89.42	1.64e-02	91.55	1.68e-02	4669.22	0.9	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
74	33.430	0.030	0.044	30.37	5.56e-03	1393.25	0.3	1462.43	0.3	0.0	0.0
75	34.531	0.029	0.044	1629.96	0.3	2.32	4.24e-04	616.95	0.1	0.0	0.0
76	34.587	0.029	0.044	243.98	4.46e-02	1.80	3.29e-04	203.20	3.72e-02	0.0	0.0
77	34.673	0.029	0.044	440.83	8.07e-02	2112.44	0.4	1329.46	0.2	0.0	0.0
78	35.054	0.029	0.044	1833.91	0.3	172.84	3.16e-02	952.09	0.2	0.0	0.0
79	35.114	0.028	0.044	250.42	4.58e-02	1434.84	0.3	1636.69	0.3	0.0	0.0
80	35.422	0.028	0.044	24.57	4.50e-03	254.12	4.65e-02	7.88	1.44e-03	0.0	0.0
81	35.593	0.028	0.044	76.16	1.39e-02	1147.40	0.2	3124.93	0.6	0.0	0.0
82	36.026	0.028	0.044	1.30	2.39e-04	410.73	7.52e-02	263.67	4.82e-02	0.0	0.0
83	36.335	0.028	0.044	52.81	9.66e-03	4.45	8.13e-04	2644.84	0.5	0.0	0.0
84	36.590	0.027	0.044	281.34	5.15e-02	1377.95	0.3	5019.00	0.9	0.0	0.0
85	37.207	0.027	0.044	1.13	2.07e-04	994.84	0.2	3512.49	0.6	0.0	0.0
86	37.386	0.027	0.044	23.03	4.21e-03	40.30	7.38e-03	1117.55	0.2	0.0	0.0
87	37.903	0.026	0.044	451.73	8.27e-02	23.39	4.28e-03	944.30	0.2	0.0	0.0
88	37.974	0.026	0.044	104.40	1.91e-02	23.77	4.35e-03	861.83	0.2	0.0	0.0
89	38.190	0.026	0.044	635.97	0.1	517.64	9.47e-02	1758.48	0.3	0.0	0.0
90	38.338	0.026	0.044	5.25	9.61e-04	272.19	4.98e-02	375.99	6.88e-02	0.0	0.0
91	38.844	0.026	0.044	0.45	8.17e-05	699.50	0.1	3751.30	0.7	0.0	0.0
92	39.388	0.025	0.044	224.87	4.11e-02	36.88	6.75e-03	1115.26	0.2	0.0	0.0
93	39.722	0.025	0.044	0.33	5.99e-05	0.93	1.70e-04	902.34	0.2	0.0	0.0
94	40.225	0.025	0.044	1113.02	0.2	610.01	0.1	67.89	1.24e-02	0.0	0.0
95	40.296	0.025	0.044	343.65	6.29e-02	156.29	2.86e-02	904.34	0.2	0.0	0.0
96	40.708	0.025	0.044	872.72	0.2	4.55	8.33e-04	5638.40	1.0	0.0	0.0
97	41.031	0.024	0.044	1029.79	0.2	224.94	4.12e-02	2350.71	0.4	0.0	0.0
98	41.277	0.024	0.044	22.12	4.05e-03	11.22	2.05e-03	2533.93	0.5	0.0	0.0
99	41.495	0.024	0.044	6.02	1.10e-03	110.20	2.02e-02	3772.24	0.7	0.0	0.0
100	41.655	0.024	0.044	119.68	2.19e-02	254.73	4.66e-02	19.55	3.58e-03	0.0	0.0
101	41.828	0.024	0.044	13.73	2.51e-03	9.81	1.79e-03	2968.25	0.5	0.0	0.0
102	42.417	0.024	0.044	143.18	2.62e-02	8.74	1.60e-03	212.84	3.89e-02	0.0	0.0
103	42.751	0.023	0.044	318.25	5.82e-02	105.43	1.93e-02	3350.09	0.6	0.0	0.0
104	42.975	0.023	0.044	63.25	1.16e-02	27.83	5.09e-03	159.18	2.91e-02	0.0	0.0
105	43.306	0.023	0.044	60.45	1.11e-02	63.10	1.15e-02	8.54	1.56e-03	0.0	0.0
106	43.788	0.023	0.044	117.53	2.15e-02	653.95	0.1	19.36	3.54e-03	0.0	0.0
107	44.034	0.023	0.044	115.48	2.11e-02	1.32	2.41e-04	3.69	6.75e-04	0.0	0.0
108	44.252	0.023	0.044	4.70	8.60e-04	35.50	6.50e-03	19.64	3.59e-03	0.0	0.0
109	44.406	0.023	0.044	13.66	2.50e-03	48.32	8.84e-03	2404.25	0.4	0.0	0.0
110	44.852	0.022	0.044	30.62	5.60e-03	576.94	0.1	22.83	4.18e-03	0.0	0.0
111	45.132	0.022	0.044	38.72	7.08e-03	158.89	2.91e-02	106.70	1.95e-02	0.0	0.0
112	45.613	0.022	0.044	9.64	1.76e-03	1.14	2.08e-04	116.50	2.13e-02	0.0	0.0
113	45.688	0.022	0.044	9.36	1.71e-03	81.81	1.50e-02	119.47	2.19e-02	0.0	0.0
114	46.069	0.022	0.044	33.15	6.07e-03	317.99	5.82e-02	123.87	2.27e-02	0.0	0.0
115	46.626	0.021	0.045	0.43	7.83e-05	536.82	9.82e-02	0.40	7.28e-05	0.0	0.0
116	46.892	0.021	0.045	22.65	4.15e-03	172.44	3.16e-02	1998.49	0.4	0.0	0.0
117	47.318	0.021	0.045	58.22	1.07e-02	11.63	2.13e-03	6157.62	1.1	0.0	0.0
118	47.727	0.021	0.045	43.56	7.97e-03	653.24	0.1	1971.34	0.4	0.0	0.0
119	48.002	0.021	0.045	4.24	7.76e-04	283.94	5.20e-02	469.45	8.59e-02	0.0	0.0
120	48.446	0.021	0.045	5.06	9.27e-04	189.53	3.47e-02	2661.37	0.5	0.0	0.0
121	48.882	0.020	0.045	19.71	3.61e-03	114.54	2.10e-02	346.07	6.33e-02	0.0	0.0
122	48.915	0.020	0.045	0.99	1.80e-04	41.00	7.50e-03	736.82	0.1	0.0	0.0
123	49.269	0.020	0.045	61.82	1.13e-02	216.14	3.95e-02	1814.47	0.3	0.0	0.0
124	49.544	0.020	0.045	55.51	1.02e-02	0.45	8.25e-05	591.98	0.1	0.0	0.0
125	49.901	0.020	0.045	81.14	1.48e-02	1.30	2.38e-04	904.40	0.2	0.0	0.0
126	50.180	0.020	0.045	86.28	1.58e-02	99.19	1.82e-02	28.98	5.30e-03	0.0	0.0
127	50.520	0.020	0.045	60.44	1.11e-02	0.44	8.05e-05	615.62	0.1	0.0	0.0
128	50.697	0.020	0.045	11.97	2.19e-03	0.24	4.39e-05	293.59	5.37e-02	0.0	0.0
129	50.974	0.020	0.045	32.21	5.89e-03	64.58	1.18e-02	330.55	6.05e-02	0.0	0.0
130	51.228	0.020	0.045	87.55	1.60e-02	9.63	1.76e-03	137.08	2.51e-02	0.0	0.0
131	51.889	0.019	0.045	319.31	5.84e-02	45.91	8.40e-03	961.60	0.2	0.0	0.0
132	52.052	0.019	0.045	3.89	7.12e-04	145.76	2.67e-02	47.04	8.61e-03	0.0	0.0
133	52.449	0.019	0.045	288.49	5.28e-02	63.37	1.16e-02	1298.61	0.2	0.0	0.0
134	52.668	0.019	0.045	213.49	3.91e-02	0.04	6.89e-06	0.30	5.57e-05	0.0	0.0
135	52.896	0.019	0.045	48.95	8.96e-03	73.60	1.35e-02	6.66	1.22e-03	0.0	0.0
136	53.252	0.019	0.045	17.56	3.21e-03	151.38	2.77e-02	24.08	4.41e-03	0.0	0.0
137	53.608	0.019	0.045	27.66	5.06e-03	349.97	6.40e-02	89.31	1.63e-02	0.0	0.0
138	53.856	0.019	0.045	416.72	7.63e-02	21.52	3.94e-03	339.16	6.21e-02	0.0	0.0
139	54.057	0.018	0.045	306.09	5.60e-02	509.82	9.33e-02	1669.47	0.3	0.0	0.0
140	54.066	0.018	0.045	92.41	1.69e-02	1.97	3.60e-04	762.05	0.1	0.0	0.0
141	54.592	0.018	0.045	1308.14	0.2	27.72	5.07e-03	4.64	8.50e-04	0.0	0.0
142	54.839	0.018	0.045	444.42	8.13e-02	14.16	2.59e-03	30.96	5.66e-03	0.0	0.0
143	55.047	0.018	0.045	950.84	0.2	44.41	8.13e-03	160.37	2.93e-02	0.0	0.0
144	55.468	0.018	0.045	88.31	1.62e-02	8.78	1.61e-03	1368.26	0.3	0.0	0.0
145	55.738	0.018	0.045	181.24	3.32e-02	219.93	4.02e-02	243.87	4.46e-02	0.0	0.0
146	55.761	0.018	0.045	508.33	9.30e-02	69.10	1.26e-02	5.33	9.76e-04	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	Z %	Energia	Energia x v
147	56.133	0.018	0.045	144.17	2.64e-02	61.61	1.13e-02	347.35	6.36e-02	0.0	0.0
148	56.647	0.018	0.045	246.52	4.51e-02	0.78	1.43e-04	1131.99	0.2	0.0	0.0
149	56.925	0.018	0.045	38.02	6.96e-03	11.35	2.08e-03	39.89	7.30e-03	0.0	0.0
150	57.019	0.018	0.045	38.97	7.13e-03	19.94	3.65e-03	1.05e-03	0.0	0.0	0.0
151	57.476	0.017	0.045	28.25	5.17e-03	57.50	1.05e-02	134.56	2.46e-02	0.0	0.0
152	57.875	0.017	0.045	8.75	1.60e-03	1.38	2.52e-04	34.58	6.33e-03	0.0	0.0
153	58.065	0.017	0.045	207.64	3.80e-02	1.49	2.72e-04	208.06	3.81e-02	0.0	0.0
154	58.146	0.017	0.045	64.87	1.19e-02	1.67	3.05e-04	37.83	6.92e-03	0.0	0.0
155	58.361	0.017	0.045	46.65	8.54e-03	2.75	5.04e-04	123.13	2.25e-02	0.0	0.0
156	58.997	0.017	0.045	27.45	5.02e-03	263.27	4.82e-02	27.55	5.04e-03	0.0	0.0
157	59.284	0.017	0.045	104.62	1.91e-02	691.50	0.1	0.05	8.78e-06	0.0	0.0
158	59.364	0.017	0.045	311.13	5.69e-02	0.05	8.23e-06	72.21	1.32e-02	0.0	0.0
159	59.936	0.017	0.045	139.80	2.56e-02	1149.26	0.2	35.71	6.53e-03	0.0	0.0
160	60.070	0.017	0.045	26.40	4.83e-03	11.63	2.13e-03	27.83	5.09e-03	0.0	0.0
161	60.458	0.017	0.045	132.08	2.42e-02	27.44	5.02e-03	12.83	2.35e-03	0.0	0.0
162	60.684	0.016	0.045	54.75	1.00e-02	7.11	1.30e-03	151.80	2.78e-02	0.0	0.0
163	60.836	0.016	0.045	208.50	3.82e-02	83.96	1.54e-02	44.28	8.10e-03	0.0	0.0
164	60.981	0.016	0.045	248.26	4.54e-02	58.23	1.07e-02	5.98	1.09e-03	0.0	0.0
165	61.332	0.016	0.045	165.40	3.03e-02	8.40	1.54e-03	17.28	3.16e-03	0.0	0.0
166	61.405	0.016	0.045	384.56	7.04e-02	688.36	0.1	378.45	6.93e-02	0.0	0.0
167	61.742	0.016	0.045	56.89	1.04e-02	347.15	6.35e-02	28.75	5.26e-03	0.0	0.0
168	61.886	0.016	0.045	5.67	1.04e-03	461.36	8.44e-02	512.57	9.38e-02	0.0	0.0
169	62.070	0.016	0.045	55.07	1.01e-02	13.05	2.39e-03	28.43	5.20e-03	0.0	0.0
170	62.523	0.016	0.045	210.13	3.84e-02	72.69	1.33e-02	864.96	0.2	0.0	0.0
171	62.751	0.016	0.045	29.64	5.42e-03	6.74	1.23e-03	194.47	3.56e-02	0.0	0.0
172	62.761	0.016	0.045	3.05	5.58e-04	188.01	3.44e-02	2.30	4.21e-04	0.0	0.0
173	63.032	0.016	0.045	11.02	2.02e-03	291.31	5.33e-02	6.20	1.13e-03	0.0	0.0
174	63.146	0.016	0.045	0.37	6.86e-05	2.76	5.05e-04	680.31	0.1	0.0	0.0
175	63.466	0.016	0.045	113.98	2.09e-02	7.14	1.31e-03	13.35	2.44e-03	0.0	0.0
176	63.885	0.016	0.045	309.02	5.65e-02	115.34	2.11e-02	4.80	8.79e-04	0.0	0.0
177	64.206	0.016	0.045	35.48	6.49e-03	14.88	2.72e-03	26.91	4.92e-03	0.0	0.0
178	64.533	0.015	0.045	27.24	4.98e-03	17.68	3.24e-03	0.93	1.69e-04	0.0	0.0
179	64.748	0.015	0.045	0.02	2.94e-06	72.98	1.34e-02	32.04	5.86e-03	0.0	0.0
180	64.970	0.015	0.045	374.43	6.85e-02	0.84	1.53e-04	5.86	1.07e-03	0.0	0.0
181	65.036	0.015	0.045	151.73	2.78e-02	41.88	7.66e-03	119.38	2.18e-02	0.0	0.0
182	65.302	0.015	0.045	19.46	3.56e-03	11.60	2.12e-03	2.41	4.40e-04	0.0	0.0
183	65.446	0.015	0.045	186.74	3.42e-02	3.49	6.39e-04	133.57	2.44e-02	0.0	0.0
184	65.724	0.015	0.045	48.68	8.91e-03	305.18	5.58e-02	162.73	2.98e-02	0.0	0.0
185	65.841	0.015	0.045	70.74	1.29e-02	0.48	8.78e-05	190.77	3.49e-02	0.0	0.0
186	66.105	0.015	0.045	0.05	9.51e-06	112.78	2.06e-02	349.22	6.39e-02	0.0	0.0
187	66.380	0.015	0.045	23.21	4.25e-03	11.19	2.05e-03	458.18	8.38e-02	0.0	0.0
188	66.606	0.015	0.045	261.60	4.79e-02	36.05	6.60e-03	248.83	4.55e-02	0.0	0.0
189	66.663	0.015	0.045	427.07	7.81e-02	0.02	3.26e-06	7.57	1.39e-03	0.0	0.0
190	66.720	0.015	0.045	17.72	3.24e-03	7.68	1.41e-03	5772.67	1.1	0.0	0.0
191	67.118	0.015	0.045	75.43	1.38e-02	6.79	1.24e-03	442.61	8.10e-02	0.0	0.0
192	67.338	0.015	0.045	7.64	1.40e-03	57.56	1.05e-02	5.07	9.28e-04	0.0	0.0
193	67.559	0.015	0.045	18.79	3.44e-03	89.66	1.64e-02	317.00	5.80e-02	0.0	0.0
194	67.886	0.015	0.045	5.05	9.25e-04	92.62	1.69e-02	526.55	9.64e-02	0.0	0.0
195	68.199	0.015	0.045	4.55	8.33e-04	287.53	5.26e-02	22.14	4.05e-03	0.0	0.0
196	68.275	0.015	0.045	192.57	3.52e-02	42.55	7.79e-03	464.88	8.51e-02	0.0	0.0
197	68.524	0.015	0.045	30.92	5.66e-03	51.50	9.42e-03	325.60	5.96e-02	0.0	0.0
198	68.817	0.015	0.045	121.91	2.23e-02	16.04	2.94e-03	228.92	4.19e-02	0.0	0.0
199	69.112	0.014	0.045	98.18	1.80e-02	22.69	4.15e-03	47.69	8.73e-03	0.0	0.0
200	69.261	0.014	0.045	77.90	1.43e-02	0.11	2.01e-05	8.17	1.49e-03	0.0	0.0
201	69.378	0.014	0.045	27.83	5.09e-03	78.98	1.45e-02	218.09	3.99e-02	0.0	0.0
202	69.711	0.014	0.045	256.44	4.69e-02	0.20	3.62e-05	184.66	3.38e-02	0.0	0.0
203	70.130	0.014	0.045	32.25	5.90e-03	13.49	2.47e-03	33.01	6.04e-03	0.0	0.0
204	70.279	0.014	0.045	63.42	1.16e-02	18.65	3.41e-03	159.03	2.91e-02	0.0	0.0
205	70.421	0.014	0.045	45.24	8.28e-03	287.79	5.27e-02	189.17	3.46e-02	0.0	0.0
206	70.610	0.014	0.045	88.79	1.62e-02	206.96	3.79e-02	25.77	4.72e-03	0.0	0.0
207	70.993	0.014	0.045	2.15	3.94e-04	163.88	3.00e-02	62.18	1.14e-02	0.0	0.0
208	71.287	0.014	0.045	21.95	4.02e-03	18.12	3.32e-03	44.40	8.12e-03	0.0	0.0
209	71.663	0.014	0.045	15.14	2.77e-03	22.89	4.19e-03	28.95	5.30e-03	0.0	0.0
210	71.804	0.014	0.045	98.03	1.79e-02	0.98	1.80e-04	153.66	2.81e-02	0.0	0.0
211	72.043	0.014	0.045	8.34	1.53e-03	19.66	3.60e-03	161.33	2.95e-02	0.0	0.0
212	72.323	0.014	0.045	32.49	5.95e-03	23.80	4.35e-03	730.57	0.1	0.0	0.0
213	72.543	0.014	0.045	4.03	7.38e-04	105.92	1.94e-02	75.37	1.38e-02	0.0	0.0
214	72.686	0.014	0.045	46.02	8.42e-03	2.31	4.22e-04	150.43	2.75e-02	0.0	0.0
215	73.269	0.014	0.045	3.60	6.58e-04	16.74	3.06e-03	1280.58	0.2	0.0	0.0
216	73.529	0.014	0.045	0.89	1.63e-04	0.11	1.94e-05	226.77	4.15e-02	0.0	0.0
217	73.692	0.014	0.045	2.22	4.07e-04	21.09	3.86e-03	6.76	1.24e-03	0.0	0.0
218	73.981	0.014	0.045	53.85	9.85e-03	162.67	2.98e-02	45.51	8.33e-03	0.0	0.0
219	74.144	0.013	0.045	34.74	6.36e-03	15.73	2.88e-03	18.42	3.37e-03	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
220	74.169	0.013	0.045	24.17	4.42e-03	57.97	1.06e-02	4.19	7.67e-04	0.0	0.0
Risulta				5.250e+05		5.297e+05		4.752e+05			
In percentuale				96.06		96.92		86.95			

CDC	Tipo	Sigla Id	Note
10	Edk	CDC=Ed (dinamico SLU) alfa=90.00 (ecc. -)	
			verifica esistenti: fattore FC 1.200
			categoria suolo: B
			fattore di sito S = 1.200
			ordinata spettro (tratto Tb-Tc) = 0.036 g
			angolo di ingresso:90.00
			eccentricità aggiuntiva: negativa
			periodo proprio T1: 0.123 sec.
			fattore q: 3.400
			fattore per spost. mu d: 7.410
			classe di duttilità CD: B
			numero di modi considerati:220
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
cm	daN	cm	cm	cm	cm	cm	cm			
1340.00	96.19	-491.36	-334.97	-5.50	0.0	-491.36	-334.97	0.155	0.0	0.0
1295.00	116.44	-491.36	-334.97	-5.50	0.0	-491.36	-334.97	1.791	0.0	0.0
1250.00	101.25	-491.36	-334.97	-5.50	0.0	-491.36	-334.97	1.791	0.0	0.0
1205.00	1203.52	-572.28	-173.84	-16.15	0.0	-635.82	-328.32	0.015	2.913	3.350
1195.00	7848.27	-175.90	173.40	-23.73	0.0	-313.36	198.69	0.654	1.046	0.168
1160.00	2326.05	-575.55	-168.23	-16.15	0.0	-635.82	-328.32	0.015	2.763	3.471
1115.00	2319.30	-575.63	-167.75	-16.15	0.0	-635.82	-328.32	0.015	2.759	3.482
1070.00	2319.30	-575.63	-167.75	-16.15	0.0	-635.82	-328.32	0.015	2.759	3.482
1025.00	1.465e+04	-128.29	99.57	-58.25	0.0	-544.49	-95.81	0.601	1.188	0.224
985.00	1.083e+04	-102.23	128.80	-58.25	0.0	-542.49	-74.78	0.744	1.130	0.289
945.00	1.083e+04	-102.21	128.80	-58.25	0.0	-542.49	-74.78	0.744	1.130	0.289
905.00	6.437e+04	-130.89	142.36	-58.25	0.0	-436.66	166.12	0.443	1.017	0.032
855.00	2.344e+04	10.15	277.19	-58.25	0.0	-430.77	347.85	0.460	1.438	0.099
805.00	1.496e+04	-105.98	181.79	-58.25	0.0	-430.86	314.26	0.449	1.073	0.180
755.00	1.478e+04	-111.83	175.63	-58.25	0.0	-430.86	314.26	0.449	1.054	0.189
705.00	1.434e+04	-113.81	161.90	-58.25	0.0	-431.46	281.46	0.467	1.028	0.157
655.00	1.389e+04	-115.92	147.28	-58.25	0.0	-431.46	281.46	0.467	1.022	0.177
605.00	1.373e+04	-110.92	157.10	-58.25	0.0	-431.43	318.26	0.449	1.058	0.210
555.00	1.499e+04	-84.11	147.58	-58.25	0.0	-417.55	263.67	0.542	1.003	0.142
535.00	462.89	-284.62	710.53	-25.37	0.0	-295.19	710.53	0.049	0.058	0.0
505.00	1.751e+04	-80.04	167.93	-58.25	0.0	-417.49	314.16	0.560	0.998	0.187
455.00	1.393e+05	-28.92	228.10	-58.25	0.0	-380.74	478.92	0.654	0.963	0.374
404.44	1.813e+04	-50.00	221.17	-58.25	0.0	-389.48	517.14	0.548	1.015	0.444
378.89	7112.79	-473.91	-262.63	-16.15	0.0	-445.72	-328.72	2.380	0.183	0.414
353.89	2.196e+04	-32.62	456.21	-58.25	0.0	-349.91	587.97	0.556	0.867	0.279
303.33	1.928e+04	-91.51	295.05	-58.25	0.0	-423.33	593.38	0.329	1.179	0.506
252.78	2.190e+04	-176.89	242.77	-58.25	0.0	-426.16	607.02	0.312	0.909	0.621
202.22	1.592e+04	-73.92	284.63	-58.25	0.0	-426.16	607.02	0.312	1.284	0.549
151.67	1.601e+04	-65.56	283.49	-58.25	0.0	-426.19	571.76	0.342	1.256	0.478
122.00	7167.74	-473.02	-262.23	-16.15	0.0	-445.72	-328.72	2.380	0.177	0.416
101.11	1.343e+04	-59.25	403.57	-58.25	0.0	-361.56	648.71	0.484	0.885	0.510
88.00	511.85	445.72	710.53	-10.71	0.0	459.84	710.53	0.039	0.268	0.0
80.00	1592.11	106.62	-334.97	-37.58	0.0	112.14	-334.97	0.080	0.025	0.0
50.56	1.912e+04	-72.11	249.76	-58.25	0.0	-425.00	501.84	0.409	1.124	0.402
Risulta	5.465e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	5.214	0.192	0.036	1511.92	0.3	4.078e+04	7.5	0.02	3.02e-06	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	Z %	Energia	Energia x v
2	5.330	0.188	0.036	1986.83	0.4	1.203e+05	22.0	0.04	7.87e-06	0.0	0.0
3	7.254	0.138	0.036	3.596e+05	65.8	5395.80	1.0	14.30	2.62e-03	0.0	0.0
4	8.143	0.123	0.036	227.12	4.16e-02	1.322e+05	24.2	15.56	2.85e-03	0.0	0.0
5	8.499	0.118	0.036	236.53	4.33e-02	3.355e+04	6.1	20.49	3.75e-03	0.0	0.0
6	8.986	0.111	0.036	6161.51	1.1	7925.58	1.5	6.00	1.10e-03	0.0	0.0
7	9.495	0.105	0.037	9085.14	1.7	1.202e+04	2.2	76.31	1.40e-02	0.0	0.0
8	9.600	0.104	0.037	7133.28	1.3	151.99	2.78e-02	33.89	6.20e-03	0.0	0.0
9	9.854	0.101	0.037	1384.67	0.3	1317.19	0.2	16.29	2.98e-03	0.0	0.0
10	10.483	0.095	0.037	3.190e+04	5.8	1.479e+04	2.7	0.05	9.32e-06	0.0	0.0
11	11.056	0.090	0.038	503.86	9.22e-02	7530.03	1.4	11.72	2.14e-03	0.0	0.0
12	11.995	0.083	0.039	1421.06	0.3	3.435e+04	6.3	0.30	5.44e-05	0.0	0.0
13	12.456	0.080	0.039	4327.94	0.8	6135.98	1.1	12.77	2.34e-03	0.0	0.0
14	12.773	0.078	0.039	1.142e+04	2.1	2038.03	0.4	2.30	4.21e-04	0.0	0.0
15	13.553	0.074	0.040	1248.42	0.2	3730.88	0.7	46.01	8.42e-03	0.0	0.0
16	13.609	0.073	0.040	8963.33	1.6	95.53	1.75e-02	43.98	8.05e-03	0.0	0.0
17	14.190	0.070	0.040	8699.83	1.6	391.46	7.16e-02	4.77	8.73e-04	0.0	0.0
18	15.004	0.067	0.040	232.39	4.25e-02	4659.84	0.9	92.39	1.69e-02	0.0	0.0
19	15.499	0.065	0.040	1443.99	0.3	5809.69	1.1	28.92	5.29e-03	0.0	0.0
20	15.859	0.063	0.041	11.92	2.18e-03	20.69	3.79e-03	0.22	4.00e-05	0.0	0.0
21	16.068	0.062	0.041	5853.25	1.1	5.47	1.00e-03	171.76	3.14e-02	0.0	0.0
22	16.251	0.062	0.041	48.06	8.79e-03	2742.10	0.5	85.67	1.57e-02	0.0	0.0
23	16.313	0.061	0.041	2718.08	0.5	52.67	9.64e-03	32.19	5.89e-03	0.0	0.0
24	16.789	0.060	0.041	462.40	8.46e-02	2887.46	0.5	46.27	8.47e-03	0.0	0.0
25	17.837	0.056	0.041	5.71	1.05e-03	164.57	3.01e-02	195.08	3.57e-02	0.0	0.0
26	18.085	0.055	0.041	357.66	6.54e-02	1.161e+04	2.1	7.21	1.32e-03	0.0	0.0
27	18.614	0.054	0.041	261.01	4.78e-02	519.15	9.50e-02	3938.30	0.7	0.0	0.0
28	19.323	0.052	0.042	186.18	3.41e-02	46.80	8.56e-03	6127.53	1.1	0.0	0.0
29	19.521	0.051	0.042	115.48	2.11e-02	4167.72	0.8	30.26	5.54e-03	0.0	0.0
30	20.147	0.050	0.042	50.29	9.20e-03	12.36	2.26e-03	4637.47	0.8	0.0	0.0
31	20.463	0.049	0.042	2809.28	0.5	68.69	1.26e-02	9693.43	1.8	0.0	0.0
32	20.755	0.048	0.042	309.21	5.66e-02	268.83	4.92e-02	726.21	0.1	0.0	0.0
33	20.951	0.048	0.042	3433.44	0.6	285.04	5.22e-02	3859.66	0.7	0.0	0.0
34	21.229	0.047	0.042	3262.09	0.6	3185.25	0.6	1221.47	0.2	0.0	0.0
35	21.768	0.046	0.042	6895.13	1.3	371.97	6.81e-02	7870.68	1.4	0.0	0.0
36	22.177	0.045	0.042	5126.64	0.9	39.22	7.18e-03	155.22	2.84e-02	0.0	0.0
37	22.423	0.045	0.042	84.36	1.54e-02	33.35	6.10e-03	1.123e+04	2.1	0.0	0.0
38	22.459	0.045	0.042	602.89	0.1	617.79	0.1	853.81	0.2	0.0	0.0
39	22.784	0.044	0.042	16.85	3.08e-03	678.61	0.1	2391.98	0.4	0.0	0.0
40	23.093	0.043	0.042	399.81	7.32e-02	1571.94	0.3	7564.03	1.4	0.0	0.0
41	23.502	0.043	0.042	1210.75	0.2	1990.52	0.4	435.48	7.97e-02	0.0	0.0
42	23.618	0.042	0.043	1781.74	0.3	2285.59	0.4	2.478e+04	4.5	0.0	0.0
43	24.009	0.042	0.043	169.71	3.11e-02	177.90	3.26e-02	567.66	0.1	0.0	0.0
44	24.540	0.041	0.043	412.80	7.55e-02	3238.30	0.6	3581.33	0.7	0.0	0.0
45	24.727	0.040	0.043	72.71	1.33e-02	4729.94	0.9	1.339e+04	2.4	0.0	0.0
46	24.884	0.040	0.043	1381.76	0.3	789.42	0.1	442.86	8.10e-02	0.0	0.0
47	24.970	0.040	0.043	52.63	9.63e-03	340.84	6.24e-02	216.04	3.95e-02	0.0	0.0
48	25.556	0.039	0.043	1417.63	0.3	1685.01	0.3	8406.92	1.5	0.0	0.0
49	25.875	0.039	0.043	820.94	0.2	2348.18	0.4	1.768e+04	3.2	0.0	0.0
50	26.506	0.038	0.043	143.16	2.62e-02	261.21	4.78e-02	4169.06	0.8	0.0	0.0
51	26.830	0.037	0.043	0.04	6.99e-06	1207.55	0.2	2.004e+04	3.7	0.0	0.0
52	27.127	0.037	0.043	0.23	4.20e-05	4527.02	0.8	1.315e+04	2.4	0.0	0.0
53	27.302	0.037	0.043	104.92	1.92e-02	3871.22	0.7	9.957e+04	18.2	0.0	0.0
54	27.491	0.036	0.043	217.18	3.97e-02	2497.99	0.5	269.79	4.94e-02	0.0	0.0
55	27.838	0.036	0.043	630.68	0.1	1098.85	0.2	2.494e+04	4.6	0.0	0.0
56	27.983	0.036	0.043	103.24	1.89e-02	3740.38	0.7	4888.87	0.9	0.0	0.0
57	28.236	0.035	0.043	6.92	1.27e-03	27.19	4.98e-03	0.03	5.21e-06	0.0	0.0
58	28.485	0.035	0.043	3.59	6.58e-04	866.50	0.2	5019.26	0.9	0.0	0.0
59	29.036	0.034	0.043	288.98	5.29e-02	1169.93	0.2	479.31	8.77e-02	0.0	0.0
60	29.185	0.034	0.043	20.61	3.77e-03	1734.49	0.3	1546.00	0.3	0.0	0.0
61	29.649	0.034	0.043	7.86e-03	1.44e-06	267.51	4.89e-02	152.14	2.78e-02	0.0	0.0
62	29.866	0.033	0.043	25.84	4.73e-03	1708.14	0.3	1241.40	0.2	0.0	0.0
63	30.522	0.033	0.043	790.99	0.1	67.48	1.23e-02	3.065e+04	5.6	0.0	0.0
64	30.692	0.033	0.043	187.32	3.43e-02	589.68	0.1	1.514e+04	2.8	0.0	0.0
65	31.061	0.032	0.043	416.57	7.62e-02	4.77	8.72e-04	1.266e+04	2.3	0.0	0.0
66	31.591	0.032	0.044	326.80	5.98e-02	433.22	7.93e-02	777.82	0.1	0.0	0.0
67	31.818	0.031	0.044	179.32	3.28e-02	0.03	4.92e-06	17.90	3.28e-03	0.0	0.0
68	32.293	0.031	0.044	2.91	5.33e-04	1481.14	0.3	1869.75	0.3	0.0	0.0
69	32.933	0.030	0.044	109.46	2.00e-02	4.25	7.78e-04	2301.14	0.4	0.0	0.0
70	33.330	0.030	0.044	16.74	3.06e-03	1333.85	0.2	1041.97	0.2	0.0	0.0
71	33.614	0.030	0.044	1314.25	0.2	45.25	8.28e-03	0.06	1.15e-05	0.0	0.0
72	33.709	0.030	0.044	8.22	1.50e-03	372.73	6.82e-02	5292.72	1.0	0.0	0.0
73	34.479	0.029	0.044	301.20	5.51e-02	41.49	7.59e-03	1111.07	0.2	0.0	0.0
74	34.594	0.029	0.044	207.99	3.81e-02	1.92	3.51e-04	11.05	2.02e-03	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
75	34.842	0.029	0.044	26.54	4.86e-03	196.98	3.60e-02	862.94	0.2	0.0	0.0
76	35.134	0.028	0.044	1578.89	0.3	564.57	0.1	397.64	7.28e-02	0.0	0.0
77	35.542	0.028	0.044	752.59	0.1	13.23	2.42e-03	18.67	3.42e-03	0.0	0.0
78	35.736	0.028	0.044	8.61e-03	1.57e-06	266.39	4.87e-02	483.78	8.85e-02	0.0	0.0
79	35.824	0.028	0.044	68.81	1.26e-02	1734.26	0.3	3918.27	0.7	0.0	0.0
80	36.194	0.028	0.044	929.84	0.2	315.51	5.77e-02	346.10	6.33e-02	0.0	0.0
81	36.407	0.027	0.044	329.15	6.02e-02	758.85	0.1	7368.08	1.3	0.0	0.0
82	36.804	0.027	0.044	19.97	3.65e-03	73.76	1.35e-02	4388.42	0.8	0.0	0.0
83	37.374	0.027	0.044	384.18	7.03e-02	407.79	7.46e-02	236.00	4.32e-02	0.0	0.0
84	37.668	0.027	0.044	14.74	2.70e-03	16.75	3.07e-03	792.66	0.1	0.0	0.0
85	37.749	0.026	0.044	2.28	4.17e-04	3.67	6.72e-04	675.54	0.1	0.0	0.0
86	38.215	0.026	0.044	876.07	0.2	10.37	1.90e-03	1516.70	0.3	0.0	0.0
87	38.360	0.026	0.044	143.58	2.63e-02	1862.15	0.3	185.06	3.39e-02	0.0	0.0
88	38.916	0.026	0.044	666.26	0.1	37.03	6.78e-03	3826.63	0.7	0.0	0.0
89	39.119	0.026	0.044	29.23	5.35e-03	39.77	7.28e-03	675.10	0.1	0.0	0.0
90	39.335	0.025	0.044	66.62	1.22e-02	322.99	5.91e-02	5.49	1.00e-03	0.0	0.0
91	39.491	0.025	0.044	7.30	1.34e-03	80.68	1.48e-02	288.57	5.28e-02	0.0	0.0
92	39.608	0.025	0.044	60.78	1.11e-02	145.02	2.65e-02	850.44	0.2	0.0	0.0
93	39.776	0.025	0.044	0.51	9.35e-05	480.73	8.80e-02	645.31	0.1	0.0	0.0
94	40.168	0.025	0.044	113.32	2.07e-02	292.29	5.35e-02	475.16	8.69e-02	0.0	0.0
95	40.427	0.025	0.044	534.23	9.78e-02	192.99	3.53e-02	1172.74	0.2	0.0	0.0
96	40.610	0.025	0.044	151.26	2.77e-02	11.30	2.07e-03	405.02	7.41e-02	0.0	0.0
97	40.790	0.025	0.044	1150.36	0.2	201.51	3.69e-02	414.04	7.58e-02	0.0	0.0
98	41.167	0.024	0.044	637.26	0.1	107.95	1.98e-02	3230.57	0.6	0.0	0.0
99	41.437	0.024	0.044	19.27	3.53e-03	35.37	6.47e-03	6730.13	1.2	0.0	0.0
100	42.094	0.024	0.044	127.00	2.32e-02	977.34	0.2	1717.91	0.3	0.0	0.0
101	42.348	0.024	0.044	2.53	4.62e-04	299.80	5.49e-02	2644.61	0.5	0.0	0.0
102	42.500	0.024	0.044	48.69	8.91e-03	77.70	1.42e-02	3455.30	0.6	0.0	0.0
103	43.069	0.023	0.044	41.90	7.67e-03	121.06	2.22e-02	2446.50	0.4	0.0	0.0
104	43.767	0.023	0.044	209.79	3.84e-02	8.17	1.49e-03	142.91	2.62e-02	0.0	0.0
105	43.919	0.023	0.044	0.10	1.76e-05	15.68	2.87e-03	370.67	6.78e-02	0.0	0.0
106	44.268	0.023	0.044	78.07	1.43e-02	105.17	1.92e-02	1201.31	0.2	0.0	0.0
107	44.726	0.022	0.044	26.27	4.81e-03	292.67	5.36e-02	125.69	2.30e-02	0.0	0.0
108	45.071	0.022	0.044	15.02	2.75e-03	260.95	4.77e-02	96.85	1.77e-02	0.0	0.0
109	45.513	0.022	0.044	77.18	1.41e-02	70.11	1.28e-02	807.28	0.1	0.0	0.0
110	45.735	0.022	0.044	9.27	1.70e-03	50.23	9.19e-03	7.70	1.41e-03	0.0	0.0
111	45.797	0.022	0.044	34.52	6.32e-03	115.93	2.12e-02	310.59	5.68e-02	0.0	0.0
112	46.437	0.022	0.045	40.12	7.34e-03	387.72	7.09e-02	1.40	2.55e-04	0.0	0.0
113	46.997	0.021	0.045	6.71	1.23e-03	131.38	2.40e-02	5426.56	1.0	0.0	0.0
114	47.144	0.021	0.045	26.15	4.78e-03	12.17	2.23e-03	8.72	1.60e-03	0.0	0.0
115	47.599	0.021	0.045	64.21	1.18e-02	65.63	1.20e-02	1172.69	0.2	0.0	0.0
116	47.679	0.021	0.045	9.99	1.83e-03	12.42	2.27e-03	1044.33	0.2	0.0	0.0
117	47.875	0.021	0.045	21.81	3.99e-03	109.41	2.00e-02	5406.28	1.0	0.0	0.0
118	48.636	0.021	0.045	87.52	1.60e-02	74.54	1.36e-02	663.19	0.1	0.0	0.0
119	48.822	0.020	0.045	6.90	1.26e-03	55.72	1.02e-02	1.02	1.87e-04	0.0	0.0
120	49.045	0.020	0.045	2.86	5.23e-04	89.99	1.65e-02	300.73	5.50e-02	0.0	0.0
121	49.238	0.020	0.045	5.11	9.36e-04	6.32	1.16e-03	2645.18	0.5	0.0	0.0
122	49.483	0.020	0.045	29.24	5.35e-03	205.62	3.76e-02	52.52	9.61e-03	0.0	0.0
123	49.598	0.020	0.045	45.88	8.39e-03	134.23	2.46e-02	448.05	8.20e-02	0.0	0.0
124	49.772	0.020	0.045	119.11	2.18e-02	81.45	1.49e-02	995.88	0.2	0.0	0.0
125	50.252	0.020	0.045	66.62	1.22e-02	0.34	6.21e-05	60.80	1.11e-02	0.0	0.0
126	50.632	0.020	0.045	77.47	1.42e-02	269.80	4.94e-02	110.52	2.02e-02	0.0	0.0
127	50.907	0.020	0.045	54.06	9.89e-03	96.02	1.76e-02	6.87	1.26e-03	0.0	0.0
128	51.082	0.020	0.045	0.03	5.76e-06	246.90	4.52e-02	1591.81	0.3	0.0	0.0
129	51.835	0.019	0.045	436.42	7.99e-02	20.59	3.77e-03	835.15	0.2	0.0	0.0
130	51.896	0.019	0.045	56.98	1.04e-02	8.53	1.56e-03	438.92	8.03e-02	0.0	0.0
131	52.215	0.019	0.045	328.07	6.00e-02	25.01	4.58e-03	153.33	2.81e-02	0.0	0.0
132	52.608	0.019	0.045	234.07	4.28e-02	10.48	1.92e-03	267.37	4.89e-02	0.0	0.0
133	53.215	0.019	0.045	234.95	4.30e-02	1.27	2.32e-04	29.42	5.38e-03	0.0	0.0
134	53.503	0.019	0.045	232.05	4.25e-02	612.46	0.1	269.87	4.94e-02	0.0	0.0
135	53.662	0.019	0.045	2.69	4.92e-04	37.64	6.89e-03	1444.57	0.3	0.0	0.0
136	53.915	0.019	0.045	39.29	7.19e-03	233.44	4.27e-02	4.76e-03	0.0	0.0	0.0
137	54.033	0.019	0.045	824.22	0.2	260.90	4.77e-02	92.49	1.69e-02	0.0	0.0
138	54.353	0.018	0.045	0.41	7.45e-05	25.99	4.76e-03	463.78	8.49e-02	0.0	0.0
139	54.855	0.018	0.045	66.54	1.22e-02	453.69	8.30e-02	343.90	6.29e-02	0.0	0.0
140	55.118	0.018	0.045	1601.08	0.3	211.08	3.86e-02	265.21	4.85e-02	0.0	0.0
141	55.197	0.018	0.045	26.76	4.90e-03	122.82	2.25e-02	609.29	0.1	0.0	0.0
142	55.305	0.018	0.045	558.45	0.1	105.46	1.93e-02	674.02	0.1	0.0	0.0
143	55.921	0.018	0.045	589.21	0.1	0.06	1.01e-05	97.87	1.79e-02	0.0	0.0
144	56.142	0.018	0.045	49.72	9.10e-03	61.76	1.13e-02	889.70	0.2	0.0	0.0
145	56.658	0.018	0.045	112.74	2.06e-02	57.41	1.05e-02	45.45	8.32e-03	0.0	0.0
146	56.798	0.018	0.045	341.78	6.25e-02	2.86	5.23e-04	190.02	3.48e-02	0.0	0.0
147	57.118	0.018	0.045	9.49	1.74e-03	527.87	9.66e-02	31.32	5.73e-03	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
148	57.339	0.017	0.045	127.84	2.34e-02	72.77	1.33e-02	205.29	3.76e-02	0.0	0.0
149	57.486	0.017	0.045	367.28	6.72e-02	0.08	1.46e-05	196.44	3.59e-02	0.0	0.0
150	57.799	0.017	0.045	21.93	4.01e-03	3.66e-03	0.0	175.35	3.21e-02	0.0	0.0
151	58.024	0.017	0.045	47.34	8.66e-03	194.45	3.56e-02	33.71	6.17e-03	0.0	0.0
152	58.189	0.017	0.045	33.86	6.20e-03	0.38	6.98e-05	166.44	3.05e-02	0.0	0.0
153	58.503	0.017	0.045	57.01	1.04e-02	58.70	1.07e-02	0.48	8.75e-05	0.0	0.0
154	58.724	0.017	0.045	73.22	1.34e-02	98.74	1.81e-02	13.67	2.50e-03	0.0	0.0
155	58.950	0.017	0.045	31.97	5.85e-03	0.94	1.73e-04	0.03	4.60e-06	0.0	0.0
156	59.230	0.017	0.045	33.58	6.14e-03	189.55	3.47e-02	120.02	2.20e-02	0.0	0.0
157	59.384	0.017	0.045	111.30	2.04e-02	172.34	3.15e-02	0.79	1.44e-04	0.0	0.0
158	59.615	0.017	0.045	132.60	2.43e-02	132.70	2.43e-02	176.62	3.23e-02	0.0	0.0
159	59.813	0.017	0.045	7.01	1.28e-03	58.46	1.07e-02	108.66	1.99e-02	0.0	0.0
160	60.260	0.017	0.045	235.37	4.31e-02	4.40	8.06e-04	6.55	1.20e-03	0.0	0.0
161	60.331	0.017	0.045	0.33	6.00e-05	66.07	1.21e-02	5.80	1.06e-03	0.0	0.0
162	60.700	0.016	0.045	229.95	4.21e-02	229.14	4.19e-02	158.27	2.90e-02	0.0	0.0
163	60.842	0.016	0.045	275.24	5.04e-02	12.06	2.21e-03	10.32	1.89e-03	0.0	0.0
164	61.518	0.016	0.045	16.66	3.05e-03	212.25	3.88e-02	157.23	2.88e-02	0.0	0.0
165	61.680	0.016	0.045	144.30	2.64e-02	58.62	1.07e-02	15.08	2.76e-03	0.0	0.0
166	61.855	0.016	0.045	12.03	2.20e-03	14.82	2.71e-03	0.67	1.22e-04	0.0	0.0
167	62.289	0.016	0.045	112.71	2.06e-02	181.91	3.33e-02	338.21	6.19e-02	0.0	0.0
168	62.483	0.016	0.045	2.33	4.27e-04	178.68	3.27e-02	2.60	4.76e-04	0.0	0.0
169	62.520	0.016	0.045	94.99	1.74e-02	15.61	2.86e-03	48.45	8.87e-03	0.0	0.0
170	62.873	0.016	0.045	21.35	3.91e-03	36.57	6.69e-03	923.43	0.2	0.0	0.0
171	63.124	0.016	0.045	331.34	6.06e-02	28.80	5.27e-03	175.36	3.21e-02	0.0	0.0
172	63.344	0.016	0.045	233.03	4.26e-02	54.66	1.00e-02	119.45	2.19e-02	0.0	0.0
173	63.465	0.016	0.045	73.34	1.34e-02	12.23	2.24e-03	92.14	1.69e-02	0.0	0.0
174	63.640	0.016	0.045	8.04	1.47e-03	5.79	1.06e-03	85.48	1.56e-02	0.0	0.0
175	64.037	0.016	0.045	100.93	1.85e-02	134.54	2.46e-02	307.15	5.62e-02	0.0	0.0
176	64.179	0.016	0.045	19.50	3.57e-03	99.85	1.83e-02	322.57	5.90e-02	0.0	0.0
177	64.400	0.016	0.045	92.98	1.70e-02	30.86	5.65e-03	22.57	4.13e-03	0.0	0.0
178	64.637	0.015	0.045	337.92	6.18e-02	4.04	7.39e-04	582.65	0.1	0.0	0.0
179	65.095	0.015	0.045	33.86	6.20e-03	26.43	4.84e-03	72.12	1.32e-02	0.0	0.0
180	65.290	0.015	0.045	10.43	1.91e-03	22.87	4.19e-03	97.38	1.78e-02	0.0	0.0
181	65.565	0.015	0.045	48.14	8.81e-03	464.45	8.50e-02	91.08	1.67e-02	0.0	0.0
182	65.599	0.015	0.045	29.70	5.44e-03	146.72	2.68e-02	7.31	1.34e-03	0.0	0.0
183	66.059	0.015	0.045	585.80	0.1	109.09	2.00e-02	1148.37	0.2	0.0	0.0
184	66.332	0.015	0.045	26.48	4.84e-03	210.64	3.85e-02	6.38	1.17e-03	0.0	0.0
185	66.449	0.015	0.045	136.14	2.49e-02	359.90	6.59e-02	104.58	1.91e-02	0.0	0.0
186	66.616	0.015	0.045	81.71	1.50e-02	371.20	6.79e-02	160.24	2.93e-02	0.0	0.0
187	66.753	0.015	0.045	6.10	1.12e-03	12.51	2.29e-03	4902.49	0.9	0.0	0.0
188	66.879	0.015	0.045	152.87	2.80e-02	32.85	6.01e-03	1023.19	0.2	0.0	0.0
189	67.067	0.015	0.045	63.59	1.16e-02	1.17	2.15e-04	45.44	8.31e-03	0.0	0.0
190	67.447	0.015	0.045	33.55	6.14e-03	8.89	1.63e-03	7.59	1.39e-03	0.0	0.0
191	67.585	0.015	0.045	474.26	8.68e-02	393.64	7.20e-02	485.16	8.88e-02	0.0	0.0
192	68.100	0.015	0.045	93.63	1.71e-02	178.85	3.27e-02	11.83	2.16e-03	0.0	0.0
193	68.320	0.015	0.045	86.28	1.58e-02	0.87	1.60e-04	629.37	0.1	0.0	0.0
194	68.366	0.015	0.045	1.92	3.51e-04	9.16	1.68e-03	0.44	8.09e-05	0.0	0.0
195	68.829	0.015	0.045	1.11	2.04e-04	145.44	2.66e-02	715.23	0.1	0.0	0.0
196	69.053	0.014	0.045	0.42	7.64e-05	451.27	8.26e-02	477.81	8.74e-02	0.0	0.0
197	69.717	0.014	0.045	49.26	9.01e-03	27.19	4.98e-03	151.21	2.77e-02	0.0	0.0
198	70.179	0.014	0.045	2.70	4.94e-04	144.07	2.64e-02	221.00	4.04e-02	0.0	0.0
199	70.356	0.014	0.045	9.55	1.75e-03	22.98	4.21e-03	200.49	3.67e-02	0.0	0.0
200	70.938	0.014	0.045	100.16	1.83e-02	256.47	4.69e-02	70.03	1.28e-02	0.0	0.0
201	71.192	0.014	0.045	0.34	6.20e-05	10.23	1.87e-03	199.29	3.65e-02	0.0	0.0
202	71.292	0.014	0.045	22.61	4.14e-03	74.62	1.37e-02	96.16	1.76e-02	0.0	0.0
203	71.456	0.014	0.045	16.79	3.07e-03	241.75	4.42e-02	88.55	1.62e-02	0.0	0.0
204	71.630	0.014	0.045	0.49	9.03e-05	1.29	2.35e-04	5.13	9.39e-04	0.0	0.0
205	71.733	0.014	0.045	45.74	8.37e-03	4.53	8.28e-04	0.12	2.13e-05	0.0	0.0
206	72.123	0.014	0.045	310.73	5.69e-02	58.87	1.08e-02	27.31	5.00e-03	0.0	0.0
207	72.522	0.014	0.045	9.44	1.73e-03	109.94	2.01e-02	2.45	4.49e-04	0.0	0.0
208	72.704	0.014	0.045	0.04	7.74e-06	34.69	6.35e-03	153.83	2.81e-02	0.0	0.0
209	72.825	0.014	0.045	3.72	6.80e-04	35.00	6.41e-03	677.18	0.1	0.0	0.0
210	73.133	0.014	0.045	29.64	5.42e-03	2.07	3.80e-04	8.43	1.54e-03	0.0	0.0
211	73.307	0.014	0.045	52.62	9.63e-03	0.14	2.62e-05	343.06	6.28e-02	0.0	0.0
212	73.369	0.014	0.045	0.49	8.90e-05	0.79	1.44e-04	1239.24	0.2	0.0	0.0
213	73.550	0.014	0.045	0.18	3.28e-05	48.30	8.84e-03	48.45	8.87e-03	0.0	0.0
214	73.650	0.014	0.045	109.34	2.00e-02	289.38	5.30e-02	43.47	7.95e-03	0.0	0.0
215	73.842	0.014	0.045	11.82	2.16e-03	34.04	6.23e-03	70.27	1.29e-02	0.0	0.0
216	74.191	0.013	0.045	147.12	2.69e-02	38.77	7.09e-03	0.32	5.90e-05	0.0	0.0
217	74.728	0.013	0.045	6.37	1.16e-03	93.26	1.71e-02	16.11	2.95e-03	0.0	0.0
218	74.984	0.013	0.045	43.36	7.93e-03	0.20	3.57e-05	184.24	3.37e-02	0.0	0.0
219	75.000	0.013	0.045	43.88	8.03e-03	109.90	2.01e-02	509.23	9.32e-02	0.0	0.0
220	75.332	0.013	0.045	22.74	4.16e-03	5.64	1.03e-03	11.40	2.09e-03	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
Risulta				5.251e+05		5.298e+05		4.763e+05			
In percentuale				96.09		96.94		87.16			

CDC	Tipo	Sigla Id	Note
11	Edk	CDC=Ed (dinamico SLD) alfa=0.0 (ecc. +)	
			verifica esistenti: fattore FC 1.200
			categoria suolo: B
			fattore di sito S = 1.200
			ordinata spettro (tratto Tb-Tc) = 0.075 g
			angolo di ingresso:0.0
			eccentricità aggiuntiva: positiva
			periodo proprio T1: 0.142 sec.
			numero di modi considerati:220
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
cm	daN	cm	cm	cm	cm	cm	cm			
1340.00	96.19	-491.36	-334.97	0.0	0.0	-491.36	-334.97	0.155	0.0	0.0
1295.00	116.44	-491.36	-334.97	0.0	0.0	-491.36	-334.97	1.791	0.0	0.0
1250.00	101.25	-491.36	-334.97	0.0	0.0	-491.36	-334.97	1.791	0.0	0.0
1205.00	1203.52	-572.28	-173.84	0.0	-26.80	-635.82	-328.32	0.015	2.913	3.350
1195.00	7848.27	-175.90	173.40	0.0	-15.15	-313.36	198.69	0.654	1.046	0.168
1160.00	2326.05	-575.55	-168.23	0.0	-26.80	-635.82	-328.32	0.015	2.763	3.471
1115.00	2319.30	-575.63	-167.75	0.0	-26.80	-635.82	-328.32	0.015	2.759	3.482
1070.00	2319.30	-575.63	-167.75	0.0	-26.80	-635.82	-328.32	0.015	2.759	3.482
1025.00	1.465e+04	-128.29	99.57	0.0	-52.28	-544.49	-95.81	0.601	1.188	0.224
985.00	1.083e+04	-102.23	128.80	0.0	-52.28	-542.49	-74.78	0.744	1.130	0.289
945.00	1.083e+04	-102.21	128.80	0.0	-52.28	-542.49	-74.78	0.744	1.130	0.289
905.00	6.437e+04	-130.89	142.36	0.0	-52.28	-436.66	166.12	0.443	1.017	0.032
855.00	2.344e+04	10.15	277.19	0.0	-52.28	-430.77	347.85	0.460	1.438	0.099
805.00	1.496e+04	-105.98	181.79	0.0	-52.28	-430.86	314.26	0.449	1.073	0.180
755.00	1.478e+04	-111.83	175.63	0.0	-52.28	-430.86	314.26	0.449	1.054	0.189
705.00	1.434e+04	-113.81	161.90	0.0	-52.28	-431.46	281.46	0.467	1.028	0.157
655.00	1.389e+04	-115.92	147.28	0.0	-52.28	-431.46	281.46	0.467	1.022	0.177
605.00	1.373e+04	-110.92	157.10	0.0	-52.28	-431.43	318.26	0.449	1.058	0.210
555.00	1.499e+04	-84.11	147.58	0.0	-52.28	-417.55	263.67	0.542	1.003	0.142
535.00	462.89	-284.62	710.53	0.0	0.0	-295.19	710.53	0.049	0.058	0.0
505.00	1.751e+04	-80.04	167.93	0.0	-52.28	-417.49	314.16	0.560	0.998	0.187
455.00	1.393e+05	-28.92	228.10	0.0	-52.28	-380.74	478.92	0.654	0.963	0.374
404.44	1.813e+04	-50.00	221.17	0.0	-52.28	-389.48	517.14	0.548	1.015	0.444
378.89	7112.79	-473.91	-262.63	0.0	-6.20	-445.72	-328.72	2.380	0.183	0.414
353.89	2.196e+04	-32.62	456.21	0.0	-61.93	-349.91	587.97	0.556	0.867	0.279
303.33	1.928e+04	-91.51	295.05	0.0	-61.93	-423.33	593.38	0.329	1.179	0.506
252.78	2.190e+04	-176.89	242.77	0.0	-61.93	-426.16	607.02	0.312	0.909	0.621
202.22	1.592e+04	-73.92	284.63	0.0	-61.93	-426.16	607.02	0.312	1.284	0.549
151.67	1.601e+04	-65.56	283.49	0.0	-61.93	-426.19	571.76	0.342	1.256	0.478
122.00	7167.74	-473.02	-262.23	0.0	-6.20	-445.72	-328.72	2.380	0.177	0.416
101.11	1.343e+04	-59.25	403.57	0.0	-61.93	-361.56	648.71	0.484	0.885	0.510
88.00	511.85	445.72	710.53	0.0	0.0	459.84	710.53	0.039	0.268	0.0
80.00	1592.11	106.62	-334.97	0.0	0.0	112.14	-334.97	0.080	0.025	0.0
50.56	1.912e+04	-72.11	249.76	0.0	-61.93	-425.00	501.84	0.409	1.124	0.402
Risulta	5.465e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	5.029	0.199	0.075	1866.06	0.3	2.721e+04	5.0	6.52e-03	1.19e-06	0.0	0.0
2	5.128	0.195	0.075	2457.01	0.4	1.427e+05	26.1	0.04	6.64e-06	0.0	0.0
3	7.049	0.142	0.075	3.504e+05	64.1	811.79	0.1	11.65	2.13e-03	0.0	0.0
4	7.913	0.126	0.075	7448.91	1.4	1.226e+05	22.4	16.77	3.07e-03	0.0	0.0
5	8.299	0.120	0.075	2104.23	0.4	1.244e+04	2.3	10.80	1.98e-03	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
6	8.598	0.116	0.075	1063.31	0.2	1.583e+04	2.9	7.32e-04	0.0	0.0	0.0
7	9.293	0.108	0.075	3202.37	0.6	311.55	5.70e-02	9.08	1.66e-03	0.0	0.0
8	9.483	0.105	0.075	1.194e+04	2.2	2.259e+04	4.1	111.32	2.04e-02	0.0	0.0
9	9.789	0.102	0.075	1549.68	0.3	2453.61	0.4	27.74	5.08e-03	0.0	0.0
10	10.492	0.095	0.075	2.455e+04	4.5	2429.66	0.4	4.84	8.86e-04	0.0	0.0
11	11.063	0.090	0.074	1.567e+04	2.9	9207.29	1.7	2.10	3.85e-04	0.0	0.0
12	11.694	0.086	0.071	4143.31	0.8	4.202e+04	7.7	0.71	1.30e-04	0.0	0.0
13	12.282	0.081	0.069	6449.23	1.2	9552.64	1.7	17.71	3.24e-03	0.0	0.0
14	13.117	0.076	0.067	7860.57	1.4	3774.59	0.7	0.18	3.25e-05	0.0	0.0
15	13.350	0.075	0.066	5.82	1.07e-03	18.48	3.38e-03	1.34	2.44e-04	0.0	0.0
16	13.449	0.074	0.066	1193.18	0.2	5209.81	1.0	69.37	1.27e-02	0.0	0.0
17	14.421	0.069	0.063	9784.36	1.8	36.87	6.75e-03	57.59	1.05e-02	0.0	0.0
18	14.733	0.068	0.063	597.10	0.1	1662.48	0.3	36.05	6.60e-03	0.0	0.0
19	15.311	0.065	0.061	766.40	0.1	9393.06	1.7	87.09	1.59e-02	0.0	0.0
20	15.578	0.064	0.061	4461.95	0.8	3.62	6.63e-04	6.32	1.16e-03	0.0	0.0
21	15.965	0.063	0.060	4954.49	0.9	471.24	8.62e-02	45.17	8.26e-03	0.0	0.0
22	16.516	0.061	0.059	5935.85	1.1	0.32	5.91e-05	286.98	5.25e-02	0.0	0.0
23	16.661	0.060	0.059	218.14	3.99e-02	4005.87	0.7	93.58	1.71e-02	0.0	0.0
24	17.136	0.058	0.058	571.36	0.1	5254.29	1.0	21.87	4.00e-03	0.0	0.0
25	17.517	0.057	0.057	8.80	1.61e-03	958.34	0.2	20.59	3.77e-03	0.0	0.0
26	17.774	0.056	0.057	43.74	8.00e-03	8140.53	1.5	0.39	7.09e-05	0.0	0.0
27	18.243	0.055	0.056	42.95	7.86e-03	1147.99	0.2	870.37	0.2	0.0	0.0
28	18.742	0.053	0.055	1565.71	0.3	2297.54	0.4	4110.75	0.8	0.0	0.0
29	19.555	0.051	0.054	44.84	8.20e-03	3926.25	0.7	2688.58	0.5	0.0	0.0
30	19.803	0.050	0.054	1933.85	0.4	188.46	3.45e-02	5886.35	1.1	0.0	0.0
31	20.171	0.050	0.054	11.93	2.18e-03	24.46	4.48e-03	7155.39	1.3	0.0	0.0
32	20.287	0.049	0.053	1775.31	0.3	342.01	6.26e-02	4494.37	0.8	0.0	0.0
33	20.629	0.048	0.053	626.28	0.1	0.04	8.22e-06	0.55	1.01e-04	0.0	0.0
34	21.018	0.048	0.053	1817.64	0.3	2454.77	0.4	868.55	0.2	0.0	0.0
35	21.224	0.047	0.052	334.59	6.12e-02	6.50	1.19e-03	2229.28	0.4	0.0	0.0
36	21.654	0.046	0.052	1.344e+04	2.5	452.70	8.28e-02	5786.46	1.1	0.0	0.0
37	22.114	0.045	0.051	161.20	2.95e-02	190.73	3.49e-02	1686.09	0.3	0.0	0.0
38	22.421	0.045	0.051	0.26	4.73e-05	0.36	6.57e-05	9816.41	1.8	0.0	0.0
39	22.627	0.044	0.051	90.47	1.66e-02	1908.54	0.3	829.52	0.2	0.0	0.0
40	22.751	0.044	0.051	75.68	1.38e-02	401.91	7.35e-02	4594.39	0.8	0.0	0.0
41	23.049	0.043	0.051	321.89	5.89e-02	2102.15	0.4	4813.82	0.9	0.0	0.0
42	23.539	0.042	0.050	888.20	0.2	34.39	6.29e-03	3.223e+04	5.9	0.0	0.0
43	23.974	0.042	0.050	457.57	8.37e-02	13.94	2.55e-03	1852.67	0.3	0.0	0.0
44	24.123	0.041	0.050	1451.64	0.3	5334.36	1.0	2931.76	0.5	0.0	0.0
45	24.382	0.041	0.049	1235.36	0.2	392.28	7.18e-02	828.08	0.2	0.0	0.0
46	24.532	0.041	0.049	445.78	8.16e-02	2527.54	0.5	39.78	7.28e-03	0.0	0.0
47	25.030	0.040	0.049	146.18	2.67e-02	31.56	5.77e-03	718.13	0.1	0.0	0.0
48	25.338	0.039	0.049	677.58	0.1	113.32	2.07e-02	1.458e+04	2.7	0.0	0.0
49	25.666	0.039	0.048	127.75	2.34e-02	4323.97	0.8	9786.24	1.8	0.0	0.0
50	26.072	0.038	0.048	8.11	1.48e-03	1351.54	0.2	2091.99	0.4	0.0	0.0
51	26.381	0.038	0.048	2003.93	0.4	69.73	1.28e-02	2260.63	0.4	0.0	0.0
52	26.843	0.037	0.047	0.29	5.23e-05	515.08	9.43e-02	1.679e+04	3.1	0.0	0.0
53	27.165	0.037	0.047	226.68	4.15e-02	5249.68	1.0	8.039e+04	14.7	0.0	0.0
54	27.258	0.037	0.047	301.40	5.52e-02	970.77	0.2	5.532e+04	10.1	0.0	0.0
55	27.582	0.036	0.047	0.12	2.19e-05	3460.28	0.6	1549.98	0.3	0.0	0.0
56	27.725	0.036	0.047	33.58	6.14e-03	446.25	8.17e-02	2.098e+04	3.8	0.0	0.0
57	27.928	0.036	0.047	0.02	3.66e-06	3712.23	0.7	47.98	8.78e-03	0.0	0.0
58	28.101	0.036	0.047	62.23	1.14e-02	19.55	3.58e-03	2055.82	0.4	0.0	0.0
59	28.433	0.035	0.046	161.28	2.95e-02	2626.03	0.5	3334.77	0.6	0.0	0.0
60	29.327	0.034	0.046	568.95	0.1	3178.03	0.6	676.29	0.1	0.0	0.0
61	29.912	0.033	0.046	5.35	9.78e-04	1821.28	0.3	3314.28	0.6	0.0	0.0
62	30.051	0.033	0.046	6.42	1.17e-03	452.14	8.27e-02	2547.75	0.5	0.0	0.0
63	30.373	0.033	0.045	3.38	6.18e-04	750.86	0.1	2053.86	0.4	0.0	0.0
64	30.647	0.033	0.045	6.00	1.10e-03	131.20	2.40e-02	1.144e+04	2.1	0.0	0.0
65	30.980	0.032	0.045	23.72	4.34e-03	1077.83	0.2	3.662e+04	6.7	0.0	0.0
66	31.224	0.032	0.045	0.52	9.54e-05	0.06	1.07e-05	1657.24	0.3	0.0	0.0
67	31.780	0.031	0.045	441.89	8.09e-02	434.61	7.95e-02	1047.37	0.2	0.0	0.0
68	32.538	0.031	0.044	755.40	0.1	92.41	1.69e-02	2130.28	0.4	0.0	0.0
69	32.677	0.031	0.044	78.63	1.44e-02	2915.48	0.5	1138.55	0.2	0.0	0.0
70	32.999	0.030	0.044	195.39	3.58e-02	227.44	4.16e-02	2206.08	0.4	0.0	0.0
71	33.219	0.030	0.044	74.00	1.35e-02	56.85	1.04e-02	1670.70	0.3	0.0	0.0
72	33.458	0.030	0.044	131.91	2.41e-02	589.71	0.1	4375.01	0.8	0.0	0.0
73	33.818	0.030	0.044	47.67	8.72e-03	172.34	3.15e-02	187.57	3.43e-02	0.0	0.0
74	33.924	0.029	0.044	252.64	4.62e-02	299.67	5.48e-02	1544.79	0.3	0.0	0.0
75	34.309	0.029	0.044	1625.37	0.3	26.57	4.86e-03	2031.61	0.4	0.0	0.0
76	34.786	0.029	0.043	85.19	1.56e-02	106.44	1.95e-02	97.05	1.78e-02	0.0	0.0
77	34.861	0.029	0.043	443.68	8.12e-02	211.03	3.86e-02	381.86	6.99e-02	0.0	0.0
78	35.161	0.028	0.043	2.38	4.35e-04	838.98	0.2	532.69	9.75e-02	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	Z %	Energia	Energia x v
79	35.340	0.028	0.043	91.88	1.68e-02	463.41	8.48e-02	66.93	1.22e-02	0.0	0.0
80	35.803	0.028	0.043	136.18	2.49e-02	715.52	0.1	3554.20	0.7	0.0	0.0
81	36.292	0.028	0.043	1017.12	0.2	24.16	4.42e-03	1734.44	0.3	0.0	0.0
82	36.426	0.027	0.043	69.34	1.27e-02	1203.31	0.2	7139.08	1.3	0.0	0.0
83	36.628	0.027	0.043	10.21	1.87e-03	435.47	7.97e-02	11.71	2.14e-03	0.0	0.0
84	37.020	0.027	0.042	507.80	9.29e-02	206.50	3.78e-02	622.70	0.1	0.0	0.0
85	37.554	0.027	0.042	0.06	1.11e-05	37.73	6.90e-03	179.27	3.28e-02	0.0	0.0
86	37.627	0.027	0.042	211.99	3.88e-02	368.92	6.75e-02	453.52	8.30e-02	0.0	0.0
87	38.110	0.026	0.042	138.53	2.53e-02	109.06	2.00e-02	616.40	0.1	0.0	0.0
88	38.390	0.026	0.042	34.51	6.31e-03	615.97	0.1	8863.21	1.6	0.0	0.0
89	38.841	0.026	0.042	180.91	3.31e-02	40.62	7.43e-03	65.45	1.20e-02	0.0	0.0
90	39.181	0.026	0.042	1113.60	0.2	452.61	8.28e-02	1511.85	0.3	0.0	0.0
91	39.461	0.025	0.042	1174.30	0.2	553.26	0.1	693.65	0.1	0.0	0.0
92	39.516	0.025	0.042	1806.71	0.3	99.03	1.81e-02	143.58	2.63e-02	0.0	0.0
93	39.944	0.025	0.041	22.99	4.21e-03	372.74	6.82e-02	34.62	6.33e-03	0.0	0.0
94	40.359	0.025	0.041	58.82	1.08e-02	0.11	1.98e-05	554.52	0.1	0.0	0.0
95	40.411	0.025	0.041	1.29	2.36e-04	5.09	9.31e-04	51.79	9.48e-03	0.0	0.0
96	40.473	0.025	0.041	55.00	1.01e-02	892.60	0.2	1076.89	0.2	0.0	0.0
97	40.604	0.025	0.041	25.68	4.70e-03	3.95	7.22e-04	1312.79	0.2	0.0	0.0
98	41.081	0.024	0.041	203.92	3.73e-02	96.97	1.77e-02	2693.53	0.5	0.0	0.0
99	41.492	0.024	0.041	2.35	4.30e-04	14.12	2.58e-03	2101.25	0.4	0.0	0.0
100	41.909	0.024	0.041	94.85	1.74e-02	361.57	6.62e-02	464.84	8.51e-02	0.0	0.0
101	42.212	0.024	0.041	19.90	3.64e-03	254.44	4.66e-02	451.84	8.27e-02	0.0	0.0
102	42.335	0.024	0.041	68.59	1.26e-02	250.08	4.58e-02	1.024e+04	1.9	0.0	0.0
103	42.388	0.024	0.041	59.95	1.10e-02	592.68	0.1	824.69	0.2	0.0	0.0
104	43.370	0.023	0.041	70.70	1.29e-02	28.11	5.14e-03	1129.51	0.2	0.0	0.0
105	43.971	0.023	0.040	79.10	1.45e-02	112.26	2.05e-02	95.07	1.74e-02	0.0	0.0
106	44.262	0.023	0.040	51.99	9.51e-03	20.33	3.72e-03	107.96	1.98e-02	0.0	0.0
107	44.407	0.023	0.040	45.26	8.28e-03	18.08	3.31e-03	659.75	0.1	0.0	0.0
108	44.917	0.022	0.040	262.82	4.81e-02	173.12	3.17e-02	2645.65	0.5	0.0	0.0
109	45.185	0.022	0.040	155.46	2.84e-02	312.72	5.72e-02	486.17	8.90e-02	0.0	0.0
110	45.342	0.022	0.040	93.91	1.72e-02	268.88	4.92e-02	238.59	4.37e-02	0.0	0.0
111	45.683	0.022	0.040	345.09	6.31e-02	89.87	1.64e-02	1.11	2.04e-04	0.0	0.0
112	46.567	0.021	0.040	132.77	2.43e-02	227.78	4.17e-02	0.14	2.52e-05	0.0	0.0
113	46.864	0.021	0.040	18.54	3.39e-03	348.71	6.38e-02	624.22	0.1	0.0	0.0
114	46.895	0.021	0.040	0.09	1.58e-05	12.94	2.37e-03	4399.06	0.8	0.0	0.0
115	47.173	0.021	0.040	0.02	4.54e-06	10.40	1.90e-03	1000.13	0.2	0.0	0.0
116	47.543	0.021	0.040	35.76	6.54e-03	105.02	1.92e-02	7058.63	1.3	0.0	0.0
117	47.801	0.021	0.039	67.17	1.23e-02	122.65	2.24e-02	186.55	3.41e-02	0.0	0.0
118	48.130	0.021	0.039	56.75	1.04e-02	140.37	2.57e-02	65.81	1.20e-02	0.0	0.0
119	48.786	0.020	0.039	7.83	1.43e-03	21.21	3.88e-03	217.17	3.97e-02	0.0	0.0
120	49.200	0.020	0.039	58.87	1.08e-02	138.10	2.53e-02	1280.56	0.2	0.0	0.0
121	49.448	0.020	0.039	0.11	2.10e-05	498.09	9.11e-02	214.81	3.93e-02	0.0	0.0
122	49.689	0.020	0.039	44.85	8.21e-03	61.25	1.12e-02	307.53	5.63e-02	0.0	0.0
123	49.838	0.020	0.039	80.88	1.48e-02	86.49	1.58e-02	289.39	5.30e-02	0.0	0.0
124	50.011	0.020	0.039	52.99	9.70e-03	70.93	1.30e-02	111.32	2.04e-02	0.0	0.0
125	50.349	0.020	0.039	202.66	3.71e-02	40.40	7.39e-03	43.67	7.99e-03	0.0	0.0
126	50.537	0.020	0.039	70.14	1.28e-02	0.57	1.04e-04	568.44	0.1	0.0	0.0
127	51.257	0.020	0.039	1560.24	0.3	3.77	6.90e-04	1363.64	0.2	0.0	0.0
128	51.687	0.019	0.039	152.46	2.79e-02	0.95	1.73e-04	641.58	0.1	0.0	0.0
129	51.800	0.019	0.039	415.52	7.60e-02	0.10	1.80e-05	5.29e-03	0.0	0.0	0.0
130	52.229	0.019	0.039	0.42	7.70e-05	36.46	6.67e-03	177.91	3.26e-02	0.0	0.0
131	52.479	0.019	0.039	201.60	3.69e-02	3.37	6.17e-04	176.92	3.24e-02	0.0	0.0
132	52.818	0.019	0.038	72.79	1.33e-02	14.65	2.68e-03	724.86	0.1	0.0	0.0
133	52.861	0.019	0.038	128.54	2.35e-02	103.69	1.90e-02	379.23	6.94e-02	0.0	0.0
134	53.184	0.019	0.038	1136.73	0.2	104.51	1.91e-02	438.94	8.03e-02	0.0	0.0
135	53.368	0.019	0.038	217.07	3.97e-02	40.71	7.45e-03	554.60	0.1	0.0	0.0
136	53.713	0.019	0.038	417.61	7.64e-02	58.80	1.08e-02	4.35	7.97e-04	0.0	0.0
137	53.778	0.019	0.038	19.43	3.56e-03	320.75	5.87e-02	4.62	8.46e-04	0.0	0.0
138	53.856	0.019	0.038	354.56	6.49e-02	156.39	2.86e-02	491.22	8.99e-02	0.0	0.0
139	54.241	0.018	0.038	0.78	1.42e-04	5.97	1.09e-03	1161.84	0.2	0.0	0.0
140	54.498	0.018	0.038	1307.27	0.2	247.13	4.52e-02	58.59	1.07e-02	0.0	0.0
141	54.531	0.018	0.038	0.07	1.24e-05	234.33	4.29e-02	1866.35	0.3	0.0	0.0
142	54.855	0.018	0.038	21.97	4.02e-03	47.15	8.63e-03	521.36	9.54e-02	0.0	0.0
143	55.194	0.018	0.038	7.95	1.46e-03	29.57	5.41e-03	479.28	8.77e-02	0.0	0.0
144	55.309	0.018	0.038	8.41	1.54e-03	68.65	1.26e-02	442.08	8.09e-02	0.0	0.0
145	55.603	0.018	0.038	0.05	9.52e-06	24.48	4.48e-03	30.68	5.61e-03	0.0	0.0
146	56.036	0.018	0.038	77.54	1.42e-02	163.27	2.99e-02	170.59	3.12e-02	0.0	0.0
147	56.297	0.018	0.038	55.83	1.02e-02	756.33	0.1	29.32	5.36e-03	0.0	0.0
148	56.457	0.018	0.038	69.96	1.28e-02	35.70	6.53e-03	0.51	9.27e-05	0.0	0.0
149	56.989	0.018	0.038	57.48	1.05e-02	10.66	1.95e-03	724.04	0.1	0.0	0.0
150	57.211	0.017	0.038	363.78	6.66e-02	4.22	7.73e-04	90.82	1.66e-02	0.0	0.0
151	57.636	0.017	0.038	68.76	1.26e-02	0.31	5.68e-05	38.63	7.07e-03	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	Z %	Energia	Energia x v
152	57.991	0.017	0.038	69.37	1.27e-02	40.60	7.43e-03	18.67	3.42e-03	0.0	0.0
153	58.025	0.017	0.038	251.99	4.61e-02	242.66	4.44e-02	110.23	2.02e-02	0.0	0.0
154	58.262	0.017	0.038	987.84	0.2	92.84	1.70e-02	168.55	3.08e-02	0.0	0.0
155	58.550	0.017	0.038	307.47	5.63e-02	15.83	2.90e-03	160.81	2.94e-02	0.0	0.0
156	58.696	0.017	0.038	158.86	2.91e-02	17.32	3.17e-03	1.07	1.95e-04	0.0	0.0
157	58.957	0.017	0.038	204.22	3.74e-02	538.37	9.85e-02	63.36	1.16e-02	0.0	0.0
158	59.088	0.017	0.037	0.07	1.36e-05	136.48	2.50e-02	166.69	3.05e-02	0.0	0.0
159	59.626	0.017	0.037	0.38	7.03e-05	3.68	6.73e-04	0.18	3.35e-05	0.0	0.0
160	59.749	0.017	0.037	2.17	3.96e-04	96.29	1.76e-02	3.37	6.17e-04	0.0	0.0
161	60.317	0.017	0.037	70.72	1.29e-02	48.19	8.82e-03	49.37	9.03e-03	0.0	0.0
162	60.507	0.017	0.037	13.66	2.50e-03	177.96	3.26e-02	30.41	5.56e-03	0.0	0.0
163	60.978	0.016	0.037	20.60	3.77e-03	14.77	2.70e-03	1.06	1.94e-04	0.0	0.0
164	61.146	0.016	0.037	149.86	2.74e-02	6.81	1.25e-03	12.19	2.23e-03	0.0	0.0
165	61.557	0.016	0.037	21.30	3.90e-03	3.51	6.43e-04	2.23	4.08e-04	0.0	0.0
166	61.919	0.016	0.037	451.98	8.27e-02	215.33	3.94e-02	324.18	5.93e-02	0.0	0.0
167	61.982	0.016	0.037	136.33	2.49e-02	0.12	2.26e-05	84.99	1.56e-02	0.0	0.0
168	62.451	0.016	0.037	192.17	3.52e-02	186.96	3.42e-02	176.73	3.23e-02	0.0	0.0
169	62.786	0.016	0.037	139.10	2.55e-02	30.12	5.51e-03	714.80	0.1	0.0	0.0
170	62.898	0.016	0.037	173.26	3.17e-02	21.85	4.00e-03	30.32	5.55e-03	0.0	0.0
171	63.280	0.016	0.037	120.99	2.21e-02	246.12	4.50e-02	3.92	7.17e-04	0.0	0.0
172	63.473	0.016	0.037	45.97	8.41e-03	0.77	1.40e-04	0.04	6.53e-06	0.0	0.0
173	63.624	0.016	0.037	150.75	2.76e-02	409.01	7.48e-02	231.54	4.24e-02	0.0	0.0
174	63.713	0.016	0.037	182.19	3.33e-02	42.75	7.82e-03	1.51e-03	0.0	0.0	0.0
175	63.980	0.016	0.037	7.18	1.31e-03	5.50	1.01e-03	1079.01	0.2	0.0	0.0
176	64.013	0.016	0.037	136.29	2.49e-02	18.59	3.40e-03	37.69	6.90e-03	0.0	0.0
177	64.183	0.016	0.037	8.74	1.60e-03	331.76	6.07e-02	139.32	2.55e-02	0.0	0.0
178	64.519	0.015	0.037	188.47	3.45e-02	214.92	3.93e-02	402.35	7.36e-02	0.0	0.0
179	64.668	0.015	0.037	89.13	1.63e-02	30.31	5.55e-03	2.15	3.94e-04	0.0	0.0
180	65.065	0.015	0.037	61.36	1.12e-02	484.11	8.86e-02	437.74	8.01e-02	0.0	0.0
181	65.425	0.015	0.037	8.69	1.59e-03	367.03	6.72e-02	14.72	2.69e-03	0.0	0.0
182	65.739	0.015	0.037	0.56	1.02e-04	475.09	8.69e-02	144.24	2.64e-02	0.0	0.0
183	66.044	0.015	0.037	3.55	6.50e-04	45.75	8.37e-03	163.76	3.00e-02	0.0	0.0
184	66.069	0.015	0.037	124.24	2.27e-02	65.61	1.20e-02	152.65	2.79e-02	0.0	0.0
185	66.353	0.015	0.037	7.28	1.33e-03	16.16	2.96e-03	57.33	1.05e-02	0.0	0.0
186	66.621	0.015	0.037	4.09	7.49e-04	81.21	1.49e-02	418.56	7.66e-02	0.0	0.0
187	66.903	0.015	0.037	17.80	3.26e-03	66.70	1.22e-02	7.14	1.31e-03	0.0	0.0
188	67.062	0.015	0.037	23.05	4.22e-03	112.66	2.06e-02	94.17	1.72e-02	0.0	0.0
189	67.147	0.015	0.036	6.40	1.17e-03	24.81	4.54e-03	6897.78	1.3	0.0	0.0
190	67.279	0.015	0.036	10.87	1.99e-03	57.75	1.06e-02	4.75	8.69e-04	0.0	0.0
191	67.622	0.015	0.036	150.17	2.75e-02	1.09	1.99e-04	99.68	1.82e-02	0.0	0.0
192	67.821	0.015	0.036	11.02	2.02e-03	26.49	4.85e-03	17.86	3.27e-03	0.0	0.0
193	68.042	0.015	0.036	5.76	1.05e-03	252.67	4.62e-02	1.68	3.07e-04	0.0	0.0
194	68.381	0.015	0.036	2.62	4.79e-04	150.90	2.76e-02	104.19	1.91e-02	0.0	0.0
195	68.452	0.015	0.036	72.38	1.32e-02	9.39	1.72e-03	277.84	5.08e-02	0.0	0.0
196	68.748	0.015	0.036	7.31	1.34e-03	2.07	3.79e-04	712.77	0.1	0.0	0.0
197	69.446	0.014	0.036	56.26	1.03e-02	0.88	1.61e-04	277.44	5.08e-02	0.0	0.0
198	69.579	0.014	0.036	5.93	1.08e-03	121.71	2.23e-02	865.33	0.2	0.0	0.0
199	69.683	0.014	0.036	1.82	3.33e-04	266.31	4.87e-02	60.14	1.10e-02	0.0	0.0
200	70.109	0.014	0.036	30.14	5.51e-03	345.11	6.31e-02	1.73	3.17e-04	0.0	0.0
201	70.486	0.014	0.036	59.23	1.08e-02	36.24	6.63e-03	143.19	2.62e-02	0.0	0.0
202	70.538	0.014	0.036	0.60	1.09e-04	0.92	1.68e-04	4.39	8.04e-04	0.0	0.0
203	70.853	0.014	0.036	4.72	8.64e-04	44.23	8.09e-03	0.02	4.17e-06	0.0	0.0
204	70.942	0.014	0.036	33.03	6.04e-03	84.26	1.54e-02	247.15	4.52e-02	0.0	0.0
205	71.037	0.014	0.036	38.82	7.10e-03	41.66	7.62e-03	510.66	9.34e-02	0.0	0.0
206	71.253	0.014	0.036	41.73	7.64e-03	2.37	4.33e-04	9.25	1.69e-03	0.0	0.0
207	71.542	0.014	0.036	56.11	1.03e-02	21.13	3.87e-03	119.62	2.19e-02	0.0	0.0
208	71.632	0.014	0.036	136.70	2.50e-02	1.50	2.74e-04	508.80	9.31e-02	0.0	0.0
209	72.194	0.014	0.036	56.97	1.04e-02	7.22	1.32e-03	13.12	2.40e-03	0.0	0.0
210	72.358	0.014	0.036	2.05e-06	0.0	4.58	8.38e-04	6.92	1.27e-03	0.0	0.0
211	72.464	0.014	0.036	173.29	3.17e-02	6.39	1.17e-03	112.01	2.05e-02	0.0	0.0
212	72.587	0.014	0.036	0.60	1.11e-04	2.15	3.94e-04	347.42	6.36e-02	0.0	0.0
213	73.035	0.014	0.036	0.75	1.37e-04	60.28	1.10e-02	297.78	5.45e-02	0.0	0.0
214	73.078	0.014	0.036	14.70	2.69e-03	146.72	2.68e-02	315.29	5.77e-02	0.0	0.0
215	73.518	0.014	0.036	0.57	1.04e-04	0.05	9.98e-06	126.14	2.31e-02	0.0	0.0
216	73.686	0.014	0.036	14.58	2.67e-03	24.25	4.44e-03	194.86	3.57e-02	0.0	0.0
217	74.012	0.014	0.036	5.89	1.08e-03	29.80	5.45e-03	467.24	8.55e-02	0.0	0.0
218	74.306	0.013	0.036	6.72	1.23e-03	8.93	1.63e-03	1103.83	0.2	0.0	0.0
219	74.431	0.013	0.036	235.87	4.32e-02	25.10	4.59e-03	211.63	3.87e-02	0.0	0.0
220	75.017	0.013	0.036	0.02	4.52e-06	47.20	8.64e-03	461.64	8.45e-02	0.0	0.0
Risulta				5.260e+05		5.295e+05		4.780e+05			
In percentuale				96.25		96.88		87.47			

CDC	Tipo	Sigla Id	Note
12	Edk	CDC=Ed (dinamico SLD) alfa=0.0 (ecc. -)	
			verifica esistenti: fattore FC 1.200
			categoria suolo: B
			fattore di sito S = 1.200
			ordinata spettro (tratto Tb-Tc) = 0.075 g
			angolo di ingresso:0.0
			eccentricità aggiuntiva: negativa
			periodo proprio T1: 0.135 sec.
			numero di modi considerati:220
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
cm	daN	cm	cm	cm	cm	cm	cm			
1340.00	96.19	-491.36	-334.97	0.0	0.0	-491.36	-334.97	0.155	0.0	0.0
1295.00	116.44	-491.36	-334.97	0.0	0.0	-491.36	-334.97	1.791	0.0	0.0
1250.00	101.25	-491.36	-334.97	0.0	0.0	-491.36	-334.97	1.791	0.0	0.0
1205.00	1203.52	-572.28	-173.84	0.0	26.80	-635.82	-328.32	0.015	2.913	3.350
1195.00	7848.27	-175.90	173.40	0.0	15.15	-313.36	198.69	0.654	1.046	0.168
1160.00	2326.05	-575.55	-168.23	0.0	26.80	-635.82	-328.32	0.015	2.763	3.471
1115.00	2319.30	-575.63	-167.75	0.0	26.80	-635.82	-328.32	0.015	2.759	3.482
1070.00	2319.30	-575.63	-167.75	0.0	26.80	-635.82	-328.32	0.015	2.759	3.482
1025.00	1.465e+04	-128.29	99.57	0.0	52.28	-544.49	-95.81	0.601	1.188	0.224
985.00	1.083e+04	-102.23	128.80	0.0	52.28	-542.49	-74.78	0.744	1.130	0.289
945.00	1.083e+04	-102.21	128.80	0.0	52.28	-542.49	-74.78	0.744	1.130	0.289
905.00	6.437e+04	-130.89	142.36	0.0	52.28	-436.66	166.12	0.443	1.017	0.032
855.00	2.344e+04	10.15	277.19	0.0	52.28	-430.77	347.85	0.460	1.438	0.099
805.00	1.496e+04	-105.98	181.79	0.0	52.28	-430.86	314.26	0.449	1.073	0.180
755.00	1.478e+04	-111.83	175.63	0.0	52.28	-430.86	314.26	0.449	1.054	0.189
705.00	1.434e+04	-113.81	161.90	0.0	52.28	-431.46	281.46	0.467	1.028	0.157
655.00	1.389e+04	-115.92	147.28	0.0	52.28	-431.46	281.46	0.467	1.022	0.177
605.00	1.373e+04	-110.92	157.10	0.0	52.28	-431.43	318.26	0.449	1.058	0.210
555.00	1.499e+04	-84.11	147.58	0.0	52.28	-417.55	263.67	0.542	1.003	0.142
535.00	462.89	-284.62	710.53	0.0	0.0	-295.19	710.53	0.049	0.058	0.0
505.00	1.751e+04	-80.04	167.93	0.0	52.28	-417.49	314.16	0.560	0.998	0.187
455.00	1.393e+05	-28.92	228.10	0.0	52.28	-380.74	478.92	0.654	0.963	0.374
404.44	1.813e+04	-50.00	221.17	0.0	52.28	-389.48	517.14	0.548	1.015	0.444
378.89	7112.79	-473.91	-262.63	0.0	6.20	-445.72	-328.72	2.380	0.183	0.414
353.89	2.196e+04	-32.62	456.21	0.0	61.93	-349.91	587.97	0.556	0.867	0.279
303.33	1.928e+04	-91.51	295.05	0.0	61.93	-423.33	593.38	0.329	1.179	0.506
252.78	2.190e+04	-176.89	242.77	0.0	61.93	-426.16	607.02	0.312	0.909	0.621
202.22	1.592e+04	-73.92	284.63	0.0	61.93	-426.16	607.02	0.312	1.284	0.549
151.67	1.601e+04	-65.56	283.49	0.0	61.93	-426.19	571.76	0.342	1.256	0.478
122.00	7167.74	-473.02	-262.23	0.0	6.20	-445.72	-328.72	2.380	0.177	0.416
101.11	1.343e+04	-59.25	403.57	0.0	61.93	-361.56	648.71	0.484	0.885	0.510
88.00	511.85	445.72	710.53	0.0	0.0	459.84	710.53	0.039	0.268	0.0
80.00	1592.11	106.62	-334.97	0.0	0.0	112.14	-334.97	0.080	0.025	0.0
50.56	1.912e+04	-72.11	249.76	0.0	61.93	-425.00	501.84	0.409	1.124	0.402
Risulta	5.465e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	5.038	0.198	0.075	1031.38	0.2	3.924e+04	7.2	6.76e-03	1.24e-06	0.0	0.0
2	5.138	0.195	0.075	1002.63	0.2	1.313e+05	24.0	0.06	1.16e-05	0.0	0.0
3	7.421	0.135	0.075	3.605e+05	66.0	98.65	1.81e-02	14.96	2.74e-03	0.0	0.0
4	7.895	0.127	0.075	9359.96	1.7	1.163e+05	21.3	18.27	3.34e-03	0.0	0.0
5	8.269	0.121	0.075	703.38	0.1	1.132e+04	2.1	12.44	2.28e-03	0.0	0.0
6	8.569	0.117	0.075	838.44	0.2	2.047e+04	3.7	0.08	1.45e-05	0.0	0.0
7	9.390	0.106	0.075	1.100e+04	2.0	2.650e+04	4.8	92.94	1.70e-02	0.0	0.0
8	9.508	0.105	0.075	3652.96	0.7	7.65	1.40e-03	17.29	3.16e-03	0.0	0.0
9	9.789	0.102	0.075	1463.78	0.3	2047.23	0.4	14.11	2.58e-03	0.0	0.0
10	10.334	0.097	0.075	2.182e+04	4.0	6159.24	1.1	0.88	1.61e-04	0.0	0.0
11	10.972	0.091	0.074	721.82	0.1	3265.21	0.6	14.43	2.64e-03	0.0	0.0
12	11.701	0.085	0.071	4956.24	0.9	3.773e+04	6.9	1.07	1.96e-04	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	Z %	Energia	Energia x v
13	12.259	0.082	0.069	1.497e+04	2.7	1.796e+04	3.3	5.25	9.61e-04	0.0	0.0
14	12.323	0.081	0.069	2134.29	0.4	2570.06	0.5	5.08	9.30e-04	0.0	0.0
15	13.284	0.075	0.066	1.183e+04	2.2	193.66	3.54e-02	1.75	3.20e-04	0.0	0.0
16	13.575	0.074	0.065	5179.70	0.9	1528.01	0.3	120.02	2.20e-02	0.0	0.0
17	14.077	0.071	0.064	2033.63	0.4	1424.85	0.3	6.91	1.26e-03	0.0	0.0
18	14.578	0.069	0.063	733.68	0.1	2426.54	0.4	101.92	1.86e-02	0.0	0.0
19	15.097	0.066	0.062	2775.07	0.5	5957.55	1.1	54.25	9.93e-03	0.0	0.0
20	15.386	0.065	0.061	1192.69	0.2	147.10	2.69e-02	1.98	3.62e-04	0.0	0.0
21	15.793	0.063	0.060	4087.57	0.7	2569.01	0.5	13.72	2.51e-03	0.0	0.0
22	15.900	0.063	0.060	372.23	6.81e-02	1214.19	0.2	189.41	3.47e-02	0.0	0.0
23	16.229	0.062	0.059	1099.24	0.2	1104.65	0.2	27.01	4.94e-03	0.0	0.0
24	16.655	0.060	0.059	0.03	6.23e-06	4731.47	0.9	46.50	8.51e-03	0.0	0.0
25	17.220	0.058	0.058	405.71	7.42e-02	128.03	2.34e-02	37.88	6.93e-03	0.0	0.0
26	17.519	0.057	0.057	323.66	5.92e-02	1.330e+04	2.4	1.09	2.00e-04	0.0	0.0
27	18.154	0.055	0.056	248.58	4.55e-02	1101.79	0.2	140.45	2.57e-02	0.0	0.0
28	18.519	0.054	0.056	516.26	9.45e-02	626.82	0.1	2911.68	0.5	0.0	0.0
29	18.967	0.053	0.055	33.63	6.15e-03	1399.27	0.3	3012.41	0.6	0.0	0.0
30	20.162	0.050	0.054	0.56	1.02e-04	145.58	2.66e-02	8108.48	1.5	0.0	0.0
31	20.197	0.050	0.054	231.53	4.24e-02	20.36	3.73e-03	1.130e+04	2.1	0.0	0.0
32	20.398	0.049	0.053	3080.17	0.6	6734.00	1.2	92.21	1.69e-02	0.0	0.0
33	20.878	0.048	0.053	7819.42	1.4	134.24	2.46e-02	2695.67	0.5	0.0	0.0
34	21.298	0.047	0.052	1.11	2.03e-04	33.19	6.07e-03	749.08	0.1	0.0	0.0
35	21.783	0.046	0.052	5383.10	1.0	102.89	1.88e-02	121.43	2.22e-02	0.0	0.0
36	22.131	0.045	0.051	3716.30	0.7	1683.67	0.3	7541.06	1.4	0.0	0.0
37	22.509	0.044	0.051	288.70	5.28e-02	256.42	4.69e-02	1.847e+04	3.4	0.0	0.0
38	22.746	0.044	0.051	331.50	6.07e-02	1111.37	0.2	1088.79	0.2	0.0	0.0
39	22.777	0.044	0.051	476.61	8.72e-02	248.90	4.55e-02	1725.91	0.3	0.0	0.0
40	23.012	0.043	0.051	3825.44	0.7	1011.29	0.2	4756.89	0.9	0.0	0.0
41	23.342	0.043	0.050	7.36	1.35e-03	107.13	1.96e-02	5451.15	1.0	0.0	0.0
42	23.452	0.043	0.050	99.93	1.83e-02	78.96	1.44e-02	1095.61	0.2	0.0	0.0
43	23.599	0.042	0.050	3861.18	0.7	1356.11	0.2	1.154e+04	2.1	0.0	0.0
44	23.965	0.042	0.050	0.15	2.83e-05	380.15	6.96e-02	4896.62	0.9	0.0	0.0
45	24.290	0.041	0.049	206.19	3.77e-02	369.02	6.75e-02	1.209e+04	2.2	0.0	0.0
46	24.482	0.041	0.049	223.17	4.08e-02	7170.25	1.3	3252.28	0.6	0.0	0.0
47	25.015	0.040	0.049	173.74	3.18e-02	48.14	8.81e-03	1.13	2.06e-04	0.0	0.0
48	25.114	0.040	0.049	4.17	7.62e-04	21.18	3.88e-03	5023.07	0.9	0.0	0.0
49	25.486	0.039	0.048	1107.81	0.2	888.73	0.2	0.82	1.50e-04	0.0	0.0
50	25.611	0.039	0.048	0.11	2.01e-05	396.00	7.25e-02	1.286e+04	2.4	0.0	0.0
51	26.142	0.038	0.048	75.42	1.38e-02	4096.96	0.7	1893.26	0.3	0.0	0.0
52	26.460	0.038	0.048	387.58	7.09e-02	79.17	1.45e-02	1769.07	0.3	0.0	0.0
53	26.993	0.037	0.047	159.10	2.91e-02	0.10	1.83e-05	3.785e+04	6.9	0.0	0.0
54	27.270	0.037	0.047	156.58	2.87e-02	9824.57	1.8	1.079e+05	19.8	0.0	0.0
55	27.569	0.036	0.047	797.70	0.1	13.46	2.46e-03	8053.38	1.5	0.0	0.0
56	27.688	0.036	0.047	97.53	1.78e-02	1580.26	0.3	7950.85	1.5	0.0	0.0
57	27.856	0.036	0.047	46.65	8.54e-03	1955.00	0.4	7254.71	1.3	0.0	0.0
58	28.030	0.036	0.047	138.77	2.54e-02	467.76	8.56e-02	1.196e+04	2.2	0.0	0.0
59	28.252	0.035	0.047	884.70	0.2	22.77	4.17e-03	1736.74	0.3	0.0	0.0
60	28.831	0.035	0.046	308.32	5.64e-02	240.44	4.40e-02	823.24	0.2	0.0	0.0
61	29.279	0.034	0.046	363.04	6.64e-02	4914.34	0.9	1368.46	0.3	0.0	0.0
62	29.467	0.034	0.046	623.62	0.1	2776.30	0.5	2016.70	0.4	0.0	0.0
63	30.331	0.033	0.045	147.92	2.71e-02	34.42	6.30e-03	4092.02	0.7	0.0	0.0
64	30.522	0.033	0.045	537.48	9.83e-02	845.07	0.2	8752.60	1.6	0.0	0.0
65	30.700	0.033	0.045	130.95	2.40e-02	898.10	0.2	200.53	3.67e-02	0.0	0.0
66	30.850	0.032	0.045	27.98	5.12e-03	79.20	1.45e-02	3.349e+04	6.1	0.0	0.0
67	30.999	0.032	0.045	316.15	5.78e-02	139.02	2.54e-02	1703.11	0.3	0.0	0.0
68	31.984	0.031	0.045	32.65	5.97e-03	590.07	0.1	401.84	7.35e-02	0.0	0.0
69	32.235	0.031	0.044	734.59	0.1	640.10	0.1	1.105e+04	2.0	0.0	0.0
70	32.386	0.031	0.044	126.31	2.31e-02	1387.35	0.3	1743.22	0.3	0.0	0.0
71	32.939	0.030	0.044	554.45	0.1	19.14	3.50e-03	295.62	5.41e-02	0.0	0.0
72	33.467	0.030	0.044	1338.78	0.2	1181.20	0.2	1247.64	0.2	0.0	0.0
73	33.708	0.030	0.044	1101.61	0.2	254.62	4.66e-02	613.15	0.1	0.0	0.0
74	33.901	0.029	0.044	726.11	0.1	104.57	1.91e-02	1075.71	0.2	0.0	0.0
75	34.398	0.029	0.043	325.37	5.95e-02	947.88	0.2	825.99	0.2	0.0	0.0
76	34.632	0.029	0.043	117.39	2.15e-02	40.97	7.50e-03	5.33	9.75e-04	0.0	0.0
77	35.053	0.029	0.043	373.03	6.83e-02	2.12	3.87e-04	1063.48	0.2	0.0	0.0
78	35.607	0.028	0.043	49.16	8.99e-03	207.44	3.80e-02	431.12	7.89e-02	0.0	0.0
79	35.871	0.028	0.043	27.91	5.11e-03	1064.32	0.2	7069.67	1.3	0.0	0.0
80	36.027	0.028	0.043	625.93	0.1	1105.93	0.2	751.97	0.1	0.0	0.0
81	36.212	0.028	0.043	25.54	4.67e-03	472.99	8.65e-02	1582.38	0.3	0.0	0.0
82	36.551	0.027	0.043	344.03	6.30e-02	1872.52	0.3	3036.60	0.6	0.0	0.0
83	36.749	0.027	0.043	202.98	3.71e-02	102.12	1.87e-02	28.96	5.30e-03	0.0	0.0
84	37.330	0.027	0.042	468.66	8.58e-02	4.74	8.68e-04	174.30	3.19e-02	0.0	0.0
85	37.405	0.027	0.042	20.49	3.75e-03	8.08	1.48e-03	3533.85	0.6	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	Z %	Energia	Energia x v
86	37.589	0.027	0.042	76.77	1.40e-02	96.01	1.76e-02	2708.93	0.5	0.0	0.0
87	37.898	0.026	0.042	350.87	6.42e-02	170.60	3.12e-02	121.98	2.23e-02	0.0	0.0
88	38.141	0.026	0.042	95.68	1.75e-02	6.89	1.26e-03	149.64	2.74e-02	0.0	0.0
89	38.540	0.026	0.042	41.06	7.51e-03	39.74	7.27e-03	1237.83	0.2	0.0	0.0
90	38.694	0.026	0.042	0.78	1.43e-04	405.29	7.42e-02	5399.72	1.0	0.0	0.0
91	39.142	0.026	0.042	51.44	9.41e-03	43.14	7.89e-03	3249.71	0.6	0.0	0.0
92	39.783	0.025	0.042	18.80	3.44e-03	634.98	0.1	18.79	3.44e-03	0.0	0.0
93	40.230	0.025	0.041	40.87	7.48e-03	515.40	9.43e-02	1527.65	0.3	0.0	0.0
94	40.428	0.025	0.041	16.18	2.96e-03	242.67	4.44e-02	91.54	1.68e-02	0.0	0.0
95	40.610	0.025	0.041	10.33	1.89e-03	1.73	3.17e-04	3751.71	0.7	0.0	0.0
96	40.670	0.025	0.041	35.45	6.49e-03	77.90	1.43e-02	3086.62	0.6	0.0	0.0
97	41.077	0.024	0.041	452.49	8.28e-02	1138.82	0.2	1371.67	0.3	0.0	0.0
98	41.214	0.024	0.041	293.19	5.36e-02	2.78	5.09e-04	1356.56	0.2	0.0	0.0
99	41.700	0.024	0.041	204.62	3.74e-02	52.00	9.52e-03	33.51	6.13e-03	0.0	0.0
100	41.763	0.024	0.041	44.43	8.13e-03	60.12	1.10e-02	223.22	4.08e-02	0.0	0.0
101	42.111	0.024	0.041	224.03	4.10e-02	15.45	2.83e-03	4167.74	0.8	0.0	0.0
102	42.251	0.024	0.041	108.94	1.99e-02	34.71	6.35e-03	128.39	2.35e-02	0.0	0.0
103	42.555	0.023	0.041	659.46	0.1	611.49	0.1	1095.81	0.2	0.0	0.0
104	42.587	0.023	0.041	418.35	7.66e-02	44.70	8.18e-03	68.09	1.25e-02	0.0	0.0
105	43.022	0.023	0.041	3.02	5.53e-04	6.58	1.20e-03	446.30	8.17e-02	0.0	0.0
106	43.236	0.023	0.041	89.27	1.63e-02	474.71	8.69e-02	4087.88	0.7	0.0	0.0
107	43.703	0.023	0.040	383.94	7.03e-02	20.42	3.74e-03	218.97	4.01e-02	0.0	0.0
108	44.165	0.023	0.040	20.83	3.81e-03	38.69	7.08e-03	403.85	7.39e-02	0.0	0.0
109	44.449	0.022	0.040	53.39	9.77e-03	4.53	8.29e-04	400.13	7.32e-02	0.0	0.0
110	44.809	0.022	0.040	83.23	1.52e-02	1.45	2.65e-04	22.24	4.07e-03	0.0	0.0
111	44.957	0.022	0.040	0.03	4.90e-06	103.75	1.90e-02	996.82	0.2	0.0	0.0
112	45.392	0.022	0.040	40.20	7.36e-03	165.00	3.02e-02	0.27	4.90e-05	0.0	0.0
113	46.246	0.022	0.040	9.96	1.82e-03	208.51	3.82e-02	4.66	8.52e-04	0.0	0.0
114	46.412	0.022	0.040	28.33	5.18e-03	250.77	4.59e-02	69.93	1.28e-02	0.0	0.0
115	46.582	0.021	0.040	36.68	6.71e-03	233.85	4.28e-02	858.65	0.2	0.0	0.0
116	46.792	0.021	0.040	2.54	4.64e-04	11.67	2.14e-03	20.77	3.80e-03	0.0	0.0
117	47.215	0.021	0.040	20.02	3.66e-03	257.30	4.71e-02	274.08	5.02e-02	0.0	0.0
118	47.324	0.021	0.040	53.23	9.74e-03	8.78	1.61e-03	2598.23	0.5	0.0	0.0
119	48.128	0.021	0.039	7.10	1.30e-03	42.37	7.75e-03	1.282e+04	2.3	0.0	0.0
120	48.414	0.021	0.039	79.39	1.45e-02	4.76	8.71e-04	79.18	1.45e-02	0.0	0.0
121	48.861	0.020	0.039	17.56	3.21e-03	1.01	1.85e-04	46.43	8.50e-03	0.0	0.0
122	49.219	0.020	0.039	130.27	2.38e-02	475.84	8.71e-02	146.89	2.69e-02	0.0	0.0
123	49.459	0.020	0.039	43.38	7.94e-03	56.60	1.04e-02	0.63	1.15e-04	0.0	0.0
124	49.676	0.020	0.039	57.92	1.06e-02	80.61	1.48e-02	54.76	1.00e-02	0.0	0.0
125	49.905	0.020	0.039	35.85	6.56e-03	3.31	6.06e-04	24.78	4.53e-03	0.0	0.0
126	50.097	0.020	0.039	7.13	1.30e-03	320.10	5.86e-02	1934.96	0.4	0.0	0.0
127	50.239	0.020	0.039	38.55	7.05e-03	4.60	8.42e-04	25.70	4.70e-03	0.0	0.0
128	50.501	0.020	0.039	9.70	1.78e-03	165.93	3.04e-02	82.35	1.51e-02	0.0	0.0
129	51.064	0.020	0.039	178.74	3.27e-02	206.05	3.77e-02	680.04	0.1	0.0	0.0
130	51.318	0.019	0.039	69.04	1.26e-02	3.35	6.12e-04	297.33	5.44e-02	0.0	0.0
131	51.558	0.019	0.039	15.82	2.89e-03	17.65	3.23e-03	2.48	4.54e-04	0.0	0.0
132	52.080	0.019	0.039	88.51	1.62e-02	24.95	4.57e-03	28.26	5.17e-03	0.0	0.0
133	52.361	0.019	0.039	25.47	4.66e-03	6.69	1.22e-03	926.30	0.2	0.0	0.0
134	53.113	0.019	0.038	216.69	3.97e-02	0.33	5.98e-05	1.56	2.86e-04	0.0	0.0
135	53.332	0.019	0.038	1.54	2.81e-04	36.75	6.72e-03	34.91	6.39e-03	0.0	0.0
136	53.433	0.019	0.038	6.08	1.11e-03	155.94	2.85e-02	1996.62	0.4	0.0	0.0
137	53.534	0.019	0.038	1.35	2.46e-04	647.86	0.1	5.38	9.84e-04	0.0	0.0
138	53.952	0.019	0.038	212.46	3.89e-02	9.10	1.67e-03	1645.02	0.3	0.0	0.0
139	54.074	0.018	0.038	1.26	2.31e-04	42.69	7.81e-03	478.91	8.76e-02	0.0	0.0
140	54.357	0.018	0.038	238.99	4.37e-02	299.42	5.48e-02	200.92	3.68e-02	0.0	0.0
141	54.659	0.018	0.038	11.51	2.11e-03	13.68	2.50e-03	225.17	4.12e-02	0.0	0.0
142	55.059	0.018	0.038	21.48	3.93e-03	29.05	5.32e-03	289.55	5.30e-02	0.0	0.0
143	55.394	0.018	0.038	214.73	3.93e-02	2.56	4.68e-04	1223.81	0.2	0.0	0.0
144	55.683	0.018	0.038	196.74	3.60e-02	18.64	3.41e-03	39.44	7.22e-03	0.0	0.0
145	55.973	0.018	0.038	484.26	8.86e-02	182.49	3.34e-02	81.32	1.49e-02	0.0	0.0
146	56.335	0.018	0.038	170.53	3.12e-02	0.02	2.81e-06	143.31	2.62e-02	0.0	0.0
147	56.502	0.018	0.038	2.15	3.93e-04	27.19	4.98e-03	9.77	1.79e-03	0.0	0.0
148	57.103	0.018	0.038	1826.88	0.3	152.85	2.80e-02	69.90	1.28e-02	0.0	0.0
149	57.150	0.017	0.038	409.73	7.50e-02	40.12	7.34e-03	471.91	8.64e-02	0.0	0.0
150	57.485	0.017	0.038	22.74	4.16e-03	14.66	2.68e-03	29.12	5.33e-03	0.0	0.0
151	57.751	0.017	0.038	81.65	1.49e-02	166.43	3.05e-02	25.50	4.67e-03	0.0	0.0
152	57.797	0.017	0.038	426.31	7.80e-02	51.08	9.35e-03	0.27	4.97e-05	0.0	0.0
153	58.195	0.017	0.038	8.09	1.48e-03	87.16	1.59e-02	356.89	6.53e-02	0.0	0.0
154	58.311	0.017	0.038	6.46	1.18e-03	157.10	2.87e-02	20.31	3.72e-03	0.0	0.0
155	58.625	0.017	0.038	629.65	0.1	231.57	4.24e-02	45.34	8.30e-03	0.0	0.0
156	58.763	0.017	0.038	5.86	1.07e-03	370.89	6.79e-02	66.54	1.22e-02	0.0	0.0
157	58.828	0.017	0.038	158.49	2.90e-02	355.76	6.51e-02	3.75	6.86e-04	0.0	0.0
158	59.463	0.017	0.037	10.55	1.93e-03	22.55	4.13e-03	156.23	2.86e-02	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	Z %	Energia	Energia x v
159	59.792	0.017	0.037	240.28	4.40e-02	78.46	1.44e-02	0.04	7.46e-06	0.0	0.0
160	60.163	0.017	0.037	25.54	4.67e-03	207.95	3.81e-02	318.18	5.82e-02	0.0	0.0
161	60.374	0.017	0.037	927.39	0.2	8.53	1.56e-03	95.79	1.75e-02	0.0	0.0
162	60.479	0.017	0.037	57.31	1.05e-02	81.20	1.49e-02	34.88	6.38e-03	0.0	0.0
163	60.670	0.016	0.037	4.22	7.72e-04	73.99	1.35e-02	2.67	4.88e-04	0.0	0.0
164	61.226	0.016	0.037	54.91	1.00e-02	1.11e-03	0.0	0.30	5.54e-05	0.0	0.0
165	61.512	0.016	0.037	87.73	1.61e-02	0.24	4.38e-05	35.13	6.43e-03	0.0	0.0
166	61.635	0.016	0.037	132.69	2.43e-02	431.92	7.90e-02	394.72	7.22e-02	0.0	0.0
167	61.769	0.016	0.037	213.29	3.90e-02	73.46	1.34e-02	195.94	3.59e-02	0.0	0.0
168	62.278	0.016	0.037	185.70	3.40e-02	84.00	1.54e-02	1.35	2.47e-04	0.0	0.0
169	62.558	0.016	0.037	11.02	2.02e-03	49.09	8.98e-03	94.86	1.74e-02	0.0	0.0
170	62.886	0.016	0.037	0.28	5.11e-05	29.74	5.44e-03	195.36	3.57e-02	0.0	0.0
171	63.101	0.016	0.037	3.54	6.49e-04	35.26	6.45e-03	1104.78	0.2	0.0	0.0
172	63.214	0.016	0.037	63.51	1.16e-02	22.78	4.17e-03	108.22	1.98e-02	0.0	0.0
173	63.640	0.016	0.037	34.85	6.38e-03	128.04	2.34e-02	131.04	2.40e-02	0.0	0.0
174	63.792	0.016	0.037	69.54	1.27e-02	2.76	5.05e-04	128.64	2.35e-02	0.0	0.0
175	63.995	0.016	0.037	80.70	1.48e-02	57.45	1.05e-02	68.44	1.25e-02	0.0	0.0
176	64.176	0.016	0.037	0.64	1.16e-04	591.65	0.1	84.09	1.54e-02	0.0	0.0
177	64.249	0.016	0.037	0.82	1.50e-04	263.04	4.81e-02	45.14	8.26e-03	0.0	0.0
178	64.602	0.015	0.037	189.85	3.47e-02	427.05	7.81e-02	130.57	2.39e-02	0.0	0.0
179	64.771	0.015	0.037	15.18	2.78e-03	24.49	4.48e-03	541.48	9.91e-02	0.0	0.0
180	65.045	0.015	0.037	5.03	9.20e-04	87.56	1.60e-02	209.79	3.84e-02	0.0	0.0
181	65.405	0.015	0.037	37.74	6.91e-03	5.83	1.07e-03	10.61	1.94e-03	0.0	0.0
182	65.577	0.015	0.037	73.95	1.35e-02	38.24	7.00e-03	430.80	7.88e-02	0.0	0.0
183	65.823	0.015	0.037	6.83	1.25e-03	97.37	1.78e-02	297.34	5.44e-02	0.0	0.0
184	66.052	0.015	0.037	0.10	1.84e-05	956.93	0.2	409.51	7.49e-02	0.0	0.0
185	66.222	0.015	0.037	54.56	9.98e-03	13.38	2.45e-03	3041.81	0.6	0.0	0.0
186	66.463	0.015	0.037	7.46	1.36e-03	39.65	7.26e-03	3.58	6.56e-04	0.0	0.0
187	66.583	0.015	0.037	153.60	2.81e-02	70.78	1.30e-02	2405.91	0.4	0.0	0.0
188	66.736	0.015	0.037	71.59	1.31e-02	23.25	4.26e-03	218.18	3.99e-02	0.0	0.0
189	66.879	0.015	0.037	1.14	2.08e-04	55.39	1.01e-02	221.72	4.06e-02	0.0	0.0
190	67.233	0.015	0.036	114.51	2.10e-02	152.53	2.79e-02	14.62	2.68e-03	0.0	0.0
191	67.439	0.015	0.036	23.74	4.34e-03	109.89	2.01e-02	8.60	1.57e-03	0.0	0.0
192	67.534	0.015	0.036	43.33	7.93e-03	275.71	5.05e-02	78.02	1.43e-02	0.0	0.0
193	67.992	0.015	0.036	191.09	3.50e-02	4.69	8.59e-04	0.07	1.26e-05	0.0	0.0
194	68.312	0.015	0.036	51.90	9.50e-03	5.52	1.01e-03	185.18	3.39e-02	0.0	0.0
195	68.420	0.015	0.036	332.52	6.08e-02	58.35	1.07e-02	67.21	1.23e-02	0.0	0.0
196	68.686	0.015	0.036	349.12	6.39e-02	16.91	3.09e-03	29.59	5.41e-03	0.0	0.0
197	68.886	0.015	0.036	67.14	1.23e-02	18.95	3.47e-03	343.46	6.28e-02	0.0	0.0
198	69.183	0.014	0.036	221.05	4.04e-02	2.68	4.91e-04	127.16	2.33e-02	0.0	0.0
199	69.381	0.014	0.036	32.78	6.00e-03	49.35	9.03e-03	371.15	6.79e-02	0.0	0.0
200	69.558	0.014	0.036	7.14	1.31e-03	340.44	6.23e-02	152.32	2.79e-02	0.0	0.0
201	69.989	0.014	0.036	3.53	6.46e-04	118.26	2.16e-02	11.12	2.03e-03	0.0	0.0
202	70.284	0.014	0.036	39.71	7.27e-03	0.23	4.26e-05	6.79	1.24e-03	0.0	0.0
203	70.502	0.014	0.036	66.62	1.22e-02	78.48	1.44e-02	161.60	2.96e-02	0.0	0.0
204	70.890	0.014	0.036	116.78	2.14e-02	68.68	1.26e-02	150.46	2.75e-02	0.0	0.0
205	71.258	0.014	0.036	44.47	8.14e-03	11.55	2.11e-03	12.58	2.30e-03	0.0	0.0
206	71.344	0.014	0.036	90.66	1.66e-02	156.82	2.87e-02	204.47	3.74e-02	0.0	0.0
207	71.698	0.014	0.036	2.38	4.36e-04	1.31	2.40e-04	13.14	2.40e-03	0.0	0.0
208	71.759	0.014	0.036	23.07	4.22e-03	28.75	5.26e-03	59.94	1.10e-02	0.0	0.0
209	72.090	0.014	0.036	0.02	4.07e-06	58.42	1.07e-02	19.11	3.50e-03	0.0	0.0
210	72.279	0.014	0.036	84.60	1.55e-02	1.52	2.78e-04	172.84	3.16e-02	0.0	0.0
211	72.403	0.014	0.036	47.13	8.62e-03	6.18	1.13e-03	216.09	3.95e-02	0.0	0.0
212	72.759	0.014	0.036	19.69	3.60e-03	4.32	7.90e-04	277.34	5.07e-02	0.0	0.0
213	73.310	0.014	0.036	172.43	3.16e-02	135.45	2.48e-02	17.83	3.26e-03	0.0	0.0
214	73.454	0.014	0.036	423.70	7.75e-02	47.31	8.66e-03	50.61	9.26e-03	0.0	0.0
215	73.633	0.014	0.036	114.67	2.10e-02	3.97	7.27e-04	18.57	3.40e-03	0.0	0.0
216	73.691	0.014	0.036	8.50	1.56e-03	26.62	4.87e-03	15.45	2.83e-03	0.0	0.0
217	73.851	0.014	0.036	8.26	1.51e-03	29.81	5.45e-03	9.47	1.73e-03	0.0	0.0
218	74.267	0.013	0.036	79.24	1.45e-02	45.40	8.31e-03	290.82	5.32e-02	0.0	0.0
219	74.553	0.013	0.036	263.68	4.82e-02	14.34	2.62e-03	1.50e-03	0.0	0.0	0.0
220	74.756	0.013	0.036	309.02	5.65e-02	1.21	2.22e-04	1032.60	0.2	0.0	0.0
Risulta				5.245e+05		5.295e+05		4.736e+05			
In percentuale				95.98		96.89		86.65			

CDC	Tipo	Sigla Id	Note
13	Edk	CDC=Ed (dinamico SLD) alfa=90.00 (ecc. +)	
			verifica esistenti: fattore FC 1.200

CDC	Tipo	Sigla Id	Note
			categoria suolo: B
			fattore di sito S = 1.200
			ordinata spettro (tratto Tb-Tc) = 0.075 g
			angolo di ingresso:90.00
			eccentricità aggiuntiva: positiva
			periodo proprio T1: 0.202 sec.
			numero di modi considerati:220
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
cm	daN	cm	cm	cm	cm	cm	cm			
1340.00	96.19	-491.36	-334.97	5.50	0.0	-491.36	-334.97	0.155	0.0	0.0
1295.00	116.44	-491.36	-334.97	5.50	0.0	-491.36	-334.97	1.791	0.0	0.0
1250.00	101.25	-491.36	-334.97	5.50	0.0	-491.36	-334.97	1.791	0.0	0.0
1205.00	1203.52	-572.28	-173.84	16.15	0.0	-635.82	-328.32	0.015	2.913	3.350
1195.00	7848.27	-175.90	173.40	23.73	0.0	-313.36	198.69	0.654	1.046	0.168
1160.00	2326.05	-575.55	-168.23	16.15	0.0	-635.82	-328.32	0.015	2.763	3.471
1115.00	2319.30	-575.63	-167.75	16.15	0.0	-635.82	-328.32	0.015	2.759	3.482
1070.00	2319.30	-575.63	-167.75	16.15	0.0	-635.82	-328.32	0.015	2.759	3.482
1025.00	1.465e+04	-128.29	99.57	58.25	0.0	-544.49	-95.81	0.601	1.188	0.224
985.00	1.083e+04	-102.23	128.80	58.25	0.0	-542.49	-74.78	0.744	1.130	0.289
945.00	1.083e+04	-102.21	128.80	58.25	0.0	-542.49	-74.78	0.744	1.130	0.289
905.00	6.437e+04	-130.89	142.36	58.25	0.0	-436.66	166.12	0.443	1.017	0.032
855.00	2.344e+04	10.15	277.19	58.25	0.0	-430.77	347.85	0.460	1.438	0.099
805.00	1.496e+04	-105.98	181.79	58.25	0.0	-430.86	314.26	0.449	1.073	0.180
755.00	1.478e+04	-111.83	175.63	58.25	0.0	-430.86	314.26	0.449	1.054	0.189
705.00	1.434e+04	-113.81	161.90	58.25	0.0	-431.46	281.46	0.467	1.028	0.157
655.00	1.389e+04	-115.92	147.28	58.25	0.0	-431.46	281.46	0.467	1.022	0.177
605.00	1.373e+04	-110.92	157.10	58.25	0.0	-431.43	318.26	0.449	1.058	0.210
555.00	1.499e+04	-84.11	147.58	58.25	0.0	-417.55	263.67	0.542	1.003	0.142
535.00	462.89	-284.62	710.53	25.37	0.0	-295.19	710.53	0.049	0.058	0.0
505.00	1.751e+04	-80.04	167.93	58.25	0.0	-417.49	314.16	0.560	0.998	0.187
455.00	1.393e+05	-28.92	228.10	58.25	0.0	-380.74	478.92	0.654	0.963	0.374
404.44	1.813e+04	-50.00	221.17	58.25	0.0	-389.48	517.14	0.548	1.015	0.444
378.89	7112.79	-473.91	-262.63	16.15	0.0	-445.72	-328.72	2.380	0.183	0.414
353.89	2.196e+04	-32.62	456.21	58.25	0.0	-349.91	587.97	0.556	0.867	0.279
303.33	1.928e+04	-91.51	295.05	58.25	0.0	-423.33	593.38	0.329	1.179	0.506
252.78	2.190e+04	-176.89	242.77	58.25	0.0	-426.16	607.02	0.312	0.909	0.621
202.22	1.592e+04	-73.92	284.63	58.25	0.0	-426.16	607.02	0.312	1.284	0.549
151.67	1.601e+04	-65.56	283.49	58.25	0.0	-426.19	571.76	0.342	1.256	0.478
122.00	7167.74	-473.02	-262.23	16.15	0.0	-445.72	-328.72	2.380	0.177	0.416
101.11	1.343e+04	-59.25	403.57	58.25	0.0	-361.56	648.71	0.484	0.885	0.510
88.00	511.85	445.72	710.53	10.71	0.0	459.84	710.53	0.039	0.268	0.0
80.00	1592.11	106.62	-334.97	37.58	0.0	112.14	-334.97	0.080	0.025	0.0
50.56	1.912e+04	-72.11	249.76	58.25	0.0	-425.00	501.84	0.409	1.124	0.402
Risulta	5.465e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	4.866	0.206	0.075	1238.75	0.2	2.719e+04	5.0	1.59e-03	0.0	0.0	0.0
2	4.953	0.202	0.075	1359.25	0.2	1.534e+05	28.1	0.05	9.52e-06	0.0	0.0
3	7.211	0.139	0.075	3.135e+05	57.4	3884.05	0.7	9.18	1.68e-03	0.0	0.0
4	7.657	0.131	0.075	4.807e+04	8.8	9.780e+04	17.9	19.44	3.56e-03	0.0	0.0
5	8.056	0.124	0.075	5115.54	0.9	1969.52	0.4	9.10	1.66e-03	0.0	0.0
6	8.239	0.121	0.075	347.97	6.37e-02	2.846e+04	5.2	1.58	2.89e-04	0.0	0.0
7	9.235	0.108	0.075	4172.92	0.8	145.69	2.67e-02	17.31	3.17e-03	0.0	0.0
8	9.445	0.106	0.075	7750.63	1.4	2.828e+04	5.2	88.49	1.62e-02	0.0	0.0
9	9.740	0.103	0.075	1998.59	0.4	4970.84	0.9	35.75	6.54e-03	0.0	0.0
10	10.324	0.097	0.075	2.745e+04	5.0	812.28	0.1	2.84	5.19e-04	0.0	0.0
11	10.833	0.092	0.075	5049.62	0.9	199.44	3.65e-02	3.03	5.54e-04	0.0	0.0
12	11.554	0.087	0.072	9123.27	1.7	3.848e+04	7.0	0.96	1.75e-04	0.0	0.0
13	12.144	0.082	0.070	861.14	0.2	9787.16	1.8	11.37	2.08e-03	0.0	0.0
14	12.674	0.079	0.068	1.035e+04	1.9	1.419e+04	2.6	1.61	2.94e-04	0.0	0.0
15	13.262	0.075	0.066	4473.95	0.8	789.92	0.1	12.85	2.35e-03	0.0	0.0
16	13.365	0.075	0.066	187.56	3.43e-02	909.95	0.2	52.00	9.52e-03	0.0	0.0
17	14.089	0.071	0.064	7030.54	1.3	323.59	5.92e-02	130.79	2.39e-02	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	Z %	Energia	Energia x v
18	14.204	0.070	0.064	1559.10	0.3	3678.30	0.7	5.90	1.08e-03	0.0	0.0
19	15.016	0.067	0.062	8193.14	1.5	5426.01	1.0	89.77	1.64e-02	0.0	0.0
20	15.065	0.066	0.062	896.77	0.2	2656.27	0.5	26.62	4.87e-03	0.0	0.0
21	15.618	0.064	0.061	3613.52	0.7	3862.02	0.7	62.80	1.15e-02	0.0	0.0
22	16.284	0.061	0.059	3397.29	0.6	121.57	2.22e-02	116.53	2.13e-02	0.0	0.0
23	16.568	0.060	0.059	0.02	3.74e-06	3962.62	0.7	134.25	2.46e-02	0.0	0.0
24	16.852	0.059	0.058	15.83	2.90e-03	2822.65	0.5	7.81e-04	0.0	0.0	0.0
25	17.050	0.059	0.058	41.16	7.53e-03	9897.50	1.8	50.93	9.32e-03	0.0	0.0
26	17.256	0.058	0.058	167.26	3.06e-02	2919.22	0.5	44.67	8.17e-03	0.0	0.0
27	17.679	0.057	0.057	23.61	4.32e-03	3347.60	0.6	0.42	7.77e-05	0.0	0.0
28	18.121	0.055	0.056	1450.82	0.3	538.56	9.85e-02	1540.11	0.3	0.0	0.0
29	19.146	0.052	0.055	1.77	3.24e-04	4048.95	0.7	1397.28	0.3	0.0	0.0
30	19.704	0.051	0.054	67.11	1.23e-02	462.87	8.47e-02	1.362e+04	2.5	0.0	0.0
31	20.012	0.050	0.054	699.58	0.1	4609.05	0.8	1907.61	0.3	0.0	0.0
32	20.198	0.050	0.054	237.87	4.35e-02	266.16	4.87e-02	4945.11	0.9	0.0	0.0
33	20.530	0.049	0.053	4501.72	0.8	303.55	5.55e-02	217.79	3.99e-02	0.0	0.0
34	20.855	0.048	0.053	1791.93	0.3	169.89	3.11e-02	1252.25	0.2	0.0	0.0
35	21.417	0.047	0.052	5852.89	1.1	266.88	4.88e-02	781.09	0.1	0.0	0.0
36	21.745	0.046	0.052	410.70	7.52e-02	698.50	0.1	9279.53	1.7	0.0	0.0
37	22.122	0.045	0.051	7414.14	1.4	385.64	7.06e-02	1239.18	0.2	0.0	0.0
38	22.357	0.045	0.051	88.92	1.63e-02	1399.21	0.3	784.67	0.1	0.0	0.0
39	22.470	0.045	0.051	124.39	2.28e-02	0.16	2.85e-05	1.376e+04	2.5	0.0	0.0
40	22.715	0.044	0.051	101.31	1.85e-02	519.34	9.50e-02	2955.65	0.5	0.0	0.0
41	22.844	0.044	0.051	550.88	0.1	236.74	4.33e-02	2507.25	0.5	0.0	0.0
42	23.347	0.043	0.050	2044.37	0.4	340.61	6.23e-02	7320.79	1.3	0.0	0.0
43	23.559	0.042	0.050	0.19	3.48e-05	658.55	0.1	1.684e+04	3.1	0.0	0.0
44	23.608	0.042	0.050	2558.50	0.5	10.39	1.90e-03	1.025e+04	1.9	0.0	0.0
45	23.984	0.042	0.050	1047.10	0.2	5969.61	1.1	2743.68	0.5	0.0	0.0
46	24.215	0.041	0.049	939.44	0.2	552.43	0.1	155.26	2.84e-02	0.0	0.0
47	24.520	0.041	0.049	135.60	2.48e-02	6.73	1.23e-03	2683.27	0.5	0.0	0.0
48	24.938	0.040	0.049	463.11	8.47e-02	2301.98	0.4	8127.91	1.5	0.0	0.0
49	25.118	0.040	0.049	52.01	9.52e-03	252.64	4.62e-02	1359.47	0.2	0.0	0.0
50	25.564	0.039	0.048	289.37	5.30e-02	4050.74	0.7	1964.48	0.4	0.0	0.0
51	26.011	0.038	0.048	815.58	0.1	109.51	2.00e-02	338.38	6.19e-02	0.0	0.0
52	26.329	0.038	0.048	10.26	1.88e-03	9.31	1.70e-03	9054.70	1.7	0.0	0.0
53	26.885	0.037	0.047	208.98	3.82e-02	500.22	9.15e-02	482.03	8.82e-02	0.0	0.0
54	27.091	0.037	0.047	0.51	9.26e-05	3473.74	0.6	9.563e+04	17.5	0.0	0.0
55	27.212	0.037	0.047	20.10	3.68e-03	1.68	3.07e-04	2.222e+04	4.1	0.0	0.0
56	27.438	0.036	0.047	266.40	4.87e-02	1139.12	0.2	2068.31	0.4	0.0	0.0
57	27.479	0.036	0.047	28.46	5.21e-03	859.39	0.2	6.590e+04	12.1	0.0	0.0
58	27.714	0.036	0.047	2.41	4.42e-04	2223.94	0.4	28.43	5.20e-03	0.0	0.0
59	28.023	0.036	0.047	199.03	3.64e-02	5680.42	1.0	609.51	0.1	0.0	0.0
60	28.863	0.035	0.046	516.85	9.46e-02	76.05	1.39e-02	1323.58	0.2	0.0	0.0
61	29.320	0.034	0.046	62.58	1.15e-02	3276.13	0.6	6467.18	1.2	0.0	0.0
62	29.532	0.034	0.046	99.84	1.83e-02	3307.30	0.6	1390.32	0.3	0.0	0.0
63	29.829	0.034	0.046	35.13	6.43e-03	484.69	8.87e-02	3735.29	0.7	0.0	0.0
64	30.162	0.033	0.045	315.57	5.77e-02	1705.15	0.3	2123.77	0.4	0.0	0.0
65	30.751	0.033	0.045	623.28	0.1	142.62	2.61e-02	1.400e+04	2.6	0.0	0.0
66	30.972	0.032	0.045	42.26	7.73e-03	284.26	5.20e-02	1.520e+04	2.8	0.0	0.0
67	31.129	0.032	0.045	194.17	3.55e-02	986.45	0.2	3311.81	0.6	0.0	0.0
68	31.346	0.032	0.045	832.08	0.2	74.73	1.37e-02	6621.95	1.2	0.0	0.0
69	31.796	0.031	0.045	111.40	2.04e-02	1007.05	0.2	64.53	1.18e-02	0.0	0.0
70	32.367	0.031	0.044	16.21	2.97e-03	8.18	1.50e-03	177.45	3.25e-02	0.0	0.0
71	32.675	0.031	0.044	235.19	4.30e-02	151.98	2.78e-02	6542.47	1.2	0.0	0.0
72	32.873	0.030	0.044	228.91	4.19e-02	5.30	9.69e-04	3210.39	0.6	0.0	0.0
73	33.015	0.030	0.044	89.42	1.64e-02	91.55	1.68e-02	4669.22	0.9	0.0	0.0
74	33.430	0.030	0.044	30.37	5.56e-03	1393.25	0.3	1462.43	0.3	0.0	0.0
75	34.531	0.029	0.043	1629.96	0.3	2.32	4.24e-04	616.95	0.1	0.0	0.0
76	34.587	0.029	0.043	243.98	4.46e-02	1.80	3.29e-04	203.20	3.72e-02	0.0	0.0
77	34.673	0.029	0.043	440.83	8.07e-02	2112.44	0.4	1329.46	0.2	0.0	0.0
78	35.054	0.029	0.043	1833.91	0.3	172.84	3.16e-02	952.09	0.2	0.0	0.0
79	35.114	0.028	0.043	250.42	4.58e-02	1434.84	0.3	1636.69	0.3	0.0	0.0
80	35.422	0.028	0.043	24.57	4.50e-03	254.12	4.65e-02	7.88	1.44e-03	0.0	0.0
81	35.593	0.028	0.043	76.16	1.39e-02	1147.40	0.2	3124.93	0.6	0.0	0.0
82	36.026	0.028	0.043	1.30	2.39e-04	410.73	7.52e-02	263.67	4.82e-02	0.0	0.0
83	36.335	0.028	0.043	52.81	9.66e-03	4.45	8.13e-04	2644.84	0.5	0.0	0.0
84	36.590	0.027	0.043	281.34	5.15e-02	1377.95	0.3	5019.00	0.9	0.0	0.0
85	37.207	0.027	0.042	1.13	2.07e-04	994.84	0.2	3512.49	0.6	0.0	0.0
86	37.386	0.027	0.042	23.03	4.21e-03	40.30	7.38e-03	1117.55	0.2	0.0	0.0
87	37.903	0.026	0.042	451.73	8.27e-02	23.39	4.28e-03	944.30	0.2	0.0	0.0
88	37.974	0.026	0.042	104.40	1.91e-02	23.77	4.35e-03	861.83	0.2	0.0	0.0
89	38.190	0.026	0.042	635.97	0.1	517.64	9.47e-02	1758.48	0.3	0.0	0.0
90	38.338	0.026	0.042	5.25	9.61e-04	272.19	4.98e-02	375.99	6.88e-02	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	Z %	Energia	Energia x v
91	38.844	0.026	0.042	0.45	8.17e-05	699.50	0.1	3751.30	0.7	0.0	0.0
92	39.388	0.025	0.042	224.87	4.11e-02	36.88	6.75e-03	1115.26	0.2	0.0	0.0
93	39.722	0.025	0.042	0.33	5.99e-05	0.93	1.70e-04	902.34	0.2	0.0	0.0
94	40.225	0.025	0.041	1113.02	0.2	610.01	0.1	67.89	1.24e-02	0.0	0.0
95	40.296	0.025	0.041	343.65	6.29e-02	156.29	2.86e-02	904.34	0.2	0.0	0.0
96	40.708	0.025	0.041	872.72	0.2	4.55	8.33e-04	5638.40	1.0	0.0	0.0
97	41.031	0.024	0.041	1029.79	0.2	224.94	4.12e-02	2350.71	0.4	0.0	0.0
98	41.277	0.024	0.041	22.12	4.05e-03	11.22	2.05e-03	2533.93	0.5	0.0	0.0
99	41.495	0.024	0.041	6.02	1.10e-03	110.20	2.02e-02	3772.24	0.7	0.0	0.0
100	41.655	0.024	0.041	119.68	2.19e-02	254.73	4.66e-02	19.55	3.58e-03	0.0	0.0
101	41.828	0.024	0.041	13.73	2.51e-03	9.81	1.79e-03	2968.25	0.5	0.0	0.0
102	42.417	0.024	0.041	143.18	2.62e-02	8.74	1.60e-03	212.84	3.89e-02	0.0	0.0
103	42.751	0.023	0.041	318.25	5.82e-02	105.43	1.93e-02	3350.09	0.6	0.0	0.0
104	42.975	0.023	0.041	63.25	1.16e-02	27.83	5.09e-03	159.18	2.91e-02	0.0	0.0
105	43.306	0.023	0.041	60.45	1.11e-02	63.10	1.15e-02	8.54	1.56e-03	0.0	0.0
106	43.788	0.023	0.040	117.53	2.15e-02	653.95	0.1	19.36	3.54e-03	0.0	0.0
107	44.034	0.023	0.040	115.48	2.11e-02	1.32	2.41e-04	3.69	6.75e-04	0.0	0.0
108	44.252	0.023	0.040	4.70	8.60e-04	35.50	6.50e-03	19.64	3.59e-03	0.0	0.0
109	44.406	0.023	0.040	13.66	2.50e-03	48.32	8.84e-03	2404.25	0.4	0.0	0.0
110	44.852	0.022	0.040	30.62	5.60e-03	576.94	0.1	22.83	4.18e-03	0.0	0.0
111	45.132	0.022	0.040	38.72	7.08e-03	158.89	2.91e-02	106.70	1.95e-02	0.0	0.0
112	45.613	0.022	0.040	9.64	1.76e-03	1.14	2.08e-04	116.50	2.13e-02	0.0	0.0
113	45.688	0.022	0.040	9.36	1.71e-03	81.81	1.50e-02	119.47	2.19e-02	0.0	0.0
114	46.069	0.022	0.040	33.15	6.07e-03	317.99	5.82e-02	123.87	2.27e-02	0.0	0.0
115	46.626	0.021	0.040	0.43	7.83e-05	536.82	9.82e-02	0.40	7.28e-05	0.0	0.0
116	46.892	0.021	0.040	22.65	4.15e-03	172.44	3.16e-02	1998.49	0.4	0.0	0.0
117	47.318	0.021	0.040	58.22	1.07e-02	11.63	2.13e-03	6157.62	1.1	0.0	0.0
118	47.727	0.021	0.039	43.56	7.97e-03	653.24	0.1	1971.34	0.4	0.0	0.0
119	48.002	0.021	0.039	4.24	7.76e-04	283.94	5.20e-02	469.45	8.59e-02	0.0	0.0
120	48.446	0.021	0.039	5.06	9.27e-04	189.53	3.47e-02	2661.37	0.5	0.0	0.0
121	48.882	0.020	0.039	19.71	3.61e-03	114.54	2.10e-02	346.07	6.33e-02	0.0	0.0
122	48.915	0.020	0.039	0.99	1.80e-04	41.00	7.50e-03	736.82	0.1	0.0	0.0
123	49.269	0.020	0.039	61.82	1.13e-02	216.14	3.95e-02	1814.47	0.3	0.0	0.0
124	49.544	0.020	0.039	55.51	1.02e-02	0.45	8.25e-05	591.98	0.1	0.0	0.0
125	49.901	0.020	0.039	81.14	1.48e-02	1.30	2.38e-04	904.40	0.2	0.0	0.0
126	50.180	0.020	0.039	86.28	1.58e-02	99.19	1.82e-02	28.98	5.30e-03	0.0	0.0
127	50.520	0.020	0.039	60.44	1.11e-02	0.44	8.05e-05	615.62	0.1	0.0	0.0
128	50.697	0.020	0.039	11.97	2.19e-03	0.24	4.39e-05	293.59	5.37e-02	0.0	0.0
129	50.974	0.020	0.039	32.21	5.89e-03	64.58	1.18e-02	330.55	6.05e-02	0.0	0.0
130	51.228	0.020	0.039	87.55	1.60e-02	9.63	1.76e-03	137.08	2.51e-02	0.0	0.0
131	51.889	0.019	0.039	319.31	5.84e-02	45.91	8.40e-03	961.60	0.2	0.0	0.0
132	52.052	0.019	0.039	3.89	7.12e-04	145.76	2.67e-02	47.04	8.61e-03	0.0	0.0
133	52.449	0.019	0.039	288.49	5.28e-02	63.37	1.16e-02	1298.61	0.2	0.0	0.0
134	52.668	0.019	0.039	213.49	3.91e-02	0.04	6.89e-06	0.30	5.57e-05	0.0	0.0
135	52.896	0.019	0.038	48.95	8.96e-03	73.60	1.35e-02	6.66	1.22e-03	0.0	0.0
136	53.252	0.019	0.038	17.56	3.21e-03	151.38	2.77e-02	24.08	4.41e-03	0.0	0.0
137	53.608	0.019	0.038	27.66	5.06e-03	349.97	6.40e-02	89.31	1.63e-02	0.0	0.0
138	53.856	0.019	0.038	416.72	7.63e-02	21.52	3.94e-03	339.16	6.21e-02	0.0	0.0
139	54.057	0.018	0.038	306.09	5.60e-02	509.82	9.33e-02	1669.47	0.3	0.0	0.0
140	54.066	0.018	0.038	92.41	1.69e-02	1.97	3.60e-04	762.05	0.1	0.0	0.0
141	54.592	0.018	0.038	1308.14	0.2	27.72	5.07e-03	4.64	8.50e-04	0.0	0.0
142	54.839	0.018	0.038	444.42	8.13e-02	14.16	2.59e-03	30.96	5.66e-03	0.0	0.0
143	55.047	0.018	0.038	950.84	0.2	44.41	8.13e-03	160.37	2.93e-02	0.0	0.0
144	55.468	0.018	0.038	88.31	1.62e-02	8.78	1.61e-03	1368.26	0.3	0.0	0.0
145	55.738	0.018	0.038	181.24	3.32e-02	219.93	4.02e-02	243.87	4.46e-02	0.0	0.0
146	55.761	0.018	0.038	508.33	9.30e-02	69.10	1.26e-02	5.33	9.76e-04	0.0	0.0
147	56.133	0.018	0.038	144.17	2.64e-02	61.61	1.13e-02	347.35	6.36e-02	0.0	0.0
148	56.647	0.018	0.038	246.52	4.51e-02	0.78	1.43e-04	1131.99	0.2	0.0	0.0
149	56.925	0.018	0.038	38.02	6.96e-03	11.35	2.08e-03	39.89	7.30e-03	0.0	0.0
150	57.019	0.018	0.038	38.97	7.13e-03	19.94	3.65e-03	1.05e-03	0.0	0.0	0.0
151	57.476	0.017	0.038	28.25	5.17e-03	57.50	1.05e-02	134.56	2.46e-02	0.0	0.0
152	57.875	0.017	0.038	8.75	1.60e-03	1.38	2.52e-04	34.58	6.33e-03	0.0	0.0
153	58.065	0.017	0.038	207.64	3.80e-02	1.49	2.72e-04	208.06	3.81e-02	0.0	0.0
154	58.146	0.017	0.038	64.87	1.19e-02	1.67	3.05e-04	37.83	6.92e-03	0.0	0.0
155	58.361	0.017	0.038	46.65	8.54e-03	2.75	5.04e-04	123.13	2.25e-02	0.0	0.0
156	58.997	0.017	0.038	27.45	5.02e-03	263.27	4.82e-02	27.55	5.04e-03	0.0	0.0
157	59.284	0.017	0.037	104.62	1.91e-02	691.50	0.1	0.05	8.78e-06	0.0	0.0
158	59.364	0.017	0.037	311.13	5.69e-02	0.05	8.23e-06	72.21	1.32e-02	0.0	0.0
159	59.936	0.017	0.037	139.80	2.56e-02	1149.26	0.2	35.71	6.53e-03	0.0	0.0
160	60.070	0.017	0.037	26.40	4.83e-03	11.63	2.13e-03	27.83	5.09e-03	0.0	0.0
161	60.458	0.017	0.037	132.08	2.42e-02	27.44	5.02e-03	12.83	2.35e-03	0.0	0.0
162	60.684	0.016	0.037	54.75	1.00e-02	7.11	1.30e-03	151.80	2.78e-02	0.0	0.0
163	60.836	0.016	0.037	208.50	3.82e-02	83.96	1.54e-02	44.28	8.10e-03	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
164	60.981	0.016	0.037	248.26	4.54e-02	58.23	1.07e-02	5.98	1.09e-03	0.0	0.0
165	61.332	0.016	0.037	165.40	3.03e-02	8.40	1.54e-03	17.28	3.16e-03	0.0	0.0
166	61.405	0.016	0.037	384.56	7.04e-02	688.36	0.1	378.45	6.93e-02	0.0	0.0
167	61.742	0.016	0.037	56.89	1.04e-02	347.15	6.35e-02	28.75	5.26e-03	0.0	0.0
168	61.886	0.016	0.037	5.67	1.04e-03	461.36	8.44e-02	512.57	9.38e-02	0.0	0.0
169	62.070	0.016	0.037	55.07	1.01e-02	13.05	2.39e-03	28.43	5.20e-03	0.0	0.0
170	62.523	0.016	0.037	210.13	3.84e-02	72.69	1.33e-02	864.96	0.2	0.0	0.0
171	62.751	0.016	0.037	29.64	5.42e-03	6.74	1.23e-03	194.47	3.56e-02	0.0	0.0
172	62.761	0.016	0.037	3.05	5.58e-04	188.01	3.44e-02	2.30	4.21e-04	0.0	0.0
173	63.032	0.016	0.037	11.02	2.02e-03	291.31	5.33e-02	6.20	1.13e-03	0.0	0.0
174	63.146	0.016	0.037	0.37	6.86e-05	2.76	5.05e-04	680.31	0.1	0.0	0.0
175	63.466	0.016	0.037	113.98	2.09e-02	7.14	1.31e-03	13.35	2.44e-03	0.0	0.0
176	63.885	0.016	0.037	309.02	5.65e-02	115.34	2.11e-02	4.80	8.79e-04	0.0	0.0
177	64.206	0.016	0.037	35.48	6.49e-03	14.88	2.72e-03	26.91	4.92e-03	0.0	0.0
178	64.533	0.015	0.037	27.24	4.98e-03	17.68	3.24e-03	0.93	1.69e-04	0.0	0.0
179	64.748	0.015	0.037	0.02	2.94e-06	72.98	1.34e-02	32.04	5.86e-03	0.0	0.0
180	64.970	0.015	0.037	374.43	6.85e-02	0.84	1.53e-04	5.86	1.07e-03	0.0	0.0
181	65.036	0.015	0.037	151.73	2.78e-02	41.88	7.66e-03	119.38	2.18e-02	0.0	0.0
182	65.302	0.015	0.037	19.46	3.56e-03	11.60	2.12e-03	2.41	4.40e-04	0.0	0.0
183	65.446	0.015	0.037	186.74	3.42e-02	3.49	6.39e-04	133.57	2.44e-02	0.0	0.0
184	65.724	0.015	0.037	48.68	8.91e-03	305.18	5.58e-02	162.73	2.98e-02	0.0	0.0
185	65.841	0.015	0.037	70.74	1.29e-02	0.48	8.78e-05	190.77	3.49e-02	0.0	0.0
186	66.105	0.015	0.037	0.05	9.51e-06	112.78	2.06e-02	349.22	6.39e-02	0.0	0.0
187	66.380	0.015	0.037	23.21	4.25e-03	11.19	2.05e-03	458.18	8.38e-02	0.0	0.0
188	66.606	0.015	0.037	261.60	4.79e-02	36.05	6.60e-03	248.83	4.55e-02	0.0	0.0
189	66.663	0.015	0.037	427.07	7.81e-02	0.02	3.26e-06	7.57	1.39e-03	0.0	0.0
190	66.720	0.015	0.037	17.72	3.24e-03	7.68	1.41e-03	5772.67	1.1	0.0	0.0
191	67.118	0.015	0.036	75.43	1.38e-02	6.79	1.24e-03	442.61	8.10e-02	0.0	0.0
192	67.338	0.015	0.036	7.64	1.40e-03	57.56	1.05e-02	5.07	9.28e-04	0.0	0.0
193	67.559	0.015	0.036	18.79	3.44e-03	89.66	1.64e-02	317.00	5.80e-02	0.0	0.0
194	67.886	0.015	0.036	5.05	9.25e-04	92.62	1.69e-02	526.55	9.64e-02	0.0	0.0
195	68.199	0.015	0.036	4.55	8.33e-04	287.53	5.26e-02	22.14	4.05e-03	0.0	0.0
196	68.275	0.015	0.036	192.57	3.52e-02	42.55	7.79e-03	464.88	8.51e-02	0.0	0.0
197	68.524	0.015	0.036	30.92	5.66e-03	51.50	9.42e-03	325.60	5.96e-02	0.0	0.0
198	68.817	0.015	0.036	121.91	2.23e-02	16.04	2.94e-03	228.92	4.19e-02	0.0	0.0
199	69.112	0.014	0.036	98.18	1.80e-02	22.69	4.15e-03	47.69	8.73e-03	0.0	0.0
200	69.261	0.014	0.036	77.90	1.43e-02	0.11	2.01e-05	8.17	1.49e-03	0.0	0.0
201	69.378	0.014	0.036	27.83	5.09e-03	78.98	1.45e-02	218.09	3.99e-02	0.0	0.0
202	69.711	0.014	0.036	256.44	4.69e-02	0.20	3.62e-05	184.66	3.38e-02	0.0	0.0
203	70.130	0.014	0.036	32.25	5.90e-03	13.49	2.47e-03	33.01	6.04e-03	0.0	0.0
204	70.279	0.014	0.036	63.42	1.16e-02	18.65	3.41e-03	159.03	2.91e-02	0.0	0.0
205	70.421	0.014	0.036	45.24	8.28e-03	287.79	5.27e-02	189.17	3.46e-02	0.0	0.0
206	70.610	0.014	0.036	88.79	1.62e-02	206.96	3.79e-02	25.77	4.72e-03	0.0	0.0
207	70.993	0.014	0.036	2.15	3.94e-04	163.88	3.00e-02	62.18	1.14e-02	0.0	0.0
208	71.287	0.014	0.036	21.95	4.02e-03	18.12	3.32e-03	44.40	8.12e-03	0.0	0.0
209	71.663	0.014	0.036	15.14	2.77e-03	22.89	4.19e-03	28.95	5.30e-03	0.0	0.0
210	71.804	0.014	0.036	98.03	1.79e-02	0.98	1.80e-04	153.66	2.81e-02	0.0	0.0
211	72.043	0.014	0.036	8.34	1.53e-03	19.66	3.60e-03	161.33	2.95e-02	0.0	0.0
212	72.323	0.014	0.036	32.49	5.95e-03	23.80	4.35e-03	730.57	0.1	0.0	0.0
213	72.543	0.014	0.036	4.03	7.38e-04	105.92	1.94e-02	75.37	1.38e-02	0.0	0.0
214	72.686	0.014	0.036	46.02	8.42e-03	2.31	4.22e-04	150.43	2.75e-02	0.0	0.0
215	73.269	0.014	0.036	3.60	6.58e-04	16.74	3.06e-03	1280.58	0.2	0.0	0.0
216	73.529	0.014	0.036	0.89	1.63e-04	0.11	1.94e-05	226.77	4.15e-02	0.0	0.0
217	73.692	0.014	0.036	2.22	4.07e-04	21.09	3.86e-03	6.76	1.24e-03	0.0	0.0
218	73.981	0.014	0.036	53.85	9.85e-03	162.67	2.98e-02	45.51	8.33e-03	0.0	0.0
219	74.144	0.013	0.036	34.74	6.36e-03	15.73	2.88e-03	18.42	3.37e-03	0.0	0.0
220	74.169	0.013	0.036	24.17	4.42e-03	57.97	1.06e-02	4.19	7.67e-04	0.0	0.0
Risulta				5.250e+05		5.297e+05		4.752e+05			
In percentuale				96.06		96.92		86.95			

CDC	Tipo	Sigla Id	Note
14	Edk	CDC=Ed (dinamico SLD) alfa=90.00 (ecc. -)	
			verifica esistenti: fattore FC 1.200
			categoria suolo: B
			fattore di sito S = 1.200
			ordinata spettro (tratto Tb-Tc) = 0.075 g
			angolo di ingresso:90.00
			eccentricità aggiuntiva: negativa

CDC	Tipo	Sigla Id	Note
			periodo proprio T1: 0.123 sec.
			numero di modi considerati:220
			combinaz. modale: CQC

Quota	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	(r/Ls)^2	rapp. ex/rx	rapp. ey/ry
cm	daN	cm	cm	cm	cm	cm	cm			
1340.00	96.19	-491.36	-334.97	-5.50	0.0	-491.36	-334.97	0.155	0.0	0.0
1295.00	116.44	-491.36	-334.97	-5.50	0.0	-491.36	-334.97	1.791	0.0	0.0
1250.00	101.25	-491.36	-334.97	-5.50	0.0	-491.36	-334.97	1.791	0.0	0.0
1205.00	1203.52	-572.28	-173.84	-16.15	0.0	-635.82	-328.32	0.015	2.913	3.350
1195.00	7848.27	-175.90	173.40	-23.73	0.0	-313.36	198.69	0.654	1.046	0.168
1160.00	2326.05	-575.55	-168.23	-16.15	0.0	-635.82	-328.32	0.015	2.763	3.471
1115.00	2319.30	-575.63	-167.75	-16.15	0.0	-635.82	-328.32	0.015	2.759	3.482
1070.00	2319.30	-575.63	-167.75	-16.15	0.0	-635.82	-328.32	0.015	2.759	3.482
1025.00	1.465e+04	-128.29	99.57	-58.25	0.0	-544.49	-95.81	0.601	1.188	0.224
985.00	1.083e+04	-102.23	128.80	-58.25	0.0	-542.49	-74.78	0.744	1.130	0.289
945.00	1.083e+04	-102.21	128.80	-58.25	0.0	-542.49	-74.78	0.744	1.130	0.289
905.00	6.437e+04	-130.89	142.36	-58.25	0.0	-436.66	166.12	0.443	1.017	0.032
855.00	2.344e+04	10.15	277.19	-58.25	0.0	-430.77	347.85	0.460	1.438	0.099
805.00	1.496e+04	-105.98	181.79	-58.25	0.0	-430.86	314.26	0.449	1.073	0.180
755.00	1.478e+04	-111.83	175.63	-58.25	0.0	-430.86	314.26	0.449	1.054	0.189
705.00	1.434e+04	-113.81	161.90	-58.25	0.0	-431.46	281.46	0.467	1.028	0.157
655.00	1.389e+04	-115.92	147.28	-58.25	0.0	-431.46	281.46	0.467	1.022	0.177
605.00	1.373e+04	-110.92	157.10	-58.25	0.0	-431.43	318.26	0.449	1.058	0.210
555.00	1.499e+04	-84.11	147.58	-58.25	0.0	-417.55	263.67	0.542	1.003	0.142
535.00	462.89	-284.62	710.53	-25.37	0.0	-295.19	710.53	0.049	0.058	0.0
505.00	1.751e+04	-80.04	167.93	-58.25	0.0	-417.49	314.16	0.560	0.998	0.187
455.00	1.393e+05	-28.92	228.10	-58.25	0.0	-380.74	478.92	0.654	0.963	0.374
404.44	1.813e+04	-50.00	221.17	-58.25	0.0	-389.48	517.14	0.548	1.015	0.444
378.89	7112.79	-473.91	-262.63	-16.15	0.0	-445.72	-328.72	2.380	0.183	0.414
353.89	2.196e+04	-32.62	456.21	-58.25	0.0	-349.91	587.97	0.556	0.867	0.279
303.33	1.928e+04	-91.51	295.05	-58.25	0.0	-423.33	593.38	0.329	1.179	0.506
252.78	2.190e+04	-176.89	242.77	-58.25	0.0	-426.16	607.02	0.312	0.909	0.621
202.22	1.592e+04	-73.92	284.63	-58.25	0.0	-426.16	607.02	0.312	1.284	0.549
151.67	1.601e+04	-65.56	283.49	-58.25	0.0	-426.19	571.76	0.342	1.256	0.478
122.00	7167.74	-473.02	-262.23	-16.15	0.0	-445.72	-328.72	2.380	0.177	0.416
101.11	1.343e+04	-59.25	403.57	-58.25	0.0	-361.56	648.71	0.484	0.885	0.510
88.00	511.85	445.72	710.53	-10.71	0.0	459.84	710.53	0.039	0.268	0.0
80.00	1592.11	106.62	-334.97	-37.58	0.0	112.14	-334.97	0.080	0.025	0.0
50.56	1.912e+04	-72.11	249.76	-58.25	0.0	-425.00	501.84	0.409	1.124	0.402
Risulta	5.465e+05									

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
	Hz	sec	g	daN		daN		daN			
1	5.214	0.192	0.075	1511.92	0.3	4.078e+04	7.5	0.02	3.02e-06	0.0	0.0
2	5.330	0.188	0.075	1986.83	0.4	1.203e+05	22.0	0.04	7.87e-06	0.0	0.0
3	7.254	0.138	0.075	3.596e+05	65.8	5395.80	1.0	14.30	2.62e-03	0.0	0.0
4	8.143	0.123	0.075	227.12	4.16e-02	1.322e+05	24.2	15.56	2.85e-03	0.0	0.0
5	8.499	0.118	0.075	236.53	4.33e-02	3.355e+04	6.1	20.49	3.75e-03	0.0	0.0
6	8.986	0.111	0.075	6161.51	1.1	7925.58	1.5	6.00	1.10e-03	0.0	0.0
7	9.495	0.105	0.075	9085.14	1.7	1.202e+04	2.2	76.31	1.40e-02	0.0	0.0
8	9.600	0.104	0.075	7133.28	1.3	151.99	2.78e-02	33.89	6.20e-03	0.0	0.0
9	9.854	0.101	0.075	1384.67	0.3	1317.19	0.2	16.29	2.98e-03	0.0	0.0
10	10.483	0.095	0.075	3.190e+04	5.8	1.479e+04	2.7	0.05	9.32e-06	0.0	0.0
11	11.056	0.090	0.074	503.86	9.22e-02	7530.03	1.4	11.72	2.14e-03	0.0	0.0
12	11.995	0.083	0.070	1421.06	0.3	3.435e+04	6.3	0.30	5.44e-05	0.0	0.0
13	12.456	0.080	0.069	4327.94	0.8	6135.98	1.1	12.77	2.34e-03	0.0	0.0
14	12.773	0.078	0.068	1.142e+04	2.1	2038.03	0.4	2.30	4.21e-04	0.0	0.0
15	13.553	0.074	0.065	1248.42	0.2	3730.88	0.7	46.01	8.42e-03	0.0	0.0
16	13.609	0.073	0.065	8963.33	1.6	95.53	1.75e-02	43.98	8.05e-03	0.0	0.0
17	14.190	0.070	0.064	8699.83	1.6	391.46	7.16e-02	4.77	8.73e-04	0.0	0.0
18	15.004	0.067	0.062	232.39	4.25e-02	4659.84	0.9	92.39	1.69e-02	0.0	0.0
19	15.499	0.065	0.061	1443.99	0.3	5809.69	1.1	28.92	5.29e-03	0.0	0.0
20	15.859	0.063	0.060	11.92	2.18e-03	20.69	3.79e-03	0.22	4.00e-05	0.0	0.0
21	16.068	0.062	0.060	5853.25	1.1	5.47	1.00e-03	171.76	3.14e-02	0.0	0.0
22	16.251	0.062	0.059	48.06	8.79e-03	2742.10	0.5	85.67	1.57e-02	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	%	Energia	Energia x v
23	16.313	0.061	0.059	2718.08	0.5	52.67	9.64e-03	32.19	5.89e-03	0.0	0.0
24	16.789	0.060	0.058	462.40	8.46e-02	2887.46	0.5	46.27	8.47e-03	0.0	0.0
25	17.837	0.056	0.057	5.71	1.05e-03	164.57	3.01e-02	195.08	3.57e-02	0.0	0.0
26	18.085	0.055	0.056	357.66	6.54e-02	1.161e+04	2.1	7.21	1.32e-03	0.0	0.0
27	18.614	0.054	0.056	261.01	4.78e-02	519.15	9.50e-02	3938.30	0.7	0.0	0.0
28	19.323	0.052	0.055	186.18	3.41e-02	46.80	8.56e-03	6127.53	1.1	0.0	0.0
29	19.521	0.051	0.054	115.48	2.11e-02	4167.72	0.8	30.26	5.54e-03	0.0	0.0
30	20.147	0.050	0.054	50.29	9.20e-03	12.36	2.26e-03	4637.47	0.8	0.0	0.0
31	20.463	0.049	0.053	2809.28	0.5	68.69	1.26e-02	9693.43	1.8	0.0	0.0
32	20.755	0.048	0.053	309.21	5.66e-02	268.83	4.92e-02	726.21	0.1	0.0	0.0
33	20.951	0.048	0.053	3433.44	0.6	285.04	5.22e-02	3859.66	0.7	0.0	0.0
34	21.229	0.047	0.052	3262.09	0.6	3185.25	0.6	1221.47	0.2	0.0	0.0
35	21.768	0.046	0.052	6895.13	1.3	371.97	6.81e-02	7870.68	1.4	0.0	0.0
36	22.177	0.045	0.051	5126.64	0.9	39.22	7.18e-03	155.22	2.84e-02	0.0	0.0
37	22.423	0.045	0.051	84.36	1.54e-02	33.35	6.10e-03	1.123e+04	2.1	0.0	0.0
38	22.459	0.045	0.051	602.89	0.1	617.79	0.1	853.81	0.2	0.0	0.0
39	22.784	0.044	0.051	16.85	3.08e-03	678.61	0.1	2391.98	0.4	0.0	0.0
40	23.093	0.043	0.050	399.81	7.32e-02	1571.94	0.3	7564.03	1.4	0.0	0.0
41	23.502	0.043	0.050	1210.75	0.2	1990.52	0.4	435.48	7.97e-02	0.0	0.0
42	23.618	0.042	0.050	1781.74	0.3	2285.59	0.4	2.478e+04	4.5	0.0	0.0
43	24.009	0.042	0.050	169.71	3.11e-02	177.90	3.26e-02	567.66	0.1	0.0	0.0
44	24.540	0.041	0.049	412.80	7.55e-02	3238.30	0.6	3581.33	0.7	0.0	0.0
45	24.727	0.040	0.049	72.71	1.33e-02	4729.94	0.9	1.339e+04	2.4	0.0	0.0
46	24.884	0.040	0.049	1381.76	0.3	789.42	0.1	442.86	8.10e-02	0.0	0.0
47	24.970	0.040	0.049	52.63	9.63e-03	340.84	6.24e-02	216.04	3.95e-02	0.0	0.0
48	25.556	0.039	0.048	1417.63	0.3	1685.01	0.3	8406.92	1.5	0.0	0.0
49	25.875	0.039	0.048	820.94	0.2	2348.18	0.4	1.768e+04	3.2	0.0	0.0
50	26.506	0.038	0.048	143.16	2.62e-02	261.21	4.78e-02	4169.06	0.8	0.0	0.0
51	26.830	0.037	0.048	0.04	6.99e-06	1207.55	0.2	2.004e+04	3.7	0.0	0.0
52	27.127	0.037	0.047	0.23	4.20e-05	4527.02	0.8	1.315e+04	2.4	0.0	0.0
53	27.302	0.037	0.047	104.92	1.92e-02	3871.22	0.7	9.957e+04	18.2	0.0	0.0
54	27.491	0.036	0.047	217.18	3.97e-02	2497.99	0.5	269.79	4.94e-02	0.0	0.0
55	27.838	0.036	0.047	630.68	0.1	1098.85	0.2	2.494e+04	4.6	0.0	0.0
56	27.983	0.036	0.047	103.24	1.89e-02	3740.38	0.7	4888.87	0.9	0.0	0.0
57	28.236	0.035	0.047	6.92	1.27e-03	27.19	4.98e-03	0.03	5.21e-06	0.0	0.0
58	28.485	0.035	0.046	3.59	6.58e-04	866.50	0.2	5019.26	0.9	0.0	0.0
59	29.036	0.034	0.046	288.98	5.29e-02	1169.93	0.2	479.31	8.77e-02	0.0	0.0
60	29.185	0.034	0.046	20.61	3.77e-03	1734.49	0.3	1546.00	0.3	0.0	0.0
61	29.649	0.034	0.046	7.86e-03	1.44e-06	267.51	4.89e-02	152.14	2.78e-02	0.0	0.0
62	29.866	0.033	0.046	25.84	4.73e-03	1708.14	0.3	1241.40	0.2	0.0	0.0
63	30.522	0.033	0.045	790.99	0.1	67.48	1.23e-02	3.065e+04	5.6	0.0	0.0
64	30.692	0.033	0.045	187.32	3.43e-02	589.68	0.1	1.514e+04	2.8	0.0	0.0
65	31.061	0.032	0.045	416.57	7.62e-02	4.77	8.72e-04	1.266e+04	2.3	0.0	0.0
66	31.591	0.032	0.045	326.80	5.98e-02	433.22	7.93e-02	777.82	0.1	0.0	0.0
67	31.818	0.031	0.045	179.32	3.28e-02	0.03	4.92e-06	17.90	3.28e-03	0.0	0.0
68	32.293	0.031	0.044	2.91	5.33e-04	1481.14	0.3	1869.75	0.3	0.0	0.0
69	32.933	0.030	0.044	109.46	2.00e-02	4.25	7.78e-04	2301.14	0.4	0.0	0.0
70	33.330	0.030	0.044	16.74	3.06e-03	1333.85	0.2	1041.97	0.2	0.0	0.0
71	33.614	0.030	0.044	1314.25	0.2	45.25	8.28e-03	0.06	1.15e-05	0.0	0.0
72	33.709	0.030	0.044	8.22	1.50e-03	372.73	6.82e-02	5292.72	1.0	0.0	0.0
73	34.479	0.029	0.043	301.20	5.51e-02	41.49	7.59e-03	1111.07	0.2	0.0	0.0
74	34.594	0.029	0.043	207.99	3.81e-02	1.92	3.51e-04	11.05	2.02e-03	0.0	0.0
75	34.842	0.029	0.043	26.54	4.86e-03	196.98	3.60e-02	862.94	0.2	0.0	0.0
76	35.134	0.028	0.043	1578.89	0.3	564.57	0.1	397.64	7.28e-02	0.0	0.0
77	35.542	0.028	0.043	752.59	0.1	13.23	2.42e-03	18.67	3.42e-03	0.0	0.0
78	35.736	0.028	0.043	8.61e-03	1.57e-06	266.39	4.87e-02	483.78	8.85e-02	0.0	0.0
79	35.824	0.028	0.043	68.81	1.26e-02	1734.26	0.3	3918.27	0.7	0.0	0.0
80	36.194	0.028	0.043	929.84	0.2	315.51	5.77e-02	346.10	6.33e-02	0.0	0.0
81	36.407	0.027	0.043	329.15	6.02e-02	758.85	0.1	7368.08	1.3	0.0	0.0
82	36.804	0.027	0.043	19.97	3.65e-03	73.76	1.35e-02	4388.42	0.8	0.0	0.0
83	37.374	0.027	0.042	384.18	7.03e-02	407.79	7.46e-02	236.00	4.32e-02	0.0	0.0
84	37.668	0.027	0.042	14.74	2.70e-03	16.75	3.07e-03	792.66	0.1	0.0	0.0
85	37.749	0.026	0.042	2.28	4.17e-04	3.67	6.72e-04	675.54	0.1	0.0	0.0
86	38.215	0.026	0.042	876.07	0.2	10.37	1.90e-03	1516.70	0.3	0.0	0.0
87	38.360	0.026	0.042	143.58	2.63e-02	1862.15	0.3	185.06	3.39e-02	0.0	0.0
88	38.916	0.026	0.042	666.26	0.1	37.03	6.78e-03	3826.63	0.7	0.0	0.0
89	39.119	0.026	0.042	29.23	5.35e-03	39.77	7.28e-03	675.10	0.1	0.0	0.0
90	39.335	0.025	0.042	66.62	1.22e-02	322.99	5.91e-02	5.49	1.00e-03	0.0	0.0
91	39.491	0.025	0.042	7.30	1.34e-03	80.68	1.48e-02	288.57	5.28e-02	0.0	0.0
92	39.608	0.025	0.042	60.78	1.11e-02	145.02	2.65e-02	850.44	0.2	0.0	0.0
93	39.776	0.025	0.042	0.51	9.35e-05	480.73	8.80e-02	645.31	0.1	0.0	0.0
94	40.168	0.025	0.041	113.32	2.07e-02	292.29	5.35e-02	475.16	8.69e-02	0.0	0.0
95	40.427	0.025	0.041	534.23	9.78e-02	192.99	3.53e-02	1172.74	0.2	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	Z %	Energia	Energia x v
96	40.610	0.025	0.041	151.26	2.77e-02	11.30	2.07e-03	405.02	7.41e-02	0.0	0.0
97	40.790	0.025	0.041	1150.36	0.2	201.51	3.69e-02	414.04	7.58e-02	0.0	0.0
98	41.167	0.024	0.041	637.26	0.1	107.95	1.98e-02	3230.57	0.6	0.0	0.0
99	41.437	0.024	0.041	19.27	3.53e-03	35.37	6.47e-03	6730.13	1.2	0.0	0.0
100	42.094	0.024	0.041	127.00	2.32e-02	977.34	0.2	1717.91	0.3	0.0	0.0
101	42.348	0.024	0.041	2.53	4.62e-04	299.80	5.49e-02	2644.61	0.5	0.0	0.0
102	42.500	0.024	0.041	48.69	8.91e-03	77.70	1.42e-02	3455.30	0.6	0.0	0.0
103	43.069	0.023	0.041	41.90	7.67e-03	121.06	2.22e-02	2446.50	0.4	0.0	0.0
104	43.767	0.023	0.040	209.79	3.84e-02	8.17	1.49e-03	142.91	2.62e-02	0.0	0.0
105	43.919	0.023	0.040	0.10	1.76e-05	15.68	2.87e-03	370.67	6.78e-02	0.0	0.0
106	44.268	0.023	0.040	78.07	1.43e-02	105.17	1.92e-02	1201.31	0.2	0.0	0.0
107	44.726	0.022	0.040	26.27	4.81e-03	292.67	5.36e-02	125.69	2.30e-02	0.0	0.0
108	45.071	0.022	0.040	15.02	2.75e-03	260.95	4.77e-02	96.85	1.77e-02	0.0	0.0
109	45.513	0.022	0.040	77.18	1.41e-02	70.11	1.28e-02	807.28	0.1	0.0	0.0
110	45.735	0.022	0.040	9.27	1.70e-03	50.23	9.19e-03	7.70	1.41e-03	0.0	0.0
111	45.797	0.022	0.040	34.52	6.32e-03	115.93	2.12e-02	310.59	5.68e-02	0.0	0.0
112	46.437	0.022	0.040	40.12	7.34e-03	387.72	7.09e-02	1.40	2.55e-04	0.0	0.0
113	46.997	0.021	0.040	6.71	1.23e-03	131.38	2.40e-02	5426.56	1.0	0.0	0.0
114	47.144	0.021	0.040	26.15	4.78e-03	12.17	2.23e-03	8.72	1.60e-03	0.0	0.0
115	47.599	0.021	0.040	64.21	1.18e-02	65.63	1.20e-02	1172.69	0.2	0.0	0.0
116	47.679	0.021	0.039	9.99	1.83e-03	12.42	2.27e-03	1044.33	0.2	0.0	0.0
117	47.875	0.021	0.039	21.81	3.99e-03	109.41	2.00e-02	5406.28	1.0	0.0	0.0
118	48.636	0.021	0.039	87.52	1.60e-02	74.54	1.36e-02	663.19	0.1	0.0	0.0
119	48.822	0.020	0.039	6.90	1.26e-03	55.72	1.02e-02	1.02	1.87e-04	0.0	0.0
120	49.045	0.020	0.039	2.86	5.23e-04	89.99	1.65e-02	300.73	5.50e-02	0.0	0.0
121	49.238	0.020	0.039	5.11	9.36e-04	6.32	1.16e-03	2645.18	0.5	0.0	0.0
122	49.483	0.020	0.039	29.24	5.35e-03	205.62	3.76e-02	52.52	9.61e-03	0.0	0.0
123	49.598	0.020	0.039	45.88	8.39e-03	134.23	2.46e-02	448.05	8.20e-02	0.0	0.0
124	49.772	0.020	0.039	119.11	2.18e-02	81.45	1.49e-02	995.88	0.2	0.0	0.0
125	50.252	0.020	0.039	66.62	1.22e-02	0.34	6.21e-05	60.80	1.11e-02	0.0	0.0
126	50.632	0.020	0.039	77.47	1.42e-02	269.80	4.94e-02	110.52	2.02e-02	0.0	0.0
127	50.907	0.020	0.039	54.06	9.89e-03	96.02	1.76e-02	6.87	1.26e-03	0.0	0.0
128	51.082	0.020	0.039	0.03	5.76e-06	246.90	4.52e-02	1591.81	0.3	0.0	0.0
129	51.835	0.019	0.039	436.42	7.99e-02	20.59	3.77e-03	835.15	0.2	0.0	0.0
130	51.896	0.019	0.039	56.98	1.04e-02	8.53	1.56e-03	438.92	8.03e-02	0.0	0.0
131	52.215	0.019	0.039	328.07	6.00e-02	25.01	4.58e-03	153.33	2.81e-02	0.0	0.0
132	52.608	0.019	0.039	234.07	4.28e-02	10.48	1.92e-03	267.37	4.89e-02	0.0	0.0
133	53.215	0.019	0.038	234.95	4.30e-02	1.27	2.32e-04	29.42	5.38e-03	0.0	0.0
134	53.503	0.019	0.038	232.05	4.25e-02	612.46	0.1	269.87	4.94e-02	0.0	0.0
135	53.662	0.019	0.038	2.69	4.92e-04	37.64	6.89e-03	1444.57	0.3	0.0	0.0
136	53.915	0.019	0.038	39.29	7.19e-03	233.44	4.27e-02	4.76e-03	0.0	0.0	0.0
137	54.033	0.019	0.038	824.22	0.2	260.90	4.77e-02	92.49	1.69e-02	0.0	0.0
138	54.353	0.018	0.038	0.41	7.45e-05	25.99	4.76e-03	463.78	8.49e-02	0.0	0.0
139	54.855	0.018	0.038	66.54	1.22e-02	453.69	8.30e-02	343.90	6.29e-02	0.0	0.0
140	55.118	0.018	0.038	1601.08	0.3	211.08	3.86e-02	265.21	4.85e-02	0.0	0.0
141	55.197	0.018	0.038	26.76	4.90e-03	122.82	2.25e-02	609.29	0.1	0.0	0.0
142	55.305	0.018	0.038	558.45	0.1	105.46	1.93e-02	674.02	0.1	0.0	0.0
143	55.921	0.018	0.038	589.21	0.1	0.06	1.01e-05	97.87	1.79e-02	0.0	0.0
144	56.142	0.018	0.038	49.72	9.10e-03	61.76	1.13e-02	889.70	0.2	0.0	0.0
145	56.658	0.018	0.038	112.74	2.06e-02	57.41	1.05e-02	45.45	8.32e-03	0.0	0.0
146	56.798	0.018	0.038	341.78	6.25e-02	2.86	5.23e-04	190.02	3.48e-02	0.0	0.0
147	57.118	0.018	0.038	9.49	1.74e-03	527.87	9.66e-02	31.32	5.73e-03	0.0	0.0
148	57.339	0.017	0.038	127.84	2.34e-02	72.77	1.33e-02	205.29	3.76e-02	0.0	0.0
149	57.486	0.017	0.038	367.28	6.72e-02	0.08	1.46e-05	196.44	3.59e-02	0.0	0.0
150	57.799	0.017	0.038	21.93	4.01e-03	3.66e-03	0.0	175.35	3.21e-02	0.0	0.0
151	58.024	0.017	0.038	47.34	8.66e-03	194.45	3.56e-02	33.71	6.17e-03	0.0	0.0
152	58.189	0.017	0.038	33.86	6.20e-03	0.38	6.98e-05	166.44	3.05e-02	0.0	0.0
153	58.503	0.017	0.038	57.01	1.04e-02	58.70	1.07e-02	0.48	8.75e-05	0.0	0.0
154	58.724	0.017	0.038	73.22	1.34e-02	98.74	1.81e-02	13.67	2.50e-03	0.0	0.0
155	58.950	0.017	0.038	31.97	5.85e-03	0.94	1.73e-04	0.03	4.60e-06	0.0	0.0
156	59.230	0.017	0.037	33.58	6.14e-03	189.55	3.47e-02	120.02	2.20e-02	0.0	0.0
157	59.384	0.017	0.037	111.30	2.04e-02	172.34	3.15e-02	0.79	1.44e-04	0.0	0.0
158	59.615	0.017	0.037	132.60	2.43e-02	132.70	2.43e-02	176.62	3.23e-02	0.0	0.0
159	59.813	0.017	0.037	7.01	1.28e-03	58.46	1.07e-02	108.66	1.99e-02	0.0	0.0
160	60.260	0.017	0.037	235.37	4.31e-02	4.40	8.06e-04	6.55	1.20e-03	0.0	0.0
161	60.331	0.017	0.037	0.33	6.00e-05	66.07	1.21e-02	5.80	1.06e-03	0.0	0.0
162	60.700	0.016	0.037	229.95	4.21e-02	229.14	4.19e-02	158.27	2.90e-02	0.0	0.0
163	60.842	0.016	0.037	275.24	5.04e-02	12.06	2.21e-03	10.32	1.89e-03	0.0	0.0
164	61.518	0.016	0.037	16.66	3.05e-03	212.25	3.88e-02	157.23	2.88e-02	0.0	0.0
165	61.680	0.016	0.037	144.30	2.64e-02	58.62	1.07e-02	15.08	2.76e-03	0.0	0.0
166	61.855	0.016	0.037	12.03	2.20e-03	14.82	2.71e-03	0.67	1.22e-04	0.0	0.0
167	62.289	0.016	0.037	112.71	2.06e-02	181.91	3.33e-02	338.21	6.19e-02	0.0	0.0
168	62.483	0.016	0.037	2.33	4.27e-04	178.68	3.27e-02	2.60	4.76e-04	0.0	0.0

Modo	Frequenza	Periodo	Acc. Spettrale	M efficace X x g	%	M efficace Y x g	%	M efficace Z x g	Z %	Energia	Energia x v
169	62.520	0.016	0.037	94.99	1.74e-02	15.61	2.86e-03	48.45	8.87e-03	0.0	0.0
170	62.873	0.016	0.037	21.35	3.91e-03	36.57	6.69e-03	923.43	0.2	0.0	0.0
171	63.124	0.016	0.037	331.34	6.06e-02	28.80	5.27e-03	175.36	3.21e-02	0.0	0.0
172	63.344	0.016	0.037	233.03	4.26e-02	54.66	1.00e-02	119.45	2.19e-02	0.0	0.0
173	63.465	0.016	0.037	73.34	1.34e-02	12.23	2.24e-03	92.14	1.69e-02	0.0	0.0
174	63.640	0.016	0.037	8.04	1.47e-03	5.79	1.06e-03	85.48	1.56e-02	0.0	0.0
175	64.037	0.016	0.037	100.93	1.85e-02	134.54	2.46e-02	307.15	5.62e-02	0.0	0.0
176	64.179	0.016	0.037	19.50	3.57e-03	99.85	1.83e-02	322.57	5.90e-02	0.0	0.0
177	64.400	0.016	0.037	92.98	1.70e-02	30.86	5.65e-03	22.57	4.13e-03	0.0	0.0
178	64.637	0.015	0.037	337.92	6.18e-02	4.04	7.39e-04	582.65	0.1	0.0	0.0
179	65.095	0.015	0.037	33.86	6.20e-03	26.43	4.84e-03	72.12	1.32e-02	0.0	0.0
180	65.290	0.015	0.037	10.43	1.91e-03	22.87	4.19e-03	97.38	1.78e-02	0.0	0.0
181	65.565	0.015	0.037	48.14	8.81e-03	464.45	8.50e-02	91.08	1.67e-02	0.0	0.0
182	65.599	0.015	0.037	29.70	5.44e-03	146.72	2.68e-02	7.31	1.34e-03	0.0	0.0
183	66.059	0.015	0.037	585.80	0.1	109.09	2.00e-02	1148.37	0.2	0.0	0.0
184	66.332	0.015	0.037	26.48	4.84e-03	210.64	3.85e-02	6.38	1.17e-03	0.0	0.0
185	66.449	0.015	0.037	136.14	2.49e-02	359.90	6.59e-02	104.58	1.91e-02	0.0	0.0
186	66.616	0.015	0.037	81.71	1.50e-02	371.20	6.79e-02	160.24	2.93e-02	0.0	0.0
187	66.753	0.015	0.037	6.10	1.12e-03	12.51	2.29e-03	4902.49	0.9	0.0	0.0
188	66.879	0.015	0.037	152.87	2.80e-02	32.85	6.01e-03	1023.19	0.2	0.0	0.0
189	67.067	0.015	0.036	63.59	1.16e-02	1.17	2.15e-04	45.44	8.31e-03	0.0	0.0
190	67.447	0.015	0.036	33.55	6.14e-03	8.89	1.63e-03	7.59	1.39e-03	0.0	0.0
191	67.585	0.015	0.036	474.26	8.68e-02	393.64	7.20e-02	485.16	8.88e-02	0.0	0.0
192	68.100	0.015	0.036	93.63	1.71e-02	178.85	3.27e-02	11.83	2.16e-03	0.0	0.0
193	68.320	0.015	0.036	86.28	1.58e-02	0.87	1.60e-04	629.37	0.1	0.0	0.0
194	68.366	0.015	0.036	1.92	3.51e-04	9.16	1.68e-03	0.44	8.09e-05	0.0	0.0
195	68.829	0.015	0.036	1.11	2.04e-04	145.44	2.66e-02	715.23	0.1	0.0	0.0
196	69.053	0.014	0.036	0.42	7.64e-05	451.27	8.26e-02	477.81	8.74e-02	0.0	0.0
197	69.717	0.014	0.036	49.26	9.01e-03	27.19	4.98e-03	151.21	2.77e-02	0.0	0.0
198	70.179	0.014	0.036	2.70	4.94e-04	144.07	2.64e-02	221.00	4.04e-02	0.0	0.0
199	70.356	0.014	0.036	9.55	1.75e-03	22.98	4.21e-03	200.49	3.67e-02	0.0	0.0
200	70.938	0.014	0.036	100.16	1.83e-02	256.47	4.69e-02	70.03	1.28e-02	0.0	0.0
201	71.192	0.014	0.036	0.34	6.20e-05	10.23	1.87e-03	199.29	3.65e-02	0.0	0.0
202	71.292	0.014	0.036	22.61	4.14e-03	74.62	1.37e-02	96.16	1.76e-02	0.0	0.0
203	71.456	0.014	0.036	16.79	3.07e-03	241.75	4.42e-02	88.55	1.62e-02	0.0	0.0
204	71.630	0.014	0.036	0.49	9.03e-05	1.29	2.35e-04	5.13	9.39e-04	0.0	0.0
205	71.733	0.014	0.036	45.74	8.37e-03	4.53	8.28e-04	0.12	2.13e-05	0.0	0.0
206	72.123	0.014	0.036	310.73	5.69e-02	58.87	1.08e-02	27.31	5.00e-03	0.0	0.0
207	72.522	0.014	0.036	9.44	1.73e-03	109.94	2.01e-02	2.45	4.49e-04	0.0	0.0
208	72.704	0.014	0.036	0.04	7.74e-06	34.69	6.35e-03	153.83	2.81e-02	0.0	0.0
209	72.825	0.014	0.036	3.72	6.80e-04	35.00	6.41e-03	677.18	0.1	0.0	0.0
210	73.133	0.014	0.036	29.64	5.42e-03	2.07	3.80e-04	8.43	1.54e-03	0.0	0.0
211	73.307	0.014	0.036	52.62	9.63e-03	0.14	2.62e-05	343.06	6.28e-02	0.0	0.0
212	73.369	0.014	0.036	0.49	8.90e-05	0.79	1.44e-04	1239.24	0.2	0.0	0.0
213	73.550	0.014	0.036	0.18	3.28e-05	48.30	8.84e-03	48.45	8.87e-03	0.0	0.0
214	73.650	0.014	0.036	109.34	2.00e-02	289.38	5.30e-02	43.47	7.95e-03	0.0	0.0
215	73.842	0.014	0.036	11.82	2.16e-03	34.04	6.23e-03	70.27	1.29e-02	0.0	0.0
216	74.191	0.013	0.036	147.12	2.69e-02	38.77	7.09e-03	0.32	5.90e-05	0.0	0.0
217	74.728	0.013	0.036	6.37	1.16e-03	93.26	1.71e-02	16.11	2.95e-03	0.0	0.0
218	74.984	0.013	0.036	43.36	7.93e-03	0.20	3.57e-05	184.24	3.37e-02	0.0	0.0
219	75.000	0.013	0.036	43.88	8.03e-03	109.90	2.01e-02	509.23	9.32e-02	0.0	0.0
220	75.332	0.013	0.036	22.74	4.16e-03	5.64	1.03e-03	11.40	2.09e-03	0.0	0.0
Risulta				5.251e+05		5.298e+05		4.763e+05			
In percentuale				96.09		96.94		87.16			

Cmb	Pilas. 1000 etaT/h	etaT cm	inter. h cm	Pilas. 1000 etaT/h	etaT cm	inter. h cm	Pilas. 1000 etaT/h	etaT cm	inter. h cm
43	293	0.031.58e-03	50.0	295	0.041.99e-03	50.6	296	0.063.07e-03	50.6
	297	0.042.13e-03	50.6	298	0.126.19e-03	50.6	338	0.042.11e-03	50.6
	339	0.041.96e-03	50.6	340	0.031.68e-03	50.6	341	0.031.39e-03	50.6
	342	0.031.39e-03	50.6	343	0.09 0.03	290.0	344	0.013.34e-03	290.0
44	293	0.052.66e-03	50.0	295	0.052.39e-03	50.6	296	0.052.54e-03	50.6
	297	0.094.73e-03	50.6	298	0.126.30e-03	50.6	338	0.031.61e-03	50.6
	339	0.031.53e-03	50.6	340	0.031.40e-03	50.6	341	0.031.38e-03	50.6
	342	0.031.69e-03	50.6	343	0.05 0.02	290.0	344	0.037.27e-03	290.0
45	293	0.052.52e-03	50.0	295	0.021.02e-03	50.6	296	0.031.48e-03	50.6
	297	0.073.52e-03	50.6	298	0.125.98e-03	50.6	338	0.115.43e-03	50.6
	339	0.105.11e-03	50.6	340	0.094.48e-03	50.6	341	0.073.55e-03	50.6
	342	0.052.34e-03	50.6	343	0.10 0.03	290.0	344	0.17 0.05	290.0

46	293	0.042.01e-03	50.0	295	0.017.09e-04	50.6	296	0.031.70e-03	50.6
	297	0.073.68e-03	50.6	298	0.126.02e-03	50.6	338	0.094.72e-03	50.6
	339	0.094.42e-03	50.6	340	0.083.83e-03	50.6	341	0.062.95e-03	50.6
	342	0.041.82e-03	50.6	343	0.05 0.01	290.0	344	0.12 0.04	290.0
47	293	0.031.58e-03	50.0	295	0.042.09e-03	50.6	296	0.063.13e-03	50.6
	297	0.042.09e-03	50.6	298	0.126.24e-03	50.6	338	0.052.29e-03	50.6
	339	0.042.15e-03	50.6	340	0.041.87e-03	50.6	341	0.031.58e-03	50.6
	342	0.031.55e-03	50.6	343	0.09 0.03	290.0	344	9.53e-032.76e-03	290.0
48	293	0.052.63e-03	50.0	295	0.052.30e-03	50.6	296	0.073.37e-03	50.6
	297	0.094.68e-03	50.6	298	0.126.25e-03	50.6	338	0.031.42e-03	50.6
	339	0.031.33e-03	50.6	340	0.021.20e-03	50.6	341	0.021.21e-03	50.6
	342	0.031.58e-03	50.6	343	0.06 0.02	290.0	344	0.027.23e-03	290.0
49	293	0.052.49e-03	50.0	295	0.029.28e-04	50.6	296	0.031.35e-03	50.6
	297	0.073.46e-03	50.6	298	0.125.96e-03	50.6	338	0.115.51e-03	50.6
	339	0.105.18e-03	50.6	340	0.094.54e-03	50.6	341	0.073.59e-03	50.6
	342	0.052.35e-03	50.6	343	0.10 0.03	290.0	344	0.17 0.05	290.0
50	293	0.041.99e-03	50.0	295	0.028.71e-04	50.6	296	0.041.81e-03	50.6
	297	0.073.74e-03	50.6	298	0.126.05e-03	50.6	338	0.094.66e-03	50.6
	339	0.094.36e-03	50.6	340	0.073.78e-03	50.6	341	0.062.93e-03	50.6
	342	0.041.84e-03	50.6	343	0.05 0.01	290.0	344	0.12 0.04	290.0
51	293	0.041.79e-03	50.0	295	0.042.04e-03	50.6	296	0.063.06e-03	50.6
	297	0.073.56e-03	50.6	298	0.126.19e-03	50.6	338	0.052.50e-03	50.6
	339	0.052.34e-03	50.6	340	0.042.05e-03	50.6	341	0.031.72e-03	50.6
	342	0.031.60e-03	50.6	343	0.11 0.03	290.0	344	0.025.62e-03	290.0
52	293	0.052.72e-03	50.0	295	0.052.41e-03	50.6	296	0.062.79e-03	50.6
	297	0.094.71e-03	50.6	298	0.126.31e-03	50.6	338	0.042.00e-03	50.6
	339	0.041.90e-03	50.6	340	0.031.74e-03	50.6	341	0.031.64e-03	50.6
	342	0.041.81e-03	50.6	343	0.06 0.02	290.0	344	0.024.95e-03	290.0
53	293	0.052.61e-03	50.0	295	0.021.12e-03	50.6	296	0.031.74e-03	50.6
	297	0.073.69e-03	50.6	298	0.126.08e-03	50.6	338	0.105.19e-03	50.6
	339	0.104.88e-03	50.6	340	0.084.27e-03	50.6	341	0.073.37e-03	50.6
	342	0.042.23e-03	50.6	343	0.09 0.03	290.0	344	0.17 0.05	290.0
54	293	0.042.22e-03	50.0	295	0.029.13e-04	50.6	296	0.041.94e-03	50.6
	297	0.083.84e-03	50.6	298	0.126.11e-03	50.6	338	0.094.48e-03	50.6
	339	0.084.19e-03	50.6	340	0.073.62e-03	50.6	341	0.052.78e-03	50.6
	342	0.031.73e-03	50.6	343	0.05 0.02	290.0	344	0.12 0.03	290.0
55	293	0.041.78e-03	50.0	295	0.042.16e-03	50.6	296	0.063.13e-03	50.6
	297	0.094.53e-03	50.6	298	0.126.00e-03	50.6	338	0.052.68e-03	50.6
	339	0.052.53e-03	50.6	340	0.042.24e-03	50.6	341	0.041.91e-03	50.6
	342	0.041.77e-03	50.6	343	0.11 0.03	290.0	344	0.026.41e-03	290.0
56	293	0.052.69e-03	50.0	295	0.052.32e-03	50.6	296	0.042.02e-03	50.6
	297	0.094.66e-03	50.6	298	0.126.25e-03	50.6	338	0.041.80e-03	50.6
	339	0.031.70e-03	50.6	340	0.031.54e-03	50.6	341	0.031.45e-03	50.6
	342	0.031.67e-03	50.6	343	0.07 0.02	290.0	344	0.024.89e-03	290.0
57	293	0.052.59e-03	50.0	295	0.029.88e-04	50.6	296	0.031.61e-03	50.6
	297	0.073.62e-03	50.6	298	0.126.05e-03	50.6	338	0.105.25e-03	50.6
	339	0.104.94e-03	50.6	340	0.094.31e-03	50.6	341	0.073.40e-03	50.6
	342	0.042.21e-03	50.6	343	0.09 0.03	290.0	344	0.17 0.05	290.0
58	293	0.042.20e-03	50.0	295	0.021.09e-03	50.6	296	0.042.06e-03	50.6
	297	0.083.91e-03	50.6	298	0.126.15e-03	50.6	338	0.094.43e-03	50.6
	339	0.084.15e-03	50.6	340	0.073.59e-03	50.6	341	0.052.77e-03	50.6
	342	0.041.78e-03	50.6	343	0.05 0.01	290.0	344	0.11 0.03	290.0
59	293	0.083.84e-03	50.0	295	0.015.32e-04	50.6	296	0.041.88e-03	50.6
	297	0.073.74e-03	50.6	298	0.125.91e-03	50.6	338	0.083.89e-03	50.6
	339	0.073.62e-03	50.6	340	0.063.08e-03	50.6	341	0.052.28e-03	50.6
	342	0.021.26e-03	50.6	343	0.17 0.05	290.0	344	0.11 0.03	290.0
60	293	0.094.69e-03	50.0	295	0.041.85e-03	50.6	296	0.042.07e-03	50.6
	297	0.094.49e-03	50.6	298	0.126.20e-03	50.6	338	0.031.62e-03	50.6
	339	0.031.45e-03	50.6	340	0.021.12e-03	50.6	341	0.028.07e-04	50.6
	342	0.021.01e-03	50.6	343	0.08 0.02	290.0	344	0.039.08e-03	290.0
61	293	0.094.28e-03	50.0	295	9.01e-034.56e-04	50.6	296	0.031.38e-03	50.6
	297	0.073.47e-03	50.6	298	0.125.87e-03	50.6	338	0.104.95e-03	50.6
	339	0.094.64e-03	50.6	340	0.084.04e-03	50.6	341	0.063.13e-03	50.6
	342	0.041.93e-03	50.6	343	0.13 0.04	290.0	344	0.18 0.05	290.0
62	293	0.094.32e-03	50.0	295	0.021.03e-03	50.6	296	0.052.43e-03	50.6
	297	0.084.15e-03	50.6	298	0.104.82e-03	50.6	338	0.052.58e-03	50.6
	339	0.052.34e-03	50.6	340	0.041.86e-03	50.6	341	0.021.15e-03	50.6
	342	5.33e-032.70e-04	50.6	343	0.06 0.02	290.0	344	0.013.90e-03	290.0
63	293	0.083.87e-03	50.0	295	0.015.83e-04	50.6	296	0.041.86e-03	50.6
	297	0.073.72e-03	50.6	298	0.125.90e-03	50.6	338	0.083.98e-03	50.6
	339	0.073.71e-03	50.6	340	0.063.17e-03	50.6	341	0.052.38e-03	50.6
	342	0.031.35e-03	50.6	343	0.18 0.05	290.0	344	0.11 0.03	290.0
64	293	0.094.68e-03	50.0	295	0.041.84e-03	50.6	296	0.063.02e-03	50.6
	297	0.094.48e-03	50.6	298	0.126.19e-03	50.6	338	0.031.73e-03	50.6
	339	0.031.56e-03	50.6	340	0.021.24e-03	50.6	341	0.029.03e-04	50.6
	342	0.021.03e-03	50.6	343	0.07 0.02	290.0	344	0.038.38e-03	290.0
65	293	0.094.27e-03	50.0	295	8.61e-034.35e-04	50.6	296	0.031.44e-03	50.6

66	297	0.073.51e-03	50.6	298	0.125.90e-03	50.6	338	0.104.87e-03	50.6
	339	0.094.56e-03	50.6	340	0.083.96e-03	50.6	341	0.063.06e-03	50.6
	342	0.041.87e-03	50.6	343	0.12 0.04	290.0	344	0.18 0.05	290.0
	293	0.094.36e-03	50.0	295	0.021.08e-03	50.6	296	0.052.50e-03	50.6
67	297	0.084.16e-03	50.6	298	0.126.02e-03	50.6	338	0.052.49e-03	50.6
	339	0.042.25e-03	50.6	340	0.041.78e-03	50.6	341	0.021.07e-03	50.6
	342	3.36e-031.70e-04	50.6	343	0.07 0.02	290.0	344	0.013.22e-03	290.0
	293	0.073.73e-03	50.0	295	0.021.10e-03	50.6	296	0.042.02e-03	50.6
68	297	0.083.82e-03	50.6	298	0.126.00e-03	50.6	338	0.094.30e-03	50.6
	339	0.084.03e-03	50.6	340	0.073.50e-03	50.6	341	0.052.71e-03	50.6
	342	0.031.75e-03	50.6	343	0.17 0.05	290.0	344	0.12 0.03	290.0
	293	0.094.58e-03	50.0	295	0.041.82e-03	50.6	296	0.052.53e-03	50.6
69	297	0.094.46e-03	50.6	298	0.126.12e-03	50.6	338	0.021.18e-03	50.6
	339	0.029.83e-04	50.6	340	0.015.98e-04	50.6	341	3.33e-031.68e-04	50.6
	342	0.028.27e-04	50.6	343	0.08 0.02	290.0	344	0.03 0.01	290.0
	293	0.084.17e-03	50.0	295	0.016.43e-04	50.6	296	0.031.32e-03	50.6
70	297	0.073.43e-03	50.6	298	0.125.88e-03	50.6	338	0.105.28e-03	50.6
	339	0.104.97e-03	50.6	340	0.094.34e-03	50.6	341	0.073.41e-03	50.6
	342	0.042.19e-03	50.6	343	0.13 0.04	290.0	344	0.18 0.05	290.0
	293	0.084.21e-03	50.0	295	0.021.23e-03	50.6	296	0.052.58e-03	50.6
71	297	0.029.79e-04	50.6	298	0.126.09e-03	50.6	338	0.052.33e-03	50.6
	339	0.042.10e-03	50.6	340	0.031.65e-03	50.6	341	0.029.94e-04	50.6
	342	8.05e-034.07e-04	50.6	343	0.06 0.02	290.0	344	0.024.94e-03	290.0
	293	0.083.76e-03	50.0	295	0.021.17e-03	50.6	296	0.042.03e-03	50.6
72	297	0.083.81e-03	50.6	298	0.125.99e-03	50.6	338	0.094.40e-03	50.6
	339	0.084.13e-03	50.6	340	0.073.60e-03	50.6	341	0.062.81e-03	50.6
	342	0.041.85e-03	50.6	343	0.17 0.05	290.0	344	0.12 0.04	290.0
	293	0.094.56e-03	50.0	295	0.041.77e-03	50.6	296	0.031.56e-03	50.6
73	297	0.094.43e-03	50.6	298	0.126.11e-03	50.6	338	0.031.27e-03	50.6
	339	0.021.07e-03	50.6	340	0.016.88e-04	50.6	341	5.02e-032.54e-04	50.6
	342	0.027.87e-04	50.6	343	0.07 0.02	290.0	344	0.039.39e-03	290.0
	293	0.084.15e-03	50.0	295	0.016.49e-04	50.6	296	0.021.26e-03	50.6
74	297	0.073.46e-03	50.6	298	0.125.89e-03	50.6	338	0.105.19e-03	50.6
	339	0.104.88e-03	50.6	340	0.084.25e-03	50.6	341	0.073.33e-03	50.6
	342	0.042.11e-03	50.6	343	0.13 0.04	290.0	344	0.18 0.05	290.0
	293	0.084.24e-03	50.0	295	0.031.31e-03	50.6	296	0.052.64e-03	50.6
	297	3.58e-031.81e-04	50.6	298	0.126.11e-03	50.6	338	0.042.26e-03	50.6
	339	0.042.04e-03	50.6	340	0.031.59e-03	50.6	341	0.029.65e-04	50.6
	342	9.66e-034.88e-04	50.6	343	0.07 0.02	290.0	344	0.024.44e-03	290.0
Cmb	1000 etaT/h	0.18							

VERIFICHE ELEMENTI MURATURA

LEGENDA TABELLA VERIFICHE ELEMENTI MURATURA

In tabella vengono riportati per ogni elemento il numero dello stesso ed il codice di verifica.

Le verifiche sono state condotte secondo il DM.LL.PP. 20 Novembre 1987.

In particolare sono previste le seguenti verifiche:

- 2.2.1 Muri soggetti a carichi verticali
- 2.4.1 Verifiche di sicurezza con il metodo delle tensioni ammissibili
 - 2.4.1.1 Verifica dei muri soggetti a carichi verticali
 - 2.4.1.2 Verifica dei muri soggetti a forze orizzontali agenti nel piano del muro
 - 2.4.1.2.1 Verifica a pressoflessione
 - 2.4.1.2.2 Verifica a taglio
- 2.4.2 Verifiche di sicurezza con il metodo semiprobabilistico agli stati limite
 - 2.4.2.2 Verifica dei muri soggetti a carichi verticali
 - 2.4.2.3 Verifica dei muri soggetti a forze orizzontali agenti nel piano del muro
 - 2.4.2.3.1 Verifica a pressoflessione
 - 2.4.2.3.2 Verifica a taglio

Con riferimento ai punti succitati le verifiche vengono così tabellate:

Setto/Fascia/Elem.	numero del macroelemento (D3) o elemento (D2) considerato	
Mat.	Materiale	
s=,m=	Indice della sezione e del materiale assegnati all' elemento (per D2)	
Spessore	spessore dell'elemento	
Stato	ok T	elemento verificato (tensioni ammissibili)
	ok L	elemento verificato (stati limite ultimi)
	NV T	elemento non verificato (tensioni ammissibili)
	NV L	elemento non verificato (stati limite ultimi)

Nodo/Pos.	numero del nodo appartenente al setto / posizione relativa al nodo I per D2		
h0/t	valore della snellezza		
Ecc/t (M)	massimo valore del rapporto e1/t o e2/t		
6 Eb/B (M)	massimo valore dell'eccentricità Eb dei carichi verticali misurata nel piano mediano amplificata del fattore 6/B		
Fi	fattore fi per la riduzione della resistenza in funzione di h0 ed EccM; utilizzato nella verifica V.N-Mo		
Fi t	fattore fi per la riduzione della resistenza in funzione di e2 e h0; utilizzato nella verifica V.N-Mp		
Fi b	fattore fi per la riduzione della resistenza in funzione di 6Eb/B; utilizzato nella verifica V.N-Mp		
Beta	fattore di parzializzazione della sezione per la verifica a taglio		
V.N-Mo	rapporto tra la tensione (sforzo normale) e la tensione ammissibile (sforzo normale ultimo) in relazione alla verifica 2.4.1.1. (2.4.2.2)		
V.N-Mp	rapporto tra la tensione (sforzo normale) e la tensione ammissibile (sforzo normale ultimo) in relazione alla verifica 2.4.1.2.1 (2.4.2.3.1)		
Ver. V	rapporto tra la tensione tangenziale (sforzo tagliante) e la tensione tangenziale ammissibile (sforzo tagliante ultimo) in relazione alla verifica 2.4.1.2.2 (2.4.2.3.2)		
Rif. cmb	Combinazioni in cui si hanno i massimi valori dei rapporti V. N-Mo	V. N-Mp	Ver. V

Affinché l'elemento sia verificato deve essere:

h0/t	non superiore a 20
Ecc/t (M)	non superiore a 0.33
6 Eb/B (M)	non superiore a 1.33 con il metodo delle tensioni ammissibili
6 Eb/B (M)	non superiore a 2.00 con il metodo agli stati limite
V.N-Mo, V.N-Mp, Ver. V	non superiore a 1

Le verifiche sismiche condotte secondo le norme tecniche allegate all' ordinanza PCM 3274 prevedono gli ulteriori controlli:

- 8.2.2.1 Pressoflessione nel piano
- 8.2.2.2 Taglio (edifici nuovi)
- 11.5.8.1 Taglio (edifici esistenti)
- 8.2.2.3 Pressoflessione fuori piano

Con riferimento ai punti succitati le verifiche vengono così tabellate:

Nodo/Pos.	numero del nodo appartenente al setto / posizione relativa al nodo I per D2		
P / A	tensione verticale media (in uso nella verifica 8.2.2.1 e 11.5.8.1)		
P / Ac	tensione verticale media nella parte compressa (in uso nella verifica 8.2.2.2)		
P / A .3	tensione verticale corrispondente allo sforzo normale unitario da equilibrare con 0.85 fd (in uso nella verifica 8.2.2.3)		
Mu	valore del momento corrispondente al collasso per pressoflessione (in uso nella verifica 8.2.2.1)		
lc	dimensione della parte compressa della parete (in uso nella verifica 8.2.2.2)		
b (h/l)	rapporto dimensionale (altezza/base) (in uso nella verifica 11.5.8.1)		
tc	dimensione (al massimo pari allo spessore) reagente (in uso nella verifica 8.2.2.3)		
V. 8.2.2.1	massimo valore del rapporto tra il momento di progetto ed il momento ultimo calcolato in presenza dello sforzo normale di progetto		
V. 8.2.2.2	massimo valore del rapporto tra la forza orizzontale di progetto e la forza orizzontale Vt corrispondente al collasso per taglio (edifici nuovi)		

V. 11.5.8.1	massimo valore del rapporto tra la forza orizzontale di progetto e la forza orizzontale V_t corrispondente al collasso per taglio (edifici esistenti)
V. 8.2.2.3	massimo valore del rapporto tra il momento di progetto ed il momento ultimo calcolato in presenza dello sforzo normale di progetto
Rif. cmb	Combinazioni in cui si hanno i massimi valori dei rapporti V. 8.2.2.1, V. 8.2.2.2, V. 8.2.2.3

Affinché l'elemento sia verificato deve essere:

h_0/t	non superiore a 12 (10)
V.8.2.2.1(2,3) V.11.5.8.1	non superiore a 1

Le verifiche condotte per gli elementi trave in muratura sono così tabellate:

Ver. V	rapporto tra il taglio di progetto e il minore dei tagli resistenti V_p e V_t in relazione alla verifica 5.4.6.2.5
Ver. M	rapporto tra il momento di progetto e il momento ultimo M_u in relazione alla verifica 5.4.6.2.5
V_t	taglio resistente, funzione della resistenza della muratura al taglio in assenza di compressione
V_p	taglio resistente in funzione del momento resistente M_u
M_u	momento resistente, funzione della resistenza della muratura alla compressione in direzione orizzontale

Elem. cmb	Note	Pos.	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l) cm	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif.
343	ok L	0.0	1.83	1.83	1.93	5.529e+04	40.00	2.33	0.17	0.02	0.23	31,31,31
	s=14,m=34	290.0	1.31	1.31	1.45	4.016e+04	40.00	1.74	1.78e-03	0.02	4.36e-04	31,31,31
344	ok L	0.0	1.73	1.73	1.61	8.194e+04	50.00	1.94	0.19	0.02	0.11	29,29,29
	s=15,m=34	290.0	1.21	1.21	1.21	5.815e+04	50.00	1.46	5.00e-04	0.02	1.08e-03	29,29,29
Elem.			P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
						4.016e+04	40.00	1.46				
			1.83	1.83	1.93	8.194e+04	50.00	2.33	0.19	0.02	0.23	

Setto	Mat.	Spessore	Stato
		cm	
3	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
1920	1.35	1.26	1.35	2.015e+05	87.50	1.09	0.38	0.11	0.14	27,13,27
1921	1.35	1.26	1.35	2.015e+05	87.50	1.09	0.38	0.11	0.14	27,13,27
1929	1.35	1.26	1.35	2.015e+05	87.50	1.09	0.38	0.11	0.14	27,13,27
1930	1.35	1.26	1.35	2.015e+05	87.50	1.09	0.38	0.11	0.14	27,13,27
1938	1.35	1.26	1.35	2.015e+05	87.50	1.09	0.38	0.11	0.14	27,13,27
1939	1.35	1.26	1.35	2.015e+05	87.50	1.09	0.38	0.11	0.14	27,13,27
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	1.35	1.26	1.35	2.015e+05	87.50	1.09				
				2.015e+05	87.50	1.09	0.38	0.11	0.14	

Setto	Mat.	Spessore	Stato
		cm	
6	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
36	2.52	2.24	2.22	1.340e+07	536.00	2.57	0.04	0.06	0.03	37,16,11
37	2.52	2.24	2.22	1.340e+07	536.00	2.57	0.04	0.06	0.03	37,16,11
77	2.52	2.24	2.22	1.340e+07	536.00	2.57	0.04	0.06	0.03	37,16,11
84	2.52	2.24	2.22	1.340e+07	536.00	2.57	0.04	0.06	0.03	37,16,11
91	2.52	2.24	2.22	1.340e+07	536.00	2.57	0.04	0.06	0.03	37,16,11
98	2.52	2.24	2.22	1.340e+07	536.00	2.57	0.04	0.06	0.03	37,16,11
105	2.52	2.24	2.22	1.340e+07	536.00	2.57	0.04	0.06	0.03	37,16,11
112	2.52	2.24	2.22	1.340e+07	536.00	2.57	0.04	0.06	0.03	37,16,11
119	2.52	2.24	2.22	1.340e+07	536.00	2.57	0.04	0.06	0.03	37,16,11
126	2.52	2.24	2.22	1.340e+07	536.00	2.57	0.04	0.06	0.03	37,16,11
133	2.52	2.24	2.22	1.340e+07	536.00	2.57	0.04	0.06	0.03	37,16,11

1103	2.49	2.24	2.21	1.329e+07	536.00	2.56	0.05	0.06	0.06	37,16,11
1105	2.38	2.22	2.21	1.274e+07	536.00	2.56	0.08	0.06	0.06	37,16,11
1107	2.28	2.07	2.14	1.225e+07	536.00	2.48	0.09	0.07	0.04	37,16,16
1109	2.28	2.03	2.03	1.225e+07	536.00	2.35	0.09	0.07	0.03	37,16,16
1111	2.20	1.93	2.03	1.185e+07	536.00	2.35	0.09	0.07	0.03	37,16,16
1113	2.06	1.93	2.20	1.111e+07	536.00	2.54	0.09	0.07	0.03	37,16,14
1115	2.01	1.87	1.86	7.843e+06	455.60	2.15	0.09	0.07	0.02	37,16,11
1169	2.43	2.24	2.17	1.299e+07	536.00	2.51	0.06	0.06	0.04	37,16,11
1170	2.43	2.24	2.17	1.299e+07	536.00	2.51	0.06	0.06	0.04	37,16,11
1171	2.32	2.19	2.17	1.244e+07	536.00	2.51	0.08	0.06	0.04	37,16,11
1172	2.32	2.19	2.17	1.244e+07	536.00	2.51	0.08	0.06	0.04	37,16,11
1173	2.28	2.07	2.10	1.225e+07	536.00	2.43	0.09	0.07	0.03	37,16,16
1174	2.28	2.07	2.10	1.225e+07	536.00	2.43	0.09	0.07	0.03	37,16,16
1175	2.28	2.03	2.03	1.225e+07	536.00	2.35	0.09	0.07	0.03	37,16,16
1176	2.28	2.03	2.03	1.225e+07	536.00	2.35	0.09	0.07	0.03	37,16,16
1177	2.20	1.93	2.03	1.185e+07	536.00	2.35	0.09	0.07	0.03	37,16,16
1178	2.20	1.93	2.03	1.185e+07	536.00	2.35	0.09	0.07	0.03	37,16,16
1179	2.06	1.93	2.20	1.111e+07	536.00	2.54	0.09	0.07	0.03	37,16,14
1180	2.06	1.93	2.20	1.111e+07	536.00	2.54	0.09	0.07	0.03	37,16,14
1187	2.43	2.24	2.19	1.299e+07	536.00	2.53	0.06	0.06	0.05	37,16,11
1188	2.32	2.21	2.19	1.244e+07	536.00	2.53	0.08	0.06	0.05	37,16,11
1189	2.28	2.07	2.12	1.225e+07	536.00	2.45	0.09	0.07	0.03	37,16,16
1190	2.28	2.03	2.03	1.225e+07	536.00	2.35	0.09	0.07	0.03	37,16,16
1191	2.20	1.93	2.03	1.185e+07	536.00	2.35	0.09	0.07	0.03	37,16,16
1192	2.06	1.93	2.20	1.111e+07	536.00	2.54	0.09	0.07	0.03	37,16,14
1196	2.46	2.24	2.21	1.314e+07	536.00	2.56	0.05	0.06	0.06	37,16,11
1197	2.35	2.22	2.21	1.259e+07	536.00	2.56	0.08	0.06	0.06	37,16,11
1198	2.28	2.07	2.14	1.225e+07	536.00	2.48	0.09	0.07	0.04	37,16,16
1199	2.28	2.03	2.03	1.225e+07	536.00	2.35	0.09	0.07	0.03	37,16,16
1200	2.20	1.93	2.03	1.185e+07	536.00	2.35	0.09	0.07	0.03	37,16,16
1201	2.06	1.93	2.20	1.111e+07	536.00	2.54	0.09	0.07	0.03	37,16,14
1202	2.01	1.87	1.86	7.843e+06	455.60	2.15	0.09	0.07	0.02	37,16,11
1205	2.49	2.24	2.21	1.329e+07	536.00	2.56	0.05	0.06	0.06	37,16,11
1206	2.38	2.22	2.21	1.274e+07	536.00	2.56	0.08	0.06	0.06	37,16,11
1207	2.28	2.07	2.14	1.225e+07	536.00	2.48	0.09	0.07	0.04	37,16,16
1208	2.28	2.03	2.03	1.225e+07	536.00	2.35	0.09	0.07	0.03	37,

1944	2.28	2.07	2.14	1.225e+07	536.00	2.48	0.09	0.07	0.04	37,16,16
1945	2.28	2.03	2.03	1.225e+07	536.00	2.35	0.09	0.07	0.03	37,16,16
1946	2.20	1.93	2.03	1.185e+07	536.00	2.35	0.09	0.07	0.03	37,16,16
1947	2.06	1.93	2.20	1.111e+07	536.00	2.54	0.09	0.07	0.03	37,16,14
1948	2.01	1.87	1.86	7.843e+06	455.60	2.15	0.09	0.07	0.02	37,16,11

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				7.843e+06	455.60	2.15			
	2.52	2.24	2.22	1.340e+07	536.00	2.57	0.09	0.07	0.06

Setto	Mat.	Spessore	Stato
		cm	
7	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1115	1.82	1.70	1.70	7.150e+06	455.60	1.97	0.13	0.07	0.02	37,16,16
1117	1.82	1.70	1.68	7.150e+06	455.60	1.95	0.13	0.07	0.03	37,16,37
1119	1.68	1.60	1.68	9.205e+06	536.00	1.95	0.13	0.06	0.03	37,16,37
1181	1.74	1.65	1.65	9.487e+06	536.00	1.91	0.14	0.06	0.04	37,16,16
1182	1.74	1.65	1.65	9.487e+06	536.00	1.91	0.14	0.06	0.04	37,16,16
1183	1.74	1.65	1.65	9.487e+06	536.00	1.91	0.14	0.06	0.04	37,16,16
1184	1.74	1.65	1.65	9.487e+06	536.00	1.91	0.14	0.06	0.04	37,16,16
1185	1.68	1.60	1.68	9.205e+06	536.00	1.95	0.13	0.06	0.03	37,16,37
1186	1.68	1.60	1.68	9.205e+06	536.00	1.95	0.13	0.06	0.03	37,16,37
1193	1.74	1.67	1.65	9.487e+06	495.80	1.91	0.14	0.07	0.04	37,16,16
1194	1.74	1.67	1.65	9.487e+06	495.80	1.91	0.14	0.07	0.04	37,16,16
1195	1.68	1.60	1.68	9.205e+06	536.00	1.95	0.13	0.06	0.03	37,16,37
1202	1.78	1.70	1.67	8.278e+06	455.60	1.94	0.14	0.07	0.03	37,16,16
1203	1.78	1.70	1.67	8.278e+06	455.60	1.94	0.14	0.07	0.03	37,16,16
1204	1.68	1.60	1.68	9.205e+06	536.00	1.95	0.13	0.06	0.03	37,16,37
1211	1.82	1.70	1.70	7.150e+06	455.60	1.97	0.13	0.07	0.02	37,16,16
1212	1.82	1.70	1.68	7.150e+06	455.60	1.95	0.13	0.07	0.03	37,16,37
1213	1.68	1.60	1.68	9.205e+06	536.00	1.95	0.13	0.06	0.03	37,16,37
1220	1.82	1.70	1.70	7.150e+06	455.60	1.97	0.13	0.07	0.02	37,16,16
1221	1.82	1.70	1.68	7.150e+06	455.60	1.95	0.13	0.07	0.03	37,16,37
1222	1.68	1.60	1.68	9.205e+06	536.00	1.95	0.13	0.06	0.03	37,16,37
1229	1.82	1.70	1.70	7.150e+06	455.60	1.97	0.13	0.07	0.02	37,16,16
1230	1.82	1.70	1.68	7.150e+06	455.60	1.95	0.13	0.07	0.03	37,16,37
1231	1.68	1.60	1.68	9.205e+06	536.00	1.95	0.13	0.06	0.03	37,16,37
1238	1.82	1.70	1.70	7.150e+06	455.60	1.97	0.13	0.07	0.02	37,16,16
1239	1.82	1.70	1.68	7.150e+06	455.60	1.95	0.13	0.07	0.03	37,16,37
1240	1.68	1.60	1.68	9.205e+06	536.00	1.95	0.13	0.06	0.03	37,16,37
1247	1.82	1.70	1.70	7.150e+06	455.60	1.97	0.13	0.07	0.02	37,16,16
1248	1.82	1.70	1.68	7.150e+06	455.60	1.95	0.13	0.07	0.03	37,16,37
1249	1.68	1.60	1.68	9.205e+06	536.00	1.95	0.13	0.06	0.03	37,16,37
1256	1.82	1.70	1.70	7.150e+06	455.60	1.97	0.13	0.07	0.02	37,16,16
1257	1.82	1.70	1.68	7.150e+06	455.60	1.95	0.13	0.07	0.03	37,16,37
1258	1.68	1.60	1.68	9.205e+06	536.00	1.95	0.13	0.06	0.03	37,16,37
1948	1.82	1.70	1.70	7.150e+06	455.60	1.97	0.13	0.07	0.02	37,16,16
1949	1.82	1.70	1.68	7.150e+06	455.60	1.95	0.13	0.07	0.03	37,16,37
1950	1.68	1.60	1.68	9.205e+06	536.00	1.95	0.13	0.06	0.03	37,16,37

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				7.150e+06	455.60	1.91			
	1.82	1.70	1.70	9.487e+06	536.00	1.97	0.14	0.07	0.04

Setto	Mat.	Spessore	Stato
		cm	
9	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
2270	0.09	0.10	0.09	1.794e+05	323.00	0.10	0.05	6.06e-03	0.15	14,26,38
3067	0.25	0.24	0.25	5.207e+05	323.00	0.29	0.10	0.02	0.15	15,14,32
3070	0.25	0.24	0.25	5.207e+05	323.00	0.29	0.10	0.02	0.15	15,14,32

3073	0.25	0.24	0.25	5.207e+05	323.00	0.29	0.10	0.02	0.15	15,14,32
3076	0.25	0.24	0.25	5.207e+05	323.00	0.29	0.10	0.02	0.15	15,14,32
3079	0.25	0.24	0.25	5.207e+05	323.00	0.29	0.10	0.02	0.15	15,14,32
3082	0.25	0.24	0.25	5.207e+05	323.00	0.29	0.10	0.02	0.15	15,14,32
3085	0.25	0.24	0.25	5.207e+05	323.00	0.29	0.10	0.02	0.15	15,14,32
3088	0.25	0.24	0.25	5.207e+05	323.00	0.29	0.10	0.02	0.15	15,14,32
3243	0.25	0.24	0.25	5.207e+05	323.00	0.29	0.10	0.02	0.15	15,14,32
3244	0.22	0.22	0.22	4.627e+05	323.00	0.26	0.08	0.01	0.11	15,14,32
3245	0.10	0.16	0.10	2.005e+05	323.00	0.11	0.05	9.37e-03	0.13	14,22,38
3246	0.10	0.10	0.10	2.005e+05	323.00	0.11	0.05	6.06e-03	0.13	14,26,38
3247	0.25	0.24	0.25	5.207e+05	323.00	0.29	0.10	0.02	0.15	15,14,32
3248	0.22	0.22	0.22	4.627e+05	323.00	0.26	0.08	0.01	0.11	15,14,32
3249	0.10	0.16	0.10	2.005e+05	323.00	0.11	0.05	9.37e-03	0.13	14,22,38
3250	0.10	0.10	0.10	2.005e+05	323.00	0.11	0.05	6.06e-03	0.13	14,26,38
3251	0.25	0.24	0.25	5.207e+05	323.00	0.29	0.10	0.02	0.15	15,14,32
3252	0.22	0.22	0.22	4.627e+05	323.00	0.26	0.08	0.01	0.11	15,14,32
3253	0.10	0.16	0.10	2.005e+05	323.00	0.11	0.05	9.37e-03	0.13	14,22,38
3254	0.10	0.10	0.10	2.005e+05	323.00	0.11	0.05	6.06e-03	0.13	14,26,38
3300	0.25	0.24	0.25	5.207e+05	323.00	0.29	0.10	0.02	0.15	15,14,32
3301	0.25	0.24	0.25	5.207e+05	323.00	0.29	0.10	0.02	0.15	15,14,32
3302	0.22	0.22	0.22	4.627e+05	323.00	0.26	0.08	0.01	0.11	15,14,32
3303	0.22	0.22	0.22	4.627e+05	323.00	0.26	0.08	0.01	0.11	15,14,32
3304	0.10	0.16	0.10	2.005e+05	323.00	0.11	0.05	9.37e-03	0.13	14,22,38
3305	0.10	0.16	0.10	2.005e+05	323.00	0.11	0.05	9.37e-03	0.13	14,22,38
3306	0.10	0.10	0.10	2.005e+05	323.00	0.11	0.05	6.06e-03	0.13	14,26,38
3307	0.10	0.10	0.10	2.005e+05	323.00	0.11	0.05	6.06e-03	0.13	14,26,38
3308	0.25	0.24	0.25	5.207e+05	323.00	0.29	0.10	0.02	0.15	15,14,32
3309	0.22	0.22	0.22	4.627e+05	323.00	0.26	0.08	0.01	0.11	15,14,32
3310	0.10	0.16	0.10	2.005e+05	323.00	0.11	0.05	9.37e-03	0.13	14,22,38
3311	0.10	0.10	0.10	2.005e+05	323.00	0.11	0.05	6.06e-03	0.13	14,26,38
3312	0.25	0.24	0.25	5.207e+05	323.00	0.29	0.10	0.02	0.15	15,14,32
3313	0.22	0.22	0.22	4.627e+05	323.00	0.26	0.08	0.01	0.11	15,14,32
3314	0.10	0.16	0.10	2.005e+05	323.00	0.11	0.05	9.37e-03	0.13	14,22,38
3315	0.09	0.10	0.09	1.794e+05	323.00	0.10	0.05	6.06e-03	0.15	14,26,38
3316	0.25	0.24	0.25	5.207e+05	323.00	0.29	0.10	0.02	0.15	15,14,32
3317	0.22	0.22	0.22	4.627e+05	323.00	0.26	0.08	0.01	0.11	15,14,32
3318	0.09	0.16	0.09	1.794e+05	323.00	0.10	0.05	9.37e-03	0.15	14,22,38
3319	0.10	0.10	0.10	2.005e+05	323.00	0.11	0.05	6.06e-03	0.13	14,26,38
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				1.794e+05	323.00	0.10				
	0.25	0.24	0.25	5.207e+05	323.00	0.29	0.10	0.02	0.15	

Setto	Mat.	Spessore	Stato
		cm	
10	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1459	3.40	3.40	3.07	4.848e+05	87.50	2.47	0.16	0.16	0.05	11,11,33
1481	3.72	3.72	3.34	5.266e+05	87.50	2.69	0.24	0.25	0.02	11,11,29
1491	3.72	3.72	3.07	5.266e+05	87.50	2.47	0.24	0.25	0.05	11,11,33
1492	3.40	3.40	3.07	4.848e+05	87.50	2.47	0.16	0.16	0.05	11,11,33
1574	3.72	3.72	3.34	5.266e+05	87.50	2.69	0.24	0.25	0.02	11,11,29
1575	3.72	3.72	3.07	5.266e+05	87.50	2.47	0.24	0.25	0.05	11,11,33
1576	3.40	3.40	3.07	4.848e+05	87.50	2.47	0.16	0.16	0.05	11,11,33
1589	3.72	3.72	3.34	5.266e+05	87.50	2.69	0.24	0.25	0.02	11,11,29
1590	3.72	3.72	3.07	5.266e+05	87.50	2.47	0.24	0.25	0.05	11,11,33
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				4.848e+05	87.50	2.47				
	3.72	3.72	3.34	5.266e+05	87.50	2.69	0.24	0.25	0.05	

Setto	Mat.	Spessore	Stato
		cm	
11	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
4	1.59	1.90	1.59	2.362e+05	87.50	1.28	0.09	0.13	0.08	11,30,11
10	1.59	1.90	1.59	2.362e+05	87.50	1.28	0.09	0.13	0.08	11,30,11
306	1.59	1.90	1.59	2.362e+05	87.50	1.28	0.09	0.13	0.08	11,30,11
307	1.59	1.90	1.59	2.362e+05	87.50	1.28	0.09	0.13	0.08	11,30,11
346	1.59	1.90	1.59	2.362e+05	87.50	1.28	0.09	0.13	0.08	11,30,11
351	1.59	1.90	1.59	2.362e+05	87.50	1.28	0.09	0.13	0.08	11,30,11
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	1.59	1.90	1.59	2.362e+05	87.50	1.28				
					87.50	1.28	0.09	0.13	0.08	

Setto	Mat.	Spessore	Stato
		cm	
21	mattoni pieni e malta di calce	37.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
3	1.49	2.44	2.24	8.602e+04	57.25	2.50	0.26	0.15	0.03	26,11,20
653	1.49	2.44	2.24	8.602e+04	57.25	2.50	0.26	0.15	0.03	26,11,20
654	1.49	2.44	2.24	8.602e+04	57.25	2.50	0.26	0.15	0.03	26,11,20
655	1.49	2.44	2.24	8.602e+04	57.25	2.50	0.26	0.15	0.03	26,11,20
656	1.82	2.70	1.75	1.045e+05	57.25	1.96	0.04	0.13	0.05	14,11,14
657	1.82	2.70	1.75	1.045e+05	57.25	1.96	0.04	0.13	0.05	14,11,14
658	2.22	2.39	1.74	1.254e+05	57.25	1.94	0.02	0.05	0.06	11,11,14
659	2.22	2.39	1.74	1.254e+05	57.25	1.94	0.02	0.05	0.06	11,11,14
660	2.12	1.76	1.93	1.202e+05	57.25	2.15	0.03	0.07	0.07	11,14,32
661	2.12	1.76	1.93	1.202e+05	57.25	2.15	0.03	0.07	0.07	11,14,32
662	2.12	1.85	1.93	1.202e+05	57.25	2.15	0.03	0.09	0.07	11,14,32
663	2.12	1.85	1.93	1.202e+05	57.25	2.15	0.03	0.09	0.07	11,14,32
664	2.18	2.05	2.09	1.235e+05	57.25	2.33	0.03	0.12	0.06	20,30,24
665	2.18	2.05	2.09	1.235e+05	57.25	2.33	0.03	0.12	0.06	20,30,24
666	2.18	2.05	2.18	1.235e+05	57.25	2.43	0.03	0.12	0.02	20,30,19
667	2.18	2.05	2.18	1.235e+05	57.25	2.43	0.03	0.12	0.02	20,30,19
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	2.22	2.70	2.24	8.602e+04	57.25	1.94				
				1.254e+05	57.25	2.50	0.26	0.15	0.07	

Setto	Mat.	Spessore	Stato
		cm	
22	mattoni pieni e malta di calce	37.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
666	2.26	2.00	2.02	4.847e+05	343.50	2.25	0.21	0.02	0.03	27,14,22
667	2.26	2.00	2.02	4.847e+05	343.50	2.25	0.21	0.02	0.03	27,14,22
668	2.26	0.99	0.99	4.847e+05	343.50	1.10	0.21	0.03	0.04	27,14,14
669	2.26	0.99	0.99	4.847e+05	343.50	1.10	0.21	0.03	0.04	27,14,14
670	1.00	0.99	0.99	9.285e+05	343.50	1.10	0.09	0.03	0.04	30,14,14
671	1.00	0.99	0.99	9.285e+05	343.50	1.10	0.09	0.03	0.04	30,14,14
679	1.00	0.99	0.99	9.285e+05	343.50	1.10	0.09	0.03	0.04	30,14,14
680	1.00	0.99	0.99	9.285e+05	343.50	1.10	0.09	0.03	0.04	30,14,14
682	2.26	2.00	2.02	4.847e+05	343.50	2.25	0.21	0.02	0.03	27,14,22
683	2.26	0.99	0.99	4.847e+05	343.50	1.10	0.21	0.03	0.04	27,14,14
684	1.00	0.99	0.99	9.285e+05	343.50	1.10	0.09	0.03	0.04	30,14,14
689	1.00	0.99	0.99	9.285e+05	343.50	1.10	0.09	0.03	0.04	30,14,14
690	1.00	0.99	0.99	9.285e+05	343.50	1.10	0.09	0.03	0.04	30,14,14
698	1.00	0.99	0.99	9.285e+05	343.50	1.10	0.09	0.03	0.04	30,14,14
699	1.00	0.99	0.99	9.285e+05	343.50	1.10	0.09	0.03	0.04	30,14,14
707	2.26	2.00	2.02	4.847e+05	343.50	2.25	0.21	0.02	0.03	27,14,22
708	2.26	0.99	0.99	4.847e+05	343.50	1.10	0.21	0.03	0.04	27,14,14
709	1.00	0.99	0.99	9.285e+05	343.50	1.10	0.09	0.03	0.04	30,14,14
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	

			4.847e+05	343.50	1.10				
2.26	2.00	2.02	9.285e+05	343.50	2.25	0.21	0.03	0.04	

Setto	Mat.	Spessore	Stato
		cm	
24	mattoni pieni e malta di calce	37.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
15	2.52	2.52	2.64	1.267e+05	54.25	2.94	0.09	0.11	0.03	27,27,19
681	2.29	2.44	2.12	1.162e+05	54.25	2.37	0.09	0.06	0.04	24,35,32
682	2.29	2.44	2.08	1.162e+05	54.25	2.32	0.09	0.06	0.04	24,35,32
700	2.52	2.52	2.62	1.267e+05	54.25	2.92	0.09	0.11	0.03	27,27,19
701	2.52	2.52	2.64	1.267e+05	54.25	2.94	0.09	0.11	0.03	27,27,19
702	2.52	2.52	2.62	1.266e+05	54.25	2.92	0.04	0.06	0.03	27,27,19
703	2.10	2.37	2.17	1.069e+05	54.25	2.42	0.03	0.05	0.04	14,33,21
704	2.09	2.36	2.17	1.068e+05	54.25	2.42	0.04	0.06	0.04	38,33,21
705	2.34	2.36	2.12	1.185e+05	54.25	2.37	0.07	0.06	0.04	24,33,32
706	2.29	2.44	2.12	1.162e+05	54.25	2.37	0.09	0.06	0.04	24,35,32
707	2.29	2.44	2.08	1.162e+05	54.25	2.32	0.09	0.06	0.04	24,35,32
710	2.52	2.52	2.62	1.267e+05	54.25	2.92	0.09	0.11	0.03	27,27,19
711	2.52	2.52	2.62	1.266e+05	54.25	2.92	0.04	0.06	0.03	27,27,19
712	2.10	2.37	2.17	1.069e+05	54.25	2.42	0.03	0.05	0.04	14,33,21
713	2.09	2.36	2.17	1.068e+05	54.25	2.42	0.04	0.06	0.04	38,33,21
714	2.34	2.36	2.12	1.185e+05	54.25	2.37	0.07	0.06	0.04	24,33,32

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				1.068e+05	54.25	2.32			
	2.52	2.52	2.64	1.267e+05	54.25	2.94	0.09	0.11	0.04

Setto	Mat.	Spessore	Stato
		cm	
27	mattoni pieni e malta di calce	42.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
15	2.44	2.59	2.13	1.196e+05	50.25	2.69	0.10	0.06	0.03	20,27,14
22	2.44	2.59	2.13	1.196e+05	50.25	2.69	0.10	0.06	0.03	20,27,14
681	2.08	1.98	2.10	1.033e+05	50.25	2.66	0.10	0.03	0.06	20,21,31
682	2.08	2.08	2.10	1.033e+05	50.25	2.66	0.10	0.03	0.06	20,20,31
710	2.44	2.59	2.13	1.196e+05	50.25	2.69	0.10	0.06	0.03	20,27,14
711	2.46	2.59	2.19	1.206e+05	50.25	2.78	0.08	0.03	0.02	20,27,14
712	2.33	2.33	2.24	1.149e+05	50.25	2.84	0.04	0.04	0.02	13,21,18
713	2.33	2.33	2.33	1.149e+05	50.25	2.96	0.04	0.04	0.04	13,21,29
714	2.04	2.14	2.28	1.017e+05	50.25	2.89	0.05	0.04	0.06	32,21,27
715	2.44	2.59	2.13	1.196e+05	50.25	2.69	0.10	0.06	0.03	20,27,14
716	2.46	2.59	2.19	1.206e+05	50.25	2.78	0.08	0.03	0.02	20,27,14
717	2.33	2.33	2.24	1.149e+05	50.25	2.84	0.04	0.04	0.02	13,21,18
718	2.33	2.33	2.33	1.149e+05	50.25	2.96	0.04	0.04	0.04	13,21,29
719	2.04	2.14	2.28	1.017e+05	50.25	2.89	0.05	0.04	0.06	32,21,27
720	2.08	1.98	2.10	1.033e+05	50.25	2.66	0.10	0.03	0.06	20,21,31
721	2.08	2.08	2.10	1.033e+05	50.25	2.66	0.10	0.03	0.06	20,20,31

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				1.017e+05	50.25	2.66			
	2.46	2.59	2.33	1.206e+05	50.25	2.96	0.10	0.06	0.06

Setto	Mat.	Spessore	Stato
		cm	
28	mattoni pieni e malta di calce	42.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
682	1.27	1.23	1.46	6.499e+04	50.25	1.85	0.09	0.06	0.05	21,22,15
683	1.27	1.23	1.46	6.499e+04	50.25	1.85	0.09	0.06	0.05	21,22,15
721	1.27	1.23	1.46	6.499e+04	50.25	1.85	0.09	0.06	0.05	21,22,15
722	1.27	1.23	1.46	6.499e+04	50.25	1.85	0.09	0.06	0.05	21,22,15
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	1.27	1.23	1.46	6.499e+04	50.25	1.85	0.09	0.06	0.05	

Setto	Mat.	Spessore	Stato
		cm	
29	muratura E = 2.000e+04 mattoni in argilla espansa e cls con malta M2	30.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
683	0.86	0.96	0.92	2.116e+06	412.37	1.30	0.13	0.09	0.08	30,20,29
684	0.86	0.96	0.92	2.116e+06	412.37	1.30	0.13	0.09	0.08	30,20,29
722	0.86	0.96	0.92	2.116e+06	412.37	1.30	0.13	0.09	0.08	30,20,29
723	0.86	0.96	0.92	2.116e+06	412.37	1.30	0.13	0.09	0.08	30,20,29
732	0.86	0.96	0.92	2.116e+06	412.37	1.30	0.13	0.09	0.08	30,20,29
733	0.86	0.96	0.92	2.116e+06	412.37	1.30	0.13	0.09	0.08	30,20,29
742	0.86	0.96	0.92	2.116e+06	412.37	1.30	0.13	0.09	0.08	30,20,29
743	0.86	0.96	0.92	2.116e+06	412.37	1.30	0.13	0.09	0.08	30,20,29
751	0.86	0.96	0.92	2.116e+06	412.37	1.30	0.13	0.09	0.08	30,20,29
752	0.86	0.96	0.92	2.116e+06	412.37	1.30	0.13	0.09	0.08	30,20,29
760	0.86	0.96	0.92	2.116e+06	412.37	1.30	0.13	0.09	0.08	30,20,29
761	0.86	0.96	0.92	2.116e+06	412.37	1.30	0.13	0.09	0.08	30,20,29
770	0.86	0.96	0.92	2.116e+06	412.37	1.30	0.13	0.09	0.08	30,20,29
771	0.86	0.96	0.92	2.116e+06	412.37	1.30	0.13	0.09	0.08	30,20,29
779	0.86	0.96	0.92	2.116e+06	412.37	1.30	0.13	0.09	0.08	30,20,29
780	0.86	0.96	0.92	2.116e+06	412.37	1.30	0.13	0.09	0.08	30,20,29
838	0.86	0.96	0.92	2.116e+06	412.37	1.30	0.13	0.09	0.08	30,20,29
839	0.86	0.96	0.92	2.116e+06	412.37	1.30	0.13	0.09	0.08	30,20,29
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	0.86	0.96	0.92	2.116e+06	412.37	1.30	0.13	0.09	0.08	

Setto	Mat.	Spessore	Stato
		cm	
31	mattoni pieni e malta di calce	42.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
25	1.87	1.71	1.78	6.966e+06	433.25	2.25	0.13	0.19	2.78e-03	20,26,30
26	1.87	1.71	1.78	6.966e+06	433.25	2.25	0.13	0.19	2.78e-03	20,26,30
27	1.87	1.71	1.78	6.966e+06	433.25	2.25	0.13	0.19	2.78e-03	20,26,30
28	1.87	1.71	1.78	6.966e+06	433.25	2.25	0.13	0.19	2.78e-03	20,26,30
727	1.84	1.63	1.68	6.833e+06	433.25	2.13	0.13	0.20	0.01	20,26,30
728	1.75	1.58	1.61	6.529e+06	433.25	2.04	0.13	0.20	0.02	20,26,30
729	1.67	1.53	1.55	6.237e+06	433.25	1.96	0.13	0.20	0.02	20,26,34
730	1.57	1.44	1.45	5.884e+06	433.25	1.84	0.12	0.21	0.02	32,26,42
737	1.45	1.44	1.35	5.482e+06	433.25	1.71	0.10	0.21	0.04	34,26,38
738	1.34	1.34	1.35	5.065e+06	433.25	1.71	0.05	0.20	0.04	26,26,38
762	1.45	1.44	1.35	5.482e+06	433.25	1.71	0.10	0.21	0.04	34,26,38
763	1.34	1.34	1.35	5.065e+06	433.25	1.71	0.05	0.20	0.04	26,26,38
766	1.84	1.69	1.75	6.833e+06	433.25	2.21	0.13	0.19	6.55e-03	20,26,30
772	1.84	1.69	1.75	6.833e+06	433.25	2.21	0.13	0.19	6.55e-03	20,26,30
773	1.84	1.63	1.68	6.833e+06	433.25	2.13	0.13	0.20	0.01	20,26,30
774	1.75	1.58	1.61	6.529e+06	433.25	2.04	0.13	0.20	0.02	20,26,30
775	1.67	1.53	1.55	6.237e+06	433.25	1.96	0.13	0.20	0.02	20,26,34
776	1.57	1.44	1.45	5.884e+06	433.25	1.84	0.12	0.21	0.02	32,26,42
777	1.45	1.44	1.35	5.482e+06	433.25	1.71	0.10	0.21	0.04	34,26,38
778	1.34	1.34	1.35	5.065e+06	433.25	1.71	0.05	0.20	0.04	26,26,38

781	1.84	1.69	1.75	6.833e+06	433.25	2.21	0.13	0.19	6.55e-03	20,26,30
782	1.87	1.71	1.78	6.966e+06	433.25	2.25	0.13	0.19	2.78e-03	20,26,30
783	1.84	1.63	1.68	6.833e+06	433.25	2.13	0.13	0.20	0.01	20,26,30
784	1.75	1.58	1.61	6.529e+06	433.25	2.04	0.13	0.20	0.02	20,26,30
785	1.67	1.53	1.55	6.237e+06	433.25	1.96	0.13	0.20	0.02	20,26,34
786	1.57	1.44	1.45	5.884e+06	433.25	1.84	0.12	0.21	0.02	32,26,42
787	1.45	1.44	1.35	5.482e+06	433.25	1.71	0.10	0.21	0.04	34,26,38
788	1.34	1.34	1.35	5.065e+06	433.25	1.71	0.05	0.20	0.04	26,26,38
791	1.84	1.69	1.75	6.833e+06	433.25	2.21	0.13	0.19	6.55e-03	20,26,30
792	1.87	1.71	1.78	6.966e+06	433.25	2.25	0.13	0.19	2.78e-03	20,26,30
793	1.84	1.63	1.68	6.833e+06	433.25	2.13	0.13	0.20	0.01	20,26,30
794	1.75	1.58	1.61	6.529e+06	433.25	2.04	0.13	0.20	0.02	20,26,30
795	1.67	1.53	1.55	6.237e+06	433.25	1.96	0.13	0.20	0.02	20,26,34
796	1.57	1.44	1.45	5.884e+06	433.25	1.84	0.12	0.21	0.02	32,26,42
797	1.45	1.44	1.35	5.482e+06	433.25	1.71	0.10	0.21	0.04	34,26,38
798	1.34	1.34	1.35	5.065e+06	433.25	1.71	0.05	0.20	0.04	26,26,38
801	1.84	1.69	1.75	6.833e+06	433.25	2.21	0.13	0.19	6.55e-03	20,26,30
802	1.87	1.71	1.78	6.966e+06	433.25	2.25	0.13	0.19	2.78e-03	20,26,30
803	1.84	1.63	1.68	6.833e+06	433.25	2.13	0.13	0.20	0.01	20,26,30
804	1.75	1.58	1.61	6.529e+06	433.25	2.04	0.13	0.20	0.02	20,26,30
805	1.67	1.53	1.55	6.237e+06	433.25	1.96	0.13	0.20	0.02	20,26,34
806	1.57	1.44	1.45	5.884e+06	433.25	1.84	0.12	0.21	0.02	32,26,42
807	1.45	1.44	1.35	5.482e+06	433.25	1.71	0.10	0.21	0.04	34,26,38
808	1.34	1.34	1.35	5.065e+06	433.25	1.71	0.05	0.20	0.04	26,26,38
811	1.84	1.69	1.75	6.833e+06	433.25	2.21	0.13	0.19	6.55e-03	20,26,30
812	1.87	1.71	1.78	6.966e+06	433.25	2.25	0.13	0.19	2.78e-03	20,26,30
813	1.84	1.63	1.68	6.833e+06	433.25	2.13	0.13	0.20	0.01	20,26,30
814	1.75	1.58	1.61	6.529e+06	433.25	2.04	0.13	0.20	0.02	20,26,30
815	1.67	1.53	1.55	6.237e+06	433.25	1.96	0.13	0.20	0.02	20,26,34
816	1.57	1.44	1.45	5.884e+06	433.25	1.84	0.12	0.21	0.02	32,26,42
817	1.45	1.44	1.35	5.482e+06	433.25	1.71	0.10	0.21	0.04	34,26,38
818	1.34	1.34	1.35	5.065e+06	433.25	1.71	0.05	0.20	0.04	26,26,38
821	1.84	1.69	1.75	6.833e+06	433.25	2.21	0.13	0.19	6.55e-03	20,26,30
822	1.84	1.63	1.68	6.833e+06	433.25	2.13	0.13	0.20	0.01	20,26,30
823	1.75	1.58	1.61	6.529e+06	433.25	2.04	0.13	0.20	0.02	20,26,30
824	1.67	1.53	1.55	6.237e+06	433.25	1.96	0.13	0.20	0.02	20,26,34
825	1.57	1.44	1.45	5.884e+06	433.25	1.84	0.12	0.21	0.02	32,26,42
826	1.45	1.44	1.35	5.482e+06	433.25	1.71	0.10	0.21	0.04	34,26,38
827	1.34	1.34	1.35	5.065e+06	433.25	1.71	0.05	0.20	0.04	26,26,38
840	1.84	1.69	1.75	6.833e+06	433.25	2.21	0.13	0.19	6.55e-03	20,26,30
841	1.87	1.71	1.78	6.966e+06	433.25	2.25	0.13	0.19	2.78e-03	20,26,30
842	1.84	1.63	1.68	6.833e+06	433.25	2.13	0.13	0.20	0.01	20,26,30
843	1.75	1.58	1.61	6.529e+06	433.25	2.04	0.13	0.20	0.02	20,26,30
844	1.67	1.53	1.55	6.237e+06	433.25	1.96	0.13	0.20	0.02	20,26,34
845	1.57	1.44	1.45	5.884e+06	433.25	1.84	0.12	0.21	0.02	32,26,42
846	1.45	1.44	1.35	5.482e+06	433.25	1.71	0.10	0.21	0.04	34,26,38
847	1.34	1.34	1.35	5.065e+06	433.25	1.71	0.05	0.20	0.04	26,26,38
850	1.84	1.69	1.75	6.833e+06	433.25	2.21	0.13	0.19	6.55e-03	20,26,30
851	1.84	1.63	1.68	6.833e+06	433.25	2.13	0.13	0.20	0.01	20,26,30
852	1.75	1.58	1.61	6.529e+06	433.25	2.04	0.13	0.20	0.02	20,26,30
853	1.67	1.53	1.55	6.237e+06	433.25	1.96	0.13	0.20	0.02	20,26,34
854	1.57	1.44	1.45	5.884e+06	433.25	1.84	0.12	0.21	0.02	32,26,42

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				5.065e+06	433.25	1.71			
	1.87	1.71	1.78	6.966e+06	433.25	2.25	0.13	0.21	0.04

Setto	Mat.	Spessore	Stato
		cm	
32	mattoni pieni e malta di calce	42.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
738	1.15	1.16	1.17	4.377e+06	433.25	1.48	0.01	0.19	0.07	21,26,38
739	1.19	1.16	1.18	4.440e+06	433.25	1.49	0.04	0.19	0.09	20,26,42
740	1.19	1.17	1.18	4.440e+06	429.63	1.49	0.04	0.18	0.09	20,26,42
763	1.15	1.16	1.17	4.377e+06	433.25	1.48	0.01	0.19	0.07	21,26,38
764	1.19	1.16	1.18	4.440e+06	433.25	1.49	0.04	0.19	0.09	20,26,42
765	1.19	1.17	1.18	4.440e+06	429.63	1.49	0.04	0.18	0.09	20,26,42
778	1.15	1.16	1.17	4.377e+06	433.25	1.48	0.01	0.19	0.07	21,26,38
779	1.19	1.16	1.18	4.440e+06	433.25	1.49	0.04	0.19	0.09	20,26,42
780	1.19	1.17	1.18	4.440e+06	429.63	1.49	0.04	0.18	0.09	20,26,42

788	1.15	1.16	1.17	4.377e+06	433.25	1.48	0.01	0.19	0.07	21,26,38
789	1.19	1.16	1.18	4.440e+06	433.25	1.49	0.04	0.19	0.09	20,26,42
790	1.19	1.17	1.18	4.440e+06	429.63	1.49	0.04	0.18	0.09	20,26,42
798	1.15	1.16	1.17	4.377e+06	433.25	1.48	0.01	0.19	0.07	21,26,38
799	1.19	1.16	1.18	4.440e+06	433.25	1.49	0.04	0.19	0.09	20,26,42
800	1.19	1.17	1.18	4.440e+06	429.63	1.49	0.04	0.18	0.09	20,26,42
808	1.15	1.16	1.17	4.377e+06	433.25	1.48	0.01	0.19	0.07	21,26,38
809	1.19	1.16	1.18	4.440e+06	433.25	1.49	0.04	0.19	0.09	20,26,42
810	1.19	1.17	1.18	4.440e+06	429.63	1.49	0.04	0.18	0.09	20,26,42
818	1.15	1.16	1.17	4.377e+06	433.25	1.48	0.01	0.19	0.07	21,26,38
819	1.19	1.16	1.18	4.440e+06	433.25	1.49	0.04	0.19	0.09	20,26,42
820	1.19	1.17	1.18	4.440e+06	429.63	1.49	0.04	0.18	0.09	20,26,42
827	1.15	1.16	1.17	4.377e+06	433.25	1.48	0.01	0.19	0.07	21,26,38
828	1.19	1.16	1.18	4.440e+06	433.25	1.49	0.04	0.19	0.09	20,26,42
829	1.19	1.17	1.18	4.440e+06	429.63	1.49	0.04	0.18	0.09	20,26,42
847	1.15	1.16	1.17	4.377e+06	433.25	1.48	0.01	0.19	0.07	21,26,38
848	1.19	1.16	1.18	4.440e+06	433.25	1.49	0.04	0.19	0.09	20,26,42
849	1.19	1.17	1.18	4.440e+06	429.63	1.49	0.04	0.18	0.09	20,26,42

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				4.377e+06	429.63	1.48			
	1.19	1.17	1.18	4.440e+06	433.25	1.49	0.04	0.19	0.09

Setto	Mat.	Spessore	Stato
		cm	
36	mattoni pieni e malta di calce	42.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
23	1.93	2.16	2.12	2.122e+05	74.50	2.69	0.05	0.07	0.05	26,24,38
24	1.93	2.16	2.12	2.122e+05	74.50	2.69	0.05	0.07	0.05	26,24,38
744	1.93	2.16	2.19	2.122e+05	74.50	2.77	0.05	0.07	0.05	26,24,42
745	2.28	2.36	2.19	2.479e+05	74.50	2.77	0.05	0.06	0.05	23,20,42
746	2.28	2.36	2.17	2.479e+05	74.50	2.75	0.05	0.07	0.05	23,20,42
747	2.12	2.27	2.17	2.314e+05	74.50	2.75	0.06	0.07	0.05	39,20,42
748	2.12	2.27	2.27	2.314e+05	74.50	2.88	0.06	0.07	0.05	39,20,24
749	1.68	1.81	1.81	1.861e+05	74.50	2.30	0.15	0.14	0.07	26,33,33
750	1.68	1.81	1.81	1.861e+05	74.50	2.30	0.15	0.14	0.07	26,33,33
753	1.93	2.16	2.12	2.122e+05	74.50	2.69	0.05	0.07	0.05	26,24,38
754	2.29	2.37	2.18	2.489e+05	74.50	2.77	0.06	0.07	0.05	23,20,42
755	2.29	2.36	2.17	2.489e+05	74.50	2.75	0.06	0.07	0.05	23,20,42
756	2.12	2.27	2.17	2.314e+05	74.50	2.75	0.06	0.07	0.05	39,20,42
757	2.12	2.27	2.27	2.314e+05	74.50	2.88	0.06	0.07	0.05	39,20,24
758	1.68	1.81	1.81	1.861e+05	74.50	2.30	0.15	0.14	0.07	26,33,33
759	1.68	1.81	1.81	1.861e+05	74.50	2.30	0.15	0.14	0.07	26,33,33
830	1.93	2.16	2.19	2.122e+05	74.50	2.77	0.05	0.07	0.05	26,24,42
831	1.93	2.16	2.12	2.122e+05	74.50	2.69	0.05	0.07	0.05	26,24,38
832	2.29	2.37	2.19	2.489e+05	74.50	2.77	0.06	0.07	0.05	23,20,42
833	2.29	2.36	2.17	2.489e+05	74.50	2.75	0.06	0.07	0.05	23,20,42
834	2.12	2.27	2.17	2.314e+05	74.50	2.75	0.06	0.07	0.05	39,20,42
835	2.12	2.27	2.27	2.314e+05	74.50	2.88	0.06	0.07	0.05	39,20,24
836	1.68	1.81	1.81	1.861e+05	74.50	2.30	0.15	0.14	0.07	26,33,33
837	1.68	1.81	1.81	1.861e+05	74.50	2.30	0.15	0.14	0.07	26,33,33

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				1.861e+05	74.50	2.30			
	2.29	2.37	2.27	2.489e+05	74.50	2.88	0.15	0.14	0.07

Setto	Mat.	Spessore	Stato
		cm	
37	mattoni pieni e malta di calce	42.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
750	1.23	1.23	1.30	1.381e+05	74.50	1.65	0.04	0.05	0.12	21,21,29
751	1.23	1.23	1.30	1.381e+05	74.50	1.65	0.04	0.05	0.12	21,21,29

759	1.23	1.23	1.30	1.381e+05	74.50	1.65	0.04	0.05	0.12	21,21,29
760	1.23	1.23	1.30	1.381e+05	74.50	1.65	0.04	0.05	0.12	21,21,29
837	1.23	1.23	1.30	1.381e+05	74.50	1.65	0.04	0.05	0.12	21,21,29
838	1.23	1.23	1.30	1.381e+05	74.50	1.65	0.04	0.05	0.12	21,21,29

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				1.381e+05	74.50	1.65			
	1.23	1.23	1.30	1.381e+05	74.50	1.65	0.04	0.05	0.12

Setto	Mat.	Spessore	Stato
		cm	
39	muratura E = 1.024e+05	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
28	3.64	3.64	3.65	8.178e+05	109.86	2.82	0.05	0.05	6.22e-03	36,36,38
30	3.64	3.64	3.65	8.178e+05	109.86	2.82	0.05	0.05	6.22e-03	36,36,38
727	3.41	3.34	3.37	7.694e+05	109.86	2.60	0.05	0.06	0.02	37,36,42
728	3.32	3.12	3.16	7.510e+05	109.86	2.44	0.04	0.06	0.02	37,36,38
729	3.25	2.90	2.95	7.345e+05	109.86	2.28	0.02	0.07	0.03	37,36,42
730	3.02	2.65	2.71	6.869e+05	109.86	2.09	0.05	0.07	0.04	37,36,42
737	2.23	2.23	2.29	5.157e+05	109.86	1.77	0.10	0.10	0.05	36,36,42
738	2.23	2.23	2.29	5.157e+05	109.86	1.77	0.10	0.10	0.05	36,36,42
766	3.64	3.54	3.55	8.178e+05	109.86	2.74	0.05	0.06	0.01	36,36,42
855	3.64	3.54	3.55	8.178e+05	109.86	2.74	0.05	0.06	0.01	36,36,42
856	3.64	3.54	3.55	8.178e+05	109.86	2.74	0.05	0.06	0.01	36,36,42
857	3.64	3.64	3.65	8.178e+05	109.86	2.82	0.05	0.05	6.22e-03	36,36,38
858	3.41	3.34	3.37	7.694e+05	109.86	2.60	0.05	0.06	0.02	37,36,42
859	3.41	3.34	3.37	7.694e+05	109.86	2.60	0.05	0.06	0.02	37,36,42
860	3.32	3.12	3.16	7.510e+05	109.86	2.44	0.04	0.06	0.02	37,36,38
861	3.32	3.12	3.16	7.510e+05	109.86	2.44	0.04	0.06	0.02	37,36,38
862	3.25	2.90	2.95	7.345e+05	109.86	2.28	0.02	0.07	0.03	37,36,42
863	3.25	2.90	2.95	7.345e+05	109.86	2.28	0.02	0.07	0.03	37,36,42
864	3.02	2.65	2.71	6.869e+05	109.86	2.09	0.05	0.07	0.04	37,36,42
865	3.02	2.65	2.71	6.869e+05	109.86	2.09	0.05	0.07	0.04	37,36,42
866	2.23	2.23	2.29	5.157e+05	109.86	1.77	0.10	0.10	0.05	36,36,42
867	2.23	2.23	2.29	5.157e+05	109.86	1.77	0.10	0.10	0.05	36,36,42
868	2.23	2.23	2.29	5.157e+05	109.86	1.77	0.10	0.10	0.05	36,36,42
869	2.23	2.23	2.29	5.157e+05	109.86	1.77	0.10	0.10	0.05	36,36,42

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				5.157e+05	109.86	1.77			
	3.64	3.64	3.65	8.178e+05	109.86	2.82	0.10	0.10	0.05

Setto	Mat.	Spessore	Stato
		cm	
40	muratura E = 1.024e+05	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
738	1.71	1.72	1.75	3.997e+05	109.86	1.35	0.25	0.10	0.04	36,16,23
739	1.09	1.11	1.75	2.582e+05	108.12	1.35	0.35	0.12	0.04	36,36,23
740	1.09	1.11	1.11	2.582e+05	108.12	0.86	0.35	0.12	0.02	36,36,23
868	1.71	1.72	1.75	3.997e+05	109.86	1.35	0.25	0.10	0.04	36,16,23
869	1.71	1.72	1.75	3.997e+05	109.86	1.35	0.25	0.10	0.04	36,16,23
870	1.09	1.11	1.75	2.582e+05	108.12	1.35	0.35	0.12	0.04	36,36,23
871	1.09	1.11	1.75	2.582e+05	108.12	1.35	0.35	0.12	0.04	36,36,23
872	1.09	1.11	1.11	2.582e+05	108.12	0.86	0.35	0.12	0.02	36,36,23
873	1.09	1.11	1.11	2.582e+05	108.12	0.86	0.35	0.12	0.02	36,36,23

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				2.582e+05	108.12	0.86			
	1.71	1.72	1.75	3.997e+05	109.86	1.35	0.35	0.12	0.04

Setto	Mat.	Spessore	Stato
		cm	
41	muratura E = 1.024e+05	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A.3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
2	4.00	4.12	3.88	5.517e+06	273.36	3.00	0.14	0.10	0.05	17,37,22
31	4.00	4.12	3.88	5.517e+06	273.36	3.00	0.14	0.10	0.05	17,37,22
32	4.00	4.12	3.88	5.517e+06	273.36	3.00	0.14	0.10	0.05	17,37,22
638	4.00	4.12	3.88	5.517e+06	273.36	3.00	0.14	0.10	0.05	17,37,22
645	4.00	4.12	3.88	5.517e+06	273.36	3.00	0.14	0.10	0.05	17,37,22
652	4.00	4.12	3.88	5.517e+06	273.36	3.00	0.14	0.10	0.05	17,37,22
874	4.00	4.12	3.88	5.517e+06	273.36	3.00	0.14	0.10	0.05	17,37,22
877	3.91	4.01	3.59	5.404e+06	273.36	2.77	0.12	0.10	0.03	17,39,24
878	4.00	4.12	3.88	5.517e+06	273.36	3.00	0.14	0.10	0.05	17,37,22
879	3.75	3.83	3.42	5.204e+06	273.36	2.64	0.09	0.10	0.05	17,39,16
880	4.00	4.12	3.88	5.517e+06	273.36	3.00	0.14	0.10	0.05	17,37,22
881	3.60	3.65	3.35	5.001e+06	273.36	2.58	0.06	0.10	0.08	17,39,26
882	3.91	4.01	3.59	5.404e+06	273.36	2.77	0.12	0.10	0.03	17,39,24
883	3.21	3.46	3.16	4.502e+06	273.36	2.44	0.04	0.09	0.11	42,39,26
884	3.75	3.83	3.42	5.204e+06	273.36	2.64	0.09	0.10	0.05	17,39,16
885	3.00	3.23	3.16	4.221e+06	273.36	2.44	0.04	0.09	0.11	36,39,26
887	2.95	2.92	2.85	4.156e+06	273.36	2.20	0.03	0.08	0.09	37,39,26
893	3.60	3.65	3.35	5.001e+06	273.36	2.58	0.06	0.10	0.08	17,39,26
894	3.21	3.46	3.16	4.502e+06	273.36	2.44	0.04	0.09	0.11	42,39,26
895	3.00	3.23	3.16	4.221e+06	273.36	2.44	0.04	0.09	0.11	36,39,26
896	2.95	2.92	2.85	4.156e+06	273.36	2.20	0.03	0.08	0.09	37,39,26
903	4.00	4.12	3.88	5.517e+06	273.36	3.00	0.14	0.10	0.05	17,37,22
904	4.00	4.12	3.88	5.517e+06	273.36	3.00	0.14	0.10	0.05	17,37,22
905	4.00	4.12	3.88	5.517e+06	273.36	3.00	0.14	0.10	0.05	17,37,22
906	3.91	4.01	3.59	5.404e+06	273.36	2.77	0.12	0.10	0.03	17,39,24
907	3.91	4.01	3.59	5.404e+06	273.36	2.77	0.12	0.10	0.03	17,39,24
908	3.75	3.83	3.42	5.204e+06	273.36	2.64	0.09	0.10	0.05	17,39,16
909	3.75	3.83	3.42	5.204e+06	273.36	2.64	0.09	0.10	0.05	17,39,16
910	3.60	3.65	3.35	5.001e+06	273.36	2.58	0.06	0.10	0.08	17,39,26
911	3.60	3.65	3.35	5.001e+06	273.36	2.58	0.06	0.10	0.08	17,39,26
912	3.21	3.46	3.16	4.502e+06	273.36	2.44	0.04	0.09	0.11	42,39,26
913	3.21	3.46	3.16	4.502e+06	273.36	2.44	0.04	0.09	0.11	42,39,26
914	3.00	3.23	3.16	4.221e+06	273.36	2.44	0.04	0.09	0.11	36,39,26
915	3.00	3.23	3.16	4.221e+06	273.36	2.44	0.04	0.09	0.11	36,39,26
916	2.95	2.92	2.85	4.156e+06	273.36	2.20	0.03	0.08	0.09	37,39,26
917	2.95	2.92	2.85	4.156e+06	273.36	2.20	0.03	0.08	0.09	37,39,26
1124	4.00	4.12	3.88	5.517e+06	273.36	3.00	0.14	0.10	0.05	17,37,22
1130	3.91	4.01	3.59	5.404e+06	273.36	2.77	0.12	0.10	0.03	17,39,24
1131	3.75	3.83	3.42	5.204e+06	273.36	2.64	0.09	0.10	0.05	17,39,16
1132	3.60	3.65	3.35	5.001e+06	273.36	2.58	0.06	0.10	0.08	17,39,26
1133	3.21	3.46	3.16	4.502e+06	273.36	2.44	0.04	0.09	0.11	42,39,26
1139	3.00	3.23	3.16	4.221e+06	273.36	2.44	0.04	0.09	0.11	36,39,26
1140	2.95	2.92	2.85	4.156e+06	273.36	2.20	0.03	0.08	0.09	37,39,26
1259	4.00	4.12	3.88	5.517e+06	273.36	3.00	0.14	0.10	0.05	17,37,22
1260	3.91	4.01	3.59	5.404e+06	273.36	2.77	0.12	0.10	0.03	17,39,24
1261	3.75	3.83	3.42	5.204e+06	273.36	2.64	0.09	0.10	0.05	17,39,16
1262	3.60	3.65	3.35	5.001e+06	273.36	2.58	0.06	0.10	0.08	17,39,26
1263	3.21	3.46	3.16	4.502e+06	273.36	2.44	0.04	0.09	0.11	42,39,26
1264	3.00	3.23	3.16	4.221e+06	273.36	2.44	0.04	0.09	0.11	36,39,26
1265	2.95	2.92	2.85	4.156e+06	273.36	2.20	0.03	0.08	0.09	37,39,26
1268	4.00	4.12	3.88	5.517e+06	273.36	3.00	0.14	0.10	0.05	17,37,22
1269	3.91	4.01	3.59	5.404e+06	273.36	2.77	0.12	0.10	0.03	17,39,24
1270	3.75	3.83	3.42	5.204e+06	273.36	2.64	0.09	0.10	0.05	17,39,16
1271	3.60	3.65	3.35	5.001e+06	273.36	2.58	0.06	0.10	0.08	17,39,26
1272	3.21	3.46	3.16	4.502e+06	273.36	2.44	0.04	0.09	0.11	42,39,26
1273	3.00	3.23	3.16	4.221e+06	273.36	2.44	0.04	0.09	0.11	36,39,26
1274	2.95	2.92	2.85	4.156e+06	273.36	2.20	0.03	0.08	0.09	37,39,26
1277	4.00	4.12	3.88	5.517e+06	273.36	3.00	0.14	0.10	0.05	17,37,22
1278	3.91	4.01	3.59	5.404e+06	273.36	2.77	0.12	0.10	0.03	17,39,24
1279	3.75	3.83	3.42	5.204e+06	273.36	2.64	0.09	0.10	0.05	17,39,16
1280	3.60	3.65	3.35	5.001e+06	273.36	2.58	0.06	0.10	0.08	17,39,26
1281	3.21	3.46	3.16	4.502e+06	273.36	2.44	0.04	0.09	0.11	42,39,26
1282	3.00	3.23	3.16	4.221e+06	273.36	2.44	0.04	0.09	0.11	36,39,26
1283	2.95	2.92	2.85	4.156e+06	273.36	2.20	0.03	0.08	0.09	37,39,26
Nodo	P / A	P / A	P / A.3	Mu 4.156e+06	b (h/l) 273.36	tc 2.20	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	

4.00 4.12 3.88 5.517e+06 273.36 3.00 0.14 0.10 0.11

Setto	Mat.	Spessore	Stato
		cm	
44	muratura E = 1.024e+05	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
875	2.20	2.20	2.01	3.148e+06	273.36	1.55	0.07	0.07	0.02	39,39,36
876	2.20	2.20	2.01	3.148e+06	273.36	1.55	0.07	0.07	0.02	39,39,36
887	2.55	2.51	2.53	3.627e+06	273.36	1.95	0.05	0.07	0.02	37,39,21
889	2.20	2.20	2.01	3.148e+06	273.36	1.55	0.07	0.07	0.02	39,39,36
891	2.20	2.20	2.01	3.148e+06	273.36	1.55	0.07	0.07	0.02	39,39,36
896	2.55	2.51	2.53	3.627e+06	273.36	1.95	0.05	0.07	0.02	37,39,21
897	2.20	2.20	2.01	3.148e+06	273.36	1.55	0.07	0.07	0.02	39,39,36
898	2.20	2.20	2.01	3.148e+06	273.36	1.55	0.07	0.07	0.02	39,39,36
916	2.55	2.51	2.53	3.627e+06	273.36	1.95	0.05	0.07	0.02	37,39,21
917	2.55	2.51	2.53	3.627e+06	273.36	1.95	0.05	0.07	0.02	37,39,21
918	2.20	2.20	2.01	3.148e+06	273.36	1.55	0.07	0.07	0.02	39,39,36
919	2.20	2.20	2.01	3.148e+06	273.36	1.55	0.07	0.07	0.02	39,39,36
1140	2.55	2.51	2.53	3.627e+06	273.36	1.95	0.05	0.07	0.02	37,39,21
1141	2.20	2.20	2.01	3.148e+06	273.36	1.55	0.07	0.07	0.02	39,39,36
1142	2.20	2.20	2.01	3.148e+06	273.36	1.55	0.07	0.07	0.02	39,39,36
1265	2.55	2.51	2.53	3.627e+06	273.36	1.95	0.05	0.07	0.02	37,39,21
1266	2.20	2.20	2.01	3.148e+06	273.36	1.55	0.07	0.07	0.02	39,39,36
1267	2.20	2.20	2.01	3.148e+06	273.36	1.55	0.07	0.07	0.02	39,39,36
1274	2.55	2.51	2.53	3.627e+06	273.36	1.95	0.05	0.07	0.02	37,39,21
1275	2.20	2.20	2.01	3.148e+06	273.36	1.55	0.07	0.07	0.02	39,39,36
1276	2.20	2.20	2.01	3.148e+06	273.36	1.55	0.07	0.07	0.02	39,39,36
1283	2.55	2.51	2.53	3.627e+06	273.36	1.95	0.05	0.07	0.02	37,39,21
1284	2.20	2.20	2.01	3.148e+06	273.36	1.55	0.07	0.07	0.02	39,39,36
1285	2.20	2.20	2.01	3.148e+06	273.36	1.55	0.07	0.07	0.02	39,39,36

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				3.148e+06	273.36	1.55			
	2.55	2.51	2.53	3.627e+06	273.36	1.95	0.07	0.07	0.02

Setto	Mat.	Spessore	Stato
		cm	
45	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
2	1.22	1.22	1.28	5.023e+04	46.00	1.03	0.17	0.13	0.07	26,26,17
16	1.22	1.22	1.28	5.023e+04	46.00	1.03	0.17	0.13	0.07	26,26,17
903	1.22	1.45	1.28	5.023e+04	46.00	1.03	0.17	0.15	0.07	26,26,17
906	1.91	1.45	1.70	7.777e+04	46.00	1.37	0.06	0.15	0.03	23,26,37
908	2.19	2.26	2.15	8.850e+04	46.00	1.73	0.06	0.15	9.70e-03	16,25,34
910	2.68	2.68	2.56	1.074e+05	46.00	2.06	0.11	0.20	0.02	26,26,30
912	3.36	3.36	2.56	1.325e+05	46.00	2.06	0.25	0.37	0.02	26,26,30
914	3.36	3.15	3.15	1.325e+05	46.00	2.53	0.25	0.51	0.02	26,25,30
916	3.10	3.15	3.14	1.230e+05	46.00	2.52	0.21	0.51	4.05e-03	26,25,13
920	1.22	1.45	1.28	5.023e+04	46.00	1.03	0.17	0.15	0.07	26,26,17
922	1.91	1.45	1.70	7.777e+04	46.00	1.37	0.06	0.15	0.03	23,26,37
923	2.19	2.26	2.15	8.850e+04	46.00	1.73	0.06	0.15	9.70e-03	16,25,34
924	2.68	2.68	2.56	1.074e+05	46.00	2.06	0.11	0.20	0.02	26,26,30
925	3.36	3.36	2.56	1.325e+05	46.00	2.06	0.25	0.37	0.02	26,26,30
926	3.36	3.15	3.15	1.325e+05	46.00	2.53	0.25	0.51	0.02	26,25,30
927	3.10	3.15	3.14	1.230e+05	46.00	2.52	0.21	0.51	4.05e-03	26,25,13

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				5.023e+04	46.00	1.03			
	3.36	3.36	3.15	1.325e+05	46.00	2.53	0.25	0.51	0.07

Setto	Mat.	Spessore	Stato
		cm	
46	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
875	2.48	2.72	2.71	9.978e+04	46.00	2.18	0.03	0.65	7.54e-03	40,17,37
916	2.32	2.34	2.33	9.356e+04	46.00	1.88	0.02	0.60	0.01	18,37,33
918	2.48	2.72	2.33	9.978e+04	46.00	1.88	0.03	0.65	0.01	40,17,33
927	2.32	2.34	2.33	9.356e+04	46.00	1.88	0.02	0.60	0.01	18,37,33
928	2.48	2.72	2.33	9.978e+04	46.00	1.88	0.03	0.65	0.01	40,17,33
929	2.48	2.72	2.71	9.978e+04	46.00	2.18	0.03	0.65	7.54e-03	40,17,37

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				9.356e+04	46.00	1.88			
	2.48	2.72	2.71	9.978e+04	46.00	2.18	0.03	0.65	0.01

Setto	Mat.	Spessore	Stato
		cm	
49	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
3	3.52	3.52	3.72	2.679e+05	64.00	2.99	0.12	0.10	0.02	20,20,27
21	3.52	3.52	3.72	2.679e+05	64.00	2.99	0.12	0.10	0.02	20,20,27
653	3.52	3.42	3.58	2.679e+05	64.00	2.88	0.12	0.11	0.03	20,20,27
656	3.25	3.58	3.58	2.488e+05	64.00	2.88	0.07	0.12	0.03	18,20,27
658	3.31	3.78	3.65	2.534e+05	64.00	2.94	0.08	0.13	0.01	14,20,27
660	3.78	4.04	3.61	2.863e+05	64.00	2.90	0.10	0.15	0.01	32,20,30
662	4.30	4.30	3.61	3.217e+05	64.00	2.90	0.17	0.19	0.01	24,20,30
664	4.30	3.82	3.43	3.217e+05	64.00	2.76	0.17	0.31	0.02	24,20,34
666	3.82	3.82	3.43	2.892e+05	64.00	2.76	0.11	0.31	0.02	24,20,34
930	3.78	4.04	3.61	2.863e+05	64.00	2.90	0.10	0.15	0.01	32,20,30
931	4.30	4.30	3.61	3.217e+05	64.00	2.90	0.17	0.19	0.01	24,20,30
932	4.30	3.82	3.43	3.217e+05	64.00	2.76	0.17	0.31	0.02	24,20,34
933	3.82	3.82	3.43	2.892e+05	64.00	2.76	0.11	0.31	0.02	24,20,34
1042	3.52	3.42	3.58	2.679e+05	64.00	2.88	0.12	0.11	0.03	20,20,27
1043	3.25	3.58	3.58	2.488e+05	64.00	2.88	0.07	0.12	0.03	18,20,27
1044	3.31	3.78	3.65	2.534e+05	64.00	2.94	0.08	0.13	0.01	14,20,27

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				2.488e+05	64.00	2.76			
	4.30	4.30	3.72	3.217e+05	64.00	2.99	0.17	0.31	0.03

Setto	Mat.	Spessore	Stato
		cm	
52	muratura E = 2.000e+04 mattoni in argilla espansa e cls con malta M2	30.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
684	0.59	0.68	0.59	1.490e+06	416.00	0.83	0.16	0.07	0.11	30,20,34
723	0.59	0.68	0.59	1.490e+06	416.00	0.83	0.16	0.07	0.11	30,20,34
733	0.59	0.68	0.59	1.490e+06	416.00	0.83	0.16	0.07	0.11	30,20,34
743	0.59	0.68	0.59	1.490e+06	416.00	0.83	0.16	0.07	0.11	30,20,34
752	0.59	0.68	0.59	1.490e+06	416.00	0.83	0.16	0.07	0.11	30,20,34
761	0.59	0.68	0.59	1.490e+06	416.00	0.83	0.16	0.07	0.11	30,20,34
771	0.59	0.68	0.59	1.490e+06	416.00	0.83	0.16	0.07	0.11	30,20,34
780	0.59	0.68	0.59	1.490e+06	416.00	0.83	0.16	0.07	0.11	30,20,34
839	0.59	0.68	0.59	1.490e+06	416.00	0.83	0.16	0.07	0.11	30,20,34
2264	0.70	0.65	0.73	6.484e+05	416.00	1.03	0.15	0.07	0.06	27,21,33
2274	0.54	0.68	0.59	1.377e+06	416.00	0.83	0.19	0.07	0.11	30,20,34
2281	0.54	0.63	0.54	1.377e+06	416.00	0.77	0.19	0.07	0.08	30,20,34

2282	0.78	0.72	0.59	7.154e+05	416.00	0.84	0.16	0.05	0.08	33,21,30
2283	0.78	0.68	0.72	7.154e+05	416.00	1.02	0.16	0.06	0.07	33,21,30
2444	0.54	0.68	0.59	1.377e+06	416.00	0.83	0.19	0.07	0.11	30,20,34
2445	0.54	0.68	0.59	1.377e+06	416.00	0.83	0.19	0.07	0.11	30,20,34
2446	0.54	0.63	0.54	1.377e+06	416.00	0.77	0.19	0.07	0.08	30,20,34
2447	0.54	0.63	0.54	1.377e+06	416.00	0.77	0.19	0.07	0.08	30,20,34
2448	0.78	0.72	0.59	7.154e+05	416.00	0.84	0.16	0.05	0.08	33,21,30
2449	0.78	0.72	0.59	7.154e+05	416.00	0.84	0.16	0.05	0.08	33,21,30
2450	0.78	0.68	0.72	7.154e+05	416.00	1.02	0.16	0.06	0.07	33,21,30
2451	0.78	0.68	0.72	7.154e+05	416.00	1.02	0.16	0.06	0.07	33,21,30
2452	0.70	0.65	0.73	6.484e+05	416.00	1.03	0.15	0.07	0.06	27,21,33
2453	0.70	0.65	0.73	6.484e+05	416.00	1.03	0.15	0.07	0.06	27,21,33
2454	0.54	0.68	0.59	1.377e+06	416.00	0.83	0.19	0.07	0.11	30,20,34
2455	0.78	0.68	0.72	7.154e+05	416.00	1.02	0.16	0.06	0.07	33,21,30
2456	0.70	0.65	0.73	6.484e+05	416.00	1.03	0.15	0.07	0.06	27,21,33
2457	0.78	0.68	0.72	7.154e+05	416.00	1.02	0.16	0.06	0.07	33,21,30
2458	0.70	0.65	0.73	6.484e+05	416.00	1.03	0.15	0.07	0.06	27,21,33
2459	0.54	0.68	0.59	1.377e+06	416.00	0.83	0.19	0.07	0.11	30,20,34
2460	0.54	0.63	0.54	1.377e+06	416.00	0.77	0.19	0.07	0.08	30,20,34
2461	0.78	0.72	0.59	7.154e+05	416.00	0.84	0.16	0.05	0.08	33,21,30
2462	0.78	0.68	0.72	7.154e+05	416.00	1.02	0.16	0.06	0.07	33,21,30
2463	0.70	0.65	0.73	6.484e+05	416.00	1.03	0.15	0.07	0.06	27,21,33
2464	0.54	0.68	0.59	1.377e+06	416.00	0.83	0.19	0.07	0.11	30,20,34
2465	0.54	0.63	0.54	1.377e+06	416.00	0.77	0.19	0.07	0.08	30,20,34
2466	0.78	0.72	0.59	7.154e+05	416.00	0.84	0.16	0.05	0.08	33,21,30
2467	0.78	0.68	0.72	7.154e+05	416.00	1.02	0.16	0.06	0.07	33,21,30
2468	0.70	0.65	0.73	6.484e+05	416.00	1.03	0.15	0.07	0.06	27,21,33
2469	0.54	0.68	0.59	1.377e+06	416.00	0.83	0.19	0.07	0.11	30,20,34
2470	0.54	0.63	0.54	1.377e+06	416.00	0.77	0.19	0.07	0.08	30,20,34
2474	0.54	0.68	0.59	1.377e+06	416.00	0.83	0.19	0.07	0.11	30,20,34
2475	0.54	0.63	0.54	1.377e+06	416.00	0.77	0.19	0.07	0.08	30,20,34
2478	0.63	0.59	0.68	5.825e+05	416.00	0.96	0.23	0.08	0.06	31,21,33
2479	0.54	0.68	0.59	1.377e+06	416.00	0.83	0.19	0.07	0.11	30,20,34
2480	0.54	0.63	0.54	1.377e+06	416.00	0.77	0.19	0.07	0.08	30,20,34
2481	0.78	0.72	0.59	7.154e+05	416.00	0.84	0.16	0.05	0.08	33,21,30
2487	0.63	0.59	0.68	5.825e+05	416.00	0.96	0.23	0.08	0.06	31,21,33
2489	0.63	0.38	0.40	5.825e+05	416.00	0.57	0.23	0.08	0.04	31,21,30
2491	0.40	0.38	0.40	6.563e+05	416.00	0.57	0.14	0.08	0.04	27,21,30
3335	0.63	0.59	0.68	5.825e+05	416.00	0.96	0.23	0.08	0.06	31,21,33
3336	0.63	0.38	0.40	5.825e+05	416.00	0.57	0.23	0.08	0.04	31,21,30
3337	0.40	0.38	0.40	6.563e+05	416.00	0.57	0.14	0.08	0.04	27,21,30
3339	0.54	0.63	0.54	1.377e+06	416.00	0.77	0.19	0.07	0.08	30,20,34
3340	0.78	0.72	0.59	7.154e+05	416.00	0.84	0.16	0.05	0.08	33,21,30
3341	0.63	0.59	0.68	5.825e+05	416.00	0.96	0.23	0.08	0.06	31,21,33
3342	0.63	0.38	0.40	5.825e+05	416.00	0.57	0.23	0.08	0.04	31,21,30
3343	0.40	0.38	0.40	6.563e+05	416.00	0.57	0.14	0.08	0.04	27,21,30
3345	0.63	0.59	0.68	5.825e+05	416.00	0.96	0.23	0.08	0.06	31,21,33
3346	0.63	0.38	0.40	5.825e+05	416.00	0.57	0.23	0.08	0.04	31,21,30
3347	0.40	0.38	0.40	6.563e+05	416.00	0.57	0.14	0.08	0.04	27,21,30
3349	0.63	0.38	0.40	5.825e+05	416.00	0.57	0.23	0.08	0.04	31,21,30
3350	0.40	0.38	0.40	6.563e+05	416.00	0.57	0.14	0.08	0.04	27,21,30
3351	0.40	0.38	0.40	6.563e+05	416.00	0.57	0.14	0.08	0.04	27,21,30
3353	0.40	0.38	0.40	6.563e+05	416.00	0.57	0.14	0.08	0.04	27,21,30
3354	0.40	0.38	0.40	6.563e+05	416.00	0.57	0.14	0.08	0.04	27,21,30
3355	0.40	0.38	0.40	6.563e+05	416.00	0.57	0.14	0.08	0.04	27,21,30
3357	0.63	0.59	0.68	5.825e+05	416.00	0.96	0.23	0.08	0.06	31,21,33
3358	0.63	0.38	0.40	5.825e+05	416.00	0.57	0.23	0.08	0.04	31,21,30
3359	0.40	0.38	0.40	6.563e+05	416.00	0.57	0.14	0.08	0.04	27,21,30
3361	0.63	0.59	0.68	5.825e+05	416.00	0.96	0.23	0.08	0.06	31,21,33
3362	0.63	0.38	0.40	5.825e+05	416.00	0.57	0.23	0.08	0.04	31,21,30
3363	0.40	0.38	0.40	6.563e+05	416.00	0.57	0.14	0.08	0.04	27,21,30
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	0.78	0.72	0.73	5.825e+05	416.00	0.57				
				1.490e+06	416.00	1.03	0.23	0.08	0.11	

Setto	Mat.	Spessore	Stato
		cm	
53	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				

666	2.56	2.94	2.74	1.986e+05	64.00	2.20	0.04	0.48	0.04	25,20,34
668	2.54	2.81	2.74	1.974e+05	64.00	2.20	0.04	0.57	0.04	33,20,34
670	2.54	2.81	2.64	1.974e+05	64.00	2.12	0.04	0.57	0.04	33,20,30
933	2.56	2.94	2.74	1.986e+05	64.00	2.20	0.04	0.48	0.04	25,20,34
934	2.54	2.81	2.74	1.974e+05	64.00	2.20	0.04	0.57	0.04	33,20,34
935	2.54	2.81	2.64	1.974e+05	64.00	2.12	0.04	0.57	0.04	33,20,30

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				1.974e+05	64.00	2.12			
	2.56	2.94	2.74	1.986e+05	64.00	2.20	0.04	0.57	0.04

Setto	Mat.	Spessore	Stato
		cm	
54	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
19	4.47	4.47	3.95	8.850e+05	104.29	3.18	0.04	0.07	0.20	25,25,31
585	4.47	4.47	3.95	8.850e+05	104.29	3.18	0.04	0.07	0.20	25,25,31
592	4.47	4.47	3.95	8.850e+05	104.29	3.18	0.04	0.07	0.20	25,25,31
967	4.47	4.47	3.95	8.850e+05	104.29	3.18	0.04	0.07	0.20	25,25,31
968	4.53	3.93	4.07	8.947e+05	104.29	3.27	0.03	0.11	0.15	25,19,31
969	4.34	3.99	4.18	8.619e+05	104.29	3.36	0.03	0.13	0.10	21,24,31
970	4.21	4.15	4.27	8.382e+05	104.29	3.43	0.05	0.16	0.07	35,23,29
971	4.28	4.28	4.21	8.504e+05	104.29	3.38	0.09	0.18	0.03	23,23,31
972	4.28	3.98	3.81	8.504e+05	104.29	3.07	0.09	0.24	0.04	23,23,32
973	3.98	3.98	3.81	7.965e+05	104.29	3.07	0.05	0.24	0.04	23,23,32
976	4.47	4.47	3.95	8.850e+05	104.29	3.18	0.04	0.07	0.20	25,25,31
977	4.53	3.93	4.07	8.947e+05	104.29	3.27	0.03	0.11	0.15	25,19,31
978	4.34	3.99	4.18	8.619e+05	104.29	3.36	0.03	0.13	0.10	21,24,31
979	4.21	4.15	4.27	8.382e+05	104.29	3.43	0.05	0.16	0.07	35,23,29
980	4.28	4.28	4.21	8.504e+05	104.29	3.38	0.09	0.18	0.03	23,23,31
981	4.28	3.98	3.81	8.504e+05	104.29	3.07	0.09	0.24	0.04	23,23,32
982	3.98	3.98	3.81	7.965e+05	104.29	3.07	0.05	0.24	0.04	23,23,32
985	4.47	4.47	3.95	8.850e+05	104.29	3.18	0.04	0.07	0.20	25,25,31
986	4.53	3.93	4.07	8.947e+05	104.29	3.27	0.03	0.11	0.15	25,19,31
987	4.34	3.99	4.18	8.619e+05	104.29	3.36	0.03	0.13	0.10	21,24,31
988	4.21	4.15	4.27	8.382e+05	104.29	3.43	0.05	0.16	0.07	35,23,29
989	4.28	4.28	4.21	8.504e+05	104.29	3.38	0.09	0.18	0.03	23,23,31
990	4.28	3.98	3.81	8.504e+05	104.29	3.07	0.09	0.24	0.04	23,23,32
991	3.98	3.98	3.81	7.965e+05	104.29	3.07	0.05	0.24	0.04	23,23,32
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				7.965e+05	104.29	3.07				
	4.53	4.47	4.27	8.947e+05	104.29	3.43	0.09	0.24	0.20	

Setto	Mat.	Spessore	Stato
		cm	
55	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
973	3.16	3.45	3.30	6.431e+05	104.29	2.66	0.05	0.24	0.08	18,23,33
974	3.02	3.45	3.16	6.175e+05	104.29	2.54	0.06	0.24	0.11	14,23,33
975	3.02	3.30	3.16	6.175e+05	104.29	2.54	0.06	0.15	0.11	14,23,33
982	3.16	3.45	3.30	6.431e+05	104.29	2.66	0.05	0.24	0.08	18,23,33
983	3.02	3.45	3.16	6.175e+05	104.29	2.54	0.06	0.24	0.11	14,23,33
984	3.02	3.30	3.16	6.175e+05	104.29	2.54	0.06	0.15	0.11	14,23,33
991	3.16	3.45	3.30	6.431e+05	104.29	2.66	0.05	0.24	0.08	18,23,33
992	3.02	3.45	3.16	6.175e+05	104.29	2.54	0.06	0.24	0.11	14,23,33
993	3.02	3.30	3.16	6.175e+05	104.29	2.54	0.06	0.15	0.11	14,23,33
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				6.175e+05	104.29	2.54				
	3.16	3.45	3.30	6.431e+05	104.29	2.66	0.06	0.24	0.11	

Setto	Mat.	Spessore	Stato
		cm	
58	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
20	4.54	4.49	4.04	8.437e+05	101.14	3.25	0.07	0.04	0.16	23,24,29
557	4.54	4.49	4.04	8.437e+05	101.14	3.25	0.07	0.04	0.16	23,24,29
564	4.54	4.49	4.04	8.437e+05	101.14	3.25	0.07	0.04	0.16	23,24,29
1012	4.54	3.81	4.04	8.437e+05	104.29	3.25	0.07	0.06	0.16	23,25,29
1013	4.60	3.96	4.14	9.085e+05	104.29	3.33	0.05	0.08	0.13	23,25,29
1014	4.37	4.00	4.21	8.668e+05	104.29	3.39	0.03	0.10	0.09	23,25,29
1015	4.08	4.08	4.17	8.150e+05	104.29	3.35	0.04	0.13	0.06	21,25,29
1016	4.16	4.16	3.99	8.290e+05	104.29	3.21	0.08	0.15	0.03	21,21,28
1017	4.16	3.85	3.61	8.290e+05	104.29	2.90	0.08	0.20	0.04	21,21,32
1018	3.85	3.85	3.61	7.719e+05	104.29	2.90	0.04	0.20	0.04	21,21,32
1021	4.54	3.81	4.04	8.437e+05	104.29	3.25	0.07	0.06	0.16	23,25,29
1023	4.60	3.96	4.14	9.085e+05	104.29	3.33	0.05	0.08	0.13	23,25,29
1024	4.37	4.00	4.21	8.668e+05	104.29	3.39	0.03	0.10	0.09	23,25,29
1025	4.08	4.08	4.17	8.150e+05	104.29	3.35	0.04	0.13	0.06	21,25,29
1026	4.16	4.16	3.99	8.290e+05	104.29	3.21	0.08	0.15	0.03	21,21,28
1027	4.16	3.85	3.61	8.290e+05	104.29	2.90	0.08	0.20	0.04	21,21,32
1028	3.85	3.85	3.61	7.719e+05	104.29	2.90	0.04	0.20	0.04	21,21,32
1031	4.54	3.81	4.04	8.437e+05	104.29	3.25	0.07	0.06	0.16	23,25,29
1032	4.60	3.96	4.14	9.085e+05	104.29	3.33	0.05	0.08	0.13	23,25,29
1033	4.37	4.00	4.21	8.668e+05	104.29	3.39	0.03	0.10	0.09	23,25,29
1034	4.08	4.08	4.17	8.150e+05	104.29	3.35	0.04	0.13	0.06	21,25,29
1035	4.16	4.16	3.99	8.290e+05	104.29	3.21	0.08	0.15	0.03	21,21,28
1036	4.16	3.85	3.61	8.290e+05	104.29	2.90	0.08	0.20	0.04	21,21,32
1037	3.85	3.85	3.61	7.719e+05	104.29	2.90	0.04	0.20	0.04	21,21,32

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				7.719e+05	101.14	2.90			
	4.60	4.49	4.21	9.085e+05	104.29	3.39	0.08	0.20	0.16

Setto	Mat.	Spessore	Stato
		cm	
59	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
1018	3.10	3.37	3.15	9.889e+05	104.29	2.53	0.05	0.27	0.08	20,25,32
1019	3.11	3.37	3.10	1.145e+06	104.29	2.50	0.06	0.27	0.11	11,25,28
1020	3.11	3.31	3.10	1.145e+06	122.76	2.50	0.06	0.16	0.11	11,25,28
1028	3.10	3.37	3.15	9.889e+05	104.29	2.53	0.05	0.27	0.08	20,25,32
1029	3.12	3.37	3.11	1.215e+06	104.29	2.50	0.05	0.27	0.10	11,25,28
1030	3.12	3.32	3.11	1.215e+06	118.14	2.50	0.05	0.19	0.10	11,25,28
1037	3.10	3.37	3.15	9.889e+05	104.29	2.53	0.05	0.27	0.08	20,25,32
1038	3.12	3.37	3.11	1.215e+06	104.29	2.50	0.05	0.27	0.10	11,25,28
1039	3.12	3.32	3.11	1.215e+06	118.14	2.50	0.05	0.19	0.10	11,25,28
2425	3.11	3.32	3.10	1.145e+06	118.14	2.50	0.06	0.19	0.11	11,25,28

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				9.889e+05	104.29	2.50			
	3.12	3.37	3.15	1.215e+06	122.76	2.53	0.06	0.27	0.11

Setto	Mat.	Spessore	Stato
		cm	
61	Tamponatura 1100 daN/mc per elemento pannello	20.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
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28	1.36	1.42	1.27	1.323e+06	323.00	1.22	0.10	0.18	7.42e-03	39,21,23
29	1.36	1.42	1.27	1.323e+06	323.00	1.22	0.10	0.18	7.42e-03	39,21,23
481	1.30	1.39	1.37	1.273e+06	323.00	1.31	0.09	0.16	0.03	36,25,37
727	1.25	1.40	1.20	1.229e+06	323.00	1.15	0.10	0.19	0.02	23,21,20
728	1.23	1.36	1.21	1.203e+06	323.00	1.16	0.10	0.19	0.03	23,21,23
729	1.21	1.33	1.30	1.189e+06	323.00	1.25	0.10	0.18	0.04	23,21,37
730	1.19	1.32	1.31	1.171e+06	323.00	1.26	0.09	0.18	0.05	20,25,37
737	1.30	1.33	1.31	1.273e+06	323.00	1.26	0.09	0.17	0.05	36,25,37
738	1.30	1.39	1.37	1.273e+06	323.00	1.31	0.09	0.16	0.03	36,25,37
766	1.36	1.40	1.22	1.323e+06	323.00	1.17	0.10	0.19	0.02	39,21,24
1047	1.36	1.40	1.22	1.323e+06	323.00	1.17	0.10	0.19	0.02	39,21,24
1048	1.36	1.40	1.22	1.323e+06	323.00	1.17	0.10	0.19	0.02	39,21,24
1049	1.36	1.42	1.27	1.323e+06	323.00	1.22	0.10	0.18	7.42e-03	39,21,23
1050	1.25	1.40	1.20	1.229e+06	323.00	1.15	0.10	0.19	0.02	23,21,20
1051	1.25	1.40	1.20	1.229e+06	323.00	1.15	0.10	0.19	0.02	23,21,20
1052	1.23	1.36	1.21	1.203e+06	323.00	1.16	0.10	0.19	0.03	23,21,23
1053	1.23	1.36	1.21	1.203e+06	323.00	1.16	0.10	0.19	0.03	23,21,23
1054	1.21	1.33	1.30	1.189e+06	323.00	1.25	0.10	0.18	0.04	23,21,37
1055	1.21	1.33	1.30	1.189e+06	323.00	1.25	0.10	0.18	0.04	23,21,37
1056	1.19	1.32	1.31	1.171e+06	323.00	1.26	0.09	0.18	0.05	20,25,37
1057	1.19	1.32	1.31	1.171e+06	323.00	1.26	0.09	0.18	0.05	20,25,37
1058	1.30	1.33	1.31	1.273e+06	323.00	1.26	0.09	0.17	0.05	36,25,37
1059	1.30	1.33	1.31	1.273e+06	323.00	1.26	0.09	0.17	0.05	36,25,37
1060	1.30	1.39	1.37	1.273e+06	323.00	1.31	0.09	0.16	0.03	36,25,37
1061	1.30	1.39	1.37	1.273e+06	323.00	1.31	0.09	0.16	0.03	36,25,37
1066	1.36	1.40	1.22	1.323e+06	323.00	1.17	0.10	0.19	0.02	39,21,24
1067	1.36	1.42	1.27	1.323e+06	323.00	1.22	0.10	0.18	7.42e-03	39,21,23
1068	1.25	1.40	1.20	1.229e+06	323.00	1.15	0.10	0.19	0.02	23,21,20
1069	1.23	1.36	1.21	1.203e+06	323.00	1.16	0.10	0.19	0.03	23,21,23
1070	1.21	1.33	1.30	1.189e+06	323.00	1.25	0.10	0.18	0.04	23,21,37
1071	1.19	1.32	1.31	1.171e+06	323.00	1.26	0.09	0.18	0.05	20,25,37
1072	1.30	1.33	1.31	1.273e+06	323.00	1.26	0.09	0.17	0.05	36,25,37
1073	1.30	1.39	1.37	1.273e+06	323.00	1.31	0.09	0.16	0.03	36,25,37
1076	1.36	1.40	1.22	1.323e+06	323.00	1.17	0.10	0.19	0.02	39,21,24
1077	1.36	1.42	1.27	1.323e+06	323.00	1.22	0.10	0.18	7.42e-03	39,21,23
1078	1.25	1.40	1.20	1.229e+06	323.00	1.15	0.10	0.19	0.02	23,21,20
1079	1.23	1.36	1.21	1.203e+06	323.00	1.16	0.10	0.19	0.03	23,21,23
1080	1.21	1.33	1.30	1.189e+06	323.00	1.25	0.10	0.18	0.04	23,21,37
1081	1.19	1.32	1.31	1.171e+06	323.00	1.26	0.09	0.18	0.05	20,25,37
1082	1.30	1.33	1.31	1.273e+06	323.00	1.26	0.09	0.17	0.05	36,25,37
1083	1.30	1.39	1.37	1.273e+06	323.00	1.31	0.09	0.16	0.03	36,25,37
1086	1.36	1.40	1.22	1.323e+06	323.00	1.17	0.10	0.19	0.02	39,21,24
1087	1.36	1.42	1.27	1.323e+06	323.00	1.22	0.10	0.18	7.42e-03	39,21,23
1088	1.25	1.40	1.20	1.229e+06	323.00	1.15	0.10	0.19	0.02	23,21,20
1089	1.23	1.36	1.21	1.203e+06	323.00	1.16	0.10	0.19	0.03	23,21,23
1090	1.21	1.33	1.30	1.189e+06	323.00	1.25	0.10	0.18	0.04	23,21,37
1091	1.19	1.32	1.31	1.171e+06	323.00	1.26	0.09	0.18	0.05	20,25,37
1092	1.30	1.33	1.31	1.273e+06	323.00	1.26	0.09	0.17	0.05	36,25,37
1093	1.30	1.39	1.37	1.273e+06	323.00	1.31	0.09	0.16	0.03	36,25,37
1096	1.36	1.40	1.22	1.323e+06	323.00	1.17	0.10	0.19	0.02	39,21,24
1097	1.36	1.42	1.27	1.323e+06	323.00	1.22	0.10	0.18	7.42e-03	39,21,23
1098	1.25	1.40	1.20	1.229e+06	323.00	1.15	0.10	0.19	0.02	23,21,20
1099	1.23	1.36	1.21	1.203e+06	323.00	1.16	0.10	0.19	0.03	23,21,23
1100	1.21	1.33	1.30	1.189e+06	323.00	1.25	0.10	0.18	0.04	23,21,37
1101	1.19	1.32	1.31	1.171e+06	323.00	1.26	0.09	0.18	0.05	20,25,37
1102	1.30	1.33	1.31	1.273e+06	323.00	1.26	0.09	0.17	0.05	36,25,37

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				1.171e+06	323.00	1.15			
	1.36	1.42	1.37	1.323e+06	323.00	1.31	0.10	0.19	0.05

Setto	Mat.	Spessore	Stato
		cm	
62	Tamponatura 1100 daN/mc per elemento pannello	20.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
481	1.44	1.50	1.39	1.397e+06	323.00	1.33	0.09	0.15	0.03	42,21,12
738	1.44	1.50	1.39	1.397e+06	323.00	1.33	0.09	0.15	0.03	42,21,12
739	1.44	1.78	1.68	1.397e+06	323.00	1.61	0.09	0.16	0.11	42,21,15
740	1.71	1.78	1.68	1.639e+06	323.00	1.61	0.07	0.16	0.11	42,21,15
921	1.44	1.78	1.68	1.397e+06	323.00	1.61	0.09	0.16	0.11	42,21,15

1022	1.71	1.78	1.68	1.639e+06	323.00	1.61	0.07	0.16	0.11	42,21,15
1060	1.44	1.50	1.39	1.397e+06	323.00	1.33	0.09	0.15	0.03	42,21,12
1061	1.44	1.50	1.39	1.397e+06	323.00	1.33	0.09	0.15	0.03	42,21,12
1062	1.44	1.78	1.68	1.397e+06	323.00	1.61	0.09	0.16	0.11	42,21,15
1063	1.44	1.78	1.68	1.397e+06	323.00	1.61	0.09	0.16	0.11	42,21,15
1064	1.71	1.78	1.68	1.639e+06	323.00	1.61	0.07	0.16	0.11	42,21,15
1065	1.71	1.78	1.68	1.639e+06	323.00	1.61	0.07	0.16	0.11	42,21,15
1073	1.44	1.50	1.39	1.397e+06	323.00	1.33	0.09	0.15	0.03	42,21,12
1074	1.44	1.78	1.68	1.397e+06	323.00	1.61	0.09	0.16	0.11	42,21,15
1075	1.71	1.78	1.68	1.639e+06	323.00	1.61	0.07	0.16	0.11	42,21,15
1083	1.44	1.50	1.39	1.397e+06	323.00	1.33	0.09	0.15	0.03	42,21,12
1084	1.44	1.78	1.68	1.397e+06	323.00	1.61	0.09	0.16	0.11	42,21,15
1085	1.71	1.78	1.68	1.639e+06	323.00	1.61	0.07	0.16	0.11	42,21,15
1093	1.44	1.50	1.39	1.397e+06	323.00	1.33	0.09	0.15	0.03	42,21,12
1094	1.44	1.78	1.68	1.397e+06	323.00	1.61	0.09	0.16	0.11	42,21,15
1095	1.71	1.78	1.68	1.639e+06	323.00	1.61	0.07	0.16	0.11	42,21,15

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				1.397e+06	323.00	1.33			
	1.71	1.78	1.68	1.639e+06	323.00	1.61	0.09	0.16	0.11

Setto	Mat.	Spessore	Stato
		cm	
63	muratura E = 1.024e+05	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
37	4.13	4.38	4.12	3.415e+05	67.00	3.18	0.12	0.07	0.02	16,23,36
38	4.13	4.38	4.12	3.415e+05	67.00	3.18	0.12	0.07	0.02	16,23,36
1103	4.13	4.38	4.12	3.415e+05	67.00	3.18	0.12	0.07	0.02	16,23,36
1104	4.13	4.38	4.12	3.415e+05	67.00	3.18	0.12	0.07	0.02	16,23,36
1105	4.09	4.30	4.08	3.378e+05	67.00	3.15	0.10	0.06	0.01	16,23,36
1106	4.09	4.30	4.08	3.378e+05	67.00	3.15	0.10	0.06	0.01	16,23,36
1107	3.89	4.07	3.89	3.230e+05	67.00	3.00	0.06	0.05	8.40e-03	16,23,16
1108	3.89	4.07	3.89	3.230e+05	67.00	3.00	0.06	0.05	8.40e-03	16,23,16
1109	4.68	3.83	4.45	3.825e+05	67.00	3.44	0.05	0.05	4.26e-03	21,23,41
1110	4.68	3.83	4.45	3.825e+05	67.00	3.44	0.05	0.05	4.26e-03	21,23,41
1111	3.11	4.06	4.06	2.625e+05	67.00	3.14	0.08	0.06	0.01	20,26,26
1112	3.11	4.06	4.06	2.625e+05	67.00	3.14	0.08	0.06	0.01	20,26,26
1113	2.89	4.06	3.51	2.452e+05	67.00	2.71	0.15	0.06	0.02	20,26,22
1114	2.89	4.06	3.51	2.452e+05	67.00	2.71	0.15	0.06	0.02	20,26,22
1115	2.89	3.51	3.51	2.452e+05	67.00	2.71	0.15	0.04	0.02	20,26,22
1116	2.89	3.51	3.51	2.452e+05	67.00	2.71	0.15	0.04	0.02	20,26,22

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				2.452e+05	67.00	2.71			
	4.68	4.38	4.45	3.825e+05	67.00	3.44	0.15	0.07	0.02

Setto	Mat.	Spessore	Stato
		cm	
64	muratura E = 1.024e+05	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1115	3.43	3.19	3.43	2.873e+05	67.00	2.65	0.12	0.07	0.04	26,23,26
1116	3.43	3.19	3.43	2.873e+05	67.00	2.65	0.12	0.07	0.04	26,23,26
1117	3.85	3.71	3.67	3.197e+05	67.00	2.84	0.15	0.14	0.12	26,23,16
1118	3.85	3.71	3.67	3.197e+05	67.00	2.84	0.15	0.14	0.12	26,23,16
1119	3.85	3.71	3.67	3.197e+05	67.00	2.84	0.15	0.14	0.12	26,23,16
1120	3.85	3.71	3.67	3.197e+05	67.00	2.84	0.15	0.14	0.12	26,23,16

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				2.873e+05	67.00	2.65			
	3.85	3.71	3.67	3.197e+05	67.00	2.84	0.15	0.14	0.12

Setto	Mat.	Spessore	Stato
		cm	
65	muratura E = 1.024e+05	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
32	3.31	3.36	3.40	1.146e+06	136.00	2.63	0.10	0.10	0.05	20,23,36
39	3.31	3.36	3.40	1.146e+06	136.00	2.63	0.10	0.10	0.05	20,23,36
150	3.31	3.36	3.40	1.146e+06	136.00	2.63	0.10	0.10	0.05	20,23,36
157	3.31	3.36	3.40	1.146e+06	136.00	2.63	0.10	0.10	0.05	20,23,36
1121	2.51	2.44	2.22	8.822e+05	136.00	1.72	0.08	0.05	0.01	17,19,36
1124	3.31	3.38	3.40	1.146e+06	136.00	2.63	0.10	0.11	0.05	20,23,36
1130	3.76	3.40	3.65	1.290e+06	136.00	2.82	0.08	0.11	0.02	21,23,37
1131	3.67	3.44	3.60	1.263e+06	136.00	2.78	0.07	0.12	0.03	13,23,17
1132	3.39	3.49	3.60	1.172e+06	136.00	2.78	0.11	0.14	0.03	24,23,17
1133	3.39	3.49	3.27	1.172e+06	136.00	2.53	0.11	0.14	0.02	24,23,42
1139	2.51	3.11	2.85	8.822e+05	136.00	2.20	0.08	0.10	0.01	17,19,36
1140	2.51	2.44	2.22	8.822e+05	136.00	1.72	0.08	0.05	0.01	17,19,36
1143	3.39	3.49	3.27	1.172e+06	136.00	2.53	0.11	0.14	0.02	24,23,42
1144	2.51	3.11	2.85	8.822e+05	136.00	2.20	0.08	0.10	0.01	17,19,36
1145	2.51	2.44	2.22	8.822e+05	136.00	1.72	0.08	0.05	0.01	17,19,36
1149	3.31	3.38	3.40	1.146e+06	136.00	2.63	0.10	0.11	0.05	20,23,36
1150	3.31	3.38	3.40	1.146e+06	136.00	2.63	0.10	0.11	0.05	20,23,36
1152	3.76	3.40	3.65	1.290e+06	136.00	2.82	0.08	0.11	0.02	21,23,37
1153	3.76	3.40	3.65	1.290e+06	136.00	2.82	0.08	0.11	0.02	21,23,37
1154	3.67	3.44	3.60	1.263e+06	136.00	2.78	0.07	0.12	0.03	13,23,17
1155	3.67	3.44	3.60	1.263e+06	136.00	2.78	0.07	0.12	0.03	13,23,17
1156	3.39	3.49	3.60	1.172e+06	136.00	2.78	0.11	0.14	0.03	24,23,17
1157	3.39	3.49	3.60	1.172e+06	136.00	2.78	0.11	0.14	0.03	24,23,17
1158	3.76	3.40	3.65	1.290e+06	136.00	2.82	0.08	0.11	0.02	21,23,37
1159	3.39	3.49	3.27	1.172e+06	136.00	2.53	0.11	0.14	0.02	24,23,42
1160	3.67	3.44	3.60	1.263e+06	136.00	2.78	0.07	0.12	0.03	13,23,17
1161	2.51	3.11	2.85	8.822e+05	136.00	2.20	0.08	0.10	0.01	17,19,36
1162	3.39	3.49	3.60	1.172e+06	136.00	2.78	0.11	0.14	0.03	24,23,17
1163	2.51	2.44	2.22	8.822e+05	136.00	1.72	0.08	0.05	0.01	17,19,36
1164	3.39	3.49	3.27	1.172e+06	136.00	2.53	0.11	0.14	0.02	24,23,42
1166	2.51	3.11	2.85	8.822e+05	136.00	2.20	0.08	0.10	0.01	17,19,36
1168	3.31	3.38	3.40	1.146e+06	136.00	2.63	0.10	0.11	0.05	20,23,36
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				8.822e+05	136.00	1.72				
	3.76	3.49	3.65	1.290e+06	136.00	2.82	0.11	0.14	0.05	

Setto	Mat.	Spessore	Stato
		cm	
66	muratura E = 1.024e+05	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
1121	2.13	1.89	2.14	7.569e+05	136.00	1.66	0.07	0.03	6.59e-03	39,24,17
1122	1.87	1.89	1.83	6.656e+05	136.00	1.42	0.09	0.03	0.02	23,24,34
1123	1.87	2.05	1.83	6.656e+05	136.00	1.42	0.09	0.02	0.02	23,25,34
1140	2.13	1.89	2.14	7.569e+05	136.00	1.66	0.07	0.03	6.59e-03	39,24,17
1141	1.87	1.89	1.83	6.656e+05	136.00	1.42	0.09	0.03	0.02	23,24,34
1142	1.87	2.05	1.83	6.656e+05	136.00	1.42	0.09	0.02	0.02	23,25,34
1145	2.13	1.89	2.14	7.569e+05	136.00	1.66	0.07	0.03	6.59e-03	39,24,17
1146	1.87	1.89	1.83	6.656e+05	136.00	1.42	0.09	0.03	0.02	23,24,34
1147	1.87	2.05	1.83	6.656e+05	136.00	1.42	0.09	0.02	0.02	23,25,34
1163	2.13	1.89	2.14	7.569e+05	136.00	1.66	0.07	0.03	6.59e-03	39,24,17
1165	1.87	1.89	1.83	6.656e+05	136.00	1.42	0.09	0.03	0.02	23,24,34
1167	1.87	2.05	1.83	6.656e+05	136.00	1.42	0.09	0.02	0.02	23,25,34
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				6.656e+05	136.00	1.42				
	2.13	2.05	2.14	7.569e+05	136.00	1.66	0.09	0.03	0.02	

Setto	Mat.	Spessore	Stato
		cm	
69	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
1179	1.57	1.67	1.57	6.084e+05	142.40	1.82	0.07	0.06	0.16	17,16,17
1180	1.57	1.67	1.57	6.084e+05	142.40	1.82	0.07	0.06	0.16	17,16,17
1181	1.57	1.67	1.57	6.084e+05	142.40	1.82	0.07	0.06	0.16	17,16,17
1182	1.57	1.67	1.57	6.084e+05	142.40	1.82	0.07	0.06	0.16	17,16,17
1192	1.59	1.67	1.57	6.978e+05	151.60	1.82	0.08	0.07	0.16	17,16,17
1193	1.59	1.67	1.57	6.978e+05	151.60	1.82	0.08	0.07	0.16	17,16,17
1201	1.59	1.67	1.59	6.978e+05	151.60	1.84	0.08	0.07	0.15	17,16,17
1202	1.59	1.67	1.59	6.978e+05	151.60	1.84	0.08	0.07	0.15	17,16,17

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				6.084e+05	142.40	1.82			
	1.59	1.67	1.59	6.978e+05	151.60	1.84	0.08	0.07	0.16

Setto	Mat.	Spessore	Stato
		cm	
70	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
1459	1.69	1.73	1.83	2.497e+05	87.50	1.47	0.19	0.21	0.09	17,22,27
1492	1.69	1.73	1.83	2.497e+05	87.50	1.47	0.19	0.21	0.09	17,22,27
1576	1.69	1.73	1.83	2.497e+05	87.50	1.47	0.19	0.21	0.09	17,22,27
1913	1.38	1.55	1.83	2.060e+05	78.22	1.47	0.42	0.21	0.09	17,25,27
1914	1.23	1.63	1.22	1.833e+05	68.25	0.98	0.49	0.42	0.15	33,35,25
1915	1.23	1.38	1.22	1.833e+05	86.67	0.98	0.49	0.49	0.15	33,11,25
1916	1.29	1.38	1.27	1.931e+05	86.67	1.02	0.36	0.49	0.14	31,11,25
1917	1.45	1.56	1.54	2.161e+05	87.50	1.24	0.13	0.46	0.07	29,11,28
1918	1.83	1.69	1.81	2.698e+05	87.50	1.45	0.24	0.45	0.09	15,15,27
1919	1.80	1.83	1.75	2.658e+05	87.50	1.41	0.36	0.43	0.15	15,15,27
1920	1.80	1.83	1.75	2.658e+05	86.21	1.41	0.36	0.38	0.15	15,15,27
1922	1.38	1.55	1.83	2.060e+05	78.22	1.47	0.42	0.21	0.09	17,25,27
1923	1.23	1.63	1.22	1.833e+05	68.25	0.98	0.49	0.42	0.15	33,35,25
1924	1.23	1.38	1.22	1.833e+05	86.67	0.98	0.49	0.49	0.15	33,11,25
1925	1.29	1.38	1.27	1.931e+05	86.67	1.02	0.36	0.49	0.14	31,11,25
1926	1.45	1.56	1.54	2.161e+05	87.50	1.24	0.13	0.46	0.07	29,11,28
1927	1.83	1.69	1.81	2.698e+05	87.50	1.45	0.24	0.45	0.09	15,15,27
1928	1.80	1.83	1.75	2.658e+05	87.50	1.41	0.36	0.43	0.15	15,15,27
1929	1.80	1.83	1.75	2.658e+05	86.21	1.41	0.36	0.38	0.15	15,15,27
1931	1.38	1.55	1.83	2.060e+05	78.22	1.47	0.42	0.21	0.09	17,25,27
1932	1.23	1.63	1.22	1.833e+05	68.25	0.98	0.49	0.42	0.15	33,35,25
1933	1.23	1.38	1.22	1.833e+05	86.67	0.98	0.49	0.49	0.15	33,11,25
1934	1.29	1.38	1.27	1.931e+05	86.67	1.02	0.36	0.49	0.14	31,11,25
1935	1.45	1.56	1.54	2.161e+05	87.50	1.24	0.13	0.46	0.07	29,11,28
1936	1.83	1.69	1.81	2.698e+05	87.50	1.45	0.24	0.45	0.09	15,15,27
1937	1.80	1.83	1.75	2.658e+05	87.50	1.41	0.36	0.43	0.15	15,15,27
1938	1.80	1.83	1.75	2.658e+05	86.21	1.41	0.36	0.38	0.15	15,15,27

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				1.833e+05	68.25	0.98			
	1.83	1.83	1.83	2.698e+05	87.50	1.47	0.49	0.49	0.15

Setto	Mat.	Spessore	Stato
		cm	
73	muratura E = 1.024e+05	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
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	daN/cm2	daN/cm2	daN/cm2	daN cm	cm					
1	3.64	3.40	3.62	1.445e+07	462.00	2.80	0.10	0.05	0.04	36,37,11
33	3.64	3.40	3.62	1.445e+07	462.00	2.80	0.10	0.05	0.04	36,37,11
231	3.64	3.40	3.62	1.445e+07	462.00	2.80	0.10	0.05	0.04	36,37,11
238	3.64	3.40	3.62	1.445e+07	462.00	2.80	0.10	0.05	0.04	36,37,11
245	3.64	3.40	3.62	1.445e+07	462.00	2.80	0.10	0.05	0.04	36,37,11
252	3.64	3.40	3.62	1.445e+07	462.00	2.80	0.10	0.05	0.04	36,37,11
259	3.64	3.40	3.62	1.445e+07	462.00	2.80	0.10	0.05	0.04	36,37,11
266	3.64	3.40	3.62	1.445e+07	462.00	2.80	0.10	0.05	0.04	36,37,11
273	3.64	3.40	3.62	1.445e+07	462.00	2.80	0.10	0.05	0.04	36,37,11
280	3.64	3.40	3.62	1.445e+07	462.00	2.80	0.10	0.05	0.04	36,37,11
1295	3.64	3.40	3.34	1.445e+07	462.00	2.58	0.10	0.05	0.04	36,37,17
1296	3.61	3.24	3.34	1.434e+07	462.00	2.58	0.09	0.04	0.04	36,37,17
1297	3.48	3.12	3.50	1.385e+07	462.00	2.70	0.06	0.05	0.03	36,37,16
1298	3.31	3.03	3.02	1.324e+07	462.00	2.33	0.06	0.05	0.03	36,37,17
1299	3.06	2.83	3.02	1.229e+07	462.00	2.33	0.08	0.05	0.03	38,37,17
1300	2.64	2.83	3.04	7.434e+06	462.00	2.35	0.08	0.05	0.02	18,37,19
1301	2.64	2.58	2.64	7.434e+06	385.00	2.04	0.08	0.04	0.02	18,37,14
1304	3.64	3.40	3.34	1.445e+07	462.00	2.58	0.10	0.05	0.04	36,37,17
1305	3.61	3.24	3.34	1.434e+07	462.00	2.58	0.09	0.04	0.04	36,37,17
1306	3.48	3.12	3.50	1.385e+07	462.00	2.70	0.06	0.05	0.03	36,37,16
1307	3.31	3.03	3.02	1.324e+07	462.00	2.33	0.06	0.05	0.03	36,37,17
1308	3.06	2.83	3.02	1.229e+07	462.00	2.33	0.08	0.05	0.03	38,37,17
1309	2.64	2.83	3.04	7.434e+06	462.00	2.35	0.08	0.05	0.02	18,37,19
1310	2.64	2.58	2.64	7.434e+06	385.00	2.04	0.08	0.04	0.02	18,37,14
1313	3.64	3.40	3.34	1.445e+07	462.00	2.58	0.10	0.05	0.04	36,37,17
1314	3.61	3.24	3.34	1.434e+07	462.00	2.58	0.09	0.04	0.04	36,37,17
1315	3.48	3.12	3.50	1.385e+07	462.00	2.70	0.06	0.05	0.03	36,37,16
1316	3.31	3.03	3.02	1.324e+07	462.00	2.33	0.06	0.05	0.03	36,37,17
1317	3.06	2.83	3.02	1.229e+07	462.00	2.33	0.08	0.05	0.03	38,37,17
1318	2.64	2.83	3.04	7.434e+06	462.00	2.35	0.08	0.05	0.02	18,37,19
1319	2.64	2.58	2.64	7.434e+06	385.00	2.04	0.08	0.04	0.02	18,37,14
1322	3.64	3.40	3.34	1.445e+07	462.00	2.58	0.10	0.05	0.04	36,37,17
1323	3.61	3.24	3.34	1.434e+07	462.00	2.58	0.09	0.04	0.04	36,37,17
1324	3.48	3.12	3.50	1.385e+07	462.00	2.70	0.06	0.05	0.03	36,37,16
1325	3.31	3.03	3.02	1.324e+07	462.00	2.33	0.06	0.05	0.03	36,37,17
1326	3.06	2.83	3.02	1.229e+07	462.00	2.33	0.08	0.05	0.03	38,37,17
1327	2.64	2.83	3.04	7.434e+06	462.00	2.35	0.08	0.05	0.02	18,37,19
1328	2.64	2.58	2.64	7.434e+06	385.00	2.04	0.08	0.04	0.02	18,37,14
1331	3.64	3.40	3.34	1.445e+07	462.00	2.58	0.10	0.05	0.04	36,37,17
1332	3.61	3.24	3.34	1.434e+07	462.00	2.58	0.09	0.04	0.04	36,37,17
1333	3.48	3.12	3.50	1.385e+07	462.00	2.70	0.06	0.05	0.03	36,37,16
1334	3.31	3.03	3.02	1.324e+07	462.00	2.33	0.06	0.05	0.03	36,37,17
1335	3.06	2.83	3.02	1.229e+07	462.00	2.33	0.08	0.05	0.03	38,37,17
1336	2.64	2.83	3.04	7.434e+06	462.00	2.35	0.08	0.05	0.02	18,37,19
1337	2.64	2.58	2.64	7.434e+06	385.00	2.04	0.08	0.04	0.02	18,37,14
1340	3.64	3.40	3.34	1.445e+07	462.00	2.58	0.10	0.05	0.04	36,37,17
1341	3.61	3.24	3.34	1.434e+07	462.00	2.58	0.09	0.04	0.04	36,37,17
1342	3.48	3.12	3.50	1.385e+07	462.00	2.70	0.06	0.05	0.03	36,37,16
1343	3.31	3.03	3.02	1.324e+07	462.00	2.33	0.06	0.05	0.03	36,37,17
1344	3.06	2.83	3.02	1.229e+07	462.00	2.33	0.08	0.05	0.03	38,37,17
1345	2.64	2.83	3.04	7.434e+06	462.00	2.35	0.08	0.05	0.02	18,37,19
1346	2.64	2.58	2.64	7.434e+06	385.00	2.04	0.08	0.04	0.02	18,37,14
1349	3.64	3.33	3.34	1.445e+07	462.00	2.58	0.10	0.05	0.04	36,37,17
1350	3.61	3.19	3.34	1.434e+07	462.00	2.58	0.09	0.05	0.04	36,37,17
1351	3.48	3.12	3.47	1.385e+07	462.00	2.68	0.06	0.05	0.04	36,37,16
1352	3.31	3.03	3.02	1.324e+07	462.00	2.33	0.06	0.05	0.03	36,37,17
1353	3.06	2.83	3.02	1.229e+07	462.00	2.33	0.08	0.05	0.03	38,37,17
1354	2.64	2.83	3.04	7.434e+06	462.00	2.35	0.08	0.05	0.02	18,37,19
1355	2.64	2.58	2.64	7.434e+06	385.00	2.04	0.08	0.04	0.02	18,37,14
1358	3.64	3.28	3.62	1.445e+07	462.00	2.80	0.10	0.05	0.04	36,37,11
1359	3.58	3.15	3.43	1.422e+07	462.00	2.65	0.08	0.05	0.04	36,37,16
1360	3.44	3.15	3.43	1.372e+07	462.00	2.65	0.05	0.05	0.04	36,37,16
1361	3.31	3.03	3.02	1.324e+07	462.00	2.33	0.06	0.05	0.03	36,37,17
1362	3.06	2.83	3.02	1.229e+07	462.00	2.33	0.08	0.05	0.03	38,37,17
1363	3.06	2.83	3.04	1.229e+07	462.00	2.35	0.08	0.05	0.02	38,37,19
1367	3.64	3.28	3.62	1.445e+07	462.00	2.80	0.10	0.05	0.04	36,37,11
1368	3.54	3.15	3.43	1.409e+07	462.00	2.65	0.08	0.05	0.04	36,37,16
1369	3.41	3.15	3.43	1.359e+07	462.00	2.65	0.05	0.05	0.04	36,37,16
1370	3.31	3.03	3.02	1.324e+07	462.00	2.33	0.06	0.05	0.03	36,37,17
1371	3.06	2.83	3.02	1.229e+07	462.00	2.33	0.08	0.05	0.03	38,37,17
1372	3.06	2.83	3.04	1.229e+07	462.00	2.35	0.08	0.05	0.02	38,37,19
1376	3.64	3.28	3.62	1.445e+07	462.00	2.80	0.10	0.05	0.04	36,37,11
1377	3.54	3.15	3.43	1.409e+07	462.00	2.65	0.08	0.05	0.04	36,37,16
1378	3.41	3.15	3.43	1.359e+07	462.00	2.65	0.05	0.05	0.04	36,37,16
1379	3.31	3.03	3.02	1.324e+07	462.00	2.33	0.06	0.05	0.03	36,37,17
1380	3.06	2.83	3.02	1.229e+07	462.00	2.33	0.08	0.05	0.03	38,37,17

1381	3.06	2.83	3.04	1.229e+07	462.00	2.35	0.08	0.05	0.02	38,37,19
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	3.64	3.40	3.62	7.434e+06 1.445e+07	385.00 462.00	2.04 2.80	0.10	0.05	0.04	

Setto	Mat.	Spessore	Stato
		cm	
74	muratura E = 1.024e+05	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1301	2.30	2.24	2.30	6.526e+06	385.00	1.78	0.06	0.05	0.03	18,37,14
1302	2.27	2.19	2.30	9.274e+06	462.00	1.78	0.09	0.06	0.03	18,37,14
1303	2.27	2.19	2.22	9.274e+06	462.00	1.71	0.09	0.06	0.02	18,37,17
1310	2.30	2.24	2.30	6.526e+06	385.00	1.78	0.06	0.05	0.03	18,37,14
1311	2.27	2.19	2.30	9.274e+06	462.00	1.78	0.09	0.06	0.03	18,37,14
1312	2.27	2.19	2.22	9.274e+06	462.00	1.71	0.09	0.06	0.02	18,37,17
1319	2.30	2.24	2.30	6.526e+06	385.00	1.78	0.06	0.05	0.03	18,37,14
1320	2.27	2.19	2.30	9.274e+06	462.00	1.78	0.09	0.06	0.03	18,37,14
1321	2.27	2.19	2.22	9.274e+06	462.00	1.71	0.09	0.06	0.02	18,37,17
1328	2.30	2.24	2.30	6.526e+06	385.00	1.78	0.06	0.05	0.03	18,37,14
1329	2.27	2.19	2.30	9.274e+06	462.00	1.78	0.09	0.06	0.03	18,37,14
1330	2.27	2.19	2.22	9.274e+06	462.00	1.71	0.09	0.06	0.02	18,37,17
1337	2.30	2.24	2.30	6.526e+06	385.00	1.78	0.06	0.05	0.03	18,37,14
1338	2.27	2.19	2.30	9.274e+06	462.00	1.78	0.09	0.06	0.03	18,37,14
1339	2.27	2.19	2.22	9.274e+06	462.00	1.71	0.09	0.06	0.02	18,37,17
1346	2.30	2.24	2.30	6.526e+06	385.00	1.78	0.06	0.05	0.03	18,37,14
1347	2.27	2.19	2.30	9.274e+06	462.00	1.78	0.09	0.06	0.03	18,37,14
1348	2.27	2.19	2.22	9.274e+06	462.00	1.71	0.09	0.06	0.02	18,37,17
1355	2.30	2.23	2.29	6.526e+06	392.50	1.77	0.06	0.05	0.04	18,37,14
1356	2.27	2.19	2.29	9.274e+06	462.00	1.77	0.09	0.06	0.04	18,37,14
1357	2.27	2.19	2.22	9.274e+06	462.00	1.71	0.09	0.06	0.02	18,37,17
1364	2.29	2.22	2.28	6.750e+06	400.00	1.76	0.06	0.05	0.04	18,37,14
1365	2.27	2.19	2.28	9.274e+06	462.00	1.76	0.09	0.06	0.04	18,37,14
1366	2.27	2.19	2.22	9.274e+06	462.00	1.71	0.09	0.06	0.02	18,37,17
1373	2.28	2.22	2.28	6.978e+06	400.00	1.76	0.06	0.05	0.04	18,37,14
1374	2.27	2.19	2.28	9.274e+06	462.00	1.76	0.09	0.06	0.04	18,37,14
1375	2.27	2.19	2.22	9.274e+06	462.00	1.71	0.09	0.06	0.02	18,37,17
1382	2.28	2.22	2.28	6.978e+06	400.00	1.76	0.06	0.05	0.04	18,37,14
1383	2.27	2.19	2.28	9.274e+06	462.00	1.76	0.09	0.06	0.04	18,37,14
1384	2.27	2.19	2.22	9.274e+06	462.00	1.71	0.09	0.06	0.02	18,37,17
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	2.30	2.24	2.30	6.526e+06 9.274e+06	385.00 462.00	1.71 1.78	0.09	0.06	0.04	

Setto	Mat.	Spessore	Stato
		cm	
75	muratura E = 1.024e+05	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1354	3.13	2.98	3.13	1.261e+06	146.50	2.42	0.05	0.07	0.04	18,39,11
1355	3.13	2.98	3.13	1.261e+06	146.50	2.42	0.05	0.07	0.04	18,39,11
1363	3.12	2.97	3.13	1.134e+06	139.00	2.42	0.05	0.09	0.04	18,39,11
1364	3.12	2.97	3.13	1.134e+06	139.00	2.42	0.05	0.09	0.04	18,39,11
1372	3.12	2.97	3.12	1.134e+06	139.00	2.41	0.05	0.09	0.04	18,39,11
1373	3.12	2.97	3.12	1.134e+06	139.00	2.41	0.05	0.09	0.04	18,39,11
1381	3.12	2.97	3.12	1.134e+06	139.00	2.41	0.05	0.09	0.04	18,39,11
1382	3.12	2.97	3.12	1.134e+06	139.00	2.41	0.05	0.09	0.04	18,39,11
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	3.13	2.98	3.13	1.134e+06 1.261e+06	139.00 146.50	2.41 2.42	0.05	0.09	0.04	

Setto	Mat.	Spessore	Stato
		cm	
76	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
35	2.40	2.54	2.54	3.623e+05	90.00	2.95	0.04	0.09	0.02	23,16,16
36	2.40	2.54	2.54	3.623e+05	90.00	2.95	0.04	0.09	0.02	23,16,16
188	2.40	2.54	2.54	3.623e+05	90.00	2.95	0.04	0.09	0.02	23,16,16
1169	2.34	2.54	2.30	3.535e+05	90.00	2.67	0.08	0.09	0.02	17,16,16
1171	2.14	2.30	2.30	3.247e+05	90.00	2.67	0.10	0.06	0.02	17,16,16
1173	2.22	2.07	2.42	3.362e+05	90.00	2.81	0.11	0.11	0.01	11,17,36
1175	2.16	2.13	1.97	3.280e+05	90.00	2.29	0.12	0.15	0.01	11,17,37
1177	2.23	2.23	1.97	3.377e+05	90.00	2.29	0.15	0.15	0.01	17,17,37
1179	2.23	2.23	2.34	3.377e+05	90.00	2.71	0.15	0.15	0.01	17,17,30
1385	2.34	2.54	2.30	3.535e+05	90.00	2.67	0.08	0.09	0.02	17,16,16
1386	2.14	2.30	2.30	3.247e+05	90.00	2.67	0.10	0.06	0.02	17,16,16
1387	2.22	2.07	2.42	3.362e+05	90.00	2.81	0.11	0.11	0.01	11,17,36
1388	2.16	2.13	1.97	3.280e+05	90.00	2.29	0.12	0.15	0.01	11,17,37
1389	2.23	2.23	1.97	3.377e+05	90.00	2.29	0.15	0.15	0.01	17,17,37
1390	2.23	2.23	2.34	3.377e+05	90.00	2.71	0.15	0.15	0.01	17,17,30
1394	2.34	2.54	2.30	3.535e+05	90.00	2.67	0.08	0.09	0.02	17,16,16
1395	2.14	2.30	2.30	3.247e+05	90.00	2.67	0.10	0.06	0.02	17,16,16
1396	2.22	2.07	2.42	3.362e+05	90.00	2.81	0.11	0.11	0.01	11,17,36
1397	2.16	2.13	1.97	3.280e+05	90.00	2.29	0.12	0.15	0.01	11,17,37
1398	2.23	2.23	1.97	3.377e+05	90.00	2.29	0.15	0.15	0.01	17,17,37
1399	2.23	2.23	2.34	3.377e+05	90.00	2.71	0.15	0.15	0.01	17,17,30
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				3.247e+05	90.00	2.29				
	2.40	2.54	2.54	3.623e+05	90.00	2.95	0.15	0.15	0.02	

Setto	Mat.	Spessore	Stato
		cm	
77	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
1179	1.75	1.75	1.51	2.686e+05	90.00	1.75	0.07	0.04	4.13e-03	17,17,35
1181	1.45	1.75	1.51	2.250e+05	90.00	1.75	0.09	0.04	4.13e-03	16,17,35
1183	1.45	1.45	1.34	2.250e+05	90.00	1.55	0.09	0.03	0.02	16,16,31
1185	1.49	1.55	1.40	2.309e+05	90.00	1.62	0.09	0.06	0.02	11,16,27
1390	1.75	1.75	1.51	2.686e+05	90.00	1.75	0.07	0.04	4.13e-03	17,17,35
1391	1.45	1.75	1.51	2.250e+05	90.00	1.75	0.09	0.04	4.13e-03	16,17,35
1392	1.45	1.45	1.34	2.250e+05	90.00	1.55	0.09	0.03	0.02	16,16,31
1393	1.49	1.55	1.40	2.309e+05	90.00	1.62	0.09	0.06	0.02	11,16,27
1399	1.75	1.75	1.51	2.686e+05	90.00	1.75	0.07	0.04	4.13e-03	17,17,35
1400	1.45	1.75	1.51	2.250e+05	90.00	1.75	0.09	0.04	4.13e-03	16,17,35
1401	1.45	1.45	1.34	2.250e+05	90.00	1.55	0.09	0.03	0.02	16,16,31
1402	1.49	1.55	1.40	2.309e+05	90.00	1.62	0.09	0.06	0.02	11,16,27
2643	1.49	1.49	1.49	2.309e+05	90.00	1.73	0.09	0.08	0.02	11,16,16
2644	1.43	1.49	1.49	2.219e+05	90.00	1.73	0.08	0.08	0.02	11,16,16
2645	1.07	1.31	1.31	1.675e+05	90.00	1.51	0.10	0.08	0.01	11,16,16
2646	0.92	0.92	0.95	1.446e+05	90.00	1.11	0.16	0.04	0.02	15,37,12
2647	0.92	0.93	0.95	1.446e+05	90.00	1.11	0.16	0.07	0.02	15,17,12
2648	0.93	0.93	0.91	1.472e+05	90.00	1.05	0.08	0.09	0.01	25,17,16
2649	0.94	0.93	0.83	1.483e+05	90.00	0.96	0.20	0.09	0.03	17,17,27
2650	0.79	0.94	0.71	1.252e+05	90.00	0.82	0.22	0.09	0.07	17,17,33
2651	0.79	0.79	0.71	1.252e+05	90.00	0.82	0.22	0.06	0.07	17,17,33
2652	1.49	1.49	1.49	2.309e+05	90.00	1.73	0.09	0.08	0.02	11,16,16
2653	1.43	1.49	1.49	2.219e+05	90.00	1.73	0.08	0.08	0.02	11,16,16
2654	1.07	1.31	1.31	1.675e+05	90.00	1.51	0.10	0.08	0.01	11,16,16
2655	0.92	0.92	0.95	1.446e+05	90.00	1.11	0.16	0.04	0.02	15,37,12
2656	0.92	0.93	0.95	1.446e+05	90.00	1.11	0.16	0.07	0.02	15,17,12
2657	0.93	0.93	0.91	1.472e+05	90.00	1.05	0.08	0.09	0.01	25,17,16
2658	0.94	0.93	0.83	1.483e+05	90.00	0.96	0.20	0.09	0.03	17,17,27
2659	0.79	0.94	0.71	1.252e+05	90.00	0.82	0.22	0.09	0.07	17,17,33
2660	0.79	0.79	0.71	1.252e+05	90.00	0.82	0.22	0.06	0.07	17,17,33

2661	1.49	1.49	1.49	2.309e+05	90.00	1.73	0.09	0.08	0.02	11,16,16
2662	1.43	1.49	1.49	2.219e+05	90.00	1.73	0.08	0.08	0.02	11,16,16
2663	1.07	1.31	1.31	1.675e+05	90.00	1.51	0.10	0.08	0.01	11,16,16
2664	0.92	0.92	0.95	1.446e+05	90.00	1.11	0.16	0.04	0.02	15,37,12
2665	0.92	0.93	0.95	1.446e+05	90.00	1.11	0.16	0.07	0.02	15,17,12
2666	0.93	0.93	0.91	1.472e+05	90.00	1.05	0.08	0.09	0.01	25,17,16
2667	0.94	0.93	0.83	1.483e+05	90.00	0.96	0.20	0.09	0.03	17,17,27
2668	0.79	0.94	0.71	1.252e+05	90.00	0.82	0.22	0.09	0.07	17,17,33
2669	0.79	0.79	0.71	1.252e+05	90.00	0.82	0.22	0.06	0.07	17,17,33
3080	0.56	0.40	0.51	8.863e+04	90.00	0.59	0.10	0.05	0.07	25,35,33
3081	0.40	0.40	0.41	6.372e+04	90.00	0.47	0.04	0.05	0.04	19,35,20
3083	0.56	0.40	0.51	8.863e+04	90.00	0.59	0.10	0.05	0.07	25,35,33
3084	0.40	0.40	0.41	6.372e+04	90.00	0.47	0.04	0.05	0.04	19,35,20
3086	0.56	0.40	0.51	8.863e+04	90.00	0.59	0.10	0.05	0.07	25,35,33
3087	0.40	0.40	0.41	6.372e+04	90.00	0.47	0.04	0.05	0.04	19,35,20
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	1.75	1.75	1.51	6.372e+04	90.00	0.47				
				2.686e+05	90.00	1.75	0.22	0.09	0.07	

Setto	Mat.	Spessore	Stato
		cm	
80	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
1	2.89	3.03	3.05	4.199e+05	89.00	3.53	0.03	0.10	0.02	17,14,16
34	2.89	3.03	3.05	4.199e+05	89.00	3.53	0.03	0.10	0.02	17,14,16
219	2.89	3.03	3.05	4.199e+05	89.00	3.53	0.03	0.10	0.02	17,14,16
1376	2.79	3.03	3.05	4.064e+05	89.00	3.53	0.08	0.10	0.02	16,14,16
1377	2.79	2.84	2.97	4.064e+05	89.00	3.44	0.08	0.09	0.01	16,14,36
1378	2.54	2.92	2.47	3.734e+05	89.00	2.87	0.07	0.13	2.87e-03	11,14,35
1379	2.80	2.81	2.51	4.073e+05	89.00	2.90	0.07	0.14	4.73e-03	17,14,37
1380	2.60	2.81	2.40	3.814e+05	89.00	2.78	0.04	0.14	0.01	11,14,17
1381	2.76	2.65	2.40	4.024e+05	89.00	2.78	0.03	0.13	0.01	16,11,17
1421	2.79	3.03	3.05	4.064e+05	89.00	3.53	0.08	0.10	0.02	16,14,16
1422	2.79	2.84	2.97	4.064e+05	89.00	3.44	0.08	0.09	0.01	16,14,36
1423	2.54	2.92	2.47	3.734e+05	89.00	2.87	0.07	0.13	2.87e-03	11,14,35
1424	2.80	2.81	2.51	4.073e+05	89.00	2.90	0.07	0.14	4.73e-03	17,14,37
1425	2.60	2.81	2.40	3.814e+05	89.00	2.78	0.04	0.14	0.01	11,14,17
1426	2.76	2.65	2.40	4.024e+05	89.00	2.78	0.03	0.13	0.01	16,11,17
1430	2.79	3.03	3.05	4.064e+05	89.00	3.53	0.08	0.10	0.02	16,14,16
1431	2.79	2.84	2.97	4.064e+05	89.00	3.44	0.08	0.09	0.01	16,14,36
1432	2.54	2.92	2.47	3.734e+05	89.00	2.87	0.07	0.13	2.87e-03	11,14,35
1433	2.80	2.81	2.51	4.073e+05	89.00	2.90	0.07	0.14	4.73e-03	17,14,37
1434	2.60	2.81	2.40	3.814e+05	89.00	2.78	0.04	0.14	0.01	11,14,17
1435	2.76	2.65	2.40	4.024e+05	89.00	2.78	0.03	0.13	0.01	16,11,17
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	2.89	3.03	3.05	3.734e+05	89.00	2.78				
				4.199e+05	89.00	3.53	0.08	0.14	0.02	

Setto	Mat.	Spessore	Stato
		cm	
81	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
1381	1.90	2.19	1.90	2.839e+05	89.00	2.20	0.14	0.06	0.02	17,11,37
1382	1.67	1.89	1.90	2.514e+05	89.00	2.20	0.18	0.09	0.02	17,11,37
1383	1.67	1.80	1.65	2.514e+05	89.00	1.92	0.18	0.14	0.02	17,11,37
1384	1.69	1.84	1.77	2.541e+05	89.00	2.05	0.14	0.17	0.02	17,11,27
1426	1.90	2.19	1.90	2.839e+05	89.00	2.20	0.14	0.06	0.02	17,11,37
1427	1.67	1.89	1.90	2.514e+05	89.00	2.20	0.18	0.09	0.02	17,11,37
1428	1.67	1.80	1.65	2.514e+05	89.00	1.92	0.18	0.14	0.02	17,11,37
1429	1.69	1.84	1.77	2.541e+05	89.00	2.05	0.14	0.17	0.02	17,11,27

1435	1.90	2.19	1.90	2.839e+05	89.00	2.20	0.14	0.06	0.02	17,11,37
1436	1.67	1.89	1.90	2.514e+05	89.00	2.20	0.18	0.09	0.02	17,11,37
1437	1.67	1.80	1.65	2.514e+05	89.00	1.92	0.18	0.14	0.02	17,11,37
1438	1.69	1.84	1.77	2.541e+05	89.00	2.05	0.14	0.17	0.02	17,11,27
1724	1.96	1.84	1.85	2.928e+05	89.00	2.14	0.10	0.17	0.03	12,11,27
1726	1.89	1.91	1.85	2.828e+05	89.00	2.14	0.15	0.10	0.03	15,11,27
1728	1.89	1.57	1.80	2.828e+05	89.00	2.09	0.15	0.09	0.03	15,14,33
1730	1.62	1.57	1.26	2.446e+05	89.00	1.46	0.09	0.09	0.01	11,14,37
1732	1.23	1.23	1.26	1.876e+05	89.00	1.46	0.01	0.10	0.01	11,14,37
1734	1.07	1.23	1.07	1.642e+05	89.00	1.24	0.05	0.10	0.05	17,14,17
1736	0.94	1.15	0.95	1.445e+05	89.00	1.10	0.08	0.09	0.15	17,11,25
1738	0.92	1.16	0.94	1.423e+05	89.00	1.09	0.14	0.15	0.18	17,11,21
1740	0.87	0.88	0.94	1.343e+05	89.00	1.09	0.21	0.19	0.18	17,25,21
2607	1.96	1.84	1.85	2.928e+05	89.00	2.14	0.10	0.17	0.03	12,11,27
2608	1.89	1.91	1.85	2.828e+05	89.00	2.14	0.15	0.10	0.03	15,11,27
2609	1.89	1.57	1.80	2.828e+05	89.00	2.09	0.15	0.09	0.03	15,14,33
2610	1.62	1.57	1.26	2.446e+05	89.00	1.46	0.09	0.09	0.01	11,14,37
2611	1.23	1.23	1.26	1.876e+05	89.00	1.46	0.01	0.10	0.01	11,14,37
2612	1.07	1.23	1.07	1.642e+05	89.00	1.24	0.05	0.10	0.05	17,14,17
2613	0.94	1.15	0.95	1.445e+05	89.00	1.10	0.08	0.09	0.15	17,11,25
2614	0.92	1.16	0.94	1.423e+05	89.00	1.09	0.14	0.15	0.18	17,11,21
2615	0.87	0.88	0.94	1.343e+05	89.00	1.09	0.21	0.19	0.18	17,25,21
2616	1.96	1.84	1.85	2.928e+05	89.00	2.14	0.10	0.17	0.03	12,11,27
2617	1.89	1.91	1.85	2.828e+05	89.00	2.14	0.15	0.10	0.03	15,11,27
2618	1.89	1.57	1.80	2.828e+05	89.00	2.09	0.15	0.09	0.03	15,14,33
2619	1.62	1.57	1.26	2.446e+05	89.00	1.46	0.09	0.09	0.01	11,14,37
2620	1.23	1.23	1.26	1.876e+05	89.00	1.46	0.01	0.10	0.01	11,14,37
2621	1.07	1.23	1.07	1.642e+05	89.00	1.24	0.05	0.10	0.05	17,14,17
2622	0.94	1.15	0.95	1.445e+05	89.00	1.10	0.08	0.09	0.15	17,11,25
2623	0.92	1.16	0.94	1.423e+05	89.00	1.09	0.14	0.15	0.18	17,11,21
2624	0.87	0.88	0.94	1.343e+05	89.00	1.09	0.21	0.19	0.18	17,25,21
3065	0.87	0.88	0.97	1.343e+05	89.00	1.12	0.21	0.19	0.16	17,25,32
3066	0.70	0.71	0.76	1.091e+05	89.00	0.88	0.11	0.18	0.16	17,25,32
3068	0.87	0.88	0.97	1.343e+05	89.00	1.12	0.21	0.19	0.16	17,25,32
3069	0.70	0.71	0.76	1.091e+05	89.00	0.88	0.11	0.18	0.16	17,25,32
3071	0.87	0.88	0.97	1.343e+05	89.00	1.12	0.21	0.19	0.16	17,25,32
3072	0.70	0.71	0.76	1.091e+05	89.00	0.88	0.11	0.18	0.16	17,25,32

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
	1.96	2.19	1.90	1.091e+05	89.00	0.88			
				2.928e+05	89.00	2.20	0.21	0.19	0.18

Setto	Mat.	Spessore	Stato
		cm	
82	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1	1.08	1.81	1.21	1.834e+05	93.50	1.46	0.09	0.12	0.02	17,16,37
5	1.08	1.81	1.21	1.834e+05	93.50	1.46	0.09	0.12	0.02	17,16,37
295	1.08	1.81	1.21	1.834e+05	93.50	1.46	0.09	0.12	0.02	17,16,37
1376	1.08	1.81	1.59	1.834e+05	93.50	1.92	0.09	0.12	0.03	17,16,42
1377	1.91	1.18	1.59	3.152e+05	93.50	1.92	0.09	0.17	0.03	11,17,42
1378	1.91	1.26	1.26	3.152e+05	93.50	1.52	0.09	0.22	0.02	11,17,14
1379	1.88	1.44	1.61	3.102e+05	93.50	1.94	0.08	0.28	0.01	11,17,27
1380	1.66	1.68	1.67	2.753e+05	93.50	2.01	0.07	0.33	0.02	39,17,31
1381	1.66	1.68	1.67	2.753e+05	93.50	2.01	0.07	0.33	0.02	39,17,31
1439	1.08	1.81	1.57	1.834e+05	93.50	1.90	0.09	0.12	0.04	17,16,38
1440	1.91	1.18	1.57	3.152e+05	93.50	1.90	0.09	0.17	0.04	11,17,38
1441	1.91	1.26	1.26	3.152e+05	93.50	1.52	0.09	0.22	0.03	11,17,14
1442	1.88	1.44	1.61	3.102e+05	93.50	1.94	0.08	0.28	0.01	11,17,27
1443	1.66	1.68	1.67	2.753e+05	93.50	2.01	0.07	0.33	0.02	39,17,31
1444	2.05	1.68	1.89	1.889e+05	93.50	2.28	0.08	0.33	0.02	17,17,31
1445	2.05	2.05	1.89	1.889e+05	70.12	2.28	0.08	0.33	0.02	17,17,31
1448	1.08	1.81	1.57	1.834e+05	93.50	1.90	0.09	0.12	0.04	17,16,38
1449	1.90	1.18	1.57	3.130e+05	93.50	1.90	0.08	0.16	0.04	11,17,38
1450	1.88	1.26	1.26	3.102e+05	93.50	1.52	0.08	0.22	0.03	11,17,14
1451	1.88	1.44	1.61	3.102e+05	93.50	1.94	0.08	0.28	0.01	11,17,27
1452	1.66	1.68	1.67	2.753e+05	93.50	2.01	0.07	0.33	0.02	39,17,31
1453	2.05	1.68	1.89	1.889e+05	93.50	2.28	0.08	0.33	0.02	17,17,31
1454	2.05	2.05	1.89	1.889e+05	70.12	2.28	0.08	0.33	0.02	17,17,31

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
	2.05	2.05	1.89	1.834e+05 3.152e+05	70.12 93.50	1.46 2.28	0.09	0.33	0.04

Setto	Mat.	Spessore	Stato
		cm	
83	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1381	1.86	1.86	1.73	1.200e+05	58.44	2.09	0.20	0.55	8.95e-03	17,17,37
1382	2.24	2.24	2.06	2.791e+05	81.81	2.49	0.30	0.63	0.02	17,17,37
1383	2.24	2.24	1.84	2.791e+05	81.81	2.22	0.30	0.63	0.04	17,17,37
1384	2.00	2.00	1.84	3.287e+05	93.50	2.22	0.22	0.51	0.04	17,17,37
1444	1.86	1.86	1.73	1.200e+05	58.44	2.09	0.20	0.55	8.95e-03	17,17,37
1445	2.14	2.14	2.06	1.971e+05	70.12	2.49	0.32	0.64	0.02	17,17,37
1446	2.14	2.14	1.84	1.971e+05	70.12	2.22	0.32	0.64	0.04	17,17,37
1447	2.00	2.00	1.84	3.287e+05	93.50	2.22	0.22	0.51	0.04	17,17,37
1454	2.14	2.14	1.98	1.971e+05	70.12	2.39	0.32	0.64	0.02	17,17,37
1455	2.14	2.14	1.84	1.971e+05	70.12	2.22	0.32	0.64	0.04	17,17,37
1456	2.00	2.00	1.84	3.287e+05	93.50	2.22	0.22	0.51	0.04	17,17,37

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
	2.24	2.24	2.06	1.200e+05 3.287e+05	58.44 93.50	2.09 2.49	0.32	0.64	0.04

Setto	Mat.	Spessore	Stato
		cm	
85	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1148	3.46	3.42	3.35	3.676e+05	77.00	4.04	0.11	0.03	0.11	16,11,30
1151	3.46	3.42	3.35	3.676e+05	77.00	4.04	0.11	0.03	0.11	16,11,30
1526	4.40	4.40	3.35	2.547e+05	57.75	4.04	0.14	0.04	0.11	16,16,30
1544	4.40	4.40	4.15	2.547e+05	57.75	5.01	0.14	0.04	0.10	16,16,30
1566	4.40	4.40	4.15	2.547e+05	57.75	5.01	0.14	0.04	0.10	16,16,30
1567	4.40	4.40	3.35	2.547e+05	57.75	4.04	0.14	0.04	0.11	16,16,30
1584	4.40	4.40	4.15	2.547e+05	57.75	5.01	0.14	0.04	0.10	16,16,30
1585	4.40	4.40	3.35	2.547e+05	57.75	4.04	0.14	0.04	0.11	16,16,30
1586	3.46	3.42	3.35	3.676e+05	77.00	4.04	0.11	0.03	0.11	16,11,30

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
	4.40	4.40	4.15	2.547e+05 3.676e+05	57.75 77.00	4.04 5.01	0.14	0.04	0.11

Setto	Mat.	Spessore	Stato
		cm	
86	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
8	3.00	3.03	3.09	3.237e+05	77.00	3.73	0.03	0.02	0.27	17,14,30
9	3.00	3.03	3.09	3.237e+05	77.00	3.73	0.03	0.02	0.27	17,14,30
320	3.00	2.98	3.00	3.237e+05	77.00	3.62	0.03	0.02	0.32	17,11,30
1525	4.64	4.64	4.68	4.732e+05	77.00	5.65	0.03	0.06	0.09	11,11,30
1536	4.00	3.81	3.00	4.173e+05	77.00	3.62	0.06	0.07	0.32	16,13,30
1537	4.46	4.46	4.35	4.573e+05	77.00	5.25	0.04	0.06	0.06	11,11,27
1538	4.65	4.65	3.94	4.741e+05	77.00	4.76	0.08	0.08	0.15	11,11,30
1544	4.36	4.36	4.26	4.489e+05	77.00	5.14	0.07	0.06	0.07	11,11,27
1545	4.65	4.65	4.64	4.741e+05	77.00	5.59	0.08	0.08	0.14	11,11,30

1560	4.00	3.81	3.09	4.173e+05	77.00	3.73	0.06	0.07	0.27	16,13,30
1561	4.65	4.65	3.94	4.741e+05	77.00	4.76	0.08	0.08	0.15	11,11,30
1562	4.65	4.65	4.64	4.741e+05	77.00	5.59	0.08	0.08	0.14	11,11,30
1563	4.64	4.64	4.68	4.732e+05	77.00	5.65	0.03	0.06	0.09	11,11,30
1564	4.46	4.46	4.35	4.573e+05	77.00	5.25	0.04	0.06	0.06	11,11,27
1565	4.36	4.46	4.26	4.489e+05	77.00	5.14	0.07	0.06	0.07	11,11,27
1566	4.36	4.36	4.26	4.489e+05	77.00	5.14	0.07	0.06	0.07	11,11,27
1568	4.36	4.46	4.26	4.489e+05	77.00	5.14	0.07	0.06	0.07	11,11,27
1577	3.00	2.98	3.00	3.237e+05	77.00	3.62	0.03	0.02	0.32	17,11,30
1578	4.00	3.81	3.09	4.173e+05	77.00	3.73	0.06	0.07	0.27	16,13,30
1579	4.65	4.65	3.94	4.741e+05	77.00	4.76	0.08	0.08	0.15	11,11,30
1580	4.65	4.65	4.64	4.741e+05	77.00	5.59	0.08	0.08	0.14	11,11,30
1581	4.64	4.64	4.68	4.732e+05	77.00	5.65	0.03	0.06	0.09	11,11,30
1582	4.46	4.46	4.35	4.573e+05	77.00	5.25	0.04	0.06	0.06	11,11,27
1583	4.36	4.46	4.26	4.489e+05	77.00	5.14	0.07	0.06	0.07	11,11,27
1584	4.36	4.36	4.26	4.489e+05	77.00	5.14	0.07	0.06	0.07	11,11,27

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				3.237e+05	77.00	3.62			
	4.65	4.65	4.68	4.741e+05	77.00	5.65	0.08	0.08	0.32

Setto	Mat.	Spessore	Stato
		cm	
89	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
4	2.09	2.64	2.64	3.059e+05	87.50	2.12	0.20	0.04	0.03	11,14,14
10	2.09	2.64	2.64	3.059e+05	87.50	2.12	0.20	0.04	0.03	11,14,14
307	2.09	2.64	2.64	3.059e+05	87.50	2.12	0.20	0.04	0.03	11,14,14
1460	2.09	2.27	2.84	3.059e+05	87.50	2.28	0.20	0.13	0.05	11,11,30
1461	2.26	2.34	2.84	3.309e+05	87.50	2.28	0.16	0.21	0.05	11,11,30
1472	2.98	2.52	2.80	4.292e+05	87.50	2.25	0.11	0.22	0.03	17,11,28
1473	2.99	2.52	2.81	4.302e+05	87.50	2.26	0.13	0.22	0.02	17,11,29
1479	3.09	2.80	2.98	4.440e+05	87.50	2.39	0.14	0.22	0.03	15,11,29
1480	3.40	3.40	2.98	4.854e+05	87.50	2.39	0.18	0.23	0.03	11,11,29
1481	3.40	3.40	3.24	4.854e+05	87.50	2.60	0.18	0.23	0.02	11,11,27
1524	2.09	2.27	2.84	3.059e+05	87.50	2.29	0.20	0.13	0.05	11,11,30
1548	2.09	2.26	2.84	3.059e+05	87.50	2.28	0.20	0.12	0.05	11,11,30
1553	2.26	2.34	2.84	3.309e+05	87.50	2.28	0.16	0.21	0.05	11,11,30
1554	2.98	2.52	2.80	4.292e+05	87.50	2.25	0.11	0.22	0.03	17,11,28
1555	2.99	2.52	2.81	4.302e+05	87.50	2.26	0.13	0.22	0.02	17,11,29
1556	3.09	2.80	2.98	4.440e+05	87.50	2.39	0.14	0.22	0.03	15,11,29
1557	3.40	3.40	2.98	4.854e+05	87.50	2.39	0.18	0.23	0.03	11,11,29
1569	2.27	2.34	2.84	3.311e+05	87.50	2.29	0.15	0.21	0.05	11,11,30
1570	2.98	2.52	2.80	4.292e+05	87.50	2.26	0.11	0.22	0.03	17,11,28
1571	2.99	2.52	2.81	4.302e+05	87.50	2.26	0.13	0.22	0.02	17,11,29
1572	3.09	2.80	2.98	4.440e+05	87.50	2.39	0.14	0.22	0.03	15,11,29
1573	3.40	3.40	2.98	4.854e+05	87.50	2.39	0.18	0.23	0.03	11,11,29
1574	3.40	3.40	3.24	4.854e+05	87.50	2.60	0.18	0.23	0.02	11,11,27
1589	3.40	3.40	3.24	4.854e+05	87.50	2.60	0.18	0.23	0.02	11,11,27
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				3.059e+05	87.50	2.12				
	3.40	3.40	3.24	4.854e+05	87.50	2.60	0.20	0.23	0.05	

Setto	Mat.	Spessore	Stato
		cm	
92	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
6	2.85	2.91	2.92	3.088e+05	77.00	3.52	0.02	0.04	0.32	17,16,30
7	2.85	2.91	2.92	3.088e+05	77.00	3.52	0.02	0.04	0.32	17,16,30
333	2.85	2.91	2.92	3.088e+05	77.00	3.52	0.02	0.04	0.32	17,16,30
1495	3.57	3.62	2.92	3.778e+05	77.00	3.52	0.04	0.04	0.32	17,16,30

1496	4.24	3.62	3.65	4.386e+05	77.00	4.41	0.05	0.04	0.16	17,16,30
1497	4.24	4.38	4.36	4.386e+05	77.00	5.26	0.05	0.07	0.14	17,17,30
1498	4.43	4.38	4.51	4.554e+05	77.00	5.45	0.03	0.07	0.10	11,17,30
1499	4.19	4.28	4.33	4.340e+05	77.00	5.23	0.04	0.07	0.05	17,17,14
1500	4.10	4.19	4.07	4.258e+05	77.00	4.91	0.08	0.07	0.06	17,17,27
1501	4.10	4.10	4.07	4.258e+05	77.00	4.91	0.08	0.07	0.06	17,17,27
1504	3.57	3.62	2.92	3.778e+05	77.00	3.52	0.04	0.04	0.32	17,16,30
1505	4.24	3.62	3.65	4.386e+05	77.00	4.41	0.05	0.04	0.16	17,16,30
1506	4.24	4.38	4.36	4.386e+05	77.00	5.26	0.05	0.07	0.14	17,17,30
1507	4.43	4.38	4.51	4.554e+05	77.00	5.45	0.03	0.07	0.10	11,17,30
1508	4.19	4.28	4.33	4.340e+05	77.00	5.23	0.04	0.07	0.05	17,17,14
1509	4.10	4.19	4.07	4.258e+05	77.00	4.91	0.08	0.07	0.06	17,17,27
1510	4.10	4.10	4.07	4.258e+05	77.00	4.91	0.08	0.07	0.06	17,17,27
1513	3.57	3.62	2.92	3.778e+05	77.00	3.52	0.04	0.04	0.32	17,16,30
1514	4.24	3.62	3.65	4.386e+05	77.00	4.41	0.05	0.04	0.16	17,16,30
1515	4.24	4.38	4.36	4.386e+05	77.00	5.26	0.05	0.07	0.14	17,17,30
1516	4.43	4.38	4.51	4.554e+05	77.00	5.45	0.03	0.07	0.10	11,17,30
1517	4.19	4.28	4.33	4.340e+05	77.00	5.23	0.04	0.07	0.05	17,17,14
1518	4.10	4.19	4.07	4.258e+05	77.00	4.91	0.08	0.07	0.06	17,17,27
1519	4.10	4.10	4.07	4.258e+05	77.00	4.91	0.08	0.07	0.06	17,17,27

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				3.088e+05	77.00	3.52			
	4.43	4.38	4.51	4.554e+05	77.00	5.45	0.08	0.07	0.32

Setto	Mat.	Spessore	Stato
		cm	
93	mattoni pieni e malta di calce	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1501	3.98	3.98	4.11	4.150e+05	77.00	4.96	0.12	0.06	0.11	17,13,30
1502	3.98	3.98	3.36	4.150e+05	77.00	4.05	0.12	0.06	0.12	17,13,30
1503	3.26	3.29	3.36	3.488e+05	77.00	4.05	0.10	7.89e-03	0.12	17,26,30
1510	3.98	3.98	4.11	4.150e+05	77.00	4.96	0.12	0.06	0.11	17,13,30
1511	3.98	3.98	3.36	4.150e+05	77.00	4.05	0.12	0.06	0.12	17,13,30
1512	3.26	3.29	3.36	3.488e+05	77.00	4.05	0.10	7.89e-03	0.12	17,26,30
1519	3.98	3.98	4.11	4.150e+05	77.00	4.96	0.12	0.06	0.11	17,13,30
1520	3.98	3.98	3.36	4.150e+05	77.00	4.05	0.12	0.06	0.12	17,13,30
1521	3.26	3.29	3.36	3.488e+05	77.00	4.05	0.10	7.89e-03	0.12	17,26,30

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				3.488e+05	77.00	4.05			
	3.98	3.98	4.11	4.150e+05	77.00	4.96	0.12	0.06	0.12

Setto	Mat.	Spessore	Stato
		cm	
95	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
3	5.44	5.81	5.90	9.381e+04	32.00	6.83	0.03	0.07	0.09	32,27,20
533	5.44	5.81	5.90	9.381e+04	32.00	6.83	0.03	0.07	0.09	32,27,20
653	4.45	5.81	5.90	7.944e+04	32.00	6.83	0.04	0.07	0.09	20,27,20
656	4.45	3.44	3.39	7.944e+04	32.00	3.93	0.04	0.08	0.05	20,30,25
658	4.15	3.53	3.20	7.486e+04	32.00	3.70	0.04	0.14	0.06	11,32,18
660	3.93	3.47	3.71	7.133e+04	32.00	4.30	0.03	0.18	0.08	11,32,24
662	3.28	3.50	3.71	6.078e+04	32.00	4.30	0.04	0.22	0.08	26,32,24
664	3.36	3.58	3.68	6.219e+04	32.00	4.26	0.05	0.27	0.07	26,32,24
666	3.36	3.58	3.72	6.219e+04	32.00	4.31	0.05	0.27	0.02	26,32,20
1591	4.45	5.81	5.90	7.944e+04	32.00	6.83	0.04	0.07	0.09	20,27,20
1592	4.45	3.44	3.39	7.944e+04	32.00	3.93	0.04	0.08	0.05	20,30,25
1593	4.15	3.53	3.20	7.486e+04	32.00	3.70	0.04	0.14	0.06	11,32,18
1594	3.93	3.47	3.71	7.133e+04	32.00	4.30	0.03	0.18	0.08	11,32,24
1595	3.28	3.50	3.71	6.078e+04	32.00	4.30	0.04	0.22	0.08	26,32,24
1596	3.36	3.58	3.68	6.219e+04	32.00	4.26	0.05	0.27	0.07	26,32,24

1597	3.36	3.58	3.72	6.219e+04	32.00	4.31	0.05	0.27	0.02	26,32,20
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	5.44	5.81	5.90	6.078e+04	32.00	3.70				
				9.381e+04	32.00	6.83	0.05	0.27	0.09	

Setto	Mat.	Spessore	Stato
		cm	
96	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
666	3.25	3.42	3.21	6.022e+04	32.00	3.72	0.05	0.32	0.04	22,30,21
668	3.15	3.38	3.22	5.862e+04	32.00	3.73	0.09	0.40	0.04	21,30,14
670	3.15	3.38	3.22	5.862e+04	32.00	3.73	0.09	0.40	0.04	21,30,14
1597	3.25	3.42	3.21	6.022e+04	32.00	3.72	0.05	0.32	0.04	22,30,21
1598	3.15	3.38	3.22	5.862e+04	32.00	3.73	0.09	0.40	0.04	21,30,14
1599	3.15	3.38	3.22	5.862e+04	32.00	3.73	0.09	0.40	0.04	21,30,14
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	3.25	3.42	3.22	5.862e+04	32.00	3.72				
				6.022e+04	32.00	3.73	0.09	0.40	0.04	

Setto	Mat.	Spessore	Stato
		cm	
99	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
487	3.81	3.51	3.79	1.961e+06	170.00	4.39	0.06	0.12	0.06	23,30,12
495	3.81	3.51	3.79	1.961e+06	170.00	4.39	0.06	0.12	0.06	23,30,12
502	3.81	3.51	3.79	1.961e+06	170.00	4.39	0.06	0.12	0.06	23,30,12
509	3.81	3.51	3.79	1.961e+06	170.00	4.39	0.06	0.12	0.06	23,30,12
515	3.81	3.51	3.79	1.961e+06	170.00	4.39	0.06	0.12	0.06	23,30,12
1610	3.81	2.97	3.79	1.961e+06	170.00	4.39	0.06	0.12	0.06	23,30,12
1611	3.24	2.62	3.22	1.697e+06	170.00	3.73	0.05	0.13	0.04	23,30,12
1612	2.58	2.37	2.31	1.379e+06	170.00	2.68	0.05	0.14	0.03	15,30,13
1613	2.35	2.17	2.31	1.266e+06	170.00	2.68	0.05	0.15	0.03	15,30,13
1614	2.35	1.98	2.13	1.266e+06	170.00	2.46	0.05	0.15	0.04	15,30,12
1615	2.14	1.98	2.13	1.159e+06	170.00	2.46	0.05	0.15	0.04	15,30,12
1616	1.87	1.79	1.92	1.024e+06	170.00	2.23	0.04	0.15	0.04	35,30,12
1619	3.81	2.97	3.79	1.961e+06	170.00	4.39	0.06	0.12	0.06	23,30,12
1620	3.24	2.62	3.22	1.697e+06	170.00	3.73	0.05	0.13	0.04	23,30,12
1621	2.58	2.37	2.31	1.379e+06	170.00	2.68	0.05	0.14	0.03	15,30,13
1622	2.35	2.17	2.31	1.266e+06	170.00	2.68	0.05	0.15	0.03	15,30,13
1623	2.35	1.98	2.13	1.266e+06	170.00	2.46	0.05	0.15	0.04	15,30,12
1624	2.14	1.98	2.13	1.159e+06	170.00	2.46	0.05	0.15	0.04	15,30,12
1625	1.87	1.79	1.92	1.024e+06	170.00	2.23	0.04	0.15	0.04	35,30,12
1628	3.81	2.97	3.79	1.961e+06	170.00	4.39	0.06	0.12	0.06	23,30,12
1629	3.24	2.62	3.22	1.697e+06	170.00	3.73	0.05	0.13	0.04	23,30,12
1630	2.58	2.37	2.31	1.379e+06	170.00	2.68	0.05	0.14	0.03	15,30,13
1631	2.35	2.17	2.31	1.266e+06	170.00	2.68	0.05	0.15	0.03	15,30,13
1632	2.35	1.98	2.13	1.266e+06	170.00	2.46	0.05	0.15	0.04	15,30,12
1633	2.14	1.98	2.13	1.159e+06	170.00	2.46	0.05	0.15	0.04	15,30,12
1634	1.87	1.79	1.92	1.024e+06	170.00	2.23	0.04	0.15	0.04	35,30,12
1637	3.81	2.97	3.79	1.961e+06	170.00	4.39	0.06	0.12	0.06	23,30,12
1638	3.24	2.62	3.22	1.697e+06	170.00	3.73	0.05	0.13	0.04	23,30,12
1639	2.58	2.37	2.31	1.379e+06	170.00	2.68	0.05	0.14	0.03	15,30,13
1640	2.35	2.17	2.31	1.266e+06	170.00	2.68	0.05	0.15	0.03	15,30,13
1641	2.35	1.98	2.13	1.266e+06	170.00	2.46	0.05	0.15	0.04	15,30,12
1642	2.14	1.98	2.13	1.159e+06	170.00	2.46	0.05	0.15	0.04	15,30,12
1643	1.87	1.79	1.92	1.024e+06	170.00	2.23	0.04	0.15	0.04	35,30,12
1646	3.81	2.97	3.79	1.961e+06	170.00	4.39	0.06	0.12	0.06	23,30,12
1647	3.24	2.62	3.22	1.697e+06	170.00	3.73	0.05	0.13	0.04	23,30,12
1648	2.58	2.37	2.31	1.379e+06	170.00	2.68	0.05	0.14	0.03	15,30,13
1649	2.35	2.17	2.31	1.266e+06	170.00	2.68	0.05	0.15	0.03	15,30,13

1650	2.35	1.98	2.13	1.266e+06	170.00	2.46	0.05	0.15	0.04	15,30,12
1651	2.14	1.98	2.13	1.159e+06	170.00	2.46	0.05	0.15	0.04	15,30,12
1652	1.87	1.79	1.92	1.024e+06	170.00	2.23	0.04	0.15	0.04	35,30,12
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				1.024e+06	170.00	2.23				
	3.81	3.51	3.79	1.961e+06	170.00	4.39	0.06	0.15	0.06	

Setto	Mat.	Spessore	Stato
		cm	
100	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1616	1.64	1.58	1.63	9.021e+05	170.00	1.88	0.04	0.14	0.04	27,30,28
1617	1.64	1.58	1.63	9.021e+05	170.00	1.88	0.04	0.14	0.04	27,30,28
1618	1.57	1.51	1.56	6.380e+05	146.00	1.80	0.02	0.12	0.03	27,30,28
1625	1.64	1.58	1.63	9.021e+05	170.00	1.88	0.04	0.14	0.04	27,30,28
1626	1.64	1.58	1.63	9.021e+05	170.00	1.88	0.04	0.14	0.04	27,30,28
1627	1.57	1.51	1.56	6.380e+05	146.00	1.80	0.02	0.12	0.03	27,30,28
1634	1.64	1.58	1.63	9.021e+05	170.00	1.88	0.04	0.14	0.04	27,30,28
1635	1.64	1.58	1.63	9.021e+05	170.00	1.88	0.04	0.14	0.04	27,30,28
1636	1.57	1.51	1.56	6.380e+05	146.00	1.80	0.02	0.12	0.03	27,30,28
1643	1.64	1.58	1.63	9.021e+05	170.00	1.88	0.04	0.14	0.04	27,30,28
1644	1.64	1.58	1.63	9.021e+05	170.00	1.88	0.04	0.14	0.04	27,30,28
1645	1.57	1.51	1.56	6.380e+05	146.00	1.80	0.02	0.12	0.03	27,30,28
1652	1.64	1.58	1.63	9.021e+05	170.00	1.88	0.04	0.14	0.04	27,30,28
1653	1.64	1.58	1.63	9.021e+05	170.00	1.88	0.04	0.14	0.04	27,30,28
1654	1.57	1.51	1.56	6.380e+05	146.00	1.80	0.02	0.12	0.03	27,30,28
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				6.380e+05	146.00	1.80				
	1.64	1.58	1.63	9.021e+05	170.00	1.88	0.04	0.14	0.04	

Setto	Mat.	Spessore	Stato
		cm	
103	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
452	3.53	3.33	3.47	1.834e+06	170.00	4.02	0.04	0.07	0.08	16,27,11
453	3.53	3.33	3.47	1.834e+06	170.00	4.02	0.04	0.07	0.08	16,27,11
460	3.53	3.33	3.47	1.834e+06	170.00	4.02	0.04	0.07	0.08	16,27,11
467	3.53	3.33	3.47	1.834e+06	170.00	4.02	0.04	0.07	0.08	16,27,11
473	3.53	3.33	3.47	1.834e+06	170.00	4.02	0.04	0.07	0.08	16,27,11
1665	3.53	2.92	3.47	1.834e+06	170.00	4.02	0.04	0.08	0.08	16,11,11
1666	2.98	2.56	2.92	1.574e+06	170.00	3.38	0.03	0.08	0.06	16,11,11
1667	2.37	2.31	2.24	1.276e+06	170.00	2.60	0.02	0.09	0.05	40,11,14
1668	2.37	2.11	2.05	1.276e+06	170.00	2.37	0.02	0.11	0.06	40,11,14
1669	2.13	1.92	2.05	1.153e+06	170.00	2.37	0.02	0.12	0.06	38,11,14
1670	1.94	1.75	1.78	1.061e+06	170.00	2.07	0.02	0.13	0.07	30,11,12
1671	1.77	1.75	1.78	9.713e+05	170.00	2.07	0.02	0.13	0.07	30,11,12
1674	3.53	2.92	3.47	1.834e+06	170.00	4.02	0.04	0.08	0.08	16,11,11
1675	2.98	2.56	2.92	1.574e+06	170.00	3.38	0.03	0.08	0.06	16,11,11
1676	2.37	2.31	2.24	1.276e+06	170.00	2.60	0.02	0.09	0.05	40,11,14
1677	2.37	2.11	2.05	1.276e+06	170.00	2.37	0.02	0.11	0.06	40,11,14
1678	2.13	1.92	2.05	1.153e+06	170.00	2.37	0.02	0.12	0.06	38,11,14
1679	1.94	1.75	1.78	1.061e+06	170.00	2.07	0.02	0.13	0.07	30,11,12
1680	1.77	1.75	1.78	9.713e+05	170.00	2.07	0.02	0.13	0.07	30,11,12
1683	3.53	2.92	3.47	1.834e+06	170.00	4.02	0.04	0.08	0.08	16,11,11
1684	2.98	2.56	2.92	1.574e+06	170.00	3.38	0.03	0.08	0.06	16,11,11
1685	2.37	2.31	2.24	1.276e+06	170.00	2.60	0.02	0.09	0.05	40,11,14
1686	2.37	2.11	2.05	1.276e+06	170.00	2.37	0.02	0.11	0.06	40,11,14
1687	2.13	1.92	2.05	1.153e+06	170.00	2.37	0.02	0.12	0.06	38,11,14
1688	1.94	1.75	1.78	1.061e+06	170.00	2.07	0.02	0.13	0.07	30,11,12
1689	1.77	1.75	1.78	9.713e+05	170.00	2.07	0.02	0.13	0.07	30,11,12

1692	3.53	2.92	3.47	1.834e+06	170.00	4.02	0.04	0.08	0.08	16,11,11
1693	2.98	2.56	2.92	1.574e+06	170.00	3.38	0.03	0.08	0.06	16,11,11
1694	2.37	2.31	2.24	1.276e+06	170.00	2.60	0.02	0.09	0.05	40,11,14
1695	2.37	2.11	2.05	1.276e+06	170.00	2.37	0.02	0.11	0.06	40,11,14
1696	2.13	1.92	2.05	1.153e+06	170.00	2.37	0.02	0.12	0.06	38,11,14
1697	1.94	1.75	1.78	1.061e+06	170.00	2.07	0.02	0.13	0.07	30,11,12
1698	1.77	1.75	1.78	9.713e+05	170.00	2.07	0.02	0.13	0.07	30,11,12
1701	3.53	2.92	3.47	1.834e+06	170.00	4.02	0.04	0.08	0.08	16,11,11
1702	2.98	2.56	2.92	1.574e+06	170.00	3.38	0.03	0.08	0.06	16,11,11
1703	2.37	2.31	2.24	1.276e+06	170.00	2.60	0.02	0.09	0.05	40,11,14
1704	2.37	2.11	2.05	1.276e+06	170.00	2.37	0.02	0.11	0.06	40,11,14
1705	2.13	1.92	2.05	1.153e+06	170.00	2.37	0.02	0.12	0.06	38,11,14
1706	1.94	1.75	1.78	1.061e+06	170.00	2.07	0.02	0.13	0.07	30,11,12
1707	1.77	1.75	1.78	9.713e+05	170.00	2.07	0.02	0.13	0.07	30,11,12

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				9.713e+05	170.00	2.07			
	3.53	3.33	3.47	1.834e+06	170.00	4.02	0.04	0.13	0.08

Setto	Mat.	Spessore	Stato
		cm	
104	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1671	1.50	1.55	1.55	8.298e+05	170.00	1.80	0.02	0.12	0.07	27,11,11
1672	1.45	1.55	1.55	6.947e+05	170.00	1.80	0.05	0.12	0.07	27,11,11
1673	1.45	1.50	1.50	6.947e+05	158.00	1.74	0.05	0.11	0.05	27,11,11
1680	1.50	1.55	1.55	8.298e+05	170.00	1.80	0.02	0.12	0.07	27,11,11
1681	1.45	1.55	1.55	6.947e+05	170.00	1.80	0.05	0.12	0.07	27,11,11
1682	1.45	1.50	1.50	6.947e+05	158.00	1.74	0.05	0.11	0.05	27,11,11
1689	1.50	1.55	1.55	8.298e+05	170.00	1.80	0.02	0.12	0.07	27,11,11
1690	1.45	1.55	1.55	6.947e+05	170.00	1.80	0.05	0.12	0.07	27,11,11
1691	1.45	1.50	1.50	6.947e+05	158.00	1.74	0.05	0.11	0.05	27,11,11
1698	1.50	1.55	1.55	8.298e+05	170.00	1.80	0.02	0.12	0.07	27,11,11
1699	1.45	1.55	1.55	6.947e+05	170.00	1.80	0.05	0.12	0.07	27,11,11
1700	1.45	1.50	1.50	6.947e+05	158.00	1.74	0.05	0.11	0.05	27,11,11
1707	1.50	1.55	1.55	8.298e+05	170.00	1.80	0.02	0.12	0.07	27,11,11
1708	1.45	1.55	1.55	6.947e+05	170.00	1.80	0.05	0.12	0.07	27,11,11
1709	1.45	1.50	1.50	6.947e+05	158.00	1.74	0.05	0.11	0.05	27,11,11

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				6.947e+05	158.00	1.74			
	1.50	1.55	1.55	8.298e+05	170.00	1.80	0.05	0.12	0.07

Setto	Mat.	Spessore	Stato
		cm	
105	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
4	4.66	4.91	5.00	7.262e+04	30.00	5.79	0.02	0.08	0.11	27,14,11
432	4.66	4.91	5.00	7.262e+04	30.00	5.79	0.02	0.08	0.11	27,14,11
1524	3.42	4.91	5.00	5.541e+04	30.00	5.79	0.06	0.08	0.11	27,14,11
1569	3.42	3.18	3.72	5.541e+04	30.00	4.31	0.06	0.11	0.07	27,11,11
1570	3.18	2.85	2.72	5.204e+04	30.00	3.15	0.04	0.17	0.07	11,11,14
1571	2.95	2.62	2.57	4.863e+04	30.00	2.97	0.02	0.21	0.09	16,11,14
1572	2.47	2.43	2.50	4.133e+04	30.00	2.90	0.02	0.24	0.10	26,11,12
1573	2.40	2.29	2.29	4.020e+04	30.00	2.65	0.02	0.25	0.15	21,11,11
1574	2.40	2.29	2.29	4.020e+04	30.00	2.65	0.02	0.25	0.15	21,11,11
1710	3.42	4.91	5.00	5.541e+04	30.00	5.79	0.06	0.08	0.11	27,14,11
1711	3.42	3.18	3.72	5.541e+04	30.00	4.31	0.06	0.11	0.07	27,11,11
1712	3.18	2.85	2.72	5.204e+04	30.00	3.15	0.04	0.17	0.07	11,11,14
1713	2.95	2.62	2.57	4.863e+04	30.00	2.97	0.02	0.21	0.09	16,11,14
1714	2.47	2.43	2.50	4.133e+04	30.00	2.90	0.02	0.24	0.10	26,11,12
1715	2.40	2.29	2.29	4.020e+04	30.00	2.65	0.02	0.25	0.15	21,11,11

1716	2.40	2.29	2.29	4.020e+04	30.00	2.65	0.02	0.25	0.15	21,11,11
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	4.66	4.91	5.00	4.020e+04	30.00	2.65				
				7.262e+04	30.00	5.79	0.06	0.25	0.15	

Setto	Mat.	Spessore	Stato
		cm	
106	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1574	2.55	2.26	2.26	4.252e+04	30.00	2.61	0.02	0.24	0.19	18,11,11
1575	2.95	2.79	2.26	4.861e+04	30.00	2.61	0.07	0.24	0.19	17,11,11
1576	2.95	2.79	2.79	4.861e+04	30.00	3.23	0.07	0.24	0.08	17,11,11
1716	2.55	2.26	2.26	4.252e+04	30.00	2.61	0.02	0.24	0.19	18,11,11
1717	2.95	2.79	2.26	4.861e+04	30.00	2.61	0.07	0.24	0.19	17,11,11
1718	2.95	2.79	2.79	4.861e+04	30.00	3.23	0.07	0.24	0.08	17,11,11
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	2.95	2.79	2.79	4.252e+04	30.00	2.61				
				4.861e+04	30.00	3.23	0.07	0.24	0.19	

Setto	Mat.	Spessore	Stato
		cm	
107	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1384	0.65	0.66	0.68	1.115e+05	93.50	0.55	0.28	0.39	0.10	15,19,31
1447	0.65	0.66	0.68	1.115e+05	93.50	0.55	0.28	0.39	0.10	15,19,31
1456	0.65	0.66	0.68	1.115e+05	93.50	0.55	0.28	0.39	0.10	15,19,31
1724	0.65	0.66	0.68	1.115e+05	93.50	0.55	0.28	0.39	0.10	15,19,31
1725	0.65	0.66	0.68	1.115e+05	93.50	0.55	0.28	0.39	0.10	15,19,31
1728	0.41	0.55	0.42	7.077e+04	69.80	0.34	0.51	0.78	7.57e-03	41,37,15
1729	0.41	0.55	0.42	7.077e+04	69.80	0.34	0.51	0.78	7.57e-03	41,37,15
1730	0.41	0.55	0.76	7.077e+04	69.80	0.61	0.51	0.78	0.06	41,37,27
1731	0.41	0.55	0.76	7.077e+04	69.80	0.61	0.51	0.78	0.06	41,37,27
1732	1.17	0.82	0.76	1.998e+05	93.50	0.61	0.08	0.48	0.06	17,17,27
1733	1.17	0.82	0.76	1.998e+05	93.50	0.61	0.08	0.48	0.06	17,17,27
1734	1.54	1.54	1.08	2.610e+05	93.50	0.87	0.16	0.51	0.06	17,17,27
1735	1.54	1.54	1.08	2.610e+05	93.50	0.87	0.16	0.51	0.06	17,17,27
1736	1.71	1.71	1.61	2.880e+05	93.50	1.30	0.24	0.57	0.06	13,13,33
1737	1.71	1.71	1.61	2.880e+05	93.50	1.30	0.24	0.57	0.06	13,13,33
1738	1.71	1.71	1.61	2.880e+05	93.50	1.30	0.24	0.57	0.06	13,13,33
1739	1.71	1.71	1.61	2.880e+05	93.50	1.30	0.24	0.57	0.06	13,13,33
1742	0.65	0.66	0.68	1.115e+05	93.50	0.55	0.28	0.39	0.10	15,19,31
1744	0.41	0.55	0.42	7.077e+04	69.80	0.34	0.51	0.78	7.57e-03	41,37,15
1745	0.41	0.55	0.76	7.077e+04	69.80	0.61	0.51	0.78	0.06	41,37,27
1746	1.17	0.82	0.76	1.998e+05	93.50	0.61	0.08	0.48	0.06	17,17,27
1747	1.54	1.54	1.08	2.610e+05	93.50	0.87	0.16	0.51	0.06	17,17,27
1748	1.71	1.71	1.61	2.880e+05	93.50	1.30	0.24	0.57	0.06	13,13,33
1749	1.71	1.71	1.61	2.880e+05	93.50	1.30	0.24	0.57	0.06	13,13,33
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	1.71	1.71	1.61	7.077e+04	69.80	0.34				
				2.880e+05	93.50	1.30	0.51	0.78	0.10	

Setto	Mat.	Spessore	Stato
		cm	
108	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
1738	1.55	1.54	1.54	2.624e+05	93.50	1.24	0.20	0.37	0.10	13,25,21
1739	1.55	1.54	1.54	2.624e+05	93.50	1.24	0.20	0.37	0.10	13,25,21
1740	1.55	1.54	1.54	2.624e+05	93.50	1.24	0.20	0.37	0.10	13,25,21
1741	1.55	1.54	1.54	2.624e+05	93.50	1.24	0.20	0.37	0.10	13,25,21
1749	1.55	1.54	1.54	2.624e+05	93.50	1.24	0.20	0.37	0.10	13,25,21
1750	1.55	1.54	1.54	2.624e+05	93.50	1.24	0.20	0.37	0.10	13,25,21

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
	1.55	1.54	1.54	2.624e+05	93.50	1.24			
				2.624e+05	93.50	1.24	0.20	0.37	0.10

Setto	Mat.	Spessore	Stato
		cm	
111	mattoni pieni e malta di calce	38.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
1888	0.72	0.74	0.72	3.996e+05	172.75	0.82	0.13	0.03	0.03	20,20,16
1890	0.59	0.49	0.49	3.274e+05	172.75	0.56	0.19	0.04	0.09	32,20,41
1897	0.66	0.67	0.66	3.694e+05	172.75	0.76	0.17	0.03	0.03	32,21,16
1898	0.59	0.59	0.58	3.274e+05	172.75	0.67	0.19	0.04	0.05	32,20,33
1991	0.72	0.74	0.72	3.996e+05	172.75	0.82	0.13	0.03	0.03	20,20,16
1992	0.66	0.67	0.66	3.694e+05	172.75	0.76	0.17	0.03	0.03	32,21,16
1993	0.59	0.59	0.58	3.274e+05	172.75	0.67	0.19	0.04	0.05	32,20,33
2045	0.39	0.39	0.39	2.193e+05	172.75	0.44	0.20	0.04	0.11	32,20,41
2046	0.25	0.26	0.25	1.383e+05	172.75	0.28	0.17	0.04	0.08	35,20,35
2099	0.25	0.26	0.25	1.383e+05	172.75	0.28	0.17	0.04	0.08	35,20,35
2123	0.39	0.39	0.39	2.193e+05	172.75	0.44	0.20	0.04	0.11	32,20,41
2133	0.25	0.26	0.25	1.383e+05	172.75	0.28	0.17	0.04	0.08	35,20,35
2146	0.72	0.74	0.72	3.996e+05	172.75	0.82	0.13	0.03	0.03	20,20,16
2151	0.74	0.74	0.74	4.081e+05	172.75	0.84	0.11	0.03	0.02	20,20,24
2152	0.74	0.74	0.74	4.081e+05	172.75	0.84	0.11	0.03	0.02	20,20,24
2155	0.74	0.74	0.74	4.081e+05	172.75	0.84	0.11	0.03	0.02	20,20,24
2156	0.74	0.74	0.74	4.081e+05	172.75	0.84	0.11	0.03	0.02	20,20,24
2157	0.59	0.49	0.49	3.274e+05	172.75	0.56	0.19	0.04	0.09	32,20,41
2159	0.72	0.74	0.72	3.996e+05	172.75	0.82	0.13	0.03	0.03	20,20,16
2161	0.66	0.67	0.66	3.694e+05	172.75	0.76	0.17	0.03	0.03	32,21,16
2163	0.59	0.59	0.58	3.274e+05	172.75	0.67	0.19	0.04	0.05	32,20,33
2165	0.59	0.49	0.49	3.274e+05	172.75	0.56	0.19	0.04	0.09	32,20,41
2167	0.39	0.39	0.39	2.193e+05	172.75	0.44	0.20	0.04	0.11	32,20,41
2169	0.39	0.39	0.39	2.193e+05	172.75	0.44	0.20	0.04	0.11	32,20,41
2171	0.25	0.26	0.25	1.383e+05	172.75	0.28	0.17	0.04	0.08	35,20,35
2172	0.39	0.39	0.39	2.193e+05	172.75	0.44	0.20	0.04	0.11	32,20,41
2173	0.66	0.67	0.66	3.694e+05	172.75	0.76	0.17	0.03	0.03	32,21,16
2174	0.39	0.39	0.39	2.193e+05	172.75	0.44	0.20	0.04	0.11	32,20,41
2182	0.25	0.26	0.25	1.383e+05	172.75	0.28	0.17	0.04	0.08	35,20,35
2187	0.59	0.49	0.49	3.274e+05	172.75	0.56	0.19	0.04	0.09	32,20,41
2188	0.39	0.39	0.39	2.193e+05	172.75	0.44	0.20	0.04	0.11	32,20,41
2189	0.39	0.39	0.39	2.193e+05	172.75	0.44	0.20	0.04	0.11	32,20,41
2212	0.59	0.59	0.58	3.274e+05	172.75	0.67	0.19	0.04	0.05	32,20,33
2213	0.72	0.74	0.72	3.996e+05	172.75	0.82	0.13	0.03	0.03	20,20,16
2216	0.74	0.74	0.74	4.081e+05	172.75	0.84	0.11	0.03	0.02	20,20,24
2218	0.66	0.67	0.66	3.694e+05	172.75	0.76	0.17	0.03	0.03	32,21,16
2220	0.59	0.59	0.58	3.274e+05	172.75	0.67	0.19	0.04	0.05	32,20,33
2222	0.59	0.49	0.49	3.274e+05	172.75	0.56	0.19	0.04	0.09	32,20,41
2224	0.39	0.39	0.39	2.193e+05	172.75	0.44	0.20	0.04	0.11	32,20,41
2226	0.39	0.39	0.39	2.193e+05	172.75	0.44	0.20	0.04	0.11	32,20,41

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
	0.74	0.74	0.74	1.383e+05	172.75	0.28			
				4.081e+05	172.75	0.84	0.20	0.04	0.11

Setto	Mat.	Spessore	Stato
		cm	
112	mattoni pieni e malta di calce	38.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
1763	0.25	0.35	0.38	1.577e+05	184.50	0.44	0.21	0.12	0.11	39,32,27
1764	0.55	0.47	0.52	3.508e+05	184.50	0.60	0.11	0.12	0.12	21,32,38
1765	0.46	0.41	0.46	2.954e+05	184.50	0.53	0.14	0.12	0.10	21,32,38
1889	0.25	0.24	0.25	1.577e+05	184.50	0.28	0.21	0.09	0.10	39,32,27
1891	0.38	0.35	0.38	2.442e+05	184.50	0.44	0.21	0.12	0.11	33,32,27
1892	0.25	0.35	0.38	1.577e+05	184.50	0.44	0.21	0.12	0.11	39,32,27
1989	0.25	0.24	0.25	1.577e+05	184.50	0.28	0.21	0.09	0.10	39,32,27
2132	0.69	0.60	0.59	4.387e+05	184.50	0.68	0.15	0.09	0.08	20,32,42
2142	0.66	0.53	0.52	4.166e+05	184.50	0.60	0.13	0.10	0.12	20,32,38
2147	0.69	0.63	0.62	4.387e+05	184.50	0.71	0.15	0.08	0.03	20,32,42
2148	0.69	0.63	0.62	4.387e+05	184.50	0.71	0.15	0.08	0.03	20,32,42
2203	0.69	0.60	0.59	4.387e+05	184.50	0.68	0.15	0.09	0.08	20,32,42
2204	0.66	0.53	0.52	4.166e+05	184.50	0.60	0.13	0.10	0.12	20,32,38
2205	0.55	0.47	0.52	3.508e+05	184.50	0.60	0.11	0.12	0.12	21,32,38
2206	0.46	0.41	0.46	2.954e+05	184.50	0.53	0.14	0.12	0.10	21,32,38
2207	0.38	0.35	0.38	2.442e+05	184.50	0.44	0.21	0.12	0.11	33,32,27
2208	0.25	0.35	0.38	1.577e+05	184.50	0.44	0.21	0.12	0.11	39,32,27
2209	0.25	0.24	0.25	1.577e+05	184.50	0.28	0.21	0.09	0.10	39,32,27
2214	0.69	0.60	0.59	4.387e+05	184.50	0.68	0.15	0.09	0.08	20,32,42
2215	0.69	0.63	0.62	4.387e+05	184.50	0.71	0.15	0.08	0.03	20,32,42
2217	0.66	0.53	0.52	4.166e+05	184.50	0.60	0.13	0.10	0.12	20,32,38
2219	0.55	0.47	0.52	3.508e+05	184.50	0.60	0.11	0.12	0.12	21,32,38
2221	0.46	0.41	0.46	2.954e+05	184.50	0.53	0.14	0.12	0.10	21,32,38
2223	0.38	0.35	0.38	2.442e+05	184.50	0.44	0.21	0.12	0.11	33,32,27
2225	0.25	0.35	0.38	1.577e+05	184.50	0.44	0.21	0.12	0.11	39,32,27
2227	0.25	0.24	0.25	1.577e+05	184.50	0.28	0.21	0.09	0.10	39,32,27
2232	0.69	0.60	0.59	4.387e+05	184.50	0.68	0.15	0.09	0.08	20,32,42
2233	0.69	0.63	0.62	4.387e+05	184.50	0.71	0.15	0.08	0.03	20,32,42
2234	0.66	0.53	0.52	4.166e+05	184.50	0.60	0.13	0.10	0.12	20,32,38
2235	0.55	0.47	0.52	3.508e+05	184.50	0.60	0.11	0.12	0.12	21,32,38
2236	0.46	0.41	0.46	2.954e+05	184.50	0.53	0.14	0.12	0.10	21,32,38
2237	0.38	0.35	0.38	2.442e+05	184.50	0.44	0.21	0.12	0.11	33,32,27
2238	0.25	0.35	0.38	1.577e+05	184.50	0.44	0.21	0.12	0.11	39,32,27
2239	0.25	0.24	0.25	1.577e+05	184.50	0.28	0.21	0.09	0.10	39,32,27
2242	0.69	0.60	0.59	4.387e+05	184.50	0.68	0.15	0.09	0.08	20,32,42
2243	0.69	0.63	0.62	4.387e+05	184.50	0.71	0.15	0.08	0.03	20,32,42
2244	0.66	0.53	0.52	4.166e+05	184.50	0.60	0.13	0.10	0.12	20,32,38
2245	0.55	0.47	0.52	3.508e+05	184.50	0.60	0.11	0.12	0.12	21,32,38
2246	0.46	0.41	0.46	2.954e+05	184.50	0.53	0.14	0.12	0.10	21,32,38
2247	0.38	0.35	0.38	2.442e+05	184.50	0.44	0.21	0.12	0.11	33,32,27

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				1.577e+05	184.50	0.28			
	0.69	0.63	0.62	4.387e+05	184.50	0.71	0.21	0.12	0.12

Setto	Mat.	Spessore	Stato
		cm	
115	mattoni pieni e malta di calce	38.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
24	1.74	1.85	1.75	1.670e+05	73.00	2.00	0.10	0.13	0.03	42,39,21
753	1.74	1.85	1.75	1.670e+05	73.00	2.00	0.10	0.13	0.03	42,39,21
754	1.67	1.96	1.97	1.609e+05	73.00	2.26	0.11	0.14	0.03	42,39,23
755	1.57	1.88	1.97	1.516e+05	73.00	2.26	0.15	0.19	0.03	42,39,23
756	1.57	1.69	1.69	1.518e+05	73.00	1.94	0.19	0.21	0.04	40,39,39
757	1.19	1.22	1.69	1.165e+05	73.00	1.94	0.24	0.29	0.04	31,39,39
758	0.41	1.22	0.41	6.862e+04	73.00	0.47	0.35	0.29	0.07	39,39,26
759	0.41	0.41	0.41	6.862e+04	92.98	0.47	0.35	0.28	0.07	39,35,26
1771	1.19	1.22	1.69	1.165e+05	73.00	1.94	0.24	0.29	0.04	31,39,39
1772	0.41	1.22	0.41	6.862e+04	73.00	0.47	0.35	0.29	0.07	39,39,26
2126	0.41	0.41	0.41	6.862e+04	92.98	0.47	0.35	0.28	0.07	39,35,26
2127	1.74	1.85	1.75	1.670e+05	73.00	2.00	0.10	0.13	0.03	42,39,21
2154	1.74	1.85	1.75	1.670e+05	73.00	2.00	0.10	0.13	0.03	42,39,21
2175	1.74	1.85	1.75	1.670e+05	73.00	2.00	0.10	0.13	0.03	42,39,21
2176	1.67	1.96	1.97	1.609e+05	73.00	2.26	0.11	0.14	0.03	42,39,23
2177	1.57	1.88	1.97	1.516e+05	73.00	2.26	0.15	0.19	0.03	42,39,23

2178	1.57	1.69	1.69	1.518e+05	73.00	1.94	0.19	0.21	0.04	40,39,39
2179	1.19	1.22	1.69	1.165e+05	73.00	1.94	0.24	0.29	0.04	31,39,39
2180	0.41	1.22	0.41	6.862e+04	73.00	0.47	0.35	0.29	0.07	39,39,26
2181	0.41	0.41	0.41	6.862e+04	92.98	0.47	0.35	0.28	0.07	39,35,26
2183	1.74	1.85	1.75	1.670e+05	73.00	2.00	0.10	0.13	0.03	42,39,21
2190	0.41	0.41	0.41	6.862e+04	92.98	0.47	0.35	0.28	0.07	39,35,26
2191	0.41	0.41	0.41	6.862e+04	92.98	0.47	0.35	0.28	0.07	39,35,26
2192	1.67	1.96	1.97	1.609e+05	73.00	2.26	0.11	0.14	0.03	42,39,23
2240	1.57	1.88	1.97	1.516e+05	73.00	2.26	0.15	0.19	0.03	42,39,23
2241	1.57	1.69	1.69	1.518e+05	73.00	1.94	0.19	0.21	0.04	40,39,39

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				6.862e+04	73.00	0.47			
	1.74	1.96	1.97	1.670e+05	92.98	2.26	0.35	0.29	0.07

Setto	Mat.	Spessore	Stato
		cm	
118	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1503	1.51	1.65	1.65	1.738e+05	77.00	1.33	0.04	0.13	0.12	15,17,30
1512	1.51	1.65	1.65	1.738e+05	77.00	1.33	0.04	0.13	0.12	15,17,30
1521	1.51	1.65	1.65	1.738e+05	77.00	1.33	0.04	0.13	0.12	15,17,30
1787	1.27	1.42	1.65	1.469e+05	77.00	1.33	0.15	0.22	0.12	27,17,30
1788	1.44	1.44	1.40	1.658e+05	77.00	1.13	0.20	0.37	0.12	17,17,30
1789	1.44	1.44	1.25	1.658e+05	77.00	1.01	0.20	0.37	0.13	17,17,30
1790	1.31	1.31	0.92	1.518e+05	77.00	0.74	0.14	0.35	0.19	17,17,30
1791	0.61	0.95	0.65	7.103e+04	77.00	0.53	0.05	0.23	0.27	31,17,30
1792	0.33	0.33	0.41	3.937e+04	77.00	0.33	0.33	0.27	0.40	17,17,30
1793	0.33	0.33	0.41	3.937e+04	77.00	0.33	0.33	0.27	0.40	17,17,30
1796	1.27	1.42	1.65	1.469e+05	77.00	1.33	0.15	0.22	0.12	27,17,30
1797	1.44	1.44	1.40	1.658e+05	77.00	1.13	0.20	0.37	0.12	17,17,30
1798	1.44	1.44	1.25	1.658e+05	77.00	1.01	0.20	0.37	0.13	17,17,30
1799	1.31	1.31	0.92	1.518e+05	77.00	0.74	0.14	0.35	0.19	17,17,30
1800	0.61	0.95	0.65	7.103e+04	77.00	0.53	0.05	0.23	0.27	31,17,30
1801	0.33	0.33	0.41	3.937e+04	77.00	0.33	0.33	0.27	0.40	17,17,30
1802	0.33	0.33	0.41	3.937e+04	77.00	0.33	0.33	0.27	0.40	17,17,30
1805	1.27	1.42	1.65	1.469e+05	77.00	1.33	0.15	0.22	0.12	27,17,30
1806	1.44	1.44	1.40	1.658e+05	77.00	1.13	0.20	0.37	0.12	17,17,30
1807	1.44	1.44	1.25	1.658e+05	77.00	1.01	0.20	0.37	0.13	17,17,30
1808	1.31	1.31	0.92	1.518e+05	77.00	0.74	0.14	0.35	0.19	17,17,30
1809	0.61	0.95	0.65	7.103e+04	77.00	0.53	0.05	0.23	0.27	31,17,30
1810	0.33	0.33	0.41	3.937e+04	77.00	0.33	0.33	0.27	0.40	17,17,30
1811	0.33	0.33	0.41	3.937e+04	77.00	0.33	0.33	0.27	0.40	17,17,30

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				3.937e+04	77.00	0.33			
	1.51	1.65	1.65	1.738e+05	77.00	1.33	0.33	0.37	0.40

Setto	Mat.	Spessore	Stato
		cm	
122	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1148	1.54	1.77	1.66	1.770e+05	77.00	1.33	0.05	0.05	0.13	17,11,30
1151	1.54	1.77	1.66	1.770e+05	77.00	1.33	0.05	0.05	0.13	17,11,30
1586	1.54	1.77	1.66	1.770e+05	77.00	1.33	0.05	0.05	0.13	17,11,30
1850	1.31	1.49	1.34	1.509e+05	77.00	1.08	0.14	0.16	0.14	41,11,30
1851	1.39	1.51	1.34	1.598e+05	77.00	1.08	0.19	0.33	0.14	35,11,30
1852	1.39	1.51	1.18	1.598e+05	77.00	0.95	0.19	0.33	0.15	35,11,30
1853	1.42	1.42	0.94	1.638e+05	77.00	0.76	0.13	0.31	0.20	11,11,30
1854	1.10	1.10	0.78	1.270e+05	77.00	0.63	0.05	0.19	0.24	11,11,30
1855	0.55	0.55	0.56	6.446e+04	77.00	0.45	0.15	0.22	0.29	11,11,27
1856	0.39	0.49	0.43	4.563e+04	60.46	0.35	0.48	0.41	0.37	11,11,27

1857	0.39	0.49	0.43	4.563e+04	60.46	0.35	0.48	0.41	0.37	11,11,27
1859	1.31	1.49	1.34	1.509e+05	77.00	1.08	0.14	0.16	0.14	41,11,30
1860	1.39	1.51	1.34	1.598e+05	77.00	1.08	0.19	0.33	0.14	35,11,30
1861	1.39	1.51	1.18	1.598e+05	77.00	0.95	0.19	0.33	0.15	35,11,30
1862	1.42	1.42	0.94	1.638e+05	77.00	0.76	0.13	0.31	0.20	11,11,30
1863	1.10	1.10	0.78	1.270e+05	77.00	0.63	0.05	0.19	0.24	11,11,30
1864	0.55	0.55	0.56	6.446e+04	77.00	0.45	0.15	0.22	0.29	11,11,27
1865	0.39	0.49	0.43	4.563e+04	60.46	0.35	0.48	0.41	0.37	11,11,27
1866	0.39	0.49	0.43	4.563e+04	60.46	0.35	0.48	0.41	0.37	11,11,27
1868	1.31	1.49	1.34	1.509e+05	77.00	1.08	0.14	0.16	0.14	41,11,30
1869	1.39	1.51	1.34	1.598e+05	77.00	1.08	0.19	0.33	0.14	35,11,30
1870	1.39	1.51	1.18	1.598e+05	77.00	0.95	0.19	0.33	0.15	35,11,30
1871	1.42	1.42	0.94	1.638e+05	77.00	0.76	0.13	0.31	0.20	11,11,30
1872	1.10	1.10	0.78	1.270e+05	77.00	0.63	0.05	0.19	0.24	11,11,30
1873	0.55	0.55	0.56	6.446e+04	77.00	0.45	0.15	0.22	0.29	11,11,27
1874	0.39	0.49	0.43	4.563e+04	60.46	0.35	0.48	0.41	0.37	11,11,27
1875	0.39	0.49	0.43	4.563e+04	60.46	0.35	0.48	0.41	0.37	11,11,27

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				4.563e+04	60.46	0.35			
	1.54	1.77	1.66	1.770e+05	77.00	1.33	0.48	0.41	0.37

Setto	Mat.	Spessore	Stato
		cm	
123	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1857	0.36	0.54	0.41	4.248e+04	51.63	0.33	0.56	0.13	0.37	11,11,27
1858	0.36	0.54	0.41	4.248e+04	51.63	0.33	0.56	0.13	0.37	11,11,27
1866	0.36	0.54	0.41	4.248e+04	51.63	0.33	0.56	0.13	0.37	11,11,27
1867	0.36	0.54	0.41	4.248e+04	51.63	0.33	0.56	0.13	0.37	11,11,27
1875	0.36	0.54	0.41	4.248e+04	51.63	0.33	0.56	0.13	0.37	11,11,27
1876	0.36	0.54	0.41	4.248e+04	51.63	0.33	0.56	0.13	0.37	11,11,27

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				4.248e+04	51.63	0.33			
	0.36	0.54	0.41	4.248e+04	51.63	0.33	0.56	0.13	0.37

Setto	Mat.	Spessore	Stato
		cm	
128	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1576	3.26	3.08	3.08	5.310e+04	30.00	3.57	0.06	0.24	0.06	28,13,17
1718	3.26	3.08	3.08	5.310e+04	30.00	3.57	0.06	0.24	0.06	28,13,17
1931	3.26	3.08	4.11	5.310e+04	30.00	4.76	0.06	0.24	0.10	28,13,13
1932	5.02	4.11	4.64	7.716e+04	30.00	5.37	0.04	0.16	0.10	27,18,18
1933	4.39	4.39	4.64	6.902e+04	30.00	5.37	0.04	0.14	0.10	27,27,18
1934	4.39	3.11	4.21	6.902e+04	30.00	4.88	0.04	0.14	0.09	27,11,28
1935	1.72	1.75	1.72	2.942e+04	30.00	1.99	0.04	0.16	0.06	27,11,27
1936	0.41	0.46	0.38	7367.33	27.03	0.44	0.40	0.19	0.77	27,27,35
1937	0.41	0.46	0.38	7367.33	27.03	0.44	0.40	0.19	0.77	27,27,35
1978	3.26	3.08	4.11	5.310e+04	30.00	4.76	0.06	0.24	0.10	28,13,13
1979	5.02	4.11	4.64	7.716e+04	30.00	5.37	0.04	0.16	0.10	27,18,18
1980	4.39	4.39	4.64	6.902e+04	30.00	5.37	0.04	0.14	0.10	27,27,18
1981	4.39	3.11	4.21	6.902e+04	30.00	4.88	0.04	0.14	0.09	27,11,28
1982	1.72	1.75	1.72	2.942e+04	30.00	1.99	0.04	0.16	0.06	27,11,27
1983	0.41	0.46	0.38	7367.33	27.03	0.44	0.40	0.19	0.77	27,27,35
1984	0.41	0.46	0.38	7367.33	27.03	0.44	0.40	0.19	0.77	27,27,35

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				7367.33	27.03	0.44			
	5.02	4.39	4.64	7.716e+04	30.00	5.37	0.40	0.24	0.77

Setto	Mat.	Spessore	Stato
		cm	
132	mattoni pieni e malta di calce	38.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
1762	0.50	0.88	0.90	6133.22	25.50	1.03	0.14	0.02	0.04	32,32,33
1766	0.50	0.51	0.52	6133.22	25.50	0.59	0.14	0.02	0.04	32,20,33
2128	0.85	0.70	0.69	1.021e+04	25.50	0.79	0.02	0.05	0.18	24,20,39
2129	1.05	0.85	0.84	1.251e+04	25.50	0.97	0.05	8.33e-03	0.15	20,21,39
2130	1.05	1.07	1.06	1.251e+04	25.50	1.21	0.05	0.03	0.05	20,20,32
2131	1.07	1.07	1.06	1.275e+04	25.50	1.21	0.04	0.03	0.05	20,20,32
2134	0.88	0.98	0.90	1.062e+04	25.50	1.03	0.11	0.03	0.04	20,20,33
2135	0.50	0.88	0.90	6133.22	25.50	1.03	0.14	0.02	0.04	32,32,33
2136	0.50	0.51	0.52	6133.22	25.50	0.59	0.14	0.02	0.04	32,20,33
2139	0.85	0.70	0.69	1.021e+04	25.50	0.79	0.02	0.05	0.18	24,20,39
2140	1.05	0.85	0.84	1.251e+04	25.50	0.97	0.05	8.33e-03	0.15	20,21,39
2141	1.05	1.07	1.06	1.251e+04	25.50	1.21	0.05	0.03	0.05	20,20,32
2144	1.07	1.07	1.06	1.275e+04	25.50	1.21	0.04	0.03	0.05	20,20,32
2145	0.88	0.98	0.90	1.062e+04	25.50	1.03	0.11	0.03	0.04	20,20,33
2149	0.70	0.70	0.69	8499.59	25.50	0.79	9.80e-03	0.05	0.18	28,20,39
2150	0.70	0.70	0.69	8499.59	25.50	0.79	9.80e-03	0.05	0.18	28,20,39
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				6133.22	25.50	0.59				
	1.07	1.07	1.06	1.275e+04	25.50	1.21	0.14	0.05	0.18	

Setto	Mat.	Spessore	Stato
		cm	
133	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
1673	1.36	1.36	1.36	5.569e+05	146.00	1.58	0.11	0.02	0.04	27,27,27
1682	1.36	1.36	1.36	5.569e+05	146.00	1.58	0.11	0.02	0.04	27,27,27
1691	1.36	1.36	1.36	5.569e+05	146.00	1.58	0.11	0.02	0.04	27,27,27
1700	1.36	1.36	1.36	5.569e+05	146.00	1.58	0.11	0.02	0.04	27,27,27
1709	1.36	1.36	1.36	5.569e+05	146.00	1.58	0.11	0.02	0.04	27,27,27
1996	1.52	1.52	1.57	6.195e+05	146.00	1.82	0.16	0.02	0.05	27,27,30
1997	1.61	1.61	1.66	6.556e+05	146.00	1.93	0.20	0.07	0.05	27,27,30
1998	1.61	1.58	1.66	6.556e+05	146.00	1.93	0.20	0.10	0.05	27,27,30
1999	1.58	1.51	1.55	6.434e+05	146.00	1.80	0.15	0.10	0.06	27,27,11
2000	1.44	1.44	1.48	5.877e+05	146.00	1.71	0.09	0.10	0.08	18,27,11
2001	1.36	1.36	1.41	5.574e+05	146.00	1.63	0.22	0.10	0.10	27,27,11
2002	1.29	1.33	1.33	5.280e+05	141.10	1.54	0.37	0.10	0.11	27,27,15
2003	1.29	1.33	1.33	5.280e+05	141.10	1.54	0.37	0.10	0.11	27,27,15
2005	1.52	1.52	1.57	6.195e+05	146.00	1.82	0.16	0.02	0.05	27,27,30
2006	1.61	1.61	1.66	6.556e+05	146.00	1.93	0.20	0.07	0.05	27,27,30
2007	1.61	1.58	1.66	6.556e+05	146.00	1.93	0.20	0.10	0.05	27,27,30
2008	1.58	1.51	1.55	6.434e+05	146.00	1.80	0.15	0.10	0.06	27,27,11
2009	1.44	1.44	1.48	5.877e+05	146.00	1.71	0.09	0.10	0.08	18,27,11
2010	1.36	1.36	1.41	5.574e+05	146.00	1.63	0.22	0.10	0.10	27,27,11
2011	1.29	1.33	1.33	5.280e+05	141.10	1.54	0.37	0.10	0.11	27,27,15
2012	1.29	1.33	1.33	5.280e+05	141.10	1.54	0.37	0.10	0.11	27,27,15
2014	1.52	1.52	1.57	6.195e+05	146.00	1.82	0.16	0.02	0.05	27,27,30
2015	1.61	1.61	1.66	6.556e+05	146.00	1.93	0.20	0.07	0.05	27,27,30
2016	1.61	1.58	1.66	6.556e+05	146.00	1.93	0.20	0.10	0.05	27,27,30
2017	1.58	1.51	1.55	6.434e+05	146.00	1.80	0.15	0.10	0.06	27,27,11
2018	1.44	1.44	1.48	5.877e+05	146.00	1.71	0.09	0.10	0.08	18,27,11
2019	1.36	1.36	1.41	5.574e+05	146.00	1.63	0.22	0.10	0.10	27,27,11
2020	1.29	1.33	1.33	5.280e+05	141.10	1.54	0.37	0.10	0.11	27,27,15
2021	1.29	1.33	1.33	5.280e+05	141.10	1.54	0.37	0.10	0.11	27,27,15
2023	1.52	1.52	1.57	6.195e+05	146.00	1.82	0.16	0.02	0.05	27,27,30
2024	1.61	1.61	1.66	6.556e+05	146.00	1.93	0.20	0.07	0.05	27,27,30
2025	1.61	1.58	1.66	6.556e+05	146.00	1.93	0.20	0.10	0.05	27,27,30
2026	1.58	1.51	1.55	6.434e+05	146.00	1.80	0.15	0.10	0.06	27,27,11
2027	1.44	1.44	1.48	5.877e+05	146.00	1.71	0.09	0.10	0.08	18,27,11
2028	1.36	1.36	1.41	5.574e+05	146.00	1.63	0.22	0.10	0.10	27,27,11

2029	1.29	1.33	1.33	5.280e+05	141.10	1.54	0.37	0.10	0.11	27,27,15
2030	1.29	1.33	1.33	5.280e+05	141.10	1.54	0.37	0.10	0.11	27,27,15
2032	1.52	1.52	1.57	6.195e+05	146.00	1.82	0.16	0.02	0.05	27,27,30
2033	1.61	1.61	1.66	6.556e+05	146.00	1.93	0.20	0.07	0.05	27,27,30
2034	1.61	1.58	1.66	6.556e+05	146.00	1.93	0.20	0.10	0.05	27,27,30
2035	1.58	1.51	1.55	6.434e+05	146.00	1.80	0.15	0.10	0.06	27,27,11
2036	1.44	1.44	1.48	5.877e+05	146.00	1.71	0.09	0.10	0.08	18,27,11
2037	1.36	1.36	1.41	5.574e+05	146.00	1.63	0.22	0.10	0.10	27,27,11
2038	1.29	1.33	1.33	5.280e+05	141.10	1.54	0.37	0.10	0.11	27,27,15
2039	1.29	1.33	1.33	5.280e+05	141.10	1.54	0.37	0.10	0.11	27,27,15

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				5.280e+05	141.10	1.54			
	1.61	1.61	1.66	6.556e+05	146.00	1.93	0.37	0.10	0.11

Setto	Mat.	Spessore	Stato
		cm	
134	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
2003	0.87	0.91	0.89	4.231e+05	158.00	1.03	0.33	0.04	0.11	27,20,11
2004	0.87	0.91	0.89	4.231e+05	158.00	1.03	0.33	0.04	0.11	27,20,11
2012	0.87	0.91	0.89	4.231e+05	158.00	1.03	0.33	0.04	0.11	27,20,11
2013	0.87	0.91	0.89	4.231e+05	158.00	1.03	0.33	0.04	0.11	27,20,11
2021	0.87	0.91	0.89	4.231e+05	158.00	1.03	0.33	0.04	0.11	27,20,11
2022	0.87	0.91	0.89	4.231e+05	158.00	1.03	0.33	0.04	0.11	27,20,11
2030	0.87	0.91	0.89	4.231e+05	158.00	1.03	0.33	0.04	0.11	27,20,11
2031	0.87	0.91	0.89	4.231e+05	158.00	1.03	0.33	0.04	0.11	27,20,11
2039	0.87	0.91	0.89	4.231e+05	158.00	1.03	0.33	0.04	0.11	27,20,11
2040	0.87	0.91	0.89	4.231e+05	158.00	1.03	0.33	0.04	0.11	27,20,11

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				4.231e+05	158.00	1.03			
	0.87	0.91	0.89	4.231e+05	158.00	1.03	0.33	0.04	0.11

Setto	Mat.	Spessore	Stato
		cm	
136	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
670	2.60	2.99	2.94	4.932e+04	32.00	3.41	6.47e-03	0.43	0.04	22,20,32
1599	2.60	2.99	2.94	4.932e+04	32.00	3.41	6.47e-03	0.43	0.04	22,20,32
2104	3.39	2.99	2.94	6.255e+04	32.00	3.41	0.03	0.43	0.04	34,20,32
2105	3.76	3.54	3.20	6.864e+04	32.00	3.71	0.06	0.30	0.02	32,20,14
2106	3.76	3.76	2.88	6.864e+04	32.00	3.34	0.06	0.19	0.01	32,32,30
2107	2.46	3.00	1.97	4.681e+04	32.00	2.28	0.03	0.14	0.02	21,32,30
2108	1.37	2.03	1.31	2.696e+04	32.00	1.52	0.03	0.09	0.02	12,32,30
2109	0.69	0.69	0.81	1.392e+04	32.00	0.94	0.15	0.09	0.04	28,32,14
2110	0.69	0.69	0.81	1.392e+04	32.00	0.94	0.15	0.09	0.04	28,32,14
2113	3.39	2.99	2.94	6.255e+04	32.00	3.41	0.03	0.43	0.04	34,20,32
2114	3.76	3.54	3.20	6.864e+04	32.00	3.71	0.06	0.30	0.02	32,20,14
2115	3.76	3.76	2.88	6.864e+04	32.00	3.34	0.06	0.19	0.01	32,32,30
2116	2.46	3.00	1.97	4.681e+04	32.00	2.28	0.03	0.14	0.02	21,32,30
2117	1.37	2.03	1.31	2.696e+04	32.00	1.52	0.03	0.09	0.02	12,32,30
2118	0.69	0.69	0.81	1.392e+04	32.00	0.94	0.15	0.09	0.04	28,32,14
2119	0.69	0.69	0.81	1.392e+04	32.00	0.94	0.15	0.09	0.04	28,32,14

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				1.392e+04	32.00	0.94			
	3.76	3.76	3.20	6.864e+04	32.00	3.71	0.15	0.43	0.04

Setto	Mat.	Spessore	Stato
		cm	

Setto	Mat.	Spessore	Stato
139	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
1618	1.39	1.39	1.42	3.963e+05	122.00	1.65	0.08	0.03	0.04	30,30,28
1627	1.39	1.39	1.42	3.963e+05	122.00	1.65	0.08	0.03	0.04	30,30,28
1636	1.39	1.39	1.42	3.963e+05	122.00	1.65	0.08	0.03	0.04	30,30,28
1645	1.39	1.39	1.42	3.963e+05	122.00	1.65	0.08	0.03	0.04	30,30,28
1654	1.39	1.39	1.42	3.963e+05	122.00	1.65	0.08	0.03	0.04	30,30,28
2050	1.59	1.39	1.42	4.503e+05	122.00	1.65	0.14	0.03	0.04	32,30,28
2051	1.70	1.70	1.71	4.821e+05	122.00	1.98	0.18	0.05	0.04	32,32,28
2052	1.70	1.69	1.75	4.821e+05	122.00	2.02	0.18	0.08	0.04	32,32,12
2053	1.69	1.61	1.67	4.773e+05	122.00	1.94	0.15	0.08	0.05	32,32,12
2054	1.47	1.54	1.59	4.198e+05	122.00	1.84	0.07	0.08	0.06	14,32,12
2055	1.47	1.47	1.59	4.177e+05	122.00	1.84	0.19	0.08	0.06	32,32,12
2056	1.39	1.39	1.52	3.967e+05	122.00	1.76	0.33	0.08	0.06	32,32,12
2057	1.39	1.39	1.44	3.967e+05	122.00	1.67	0.33	0.08	0.05	32,32,15
2059	1.59	1.39	1.42	4.503e+05	122.00	1.65	0.14	0.03	0.04	32,30,28
2060	1.70	1.70	1.71	4.821e+05	122.00	1.98	0.18	0.05	0.04	32,32,28
2061	1.70	1.69	1.75	4.821e+05	122.00	2.02	0.18	0.08	0.04	32,32,12
2062	1.69	1.61	1.67	4.773e+05	122.00	1.94	0.15	0.08	0.05	32,32,12
2063	1.47	1.54	1.59	4.198e+05	122.00	1.84	0.07	0.08	0.06	14,32,12
2064	1.47	1.47	1.59	4.177e+05	122.00	1.84	0.19	0.08	0.06	32,32,12
2065	1.39	1.39	1.52	3.967e+05	122.00	1.76	0.33	0.08	0.06	32,32,12
2066	1.39	1.39	1.44	3.967e+05	122.00	1.67	0.33	0.08	0.05	32,32,15
2068	1.59	1.39	1.42	4.503e+05	122.00	1.65	0.14	0.03	0.04	32,30,28
2069	1.70	1.70	1.71	4.821e+05	122.00	1.98	0.18	0.05	0.04	32,32,28
2070	1.70	1.69	1.75	4.821e+05	122.00	2.02	0.18	0.08	0.04	32,32,12
2071	1.69	1.61	1.67	4.773e+05	122.00	1.94	0.15	0.08	0.05	32,32,12
2072	1.47	1.54	1.59	4.198e+05	122.00	1.84	0.07	0.08	0.06	14,32,12
2073	1.47	1.47	1.59	4.177e+05	122.00	1.84	0.19	0.08	0.06	32,32,12
2074	1.39	1.39	1.52	3.967e+05	122.00	1.76	0.33	0.08	0.06	32,32,12
2075	1.39	1.39	1.44	3.967e+05	122.00	1.67	0.33	0.08	0.05	32,32,15
2077	1.59	1.39	1.42	4.503e+05	122.00	1.65	0.14	0.03	0.04	32,30,28
2078	1.70	1.70	1.71	4.821e+05	122.00	1.98	0.18	0.05	0.04	32,32,28
2079	1.70	1.69	1.75	4.821e+05	122.00	2.02	0.18	0.08	0.04	32,32,12
2080	1.69	1.61	1.67	4.773e+05	122.00	1.94	0.15	0.08	0.05	32,32,12
2081	1.47	1.54	1.59	4.198e+05	122.00	1.84	0.07	0.08	0.06	14,32,12
2082	1.47	1.47	1.59	4.177e+05	122.00	1.84	0.19	0.08	0.06	32,32,12
2083	1.39	1.39	1.52	3.967e+05	122.00	1.76	0.33	0.08	0.06	32,32,12
2084	1.39	1.39	1.44	3.967e+05	122.00	1.67	0.33	0.08	0.05	32,32,15
2086	1.59	1.39	1.42	4.503e+05	122.00	1.65	0.14	0.03	0.04	32,30,28
2087	1.70	1.70	1.71	4.821e+05	122.00	1.98	0.18	0.05	0.04	32,32,28
2088	1.70	1.69	1.75	4.821e+05	122.00	2.02	0.18	0.08	0.04	32,32,12
2089	1.69	1.61	1.67	4.773e+05	122.00	1.94	0.15	0.08	0.05	32,32,12
2090	1.47	1.54	1.59	4.198e+05	122.00	1.84	0.07	0.08	0.06	14,32,12
2091	1.47	1.47	1.59	4.177e+05	122.00	1.84	0.19	0.08	0.06	32,32,12
2092	1.39	1.39	1.52	3.967e+05	122.00	1.76	0.33	0.08	0.06	32,32,12
2093	1.39	1.39	1.44	3.967e+05	122.00	1.67	0.33	0.08	0.05	32,32,15

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				3.963e+05	122.00	1.65			
	1.70	1.70	1.75	4.821e+05	122.00	2.02	0.33	0.08	0.06

Setto	Mat.	Spessore	Stato
		cm	
140	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
2057	0.85	0.79	0.87	3.528e+05	146.00	1.00	0.32	0.03	0.04	32,18,27
2058	0.85	0.79	0.87	3.528e+05	146.00	1.00	0.32	0.03	0.04	32,18,27
2066	0.85	0.79	0.87	3.528e+05	146.00	1.00	0.32	0.03	0.04	32,18,27
2067	0.85	0.79	0.87	3.528e+05	146.00	1.00	0.32	0.03	0.04	32,18,27
2075	0.85	0.79	0.87	3.528e+05	146.00	1.00	0.32	0.03	0.04	32,18,27
2076	0.85	0.79	0.87	3.528e+05	146.00	1.00	0.32	0.03	0.04	32,18,27
2084	0.85	0.79	0.87	3.528e+05	146.00	1.00	0.32	0.03	0.04	32,18,27

2085	0.85	0.79	0.87	3.528e+05	146.00	1.00	0.32	0.03	0.04	32,18,27
2093	0.85	0.79	0.87	3.528e+05	146.00	1.00	0.32	0.03	0.04	32,18,27
2094	0.85	0.79	0.87	3.528e+05	146.00	1.00	0.32	0.03	0.04	32,18,27

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				3.528e+05	146.00	1.00			
	0.85	0.79	0.87	3.528e+05	146.00	1.00	0.32	0.03	0.04

Setto	Mat.	Spessore	Stato
		cm	
142	mattoni pieni e malta di calce	38.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
2146	0.61	0.43	0.72	6144.88	23.16	0.83	0.07	0.07	0.03	31,36,21
2152	0.71	0.43	0.72	7062.82	23.16	0.83	0.04	0.07	0.03	41,36,21
2157	0.41	0.50	0.31	4171.70	23.16	0.36	0.07	0.03	0.12	32,35,32
2172	0.30	0.35	0.29	3028.94	23.16	0.33	0.22	0.07	0.16	20,15,32
2173	0.53	0.55	0.44	5307.24	23.16	0.50	0.08	0.05	0.06	31,42,20
2174	0.30	0.20	0.19	3028.94	23.16	0.22	0.22	0.09	0.17	20,15,20
2182	0.26	0.20	0.19	2584.24	23.16	0.22	0.17	0.09	0.17	39,15,20
2193	0.71	0.43	0.72	7062.82	23.16	0.83	0.04	0.07	0.03	41,36,21
2202	0.61	0.43	0.72	6144.88	23.16	0.83	0.07	0.07	0.03	31,36,21
2210	0.53	0.55	0.44	5307.24	23.16	0.50	0.08	0.05	0.06	31,42,20
2211	0.53	0.64	0.37	5307.24	23.16	0.43	0.08	0.03	0.08	31,18,20
2212	0.53	0.64	0.37	5307.24	23.16	0.43	0.08	0.03	0.08	31,18,20
2228	0.41	0.50	0.31	4171.70	23.16	0.36	0.07	0.03	0.12	32,35,32
2229	0.30	0.35	0.29	3028.94	23.16	0.33	0.22	0.07	0.16	20,15,32
2230	0.30	0.20	0.19	3028.94	23.16	0.22	0.22	0.09	0.17	20,15,20
2231	0.26	0.20	0.19	2584.24	23.16	0.22	0.17	0.09	0.17	39,15,20

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				2584.24	23.16	0.22			
	0.71	0.64	0.72	7062.82	23.16	0.83	0.22	0.09	0.17

Setto	Mat.	Spessore	Stato
		cm	
143	mattoni pieni e malta di calce	38.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
28	0.92	1.22	1.22	4.438e+04	51.16	1.40	0.06	0.09	0.02	36,37,37
727	1.32	1.32	1.01	6.307e+04	51.16	1.16	0.03	0.09	0.02	37,37,36
728	1.32	1.32	1.01	6.307e+04	51.16	1.16	0.03	0.09	0.02	37,37,36
729	1.19	1.19	0.94	5.721e+04	51.16	1.08	0.02	0.09	0.01	37,37,35
730	0.71	0.72	0.71	3.436e+04	51.16	0.81	0.07	0.12	0.02	35,37,35
737	0.36	0.41	0.40	1.758e+04	51.16	0.46	0.32	0.14	0.03	35,17,20
738	0.36	0.41	0.40	1.758e+04	51.16	0.46	0.32	0.14	0.03	35,17,20
766	0.92	1.28	1.22	4.438e+04	51.16	1.40	0.06	0.09	0.02	36,37,37
2158	0.92	1.28	1.22	4.438e+04	51.16	1.40	0.06	0.09	0.02	36,37,37
2160	1.32	1.32	1.01	6.307e+04	51.16	1.16	0.03	0.09	0.02	37,37,36
2162	1.32	1.32	1.01	6.307e+04	51.16	1.16	0.03	0.09	0.02	37,37,36
2164	1.19	1.19	0.94	5.721e+04	51.16	1.08	0.02	0.09	0.01	37,37,35
2166	0.71	0.72	0.71	3.436e+04	51.16	0.81	0.07	0.12	0.02	35,37,35
2168	0.36	0.41	0.40	1.758e+04	51.16	0.46	0.32	0.14	0.03	35,17,20
2170	0.36	0.41	0.40	1.758e+04	51.16	0.46	0.32	0.14	0.03	35,17,20
2201	0.92	1.22	1.22	4.438e+04	51.16	1.40	0.06	0.09	0.02	36,37,37

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				1.758e+04	51.16	0.46			
	1.32	1.32	1.22	6.307e+04	51.16	1.40	0.32	0.14	0.03

Setto	Mat.	Spessore	Stato
		cm	
146	mattoni pieni e malta di calce	38.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
2147	0.87	0.82	0.70	1.962e+04	35.00	0.81	0.05	0.11	0.05	39,42,21
2153	0.87	0.82	0.70	1.962e+04	35.00	0.81	0.05	0.11	0.05	39,42,21
2194	0.83	0.82	0.70	1.893e+04	35.00	0.81	0.07	0.11	0.05	42,42,21
2195	0.90	0.92	0.68	2.040e+04	35.00	0.78	0.13	0.09	0.03	42,30,21
2196	0.77	0.80	0.55	1.751e+04	35.00	0.63	0.14	0.11	0.03	42,30,21
2197	0.77	0.80	0.45	1.751e+04	35.00	0.52	0.14	0.11	0.04	42,30,26
2198	0.48	0.26	0.33	1.102e+04	35.00	0.38	0.22	0.10	0.06	33,38,32
2199	0.10	0.47	0.10	2266.13	7.27	0.11	0.86	0.28	0.41	42,42,38
2200	0.10	0.47	0.10	2266.13	7.27	0.11	0.86	0.28	0.41	42,42,38
2203	0.83	0.82	0.70	1.893e+04	35.00	0.81	0.07	0.11	0.05	42,42,21
2204	0.90	0.92	0.68	2.040e+04	35.00	0.78	0.13	0.09	0.03	42,30,21
2205	0.77	0.80	0.55	1.751e+04	35.00	0.63	0.14	0.11	0.03	42,30,21
2206	0.77	0.80	0.45	1.751e+04	35.00	0.52	0.14	0.11	0.04	42,30,26
2207	0.48	0.26	0.33	1.102e+04	35.00	0.38	0.22	0.10	0.06	33,38,32
2208	0.10	0.47	0.10	2266.13	7.27	0.11	0.86	0.28	0.41	42,42,38
2209	0.10	0.47	0.10	2266.13	7.27	0.11	0.86	0.28	0.41	42,42,38

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				2266.13	7.27	0.11			
	0.90	0.92	0.70	2.040e+04	35.00	0.81	0.86	0.28	0.41

Setto	Mat.	Spessore	Stato
		cm	
147	muratura E = 2.000e+04 mattoni in argilla espansa e cls con malta M2	30.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
670	0.61	0.61	0.60	1.048e+06	343.50	0.84	0.16	0.20	0.07	27,27,20
671	0.61	0.61	0.60	1.048e+06	343.50	0.84	0.16	0.20	0.07	27,27,20
680	0.61	0.61	0.60	1.048e+06	343.50	0.84	0.16	0.20	0.07	27,27,20
684	0.61	0.61	0.60	1.048e+06	343.50	0.84	0.16	0.20	0.07	27,27,20
690	0.61	0.61	0.60	1.048e+06	343.50	0.84	0.16	0.20	0.07	27,27,20
699	0.61	0.61	0.60	1.048e+06	343.50	0.84	0.16	0.20	0.07	27,27,20
709	0.61	0.61	0.60	1.048e+06	343.50	0.84	0.16	0.20	0.07	27,27,20
2113	0.61	0.61	0.60	1.048e+06	343.50	0.84	0.16	0.20	0.07	27,27,20
2114	0.58	0.58	0.57	1.005e+06	343.50	0.81	0.13	0.18	0.06	27,27,20
2115	0.53	0.53	0.46	9.089e+05	343.50	0.65	0.09	0.12	0.06	27,27,29
2116	0.37	0.37	0.41	6.463e+05	343.50	0.58	0.08	0.13	0.09	30,30,31
2117	0.37	0.30	0.34	6.463e+05	343.50	0.48	0.08	0.14	0.11	30,30,31
2118	0.31	0.30	0.24	5.425e+05	343.50	0.34	0.08	0.14	0.12	32,30,20
2119	0.23	0.23	0.24	4.070e+05	343.50	0.34	0.07	0.12	0.12	32,30,20
2120	0.17	0.15	0.15	2.920e+05	343.50	0.21	0.06	0.10	0.10	33,30,32
2248	0.61	0.61	0.60	1.048e+06	343.50	0.84	0.16	0.20	0.07	27,27,20
2249	0.58	0.58	0.57	1.005e+06	343.50	0.81	0.13	0.18	0.06	27,27,20
2257	0.61	0.61	0.60	1.048e+06	343.50	0.84	0.16	0.20	0.07	27,27,20
2258	0.58	0.58	0.57	1.005e+06	343.50	0.81	0.13	0.18	0.06	27,27,20
2264	0.37	0.30	0.34	6.463e+05	343.50	0.48	0.08	0.14	0.11	30,30,31
2266	0.61	0.61	0.60	1.048e+06	343.50	0.84	0.16	0.20	0.07	27,27,20
2267	0.58	0.58	0.57	1.005e+06	343.50	0.81	0.13	0.18	0.06	27,27,20
2274	0.61	0.61	0.60	1.048e+06	343.50	0.84	0.16	0.20	0.07	27,27,20
2275	0.61	0.61	0.60	1.048e+06	343.50	0.84	0.16	0.20	0.07	27,27,20
2276	0.58	0.58	0.57	1.005e+06	343.50	0.81	0.13	0.18	0.06	27,27,20
2281	0.58	0.58	0.57	1.005e+06	343.50	0.81	0.13	0.18	0.06	27,27,20
2282	0.53	0.53	0.46	9.089e+05	343.50	0.65	0.09	0.12	0.06	27,27,29
2283	0.37	0.37	0.41	6.463e+05	343.50	0.58	0.08	0.13	0.09	30,30,31
2284	0.61	0.61	0.60	1.048e+06	343.50	0.84	0.16	0.20	0.07	27,27,20
2285	0.58	0.58	0.57	1.005e+06	343.50	0.81	0.13	0.18	0.06	27,27,20
2471	0.23	0.23	0.24	4.070e+05	343.50	0.34	0.07	0.12	0.12	32,30,20
2472	0.17	0.15	0.15	2.920e+05	343.50	0.21	0.06	0.10	0.10	33,30,32
2473	0.53	0.53	0.46	9.089e+05	343.50	0.65	0.09	0.12	0.06	27,27,29
2476	0.53	0.53	0.46	9.089e+05	343.50	0.65	0.09	0.12	0.06	27,27,29
2477	0.37	0.37	0.41	6.463e+05	343.50	0.58	0.08	0.13	0.09	30,30,31
3338	0.37	0.37	0.41	6.463e+05	343.50	0.58	0.08	0.13	0.09	30,30,31
3344	0.37	0.30	0.34	6.463e+05	343.50	0.48	0.08	0.14	0.11	30,30,31
3348	0.31	0.30	0.24	5.425e+05	343.50	0.34	0.08	0.14	0.12	32,30,20

3352	0.23	0.23	0.24	4.070e+05	343.50	0.34	0.07	0.12	0.12	32,30,20
3356	0.17	0.15	0.15	2.920e+05	343.50	0.21	0.06	0.10	0.10	33,30,32
3360	0.37	0.30	0.34	6.463e+05	343.50	0.48	0.08	0.14	0.11	30,30,31
3361	0.31	0.30	0.24	5.425e+05	343.50	0.34	0.08	0.14	0.12	32,30,20
3362	0.23	0.23	0.24	4.070e+05	343.50	0.34	0.07	0.12	0.12	32,30,20
3363	0.17	0.15	0.15	2.920e+05	343.50	0.21	0.06	0.10	0.10	33,30,32
3364	0.31	0.30	0.24	5.425e+05	343.50	0.34	0.08	0.14	0.12	32,30,20
3365	0.53	0.53	0.46	9.089e+05	343.50	0.65	0.09	0.12	0.06	27,27,29
3366	0.37	0.37	0.41	6.463e+05	343.50	0.58	0.08	0.13	0.09	30,30,31
3367	0.37	0.30	0.34	6.463e+05	343.50	0.48	0.08	0.14	0.11	30,30,31
3368	0.31	0.30	0.24	5.425e+05	343.50	0.34	0.08	0.14	0.12	32,30,20
3369	0.23	0.23	0.24	4.070e+05	343.50	0.34	0.07	0.12	0.12	32,30,20
3370	0.17	0.15	0.15	2.920e+05	343.50	0.21	0.06	0.10	0.10	33,30,32
3371	0.23	0.23	0.24	4.070e+05	343.50	0.34	0.07	0.12	0.12	32,30,20
3372	0.53	0.53	0.46	9.089e+05	343.50	0.65	0.09	0.12	0.06	27,27,29
3373	0.37	0.37	0.41	6.463e+05	343.50	0.58	0.08	0.13	0.09	30,30,31
3374	0.37	0.30	0.34	6.463e+05	343.50	0.48	0.08	0.14	0.11	30,30,31
3375	0.31	0.30	0.24	5.425e+05	343.50	0.34	0.08	0.14	0.12	32,30,20
3376	0.23	0.23	0.24	4.070e+05	343.50	0.34	0.07	0.12	0.12	32,30,20
3377	0.17	0.15	0.15	2.920e+05	343.50	0.21	0.06	0.10	0.10	33,30,32
3378	0.17	0.15	0.15	2.920e+05	343.50	0.21	0.06	0.10	0.10	33,30,32
3379	0.53	0.53	0.46	9.089e+05	343.50	0.65	0.09	0.12	0.06	27,27,29
3380	0.37	0.37	0.41	6.463e+05	343.50	0.58	0.08	0.13	0.09	30,30,31
3381	0.37	0.30	0.34	6.463e+05	343.50	0.48	0.08	0.14	0.11	30,30,31
3382	0.31	0.30	0.24	5.425e+05	343.50	0.34	0.08	0.14	0.12	32,30,20

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				2.920e+05	343.50	0.21			
	0.61	0.61	0.60	1.048e+06	343.50	0.84	0.16	0.20	0.12

Setto	Mat.	Spessore	Stato
		cm	
150	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
2251	0.17	0.15	0.16	5.800e+04	129.00	0.13	0.08	0.05	0.99	24,22,31
2252	0.17	0.15	0.15	5.800e+04	129.00	0.12	0.08	0.05	0.78	24,22,31
2254	0.17	0.15	0.16	5.800e+04	129.00	0.13	0.08	0.05	0.99	24,22,31
2255	0.17	0.15	0.15	5.800e+04	129.00	0.12	0.08	0.05	0.78	24,22,31
2313	0.19	0.16	0.16	6.304e+04	129.00	0.13	0.07	0.03	0.99	24,22,31
2322	0.19	0.16	0.16	6.304e+04	129.00	0.13	0.07	0.03	0.99	24,22,31
2331	0.19	0.16	0.16	6.304e+04	129.00	0.13	0.07	0.03	0.99	24,22,31
2407	0.19	0.16	0.16	6.304e+04	129.00	0.13	0.07	0.03	0.99	24,22,31
3330	0.17	0.15	0.16	5.800e+04	129.00	0.13	0.08	0.05	0.99	24,22,31
3331	0.17	0.15	0.15	5.800e+04	129.00	0.12	0.08	0.05	0.78	24,22,31
3333	0.17	0.15	0.16	5.800e+04	129.00	0.13	0.08	0.05	0.99	24,22,31
3334	0.17	0.15	0.15	5.800e+04	129.00	0.12	0.08	0.05	0.78	24,22,31

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				5.800e+04	129.00	0.12			
	0.19	0.16	0.16	6.304e+04	129.00	0.13	0.08	0.05	0.99

Setto	Mat.	Spessore	Stato
		cm	
151	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
2250	0.07	0.07	0.07	2.361e+04	129.00	0.05	0.07	0.03	0.43	32,22,31
2252	0.07	0.07	0.07	2.361e+04	129.00	0.05	0.07	0.03	0.43	32,22,31
2253	0.07	0.07	0.07	2.361e+04	129.00	0.05	0.07	0.03	0.43	32,22,31
2255	0.07	0.07	0.07	2.361e+04	129.00	0.05	0.07	0.03	0.43	32,22,31
2256	0.07	0.07	0.07	2.361e+04	129.00	0.05	0.07	0.03	0.43	32,22,31
3331	0.07	0.07	0.07	2.361e+04	129.00	0.05	0.07	0.03	0.43	32,22,31
3332	0.07	0.07	0.07	2.361e+04	129.00	0.05	0.07	0.03	0.43	32,22,31

3334	0.07	0.07	0.07	2.361e+04	129.00	0.05	0.07	0.03	0.43	32,22,31
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	0.07	0.07	0.07	2.361e+04	129.00	0.05	0.07	0.03	0.43	

Setto	Mat.	Spessore	Stato
		cm	
154	mattoni pieni e malta di calce INTONACO ARMATO	25.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
2270	0.27	0.27	0.24	2075.92	25.00	0.12	0.13	0.02	0.96	21,21,36
2271	0.08	0.08	0.07	1589.14	40.00	0.04	0.13	7.91e-03	0.64	22,22,29
2277	0.08	0.08	0.07	1589.14	40.00	0.04	0.13	7.91e-03	0.64	22,22,29
2278	0.20	0.27	0.24	1530.79	25.00	0.12	0.14	0.02	0.96	20,21,36
2279	0.20	0.27	0.24	1530.79	25.00	0.12	0.14	0.02	0.96	20,21,36
2280	0.20	0.22	0.21	1530.79	25.00	0.10	0.14	0.02	0.83	20,21,36
2286	0.20	0.22	0.21	1530.79	25.00	0.10	0.14	0.02	0.83	20,21,36
3246	0.27	0.27	0.24	2075.92	25.00	0.12	0.13	0.02	0.96	21,21,36
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				1530.79	25.00	0.04				
	0.27	0.27	0.24	2075.92	40.00	0.12	0.14	0.02	0.96	

Setto	Mat.	Spessore	Stato
		cm	
155	mattoni pieni e malta di calce INTONACO ARMATO	25.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
286	0.20	0.27	0.24	1531.45	25.00	0.12	0.14	0.02	0.83	22,19,38
287	0.20	0.27	0.24	1531.45	25.00	0.12	0.14	0.02	0.83	22,19,38
288	0.20	0.22	0.21	1531.45	25.00	0.10	0.14	0.02	0.73	22,19,38
2277	0.08	0.08	0.07	1588.84	40.00	0.04	0.13	8.46e-03	0.58	20,19,35
3159	0.08	0.08	0.07	1588.84	40.00	0.04	0.13	8.46e-03	0.58	20,19,35
3315	0.27	0.27	0.24	2071.72	25.00	0.12	0.14	0.02	0.83	19,19,38
3319	0.27	0.27	0.24	2071.72	25.00	0.12	0.14	0.02	0.83	19,19,38
3324	0.20	0.22	0.21	1531.45	25.00	0.10	0.14	0.02	0.73	22,19,38
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				1531.45	25.00	0.04				
	0.27	0.27	0.24	2071.72	40.00	0.12	0.14	0.02	0.83	

Setto	Mat.	Spessore	Stato
		cm	
156	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
670	1.41	1.68	1.57	1.123e+05	64.00	1.27	0.23	0.68	0.05	21,20,30
935	1.41	1.68	1.57	1.123e+05	64.00	1.27	0.23	0.68	0.05	21,20,30
2113	1.41	1.68	1.67	1.123e+05	64.00	1.35	0.23	0.68	0.06	21,20,16
2114	1.66	1.70	1.58	1.315e+05	64.00	1.27	0.08	0.53	0.12	32,20,28
2115	1.59	1.62	1.58	1.260e+05	64.00	1.27	0.07	0.44	0.12	32,20,28
2116	1.49	1.51	1.51	1.187e+05	64.00	1.21	0.06	0.36	0.05	32,20,24
2117	1.31	1.32	1.04	1.043e+05	64.00	0.84	0.04	0.30	0.05	32,20,34
2118	0.84	1.08	0.83	6.773e+04	64.00	0.67	0.05	0.27	0.10	28,20,30
2119	0.71	0.70	0.70	5.765e+04	64.00	0.56	0.08	0.28	0.24	40,32,32
2120	0.71	0.70	0.70	5.765e+04	64.00	0.56	0.08	0.28	0.24	40,32,32
2287	1.41	1.68	1.67	1.123e+05	64.00	1.35	0.23	0.68	0.06	21,20,16

2288	1.66	1.70	1.58	1.315e+05	64.00	1.27	0.08	0.53	0.12	32,20,28
2289	1.59	1.62	1.58	1.260e+05	64.00	1.27	0.07	0.44	0.12	32,20,28
2290	1.49	1.51	1.51	1.187e+05	64.00	1.21	0.06	0.36	0.05	32,20,24
2291	1.31	1.32	1.04	1.043e+05	64.00	0.84	0.04	0.30	0.05	32,20,34
2292	0.84	1.08	0.83	6.773e+04	64.00	0.67	0.05	0.27	0.10	28,20,30
2293	0.71	0.70	0.70	5.765e+04	64.00	0.56	0.08	0.28	0.24	40,32,32
2294	0.71	0.70	0.70	5.765e+04	64.00	0.56	0.08	0.28	0.24	40,32,32

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				5.765e+04	64.00	0.56				
	1.66	1.70	1.67	1.315e+05	64.00	1.35	0.23	0.68	0.24	

Setto	Mat.	Spessore	Stato
		cm	
157	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
2120	0.40	0.53	0.40	3.266e+04	64.00	0.32	0.18	0.27	0.36	30,27,32
2121	0.40	0.53	0.40	3.266e+04	64.00	0.32	0.18	0.27	0.36	30,27,32
2294	0.40	0.53	0.40	3.266e+04	64.00	0.32	0.18	0.27	0.36	30,27,32
2295	0.40	0.53	0.40	3.266e+04	64.00	0.32	0.18	0.27	0.36	30,27,32

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				3.266e+04	64.00	0.32				
	0.40	0.53	0.40	3.266e+04	64.00	0.32	0.18	0.27	0.36	

Setto	Mat.	Spessore	Stato
		cm	
160	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1020	1.51	1.51	1.30	5.102e+05	132.00	1.05	0.19	0.11	0.30	21,21,28
1030	1.51	1.51	1.30	5.102e+05	132.00	1.05	0.19	0.11	0.30	21,21,28
1039	1.51	1.51	1.30	5.102e+05	132.00	1.05	0.19	0.11	0.30	21,21,28
2305	1.51	1.51	1.30	5.102e+05	132.00	1.05	0.19	0.11	0.30	21,21,28
2306	1.48	1.29	1.30	4.994e+05	132.00	1.05	0.13	0.09	0.25	21,20,28
2307	1.41	1.34	1.31	4.783e+05	132.00	1.05	0.09	0.14	0.16	21,20,28
2308	1.39	1.39	1.33	4.721e+05	132.00	1.07	0.13	0.18	0.10	20,20,28
2309	1.39	1.31	1.37	4.721e+05	132.00	1.10	0.13	0.22	0.06	20,20,28
2310	1.31	1.12	1.06	4.431e+05	132.00	0.86	0.10	0.26	0.10	20,20,27
2311	1.02	0.99	0.94	3.498e+05	132.00	0.76	0.02	0.26	0.17	21,20,31
2312	0.91	0.99	0.94	3.109e+05	132.00	0.76	0.02	0.26	0.17	21,20,31
2314	1.51	1.51	1.30	5.102e+05	132.00	1.05	0.19	0.11	0.30	21,21,28
2315	1.48	1.29	1.30	4.994e+05	132.00	1.05	0.13	0.09	0.25	21,20,28
2316	1.41	1.34	1.31	4.783e+05	132.00	1.05	0.09	0.14	0.16	21,20,28
2317	1.39	1.39	1.33	4.721e+05	132.00	1.07	0.13	0.18	0.10	20,20,28
2318	1.39	1.31	1.37	4.721e+05	132.00	1.10	0.13	0.22	0.06	20,20,28
2319	1.31	1.12	1.06	4.431e+05	132.00	0.86	0.10	0.26	0.10	20,20,27
2320	1.02	0.99	0.94	3.498e+05	132.00	0.76	0.02	0.26	0.17	21,20,31
2321	0.91	0.99	0.94	3.109e+05	132.00	0.76	0.02	0.26	0.17	21,20,31
2327	1.39	1.31	1.37	4.721e+05	132.00	1.10	0.13	0.22	0.06	20,20,28
2328	1.31	1.12	1.06	4.431e+05	132.00	0.86	0.10	0.26	0.10	20,20,27
2329	1.02	0.99	0.94	3.498e+05	132.00	0.76	0.02	0.26	0.17	21,20,31
2330	0.91	0.99	0.94	3.109e+05	132.00	0.76	0.02	0.26	0.17	21,20,31
2386	1.48	1.29	1.30	4.994e+05	132.00	1.05	0.13	0.09	0.25	21,20,28
2387	1.41	1.34	1.31	4.783e+05	132.00	1.05	0.09	0.14	0.16	21,20,28
2388	1.39	1.39	1.33	4.721e+05	132.00	1.07	0.13	0.18	0.10	20,20,28
2404	1.02	0.99	0.94	3.498e+05	132.00	0.76	0.02	0.26	0.17	21,20,31
2406	0.91	0.99	0.94	3.109e+05	132.00	0.76	0.02	0.26	0.17	21,20,31
2408	1.51	1.51	1.30	5.102e+05	132.00	1.05	0.19	0.11	0.30	21,21,28
2424	1.51	1.51	1.30	5.102e+05	132.00	1.05	0.19	0.11	0.30	21,21,28
2425	1.51	1.51	1.30	5.102e+05	132.00	1.05	0.19	0.11	0.30	21,21,28
2426	1.48	1.29	1.30	4.994e+05	132.00	1.05	0.13	0.09	0.25	21,20,28
2427	1.41	1.34	1.31	4.783e+05	132.00	1.05	0.09	0.14	0.16	21,20,28

2428	1.39	1.39	1.33	4.721e+05	132.00	1.07	0.13	0.18	0.10	20,20,28
2429	1.39	1.31	1.37	4.721e+05	132.00	1.10	0.13	0.22	0.06	20,20,28
2430	1.31	1.12	1.06	4.431e+05	132.00	0.86	0.10	0.26	0.10	20,20,27

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				3.109e+05	132.00	0.76				
	1.51	1.51	1.37	5.102e+05	132.00	1.10	0.19	0.26	0.30	

Setto	Mat.	Spessore	Stato
		cm	
161	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
2312	0.62	0.68	0.64	2.092e+05	130.50	0.51	0.01	0.23	0.30	21,20,31
2313	0.62	0.68	0.64	2.092e+05	130.50	0.51	0.01	0.23	0.30	21,20,31
2321	0.62	0.68	0.64	2.092e+05	130.50	0.51	0.01	0.23	0.30	21,20,31
2322	0.62	0.68	0.64	2.092e+05	130.50	0.51	0.01	0.23	0.30	21,20,31
2330	0.62	0.68	0.64	2.092e+05	130.50	0.51	0.01	0.23	0.30	21,20,31
2331	0.62	0.68	0.64	2.092e+05	130.50	0.51	0.01	0.23	0.30	21,20,31
2406	0.62	0.68	0.64	2.092e+05	130.50	0.51	0.01	0.23	0.30	21,20,31
2407	0.62	0.68	0.64	2.092e+05	130.50	0.51	0.01	0.23	0.30	21,20,31

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				2.092e+05	130.50	0.51				
	0.62	0.68	0.64	2.092e+05	130.50	0.51	0.01	0.23	0.30	

Setto	Mat.	Spessore	Stato
		cm	
163	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
875	1.70	2.04	2.02	6.955e+04	46.00	1.62	0.27	0.66	0.03	36,21,13
929	1.70	2.04	2.02	6.955e+04	46.00	1.62	0.27	0.66	0.03	36,21,13
2323	1.94	1.73	1.94	7.878e+04	46.00	1.56	0.07	0.59	0.04	21,26,29
2324	1.79	1.73	1.42	7.321e+04	46.00	1.14	0.06	0.59	0.07	21,26,28
2325	1.60	1.55	1.29	6.544e+04	46.00	1.04	0.02	0.58	0.11	39,26,42
2326	1.21	1.37	1.29	4.991e+04	46.00	1.04	0.04	0.49	0.11	26,26,42
2332	1.20	1.21	1.16	4.974e+04	46.00	0.93	0.04	0.33	0.08	26,26,42
2333	1.55	1.20	1.62	6.342e+04	46.00	1.30	0.10	0.22	0.14	20,26,35
2334	1.55	1.47	1.62	6.342e+04	46.00	1.30	0.10	0.14	0.14	20,38,35
2414	1.70	2.04	1.94	6.955e+04	46.00	1.56	0.27	0.66	0.04	36,21,29
2415	1.94	1.73	1.94	7.878e+04	46.00	1.56	0.07	0.59	0.04	21,26,29
2416	1.79	1.73	1.42	7.321e+04	46.00	1.14	0.06	0.59	0.07	21,26,28
2417	1.60	1.55	1.29	6.544e+04	46.00	1.04	0.02	0.58	0.11	39,26,42
2418	1.21	1.37	1.29	4.991e+04	46.00	1.04	0.04	0.49	0.11	26,26,42
2419	1.20	1.21	1.16	4.974e+04	46.00	0.93	0.04	0.33	0.08	26,26,42
2420	1.55	1.20	1.62	6.342e+04	46.00	1.30	0.10	0.22	0.14	20,26,35
2421	1.55	1.47	1.62	6.342e+04	46.00	1.30	0.10	0.14	0.14	20,38,35
2423	1.70	2.04	1.94	6.955e+04	46.00	1.56	0.27	0.66	0.04	36,21,29

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				4.974e+04	46.00	0.93				
	1.94	2.04	2.02	7.878e+04	46.00	1.62	0.27	0.66	0.14	

Setto	Mat.	Spessore	Stato
		cm	
166	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
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	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
2334	1.55	1.58	1.66	6.358e+04	45.54	1.34	0.35	0.09	0.19	42,26,33
2335	1.55	1.58	1.66	6.358e+04	45.54	1.34	0.35	0.09	0.19	42,26,33
2421	1.55	1.58	1.66	6.358e+04	45.54	1.34	0.35	0.09	0.19	42,26,33
2422	1.55	1.58	1.66	6.358e+04	45.54	1.34	0.35	0.09	0.19	42,26,33
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	1.55	1.58	1.66	6.358e+04	45.54	1.34	0.35	0.09	0.19	

Setto	Mat.	Spessore	Stato
		cm	
167	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
975	1.61	1.61	1.36	5.522e+05	133.00	1.10	0.17	0.09	0.36	19,23,34
984	1.61	1.61	1.36	5.522e+05	133.00	1.10	0.17	0.09	0.36	19,23,34
993	1.61	1.61	1.36	5.522e+05	133.00	1.10	0.17	0.09	0.36	19,23,34
1002	1.61	1.61	1.36	5.522e+05	133.00	1.10	0.17	0.09	0.36	19,23,34
2341	1.61	1.61	1.36	5.522e+05	133.00	1.10	0.17	0.09	0.36	19,23,34
2342	1.53	1.41	1.41	5.240e+05	133.00	1.14	0.15	0.07	0.33	24,23,28
2343	1.20	1.41	1.32	4.141e+05	133.00	1.06	0.17	0.07	0.26	26,23,28
2344	1.15	1.27	1.21	3.991e+05	133.00	0.98	0.19	0.07	0.19	26,23,32
2345	1.15	1.02	1.10	3.991e+05	133.00	0.89	0.19	0.08	0.11	26,21,32
2346	1.02	0.82	0.81	3.542e+05	133.00	0.65	0.16	0.15	0.12	21,21,31
2347	0.69	0.70	0.69	2.415e+05	133.00	0.56	0.14	0.20	0.19	26,21,31
2348	0.69	0.70	0.69	2.415e+05	133.00	0.56	0.14	0.20	0.19	26,21,31
2350	1.61	1.61	1.36	5.522e+05	133.00	1.10	0.17	0.09	0.36	19,23,34
2351	1.53	1.41	1.41	5.240e+05	133.00	1.14	0.15	0.07	0.33	24,23,28
2352	1.20	1.41	1.32	4.141e+05	133.00	1.06	0.17	0.07	0.26	26,23,28
2353	1.15	1.27	1.21	3.991e+05	133.00	0.98	0.19	0.07	0.19	26,23,32
2354	1.15	1.02	1.10	3.991e+05	133.00	0.89	0.19	0.08	0.11	26,21,32
2355	1.02	0.82	0.81	3.542e+05	133.00	0.65	0.16	0.15	0.12	21,21,31
2356	0.69	0.70	0.69	2.415e+05	133.00	0.56	0.14	0.20	0.19	26,21,31
2357	0.69	0.70	0.69	2.415e+05	133.00	0.56	0.14	0.20	0.19	26,21,31
2359	1.61	1.61	1.36	5.522e+05	133.00	1.10	0.17	0.09	0.36	19,23,34
2360	1.53	1.41	1.41	5.240e+05	133.00	1.14	0.15	0.07	0.33	24,23,28
2361	1.20	1.41	1.32	4.141e+05	133.00	1.06	0.17	0.07	0.26	26,23,28
2362	1.15	1.27	1.21	3.991e+05	133.00	0.98	0.19	0.07	0.19	26,23,32
2363	1.15	1.02	1.10	3.991e+05	133.00	0.89	0.19	0.08	0.11	26,21,32
2364	1.02	0.82	0.81	3.542e+05	133.00	0.65	0.16	0.15	0.12	21,21,31
2365	0.69	0.70	0.69	2.415e+05	133.00	0.56	0.14	0.20	0.19	26,21,31
2366	0.69	0.70	0.69	2.415e+05	133.00	0.56	0.14	0.20	0.19	26,21,31
2368	1.61	1.61	1.36	5.522e+05	133.00	1.10	0.17	0.09	0.36	19,23,34
2369	1.53	1.41	1.41	5.240e+05	133.00	1.14	0.15	0.07	0.33	24,23,28
2370	1.20	1.41	1.32	4.141e+05	133.00	1.06	0.17	0.07	0.26	26,23,28
2371	1.15	1.27	1.21	3.991e+05	133.00	0.98	0.19	0.07	0.19	26,23,32
2372	1.15	1.02	1.10	3.991e+05	133.00	0.89	0.19	0.08	0.11	26,21,32
2373	1.02	0.82	0.81	3.542e+05	133.00	0.65	0.16	0.15	0.12	21,21,31
2374	0.69	0.70	0.69	2.415e+05	133.00	0.56	0.14	0.20	0.19	26,21,31
2375	0.69	0.70	0.69	2.415e+05	133.00	0.56	0.14	0.20	0.19	26,21,31
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	1.61	1.61	1.41	2.415e+05	133.00	0.56				
	1.61	1.61	1.41	5.522e+05	133.00	1.14	0.19	0.20	0.36	

Setto	Mat.	Spessore	Stato
		cm	
168	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
2348	0.54	0.55	0.53	1.905e+05	133.00	0.43	0.16	0.21	0.20	21,26,31
2349	0.54	0.55	0.53	1.905e+05	133.00	0.43	0.16	0.21	0.20	21,26,31
2357	0.54	0.55	0.53	1.905e+05	133.00	0.43	0.16	0.21	0.20	21,26,31

2358	0.54	0.55	0.53	1.905e+05	133.00	0.43	0.16	0.21	0.20	21,26,31
2366	0.54	0.55	0.53	1.905e+05	133.00	0.43	0.16	0.21	0.20	21,26,31
2367	0.54	0.55	0.53	1.905e+05	133.00	0.43	0.16	0.21	0.20	21,26,31
2375	0.54	0.55	0.53	1.905e+05	133.00	0.43	0.16	0.21	0.20	21,26,31
2376	0.54	0.55	0.53	1.905e+05	133.00	0.43	0.16	0.21	0.20	21,26,31

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
	0.54	0.55	0.53	1.905e+05	133.00	0.43			
	0.54	0.55	0.53	1.905e+05	133.00	0.43	0.16	0.21	0.20

Setto	Mat.	Spessore	Stato
		cm	
169	mattoni pieni e malta di calce	37.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
780	1.23	1.23	1.16	5.164e+05	153.50	1.30	0.15	0.15	0.09	22,26,39
790	1.23	1.23	1.16	5.164e+05	153.50	1.30	0.15	0.15	0.09	22,26,39
800	1.23	1.23	1.16	5.164e+05	153.50	1.30	0.15	0.15	0.09	22,26,39
810	1.23	1.23	1.16	5.164e+05	153.50	1.30	0.15	0.15	0.09	22,26,39
2444	1.23	1.28	1.27	5.164e+05	153.50	1.42	0.15	0.16	0.10	22,26,42
2446	1.28	1.28	1.25	5.383e+05	153.50	1.39	0.14	0.16	0.13	26,26,42
2448	1.27	1.27	1.25	5.316e+05	153.50	1.39	0.13	0.15	0.13	26,26,42
2450	1.02	1.17	1.16	4.298e+05	153.50	1.29	0.10	0.13	0.13	21,26,38
2452	0.88	1.02	0.89	3.752e+05	153.50	0.99	0.12	0.10	0.13	33,26,29
2482	1.23	1.28	1.27	5.164e+05	153.50	1.42	0.15	0.16	0.10	22,26,42
2483	1.28	1.28	1.25	5.383e+05	153.50	1.39	0.14	0.16	0.13	26,26,42
2484	1.27	1.27	1.25	5.316e+05	153.50	1.39	0.13	0.15	0.13	26,26,42
2485	1.02	1.17	1.16	4.298e+05	153.50	1.29	0.10	0.13	0.13	21,26,38
2486	0.88	1.02	0.89	3.752e+05	153.50	0.99	0.12	0.10	0.13	33,26,29
2487	0.81	0.89	0.79	3.441e+05	153.50	0.88	0.13	0.08	0.13	27,26,33
2488	0.81	0.89	0.79	3.441e+05	153.50	0.88	0.13	0.08	0.13	27,26,33
2489	0.81	0.78	0.69	3.441e+05	153.50	0.77	0.13	0.06	0.17	27,26,26
2490	0.81	0.78	0.69	3.441e+05	153.50	0.77	0.13	0.06	0.17	27,26,26
2491	0.75	0.69	0.69	3.184e+05	153.50	0.77	0.12	0.06	0.17	27,26,26
2492	0.75	0.69	0.69	3.184e+05	153.50	0.77	0.12	0.06	0.17	27,26,26
2495	1.23	1.28	1.27	5.164e+05	153.50	1.42	0.15	0.16	0.10	22,26,42
2496	1.28	1.28	1.25	5.381e+05	153.50	1.39	0.14	0.16	0.13	26,26,42
2497	1.27	1.27	1.25	5.314e+05	153.50	1.39	0.13	0.15	0.13	26,26,42
2498	1.02	1.17	1.16	4.298e+05	153.50	1.29	0.10	0.13	0.13	21,26,38
2499	0.88	1.02	0.89	3.752e+05	153.50	0.99	0.12	0.10	0.13	33,26,29
2500	0.81	0.89	0.79	3.441e+05	153.50	0.88	0.13	0.08	0.13	27,26,33
2501	0.81	0.78	0.69	3.441e+05	153.50	0.77	0.13	0.06	0.17	27,26,26
2502	0.75	0.69	0.69	3.184e+05	153.50	0.77	0.12	0.06	0.17	27,26,26
2504	1.23	1.28	1.27	5.164e+05	153.50	1.42	0.15	0.15	0.09	22,26,42
2505	1.28	1.28	1.25	5.381e+05	153.50	1.39	0.14	0.15	0.12	26,26,42
2506	1.27	1.27	1.16	5.314e+05	153.50	1.29	0.13	0.15	0.13	26,26,38
2507	1.02	1.17	1.16	4.298e+05	153.50	1.29	0.10	0.13	0.13	21,26,38
2508	0.88	1.02	0.89	3.752e+05	153.50	0.99	0.12	0.10	0.13	33,26,29
2509	0.81	0.89	0.79	3.441e+05	153.50	0.88	0.13	0.08	0.13	27,26,33
2510	0.81	0.78	0.69	3.441e+05	153.50	0.77	0.13	0.06	0.17	27,26,26
2511	0.75	0.69	0.69	3.184e+05	153.50	0.77	0.12	0.06	0.17	27,26,26
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				3.184e+05	153.50	0.77				
	1.28	1.28	1.27	5.383e+05	153.50	1.42	0.15	0.16	0.17	

Setto	Mat.	Spessore	Stato
		cm	
170	mattoni pieni e malta di calce	37.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
2491	0.52	0.52	0.54	2.218e+05	153.50	0.60	0.09	0.22	0.44	22,33,42
2492	0.52	0.52	0.54	2.218e+05	153.50	0.60	0.09	0.22	0.44	22,33,42
2493	0.52	0.52	0.54	2.218e+05	153.50	0.60	0.09	0.22	0.44	22,33,42

2494	0.52	0.52	0.54	2.218e+05	153.50	0.60	0.09	0.22	0.44	22,33,42
2502	0.52	0.52	0.54	2.218e+05	153.50	0.60	0.09	0.22	0.44	22,33,42
2503	0.52	0.52	0.54	2.218e+05	153.50	0.60	0.09	0.22	0.44	22,33,42
2511	0.52	0.52	0.54	2.218e+05	153.50	0.60	0.09	0.22	0.44	22,33,42
2512	0.52	0.52	0.54	2.218e+05	153.50	0.60	0.09	0.22	0.44	22,33,42
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	0.52	0.52	0.54	2.218e+05	153.50	0.60	0.09	0.22	0.44	

Setto	Mat.	Spessore	Stato
		cm	
172	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
2805	0.37	0.33	0.37	7.609e+04	101.90	0.29	0.52	0.03	0.17	37,36,21
2806	0.58	0.83	0.37	1.198e+05	71.72	0.29	0.54	0.05	0.17	37,37,21
2807	0.58	0.79	0.58	1.198e+05	79.82	0.47	0.54	0.11	0.13	37,37,21
2808	0.62	0.79	0.47	1.263e+05	79.82	0.38	0.48	0.11	0.11	37,37,23
2809	0.53	0.53	0.38	1.080e+05	101.90	0.31	0.33	0.08	0.13	17,37,23
2810	0.35	0.44	0.29	7.131e+04	101.90	0.23	0.19	0.08	0.17	37,37,23
2811	0.25	0.61	0.29	5.244e+04	42.68	0.23	0.72	0.19	0.17	37,37,23
2812	0.25	0.61	0.24	5.244e+04	42.68	0.19	0.72	0.19	0.13	37,37,31
2814	0.37	0.33	0.37	7.609e+04	101.90	0.29	0.52	0.03	0.17	37,36,21
2815	0.58	0.83	0.37	1.198e+05	71.72	0.29	0.54	0.05	0.17	37,37,21
2816	0.58	0.79	0.58	1.198e+05	79.82	0.47	0.54	0.11	0.13	37,37,21
2817	0.62	0.79	0.47	1.263e+05	79.82	0.38	0.48	0.11	0.11	37,37,23
2818	0.53	0.53	0.38	1.080e+05	101.90	0.31	0.33	0.08	0.13	17,37,23
2819	0.35	0.44	0.29	7.131e+04	101.90	0.23	0.19	0.08	0.17	37,37,23
2820	0.25	0.61	0.29	5.244e+04	42.68	0.23	0.72	0.19	0.17	37,37,23
2821	0.25	0.61	0.24	5.244e+04	42.68	0.19	0.72	0.19	0.13	37,37,31
2823	0.37	0.33	0.37	7.609e+04	101.90	0.29	0.52	0.03	0.17	37,36,21
2824	0.58	0.83	0.37	1.198e+05	71.72	0.29	0.54	0.05	0.17	37,37,21
2825	0.58	0.79	0.58	1.198e+05	79.82	0.47	0.54	0.11	0.13	37,37,21
2826	0.62	0.79	0.47	1.263e+05	79.82	0.38	0.48	0.11	0.11	37,37,23
2827	0.53	0.53	0.38	1.080e+05	101.90	0.31	0.33	0.08	0.13	17,37,23
2828	0.35	0.44	0.29	7.131e+04	101.90	0.23	0.19	0.08	0.17	37,37,23
2829	0.25	0.61	0.29	5.244e+04	42.68	0.23	0.72	0.19	0.17	37,37,23
2830	0.25	0.61	0.24	5.244e+04	42.68	0.19	0.72	0.19	0.13	37,37,31
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	0.62	0.83	0.58	5.244e+04	42.68	0.19				
				1.263e+05	101.90	0.47	0.72	0.19	0.17	

Setto	Mat.	Spessore	Stato
		cm	
173	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
2812	0.20	0.30	0.16	4.154e+04	68.70	0.13	0.55	0.06	0.13	37,37,20
2813	0.20	0.30	0.16	4.154e+04	68.70	0.13	0.55	0.06	0.13	37,37,20
2821	0.20	0.30	0.16	4.154e+04	68.70	0.13	0.55	0.06	0.13	37,37,20
2822	0.20	0.30	0.16	4.154e+04	68.70	0.13	0.55	0.06	0.13	37,37,20
2830	0.20	0.30	0.16	4.154e+04	68.70	0.13	0.55	0.06	0.13	37,37,20
2831	0.20	0.30	0.16	4.154e+04	68.70	0.13	0.55	0.06	0.13	37,37,20
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	0.20	0.30	0.16	4.154e+04	68.70	0.13				
				4.154e+04	68.70	0.13	0.55	0.06	0.13	

Setto	Mat.	Spessore	Stato
		cm	
175	mattoni pieni e malta di calce	37.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
740	1.57	1.57	1.57	1.399e+06	224.67	1.76	0.07	0.03	0.09	21,23,35
765	1.57	1.57	1.57	1.399e+06	224.67	1.76	0.07	0.03	0.09	21,23,35
829	1.57	1.57	1.57	1.399e+06	224.67	1.76	0.07	0.03	0.09	21,23,35
849	1.57	1.57	1.57	1.399e+06	224.67	1.76	0.07	0.03	0.09	21,23,35
1022	1.57	1.57	1.57	1.399e+06	224.67	1.76	0.07	0.03	0.09	21,23,35
1095	1.57	1.57	1.57	1.399e+06	224.67	1.76	0.07	0.03	0.09	21,23,35
2522	1.63	1.63	1.57	1.448e+06	224.67	1.76	0.07	0.03	0.09	21,21,35
2523	1.62	1.62	1.63	1.439e+06	224.67	1.82	0.08	0.07	0.06	21,21,35
2524	1.62	1.56	1.56	1.439e+06	224.67	1.74	0.08	0.07	0.07	21,21,35
2525	1.56	1.47	1.47	1.388e+06	224.67	1.64	0.07	0.08	0.16	21,21,35
2526	1.47	1.47	1.39	1.315e+06	224.67	1.55	0.04	0.08	0.25	21,21,37
2527	1.27	1.38	1.29	1.144e+06	224.67	1.45	0.04	0.07	0.35	20,21,37
2528	1.18	1.29	1.20	1.066e+06	224.67	1.34	0.05	0.07	0.46	20,21,13
2529	1.18	1.20	1.20	1.066e+06	224.67	1.34	0.05	0.07	0.46	20,21,13
2531	1.63	1.63	1.57	1.446e+06	224.67	1.76	0.08	0.04	0.09	21,21,35
2532	1.62	1.62	1.63	1.438e+06	224.67	1.82	0.08	0.07	0.06	21,21,35
2533	1.62	1.56	1.56	1.438e+06	224.67	1.74	0.08	0.07	0.07	21,21,35
2534	1.56	1.47	1.47	1.388e+06	224.67	1.64	0.07	0.08	0.16	21,21,35
2535	1.47	1.47	1.39	1.315e+06	224.67	1.55	0.04	0.08	0.25	21,21,37
2536	1.27	1.38	1.29	1.144e+06	224.67	1.45	0.04	0.07	0.35	20,21,37
2537	1.18	1.29	1.20	1.066e+06	224.67	1.34	0.05	0.07	0.46	20,21,13
2538	1.18	1.20	1.20	1.066e+06	224.67	1.34	0.05	0.07	0.46	20,21,13
2540	1.63	1.63	1.57	1.446e+06	224.67	1.76	0.08	0.04	0.09	21,21,35
2541	1.62	1.62	1.63	1.438e+06	224.67	1.81	0.08	0.07	0.06	21,21,35
2542	1.62	1.56	1.56	1.438e+06	224.67	1.74	0.08	0.07	0.07	21,21,35
2543	1.56	1.47	1.47	1.388e+06	224.67	1.64	0.07	0.08	0.16	21,21,35
2544	1.47	1.47	1.39	1.315e+06	224.67	1.55	0.04	0.08	0.25	21,21,37
2545	1.27	1.38	1.29	1.144e+06	224.67	1.45	0.04	0.07	0.35	20,21,37
2546	1.18	1.29	1.20	1.066e+06	224.67	1.34	0.05	0.07	0.46	20,21,13
2547	1.18	1.20	1.20	1.066e+06	224.67	1.34	0.05	0.07	0.46	20,21,13
2549	1.63	1.63	1.57	1.446e+06	224.67	1.76	0.08	0.04	0.09	21,21,35
2550	1.62	1.62	1.63	1.438e+06	224.67	1.81	0.08	0.07	0.06	21,21,35
2551	1.62	1.56	1.56	1.438e+06	224.67	1.74	0.08	0.07	0.07	21,21,35
2552	1.56	1.47	1.47	1.388e+06	224.67	1.64	0.07	0.08	0.16	21,21,35
2553	1.47	1.47	1.39	1.315e+06	224.67	1.55	0.04	0.08	0.25	21,21,37
2554	1.27	1.38	1.29	1.144e+06	224.67	1.45	0.04	0.07	0.35	20,21,37
2555	1.18	1.29	1.20	1.066e+06	224.67	1.34	0.05	0.07	0.46	20,21,13
2556	1.18	1.20	1.20	1.066e+06	224.67	1.34	0.05	0.07	0.46	20,21,13
2587	1.47	1.47	1.39	1.315e+06	224.67	1.55	0.04	0.08	0.25	21,21,37
2588	1.27	1.38	1.29	1.144e+06	224.67	1.45	0.04	0.07	0.35	20,21,37
2589	1.18	1.29	1.20	1.066e+06	224.67	1.34	0.05	0.07	0.46	20,21,13
2590	1.18	1.20	1.20	1.066e+06	224.67	1.34	0.05	0.07	0.46	20,21,13
2594	1.63	1.63	1.57	1.448e+06	224.67	1.76	0.07	0.03	0.09	21,21,35
2595	1.62	1.62	1.63	1.439e+06	224.67	1.82	0.08	0.07	0.06	21,21,35
2596	1.62	1.56	1.56	1.439e+06	224.67	1.74	0.08	0.07	0.07	21,21,35
2597	1.56	1.47	1.47	1.388e+06	224.67	1.64	0.07	0.08	0.16	21,21,35
2598	1.47	1.47	1.39	1.315e+06	224.67	1.55	0.04	0.08	0.25	21,21,37
2599	1.27	1.38	1.29	1.144e+06	224.67	1.45	0.04	0.07	0.35	20,21,37
2600	1.18	1.29	1.20	1.066e+06	224.67	1.34	0.05	0.07	0.46	20,21,13
2601	1.18	1.20	1.20	1.066e+06	224.67	1.34	0.05	0.07	0.46	20,21,13
2603	1.63	1.63	1.57	1.446e+06	224.67	1.76	0.08	0.04	0.09	21,21,35
2604	1.62	1.62	1.63	1.438e+06	224.67	1.82	0.08	0.07	0.06	21,21,35
2605	1.62	1.56	1.56	1.438e+06	224.67	1.74	0.08	0.07	0.07	21,21,35
2606	1.56	1.47	1.47	1.388e+06	224.67	1.64	0.07	0.08	0.16	21,21,35
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	1.63	1.63	1.63	1.066e+06	224.67	1.34				
				1.448e+06	224.67	1.82	0.08	0.08	0.46	

Setto	Mat.	Spessore	Stato
		cm	
176	mattoni pieni e malta di calce	37.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
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2529	0.88	0.87	0.87	8.004e+05	224.67	0.97	0.05	0.03	0.81	21,40,42
2530	0.88	0.87	0.87	8.004e+05	224.67	0.97	0.05	0.03	0.81	21,40,42
2538	0.88	0.87	0.87	8.004e+05	224.67	0.97	0.05	0.03	0.81	21,40,42
2539	0.88	0.87	0.87	8.004e+05	224.67	0.97	0.05	0.03	0.81	21,40,42
2547	0.88	0.87	0.87	8.004e+05	224.67	0.97	0.05	0.03	0.81	21,40,42
2548	0.88	0.87	0.87	8.004e+05	224.67	0.97	0.05	0.03	0.81	21,40,42
2556	0.88	0.87	0.87	8.004e+05	224.67	0.97	0.05	0.03	0.81	21,40,42
2557	0.88	0.87	0.87	8.004e+05	224.67	0.97	0.05	0.03	0.81	21,40,42
2590	0.88	0.87	0.87	8.004e+05	224.67	0.97	0.05	0.03	0.81	21,40,42
2591	0.88	0.87	0.87	8.004e+05	224.67	0.97	0.05	0.03	0.81	21,40,42
2601	0.88	0.87	0.87	8.004e+05	224.67	0.97	0.05	0.03	0.81	21,40,42
2602	0.88	0.87	0.87	8.004e+05	224.67	0.97	0.05	0.03	0.81	21,40,42

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
	0.88	0.87	0.87	8.004e+05	224.67	0.97			
				8.004e+05	224.67	0.97	0.05	0.03	0.81

Setto	Mat.	Spessore	Stato
		cm	
177	mattoni pieni e malta di calce	37.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1064	1.84	1.84	1.84	2.499e+05	88.17	2.05	0.20	0.13	0.04	21,21,21
1065	1.84	1.84	1.84	2.499e+05	88.17	2.05	0.20	0.13	0.04	21,21,21
1075	1.84	1.84	1.84	2.499e+05	88.17	2.05	0.20	0.13	0.04	21,21,21
2558	1.84	1.84	2.02	2.499e+05	88.17	2.26	0.20	0.13	0.10	21,21,17
2559	1.84	1.84	2.02	2.499e+05	88.17	2.26	0.20	0.13	0.10	21,21,17
2560	2.01	1.91	2.03	2.713e+05	88.17	2.27	0.13	0.05	0.14	21,20,17
2561	2.00	2.00	2.03	2.702e+05	88.17	2.27	0.14	0.05	0.14	21,21,17
2562	2.00	1.78	2.03	2.700e+05	88.17	2.27	0.10	0.06	0.14	21,23,17
2563	1.99	1.78	2.03	2.690e+05	88.17	2.27	0.10	0.06	0.14	21,23,17
2564	1.87	1.56	1.89	2.540e+05	88.17	2.10	0.07	0.06	0.10	21,23,17
2565	1.87	1.56	1.89	2.540e+05	88.17	2.10	0.07	0.06	0.10	21,23,17
2566	1.49	1.56	1.44	2.048e+05	88.17	1.61	0.04	0.06	0.05	26,23,39
2567	1.49	1.56	1.44	2.048e+05	88.17	1.61	0.04	0.06	0.05	26,23,39
2568	1.33	1.35	1.24	1.835e+05	88.17	1.38	0.11	0.06	0.15	21,23,39
2569	1.33	1.35	1.24	1.835e+05	88.17	1.38	0.11	0.06	0.15	21,23,39
2570	1.16	1.16	1.07	1.616e+05	88.17	1.19	0.18	0.05	0.26	21,23,39
2571	1.16	1.16	1.07	1.616e+05	88.17	1.19	0.18	0.05	0.26	21,23,39
2572	1.16	0.97	1.07	1.616e+05	88.17	1.19	0.18	0.03	0.26	21,20,39
2573	1.16	0.97	1.07	1.616e+05	88.17	1.19	0.18	0.03	0.26	21,20,39
2576	1.84	1.84	2.01	2.499e+05	88.17	2.24	0.20	0.13	0.09	21,21,13
2577	2.00	2.00	2.02	2.702e+05	88.17	2.26	0.14	0.05	0.13	21,21,17
2578	1.99	1.78	2.02	2.690e+05	88.17	2.26	0.10	0.06	0.13	21,23,17
2579	1.87	1.56	1.89	2.540e+05	88.17	2.10	0.07	0.06	0.10	21,23,17
2580	1.49	1.56	1.44	2.048e+05	88.17	1.61	0.04	0.06	0.05	26,23,39
2581	1.33	1.35	1.24	1.835e+05	88.17	1.38	0.11	0.06	0.15	21,23,39
2582	1.16	1.16	1.07	1.616e+05	88.17	1.19	0.18	0.05	0.26	21,23,39
2583	1.16	0.97	1.07	1.616e+05	88.17	1.19	0.18	0.03	0.26	21,20,39

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
	2.01	2.00	2.03	1.616e+05	88.17	1.19			
				2.713e+05	88.17	2.27	0.20	0.13	0.26

Setto	Mat.	Spessore	Stato
		cm	
178	mattoni pieni e malta di calce	37.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
2572	0.78	0.83	0.69	1.100e+05	88.17	0.77	0.04	0.05	0.23	29,25,19
2573	0.78	0.83	0.69	1.100e+05	88.17	0.77	0.04	0.05	0.23	29,25,19
2574	0.78	0.83	0.69	1.100e+05	88.17	0.77	0.04	0.05	0.23	29,25,19
2575	0.78	0.83	0.69	1.100e+05	88.17	0.77	0.04	0.05	0.23	29,25,19
2583	0.78	0.83	0.69	1.100e+05	88.17	0.77	0.04	0.05	0.23	29,25,19

2584	0.78	0.83	0.69	1.100e+05	88.17	0.77	0.04	0.05	0.23	29,25,19
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	0.78	0.83	0.69	1.100e+05	88.17	0.77	0.04	0.05	0.23	

Setto	Mat.	Spessore	Stato
		cm	
182	muratura E = 1.024e+05	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
875	6.30	6.32	6.77	1.907e+05	41.50	5.23	0.08	0.18	0.06	38,42,21
1285	6.30	6.32	6.77	1.907e+05	41.50	5.23	0.08	0.18	0.06	38,42,21
2323	5.19	5.21	5.52	1.610e+05	41.50	4.26	0.03	0.17	0.07	38,42,33
2324	2.77	3.02	4.38	9.032e+04	41.50	3.38	0.05	0.17	0.06	38,26,29
2325	1.71	1.86	1.86	5.692e+04	41.50	1.44	0.24	0.20	0.07	38,26,26
2326	1.22	1.86	1.45	4.110e+04	41.50	1.12	0.32	0.20	0.12	42,26,21
2332	1.22	1.60	1.45	4.110e+04	41.50	1.12	0.32	0.26	0.12	42,26,21
2333	2.45	2.37	1.85	8.030e+04	41.50	1.43	0.26	0.53	0.07	21,42,33
2334	2.45	2.37	2.40	8.030e+04	41.50	1.85	0.26	0.53	0.07	21,42,40
2423	6.30	6.32	5.52	1.907e+05	41.50	4.26	0.08	0.18	0.07	38,42,33
2625	5.19	5.21	5.52	1.610e+05	41.50	4.26	0.03	0.17	0.07	38,42,33
2626	2.77	3.02	4.38	9.032e+04	41.50	3.38	0.05	0.17	0.06	38,26,29
2634	1.71	1.86	1.86	5.692e+04	41.50	1.44	0.24	0.20	0.07	38,26,26
2635	1.22	1.86	1.45	4.110e+04	41.50	1.12	0.32	0.20	0.12	42,26,21
2640	6.30	6.32	5.52	1.907e+05	41.50	4.26	0.08	0.18	0.07	38,42,33
2981	2.45	2.37	2.40	8.030e+04	41.50	1.85	0.26	0.53	0.07	21,42,40
2990	1.22	1.60	1.45	4.110e+04	41.50	1.12	0.32	0.26	0.12	42,26,21
2991	2.45	2.37	1.85	8.030e+04	41.50	1.43	0.26	0.53	0.07	21,42,33

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				4.110e+04	41.50	1.12			
	6.30	6.32	6.77	1.907e+05	41.50	5.23	0.32	0.53	0.12

Setto	Mat.	Spessore	Stato
		cm	
186	muratura E = 1.024e+05	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
2334	3.11	3.11	3.11	1.007e+05	41.50	2.40	0.38	0.12	0.09	39,42,35
2335	3.11	3.11	3.11	1.007e+05	41.50	2.40	0.38	0.12	0.09	39,42,35
2981	3.11	3.11	3.11	1.007e+05	41.50	2.40	0.38	0.12	0.09	39,42,35
2982	3.11	3.11	3.11	1.007e+05	41.50	2.40	0.38	0.12	0.09	39,42,35

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				1.007e+05	41.50	2.40			
	3.11	3.11	3.11	1.007e+05	41.50	2.40	0.38	0.12	0.09

Setto	Mat.	Spessore	Stato
		cm	
188	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1119	1.43	1.51	1.50	7.867e+06	536.00	1.74	0.05	0.03	0.04	37,17,38
1185	1.43	1.51	1.50	7.867e+06	536.00	1.74	0.05	0.03	0.04	37,17,38
1186	1.43	1.51	1.50	7.867e+06	536.00	1.74	0.05	0.03	0.04	37,17,38
1195	1.43	1.51	1.50	7.867e+06	536.00	1.74	0.05	0.03	0.04	37,17,38
1204	1.43	1.51	1.50	7.867e+06	536.00	1.74	0.05	0.03	0.04	37,17,38

1213	1.43	1.51	1.50	7.867e+06	536.00	1.74	0.05	0.03	0.04	37,17,38
1222	1.43	1.51	1.50	7.867e+06	536.00	1.74	0.05	0.03	0.04	37,17,38
1231	1.43	1.51	1.50	7.867e+06	536.00	1.74	0.05	0.03	0.04	37,17,38
1240	1.43	1.51	1.50	7.867e+06	536.00	1.74	0.05	0.03	0.04	37,17,38
1249	1.43	1.51	1.50	7.867e+06	536.00	1.74	0.05	0.03	0.04	37,17,38
1258	1.43	1.51	1.50	7.867e+06	536.00	1.74	0.05	0.03	0.04	37,17,38
1950	1.43	1.51	1.50	7.867e+06	536.00	1.74	0.05	0.03	0.04	37,17,38
2661	1.43	1.51	1.50	7.867e+06	536.00	1.74	0.05	0.03	0.04	37,17,38
2662	1.38	1.35	1.46	7.633e+06	536.00	1.69	0.03	0.03	0.02	37,36,42
2663	1.31	1.26	1.19	7.238e+06	536.00	1.38	0.02	0.05	0.03	37,36,19
2664	1.14	1.18	1.11	6.325e+06	536.00	1.29	0.02	0.06	0.04	37,36,19
2665	1.04	1.08	1.11	5.779e+06	536.00	1.29	0.04	0.06	0.04	39,36,19
2666	0.95	1.08	1.04	5.288e+06	536.00	1.20	0.05	0.06	0.04	39,36,11
2667	0.86	0.98	0.86	4.796e+06	536.00	1.00	0.06	0.05	0.07	39,36,20
2668	0.86	0.89	0.86	4.796e+06	536.00	1.00	0.06	0.04	0.07	39,36,20
2670	1.43	1.51	1.50	7.867e+06	536.00	1.74	0.05	0.03	0.04	37,17,38
2671	1.38	1.35	1.46	7.633e+06	536.00	1.69	0.03	0.03	0.02	37,36,42
2672	1.31	1.26	1.19	7.238e+06	536.00	1.38	0.02	0.05	0.03	37,36,19
2673	1.14	1.18	1.11	6.325e+06	536.00	1.29	0.02	0.06	0.04	37,36,19
2674	1.04	1.08	1.11	5.779e+06	536.00	1.29	0.04	0.06	0.04	39,36,19
2675	0.95	1.08	1.04	5.288e+06	536.00	1.20	0.05	0.06	0.04	39,36,11
2676	0.86	0.98	0.86	4.796e+06	536.00	1.00	0.06	0.05	0.07	39,36,20
2677	0.86	0.89	0.86	4.796e+06	536.00	1.00	0.06	0.04	0.07	39,36,20
2679	1.43	1.51	1.50	7.867e+06	536.00	1.74	0.05	0.03	0.04	37,17,38
2680	1.38	1.35	1.46	7.633e+06	536.00	1.69	0.03	0.03	0.02	37,36,42
2681	1.31	1.26	1.19	7.238e+06	536.00	1.38	0.02	0.05	0.03	37,36,19
2682	1.14	1.18	1.11	6.325e+06	536.00	1.29	0.02	0.06	0.04	37,36,19
2683	1.04	1.08	1.11	5.779e+06	536.00	1.29	0.04	0.06	0.04	39,36,19
2684	0.95	1.08	1.04	5.288e+06	536.00	1.20	0.05	0.06	0.04	39,36,11
2685	0.86	0.98	0.86	4.796e+06	536.00	1.00	0.06	0.05	0.07	39,36,20
2686	0.86	0.89	0.86	4.796e+06	536.00	1.00	0.06	0.04	0.07	39,36,20
2688	1.43	1.51	1.50	7.867e+06	536.00	1.74	0.05	0.03	0.04	37,17,38
2689	1.38	1.35	1.46	7.633e+06	536.00	1.69	0.03	0.03	0.02	37,36,42
2690	1.31	1.26	1.19	7.238e+06	536.00	1.38	0.02	0.05	0.03	37,36,19
2691	1.14	1.18	1.11	6.325e+06	536.00	1.29	0.02	0.06	0.04	37,36,19
2692	1.04	1.08	1.11	5.779e+06	536.00	1.29	0.04	0.06	0.04	39,

2739	0.86	0.98	0.86	4.796e+06	536.00	1.00	0.06	0.05	0.07	39,36,20
2740	0.86	0.89	0.86	4.796e+06	536.00	1.00	0.06	0.04	0.07	39,36,20
2742	1.43	1.51	1.50	7.867e+06	536.00	1.74	0.05	0.03	0.04	37,17,38
2743	1.38	1.35	1.46	7.633e+06	536.00	1.69	0.03	0.03	0.02	37,36,42
2744	1.31	1.26	1.19	7.238e+06	536.00	1.38	0.02	0.05	0.03	37,36,19
2745	1.14	1.18	1.11	6.325e+06	536.00	1.29	0.02	0.06	0.04	37,36,19
2746	1.04	1.08	1.11	5.779e+06	536.00	1.29	0.04	0.06	0.04	39,36,19
2747	0.95	1.08	1.04	5.288e+06	536.00	1.20	0.05	0.06	0.04	39,36,11
2748	0.86	0.98	0.86	4.796e+06	536.00	1.00	0.06	0.05	0.07	39,36,20
2749	0.86	0.89	0.86	4.796e+06	536.00	1.00	0.06	0.04	0.07	39,36,20
2751	1.43	1.51	1.50	7.867e+06	536.00	1.74	0.05	0.03	0.04	37,17,38
2752	1.38	1.35	1.46	7.633e+06	536.00	1.69	0.03	0.03	0.02	37,36,42
2753	1.31	1.26	1.19	7.238e+06	536.00	1.38	0.02	0.05	0.03	37,36,19
2754	1.14	1.18	1.11	6.325e+06	536.00	1.29	0.02	0.06	0.04	37,36,19
2755	1.04	1.08	1.11	5.779e+06	536.00	1.29	0.04	0.06	0.04	39,36,19
2756	0.95	1.08	1.04	5.288e+06	536.00	1.20	0.05	0.06	0.04	39,36,11
2757	0.86	0.98	0.86	4.796e+06	536.00	1.00	0.06	0.05	0.07	39,36,20
2758	0.86	0.89	0.86	4.796e+06	536.00	1.00	0.06	0.04	0.07	39,36,20
2760	1.43	1.51	1.50	7.867e+06	536.00	1.74	0.05	0.03	0.04	37,17,38
2761	1.38	1.35	1.46	7.633e+06	536.00	1.69	0.03	0.03	0.02	37,36,42
2762	1.31	1.26	1.19	7.238e+06	536.00	1.38	0.02	0.05	0.03	37,36,19
2763	1.14	1.18	1.11	6.325e+06	536.00	1.29	0.02	0.06	0.04	37,36,19
2764	1.04	1.08	1.11	5.779e+06	536.00	1.29	0.04	0.06	0.04	39,36,19
2765	0.95	1.08	1.04	5.288e+06	536.00	1.20	0.05	0.06	0.04	39,36,11
2766	0.86	0.98	0.86	4.796e+06	536.00	1.00	0.06	0.05	0.07	39,36,20
2767	0.86	0.89	0.86	4.796e+06	536.00	1.00	0.06	0.04	0.07	39,36,20

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				4.796e+06	536.00	1.00			
	1.43	1.51	1.50	7.867e+06	536.00	1.74	0.06	0.06	0.07

Setto	Mat.	Spessore	Stato
		cm	
189	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
2668	0.75	0.75	0.75	4.235e+06	536.00	0.87	0.08	0.02	0.17	37,37,20
2669	0.75	0.75	0.75	4.235e+06	536.00	0.87	0.08	0.02	0.17	37,37,20
2677	0.75	0.75	0.75	4.235e+06	536.00	0.87	0.08	0.02	0.17	37,37,20
2678	0.75	0.75	0.75	4.235e+06	536.00	0.87	0.08	0.02	0.17	37,37,20
2686	0.75	0.75	0.75	4.235e+06	536.00	0.87	0.08	0.02	0.17	37,37,20
2687	0.75	0.75	0.75	4.235e+06	536.00	0.87	0.08	0.02	0.17	37,37,20
2695	0.75	0.75	0.75	4.235e+06	536.00	0.87	0.08	0.02	0.17	37,37,20
2696	0.75	0.75	0.75	4.235e+06	536.00	0.87	0.08	0.02	0.17	37,37,20
2704	0.75	0.75	0.75	4.235e+06	536.00	0.87	0.08	0.02	0.17	37,37,20
2705	0.75	0.75	0.75	4.235e+06	536.00	0.87	0.08	0.02	0.17	37,37,20
2713	0.75	0.75	0.75	4.235e+06	536.00	0.87	0.08	0.02	0.17	37,37,20
2714	0.75	0.75	0.75	4.235e+06	536.00	0.87	0.08	0.02	0.17	37,37,20
2722	0.75	0.75	0.75	4.235e+06	536.00	0.87	0.08	0.02	0.17	37,37,20
2723	0.75	0.75	0.75	4.235e+06	536.00	0.87	0.08	0.02	0.17	37,37,20
2731	0.75	0.75	0.75	4.235e+06	536.00	0.87	0.08	0.02	0.17	37,37,20
2732	0.75	0.75	0.75	4.235e+06	536.00	0.87	0.08	0.02	0.17	37,37,20
2740	0.75	0.75	0.75	4.235e+06	536.00	0.87	0.08	0.02	0.17	37,37,20
2741	0.75	0.75	0.75	4.235e+06	536.00	0.87	0.08	0.02	0.17	37,37,20
2749	0.75	0.75	0.75	4.235e+06	536.00	0.87	0.08	0.02	0.17	37,37,20
2750	0.75	0.75	0.75	4.235e+06	536.00	0.87	0.08	0.02	0.17	37,37,20
2758	0.75	0.75	0.75	4.235e+06	536.00	0.87	0.08	0.02	0.17	37,37,20
2759	0.75	0.75	0.75	4.235e+06	536.00	0.87	0.08	0.02	0.17	37,37,20
2767	0.75	0.75	0.75	4.235e+06	536.00	0.87	0.08	0.02	0.17	37,37,20
2768	0.75	0.75	0.75	4.235e+06	536.00	0.87	0.08	0.02	0.17	37,37,20

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				4.235e+06	536.00	0.87			
	0.75	0.75	0.75	4.235e+06	536.00	0.87	0.08	0.02	0.17

Setto	Mat.	Spessore	Stato
		cm	
190	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
2763	0.64	0.64	0.67	3.282e+04	50.95	0.54	0.04	0.14	0.13	16,16,15
2764	0.64	0.64	0.67	3.282e+04	50.95	0.54	0.04	0.14	0.13	16,16,15
2765	1.09	1.09	0.89	5.525e+04	50.95	0.72	0.07	0.15	0.13	36,36,23
2766	1.37	1.46	1.43	6.899e+04	50.95	1.15	0.26	0.33	0.06	26,36,19
2767	1.37	1.46	1.43	6.899e+04	50.95	1.15	0.26	0.33	0.06	26,36,19
2781	0.64	0.64	0.67	3.282e+04	50.95	0.54	0.04	0.14	0.13	16,16,15
2782	0.64	0.64	0.67	3.282e+04	50.95	0.54	0.04	0.14	0.13	16,16,15
2783	1.09	1.09	0.89	5.525e+04	50.95	0.72	0.07	0.15	0.13	36,36,23
2784	1.37	1.46	1.43	6.899e+04	50.95	1.15	0.26	0.33	0.06	26,36,19
2785	1.37	1.46	1.43	6.899e+04	50.95	1.15	0.26	0.33	0.06	26,36,19
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				3.282e+04	50.95	0.54				
	1.37	1.46	1.43	6.899e+04	50.95	1.15	0.26	0.33	0.13	

Setto	Mat.	Spessore	Stato
		cm	
191	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
2767	1.24	1.24	1.22	6.269e+04	50.95	0.98	0.13	0.31	0.24	16,16,20
2768	1.24	1.24	1.22	6.269e+04	50.95	0.98	0.13	0.31	0.24	16,16,20
2785	1.24	1.24	1.22	6.269e+04	50.95	0.98	0.13	0.31	0.24	16,16,20
2786	1.24	1.24	1.22	6.269e+04	50.95	0.98	0.13	0.31	0.24	16,16,20
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				6.269e+04	50.95	0.98				
	1.24	1.24	1.22	6.269e+04	50.95	0.98	0.13	0.31	0.24	

Setto	Mat.	Spessore	Stato
		cm	
194	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
1064	2.96	2.93	3.33	1.444e+05	50.95	2.68	0.23	0.22	0.02	23,16,17
2516	2.42	2.93	2.21	1.195e+05	50.95	1.78	0.26	0.22	0.04	39,16,16
2517	2.09	2.21	2.30	1.040e+05	50.95	1.85	0.29	0.06	0.05	35,16,21
2518	2.09	2.11	2.30	1.040e+05	50.95	1.85	0.29	0.12	0.05	35,39,21
2519	2.11	2.11	2.30	1.047e+05	50.95	1.85	0.17	0.12	0.04	39,39,21
2558	2.42	2.93	2.21	1.195e+05	50.95	1.78	0.26	0.22	0.04	39,16,16
2560	2.09	2.21	2.30	1.040e+05	50.95	1.85	0.29	0.06	0.05	35,16,21
2562	2.09	2.11	2.30	1.040e+05	50.95	1.85	0.29	0.12	0.05	35,39,21
2564	2.11	2.11	2.30	1.047e+05	50.95	1.85	0.17	0.12	0.04	39,39,21
2566	2.43	2.23	2.37	1.199e+05	50.95	1.91	0.05	0.12	0.02	25,39,26
2568	2.47	2.34	2.46	1.220e+05	50.95	1.98	0.16	0.11	0.03	37,39,21
2570	2.50	2.51	2.47	1.235e+05	50.95	1.99	0.28	0.12	0.04	17,37,21
2572	2.50	2.51	2.47	1.235e+05	50.95	1.99	0.28	0.12	0.04	17,37,21
2777	2.96	2.93	3.33	1.444e+05	50.95	2.68	0.23	0.22	0.02	23,16,17
2793	2.43	2.23	2.37	1.199e+05	50.95	1.91	0.05	0.12	0.02	25,39,26
2798	2.47	2.34	2.46	1.220e+05	50.95	1.98	0.16	0.11	0.03	37,39,21
2799	2.50	2.51	2.47	1.235e+05	50.95	1.99	0.28	0.12	0.04	17,37,21
2800	2.50	2.51	2.47	1.235e+05	50.95	1.99	0.28	0.12	0.04	17,37,21
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				1.040e+05	50.95	1.78				
	2.96	2.93	3.33	1.444e+05	50.95	2.68	0.29	0.22	0.05	

Setto	Mat.	Spessore	Stato
		cm	
197	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
2572	1.64	1.54	1.56	8.224e+04	50.95	1.25	0.11	0.05	0.01	31,36,20
2574	1.64	1.54	1.56	8.224e+04	50.95	1.25	0.11	0.05	0.01	31,36,20
2800	1.64	1.54	1.56	8.224e+04	50.95	1.25	0.11	0.05	0.01	31,36,20
2801	1.64	1.54	1.56	8.224e+04	50.95	1.25	0.11	0.05	0.01	31,36,20

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				8.224e+04	50.95	1.25			
	1.64	1.54	1.56	8.224e+04	50.95	1.25	0.11	0.05	0.01

Setto	Mat.	Spessore	Stato
		cm	
198	muratura E = 1.024e+05	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
1119	3.12	3.12	2.89	2.631e+05	67.00	2.23	0.20	0.21	0.05	23,23,26
1120	3.12	3.12	2.89	2.631e+05	67.00	2.23	0.20	0.21	0.05	23,23,26
2760	3.12	3.12	2.31	2.631e+05	67.00	1.79	0.20	0.21	0.08	23,23,42
2761	2.46	2.46	1.81	2.107e+05	67.00	1.40	0.17	0.18	0.11	23,23,36
2762	1.92	1.86	1.81	1.664e+05	67.00	1.40	0.12	0.16	0.11	41,23,36
2763	0.94	0.94	1.36	8.279e+04	67.00	1.05	0.32	0.15	0.08	23,23,16
2764	0.79	0.94	1.01	6.976e+04	67.00	0.78	0.50	0.15	0.05	23,23,38
2765	0.79	1.04	0.97	6.976e+04	50.88	0.75	0.50	0.13	0.06	23,23,42
2766	0.85	0.85	0.89	7.546e+04	67.00	0.69	0.34	0.15	0.10	23,23,36
2767	0.85	0.85	0.89	7.540e+04	67.00	0.69	0.29	0.15	0.10	23,23,36
2832	3.12	3.12	2.31	2.631e+05	67.00	1.79	0.20	0.21	0.08	23,23,42
2833	2.46	2.46	1.81	2.107e+05	67.00	1.40	0.17	0.18	0.11	23,23,36
2834	1.92	1.86	1.81	1.664e+05	67.00	1.40	0.12	0.16	0.11	41,23,36
2835	0.94	0.94	1.36	8.279e+04	67.00	1.05	0.32	0.15	0.08	23,23,16
2836	0.79	0.94	1.01	6.976e+04	67.00	0.78	0.50	0.15	0.05	23,23,38
2837	0.79	1.04	0.97	6.976e+04	50.88	0.75	0.50	0.13	0.06	23,23,42
2838	0.85	0.85	0.89	7.546e+04	67.00	0.69	0.34	0.15	0.10	23,23,36
2839	0.85	0.85	0.89	7.540e+04	67.00	0.69	0.29	0.15	0.10	23,23,36

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				6.976e+04	50.88	0.69			
	3.12	3.12	2.89	2.631e+05	67.00	2.23	0.50	0.21	0.11

Setto	Mat.	Spessore	Stato
		cm	
199	muratura E = 1.024e+05	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
2767	0.53	0.67	0.57	4.716e+04	57.48	0.44	0.47	0.29	0.10	21,19,36
2768	0.53	0.67	0.57	4.716e+04	57.48	0.44	0.47	0.29	0.10	21,19,36
2839	0.53	0.67	0.57	4.716e+04	57.48	0.44	0.47	0.29	0.10	21,19,36
2840	0.53	0.67	0.57	4.716e+04	57.48	0.44	0.47	0.29	0.10	21,19,36

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				4.716e+04	57.48	0.44			
	0.53	0.67	0.57	4.716e+04	57.48	0.44	0.47	0.29	0.10

Setto	Mat.	Spessore	Stato
		cm	

Setto	Mat.	Spessore	Stato
200	muratura E = 1.024e+05	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
1123	1.58	1.58	1.65	5.662e+05	136.00	1.28	0.11	0.10	0.04	23,23,38
1142	1.58	1.58	1.65	5.662e+05	136.00	1.28	0.11	0.10	0.04	23,23,38
1147	1.58	1.58	1.65	5.662e+05	136.00	1.28	0.11	0.10	0.04	23,23,38
1167	1.58	1.58	1.65	5.662e+05	136.00	1.28	0.11	0.10	0.04	23,23,38
2841	1.65	1.71	1.68	5.894e+05	136.00	1.29	0.06	0.10	0.03	23,23,38
2842	1.75	1.75	1.79	6.253e+05	136.00	1.38	0.05	0.10	0.02	23,23,18
2843	1.74	1.74	1.60	6.210e+05	136.00	1.24	0.14	0.11	0.07	23,23,42
2844	1.42	1.74	1.29	5.126e+05	136.00	1.00	0.16	0.11	0.12	23,23,42
2850	1.42	1.42	0.84	5.126e+05	136.00	0.65	0.16	0.05	0.15	23,23,42
2851	0.47	0.48	0.47	1.724e+05	136.00	0.36	0.12	0.05	0.21	26,21,26
2852	0.47	0.48	0.47	1.724e+05	136.00	0.36	0.12	0.05	0.21	26,21,26
2859	1.58	1.58	1.65	5.662e+05	136.00	1.28	0.11	0.10	0.04	23,23,38
2860	1.65	1.71	1.68	5.894e+05	136.00	1.29	0.06	0.10	0.03	23,23,38
2861	1.75	1.75	1.79	6.253e+05	136.00	1.38	0.05	0.10	0.02	23,23,18
2862	1.74	1.74	1.60	6.210e+05	136.00	1.24	0.14	0.11	0.07	23,23,42
2863	1.42	1.74	1.29	5.126e+05	136.00	1.00	0.16	0.11	0.12	23,23,42
2864	1.42	1.42	0.84	5.126e+05	136.00	0.65	0.16	0.05	0.15	23,23,42
2865	0.47	0.48	0.47	1.724e+05	136.00	0.36	0.12	0.05	0.21	26,21,26
2866	0.47	0.48	0.47	1.724e+05	136.00	0.36	0.12	0.05	0.21	26,21,26
2868	1.58	1.58	1.65	5.662e+05	136.00	1.28	0.11	0.10	0.04	23,23,38
2869	1.65	1.71	1.68	5.894e+05	136.00	1.29	0.06	0.10	0.03	23,23,38
2870	1.75	1.75	1.79	6.253e+05	136.00	1.38	0.05	0.10	0.02	23,23,18
2871	1.74	1.74	1.60	6.210e+05	136.00	1.24	0.14	0.11	0.07	23,23,42
2872	1.42	1.74	1.29	5.126e+05	136.00	1.00	0.16	0.11	0.12	23,23,42
2873	1.42	1.42	0.84	5.126e+05	136.00	0.65	0.16	0.05	0.15	23,23,42
2874	0.47	0.48	0.47	1.724e+05	136.00	0.36	0.12	0.05	0.21	26,21,26
2875	0.47	0.48	0.47	1.724e+05	136.00	0.36	0.12	0.05	0.21	26,21,26
2877	1.58	1.58	1.65	5.662e+05	136.00	1.28	0.11	0.10	0.04	23,23,38
2878	1.65	1.71	1.68	5.894e+05	136.00	1.29	0.06	0.10	0.03	23,23,38
2879	1.75	1.75	1.79	6.253e+05	136.00	1.38	0.05	0.10	0.02	23,23,18
2880	1.74	1.74	1.60	6.210e+05	136.00	1.24	0.14	0.11	0.07	23,23,42
2881	1.42	1.74	1.29	5.126e+05	136.00	1.00	0.16	0.11	0.12	23,23,42
2882	1.42	1.42	0.84	5.126e+05	136.00	0.65	0.16	0.05	0.15	23,23,42
2883	0.47	0.48	0.47	1.724e+05	136.00	0.36	0.12	0.05	0.21	26,21,26
2884	0.47	0.48	0.47	1.724e+05	136.00	0.36	0.12	0.05	0.21	26,21,26
2886	1.58	1.58	1.65	5.662e+05	136.00	1.28	0.11	0.10	0.04	23,23,38
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				1.724e+05	136.00	0.36				
	1.75	1.75	1.79	6.253e+05	136.00	1.38	0.16	0.11	0.21	

Setto	Mat.	Spessore	Stato
		cm	
203	muratura E = 1.024e+05	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
2852	0.12	0.12	0.12	4.440e+04	136.00	0.10	0.24	0.03	0.51	26,21,39
2853	0.12	0.12	0.12	4.440e+04	136.00	0.10	0.24	0.03	0.51	26,21,39
2866	0.12	0.12	0.12	4.440e+04	136.00	0.10	0.24	0.03	0.51	26,21,39
2867	0.12	0.12	0.12	4.440e+04	136.00	0.10	0.24	0.03	0.51	26,21,39
2875	0.12	0.12	0.12	4.440e+04	136.00	0.10	0.24	0.03	0.51	26,21,39
2876	0.12	0.12	0.12	4.440e+04	136.00	0.10	0.24	0.03	0.51	26,21,39
2884	0.12	0.12	0.12	4.440e+04	136.00	0.10	0.24	0.03	0.51	26,21,39
2885	0.12	0.12	0.12	4.440e+04	136.00	0.10	0.24	0.03	0.51	26,21,39
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				4.440e+04	136.00	0.10				
	0.12	0.12	0.12	4.440e+04	136.00	0.10	0.24	0.03	0.51	

Setto	Mat.	Spessore	Stato
		cm	
204	muratura E = 1.024e+05	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
1303	1.91	1.87	1.85	7.869e+06	462.00	1.43	0.12	0.08	0.06	18,35,37
1312	1.91	1.87	1.85	7.869e+06	462.00	1.43	0.12	0.08	0.06	18,35,37
1321	1.91	1.87	1.85	7.869e+06	462.00	1.43	0.12	0.08	0.06	18,35,37
1330	1.91	1.87	1.85	7.869e+06	462.00	1.43	0.12	0.08	0.06	18,35,37
1339	1.91	1.87	1.85	7.869e+06	462.00	1.43	0.12	0.08	0.06	18,35,37
1348	1.91	1.87	1.85	7.869e+06	462.00	1.43	0.12	0.08	0.06	18,35,37
1357	1.91	1.87	1.85	7.869e+06	462.00	1.43	0.12	0.08	0.06	18,35,37
1366	1.91	1.87	1.85	7.869e+06	462.00	1.43	0.12	0.08	0.06	18,35,37
1375	1.91	1.87	1.85	7.869e+06	462.00	1.43	0.12	0.08	0.06	18,35,37
1384	1.91	1.87	1.85	7.869e+06	462.00	1.43	0.12	0.08	0.06	18,35,37
1724	1.91	1.74	1.85	7.869e+06	462.00	1.43	0.12	0.09	0.06	18,35,37
1726	1.78	1.56	1.68	7.342e+06	462.00	1.29	0.11	0.10	0.03	18,35,36
1728	1.41	1.38	1.44	5.855e+06	462.00	1.11	0.11	0.11	0.04	18,35,12
1730	1.21	1.19	1.44	5.052e+06	462.00	1.11	0.13	0.13	0.04	18,35,12
1732	1.03	1.00	1.23	4.291e+06	462.00	0.95	0.15	0.16	0.04	18,41,12
1734	0.85	0.84	1.04	3.570e+06	462.00	0.80	0.16	0.18	0.02	21,41,12
1736	0.85	0.69	0.69	3.570e+06	462.00	0.53	0.16	0.18	0.03	21,41,18
1738	0.69	0.69	0.69	2.902e+06	462.00	0.53	0.15	0.18	0.03	33,41,18
2891	1.91	1.74	1.85	7.869e+06	462.00	1.43	0.12	0.09	0.06	18,35,37
2892	1.78	1.56	1.68	7.342e+06	462.00	1.29	0.11	0.10	0.03	18,35,36
2893	1.41	1.38	1.44	5.855e+06	462.00	1.11	0.11	0.11	0.04	18,35,12
2894	1.21	1.19	1.44	5.052e+06	462.00	1.11	0.13	0.13	0.04	18,35,12
2895	1.03	1.00	1.23	4.291e+06	462.00	0.95	0.15	0.16	0.04	18,41,12
2896	0.85	0.84	1.04	3.570e+06	462.00	0.80	0.16	0.18	0.02	21,41,12
2897	0.85	0.69	0.69	3.570e+06	462.00	0.53	0.16	0.18	0.03	21,41,18
2898	0.69	0.69	0.69	2.902e+06	462.00	0.53	0.15	0.18	0.03	33,41,18
2900	1.91	1.74	1.85	7.869e+06	462.00	1.43	0.12	0.09	0.06	18,35,37
2901	1.78	1.56	1.68	7.342e+06	462.00	1.29	0.11	0.10	0.03	18,35,36
2902	1.41	1.38	1.44	5.855e+06	462.00	1.11	0.11	0.11	0.04	18,35,12
2903	1.21	1.19	1.44	5.052e+06	462.00	1.11	0.13	0.13	0.04	18,35,12
2904	1.03	1.00	1.23	4.291e+06	462.00	0.95	0.15	0.16	0.04	18,41,12
2905	0.85	0.84	1.04	3.570e+06	462.00	0.80	0.16	0.18	0.02	21,41,12
2906	0.85	0.69	0.69	3.570e+06	462.00	0.53	0.16	0.18	0.03	21,41,18
2907	0.69	0.69	0.69	2.902e+06	462.00	0.53	0.15	0.18	0.03	33,41,18
2909	1.91	1.74	1.85	7.869e+06	462.00	1.43	0.12	0.09	0.06	18,35,37
2910	1.78	1.56	1.68	7.342e+06	462.00	1.29	0.11	0.10	0.03	18,35,36
2911	1.41	1.38	1.44	5.855e+06	462.00	1.11	0.11	0.11	0.04	18,35,12
2912	1.21	1.19	1.44	5.052e+06	462.00	1.11	0.13	0.13	0.04	18,35,12
2913	1.03	1.00	1.23	4.291e+06	462.00	0.95	0.15	0.16	0.04	18,41,12
2914	0.85	0.84	1.04	3.570e+06	462.00	0.80	0.16	0.18	0.02	21,41,12
2915	0.85	0.69	0.69	3.570e+06	462.00	0.53	0.16	0.18	0.03	21,41,18
2916	0.69	0.69	0.69	2.902e+06	462.00	0.53	0.15	0.18	0.03	33,41,18
2918	1.91	1.74	1.85	7.869e+06	462.00	1.43	0.12	0.09	0.06	18,35,37
2919	1.78	1.56	1.68	7.342e+06	462.00	1.29	0.11	0.10	0.03	18,35,36
2920	1.41	1.38	1.44	5.855e+06	462.00	1.11	0.11	0.11	0.04	18,35,12
2921	1.21	1.19	1.44	5.052e+06	462.00	1.11	0.13	0.13	0.04	18,35,12
2922	1.03	1.00	1.23	4.291e+06	462.00	0.95	0.15	0.16	0.04	18,41,12
2923	0.85	0.84	1.04	3.570e+06	462.00	0.80	0.16	0.18	0.02	21,41,12
2924	0.85	0.69	0.69	3.570e+06	462.00	0.53	0.16	0.18	0.03	21,41,18
2925	0.69	0.69	0.69	2.902e+06	462.00	0.53	0.15	0.18	0.03	33,41,18
2927	1.91	1.74	1.85	7.869e+06	462.00	1.43	0.12	0.09	0.06	18,35,37
2928	1.78	1.56	1.68	7.342e+06	462.00	1.29	0.11	0.10	0.03	18,35,36
2929	1.41	1.38	1.44	5.855e+06	462.00	1.11	0.11	0.11	0.04	18,35,12
2930	1.21	1.19	1.44	5.052e+06	462.00	1.11	0.13	0.13	0.04	18,35,12
2931	1.03	1.00	1.23	4.291e+06	462.00	0.95	0.15	0.16	0.04	18,41,12
2932	0.85	0.84	1.04	3.570e+06	462.00	0.80	0.16	0.18	0.02	21,41,12
2933	0.85	0.69	0.69	3.570e+06	462.00	0.53	0.16	0.18	0.03	21,41,18
2934	0.69	0.69	0.69	2.902e+06	462.00	0.53	0.15	0.18	0.03	33,41,18
2936	1.91	1.74	1.85	7.869e+06	462.00	1.43	0.12	0.09	0.06	18,35,37
2937	1.78	1.56	1.68	7.342e+06	462.00	1.29	0.11	0.10	0.03	18,35,36
2938	1.41	1.38	1.44	5.855e+06	462.00	1.11	0.11	0.11	0.04	18,35,12
2939	1.21	1.19	1.44	5.052e+06	462.00	1.11	0.13	0.13	0.04	18,35,12
2940	1.03	1.00	1.23	4.291e+06	462.00	0.95	0.15	0.16	0.04	18,41,12
2941	0.85	0.84	1.04	3.570e+06	462.00	0.80	0.16	0.18	0.02	21,41,12
2942	0.85	0.69	0.69	3.570e+06	462.00	0.53	0.16	0.18	0.03	21,41,18
2943	0.69	0.69	0.69	2.902e+06	462.00	0.53	0.15	0.18	0.03	33,41,18
2945	1.91	1.74	1.85	7.869e+06	462.00	1.43	0.12	0.09	0.06	18,35,37

2946	1.78	1.56	1.68	7.342e+06	462.00	1.29	0.11	0.10	0.03	18,35,36
2947	1.41	1.38	1.44	5.855e+06	462.00	1.11	0.11	0.11	0.04	18,35,12
2948	1.21	1.19	1.44	5.052e+06	462.00	1.11	0.13	0.13	0.04	18,35,12
2949	1.03	1.00	1.23	4.291e+06	462.00	0.95	0.15	0.16	0.04	18,41,12
2950	0.85	0.84	1.04	3.570e+06	462.00	0.80	0.16	0.18	0.02	21,41,12
2951	0.85	0.69	0.69	3.570e+06	462.00	0.53	0.16	0.18	0.03	21,41,18
2952	0.69	0.69	0.69	2.902e+06	462.00	0.53	0.15	0.18	0.03	33,41,18
2954	1.91	1.74	1.85	7.869e+06	462.00	1.43	0.12	0.09	0.06	18,35,37
2955	1.78	1.56	1.68	7.342e+06	462.00	1.29	0.11	0.10	0.03	18,35,36
2956	1.41	1.38	1.44	5.855e+06	462.00	1.11	0.11	0.11	0.04	18,35,12
2957	1.21	1.19	1.44	5.052e+06	462.00	1.11	0.13	0.13	0.04	18,35,12
2958	1.03	1.00	1.23	4.291e+06	462.00	0.95	0.15	0.16	0.04	18,41,12
2959	0.85	0.84	1.04	3.570e+06	462.00	0.80	0.16	0.18	0.02	21,41,12
2960	0.85	0.69	0.69	3.570e+06	462.00	0.53	0.16	0.18	0.03	21,41,18
2961	0.69	0.69	0.69	2.902e+06	462.00	0.53	0.15	0.18	0.03	33,41,18
2963	1.91	1.74	1.85	7.869e+06	462.00	1.43	0.12	0.09	0.06	18,35,37
2964	1.78	1.56	1.68	7.342e+06	462.00	1.29	0.11	0.10	0.03	18,35,36
2965	1.41	1.38	1.44	5.855e+06	462.00	1.11	0.11	0.11	0.04	18,35,12
2966	1.21	1.19	1.44	5.052e+06	462.00	1.11	0.13	0.13	0.04	18,35,12
2967	1.03	1.00	1.23	4.291e+06	462.00	0.95	0.15	0.16	0.04	18,41,12
2968	0.85	0.84	1.04	3.570e+06	462.00	0.80	0.16	0.18	0.02	21,41,12
2969	0.85	0.69	0.69	3.570e+06	462.00	0.53	0.16	0.18	0.03	21,41,18
2970	0.69	0.69	0.69	2.902e+06	462.00	0.53	0.15	0.18	0.03	33,41,18

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				2.902e+06	462.00	0.53			
	1.91	1.87	1.85	7.869e+06	462.00	1.43	0.16	0.18	0.06

Setto	Mat.	Spessore	Stato
		cm	
205	muratura E = 1.024e+05	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1738	0.43	0.43	0.43	1.808e+06	462.00	0.33	0.14	0.13	0.02	27,41,29
1740	0.43	0.43	0.43	1.808e+06	462.00	0.33	0.14	0.13	0.02	27,41,29
2898	0.43	0.43	0.43	1.808e+06	462.00	0.33	0.14	0.13	0.02	27,41,29
2899	0.43	0.43	0.43	1.808e+06	462.00	0.33	0.14	0.13	0.02	27,41,29
2907	0.43	0.43	0.43	1.808e+06	462.00	0.33	0.14	0.13	0.02	27,41,29
2908	0.43	0.43	0.43	1.808e+06	462.00	0.33	0.14	0.13	0.02	27,41,29
2916	0.43	0.43	0.43	1.808e+06	462.00	0.33	0.14	0.13	0.02	27,41,29
2917	0.43	0.43	0.43	1.808e+06	462.00	0.33	0.14	0.13	0.02	27,41,29
2925	0.43	0.43	0.43	1.808e+06	462.00	0.33	0.14	0.13	0.02	27,41,29
2926	0.43	0.43	0.43	1.808e+06	462.00	0.33	0.14	0.13	0.02	27,41,29
2934	0.43	0.43	0.43	1.808e+06	462.00	0.33	0.14	0.13	0.02	27,41,29
2935	0.43	0.43	0.43	1.808e+06	462.00	0.33	0.14	0.13	0.02	27,41,29
2943	0.43	0.43	0.43	1.808e+06	462.00	0.33	0.14	0.13	0.02	27,41,29
2944	0.43	0.43	0.43	1.808e+06	462.00	0.33	0.14	0.13	0.02	27,41,29
2952	0.43	0.43	0.43	1.808e+06	462.00	0.33	0.14	0.13	0.02	27,41,29
2953	0.43	0.43	0.43	1.808e+06	462.00	0.33	0.14	0.13	0.02	27,41,29
2961	0.43	0.43	0.43	1.808e+06	462.00	0.33	0.14	0.13	0.02	27,41,29
2962	0.43	0.43	0.43	1.808e+06	462.00	0.33	0.14	0.13	0.02	27,41,29
2970	0.43	0.43	0.43	1.808e+06	462.00	0.33	0.14	0.13	0.02	27,41,29
2971	0.43	0.43	0.43	1.808e+06	462.00	0.33	0.14	0.13	0.02	27,41,29

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				1.808e+06	462.00	0.33			
	0.43	0.43	0.43	1.808e+06	462.00	0.33	0.14	0.13	0.02

Setto	Mat.	Spessore	Stato
		cm	
207	muratura E = 1.024e+05	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1142	2.27	2.27	1.87	7.469e+04	41.50	1.45	0.04	0.05	0.03	35,39,20

1267	2.27	2.27	1.87	7.469e+04	41.50	1.45	0.04	0.05	0.03	35,39,20
2841	1.50	1.69	2.00	5.015e+04	41.50	1.55	0.03	0.05	0.03	42,42,23
2842	2.19	2.04	1.97	7.222e+04	41.50	1.52	0.04	0.10	0.03	41,42,20
2843	2.51	2.78	2.48	8.238e+04	41.50	1.92	0.25	0.32	0.04	24,42,23
2844	2.12	2.51	2.11	6.992e+04	41.50	1.63	0.26	0.40	0.05	19,42,23
2850	2.12	2.51	2.11	6.992e+04	41.50	1.63	0.26	0.40	0.05	19,42,23
2851	0.60	1.35	0.73	2.045e+04	41.50	0.56	0.03	0.32	0.06	16,42,14
2852	0.60	0.72	0.73	2.045e+04	41.50	0.56	0.03	0.28	0.06	16,42,14
2886	2.27	2.27	1.87	7.469e+04	41.50	1.45	0.04	0.05	0.03	35,39,20
2985	2.12	2.51	2.11	6.992e+04	41.50	1.63	0.26	0.40	0.05	19,42,23
2986	2.12	2.51	2.11	6.992e+04	41.50	1.63	0.26	0.40	0.05	19,42,23
2987	0.60	1.35	0.73	2.045e+04	41.50	0.56	0.03	0.32	0.06	16,42,14
2988	0.60	0.72	0.73	2.045e+04	41.50	0.56	0.03	0.28	0.06	16,42,14
2992	2.27	2.27	1.87	7.469e+04	41.50	1.45	0.04	0.05	0.03	35,39,20
2993	1.50	1.69	2.00	5.015e+04	41.50	1.55	0.03	0.05	0.03	42,42,23
2994	2.19	2.04	1.97	7.222e+04	41.50	1.52	0.04	0.10	0.03	41,42,20
2995	2.51	2.78	2.48	8.238e+04	41.50	1.92	0.25	0.32	0.04	24,42,23
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				2.045e+04	41.50	0.56				
	2.51	2.78	2.48	8.238e+04	41.50	1.92	0.26	0.40	0.06	

Setto	Mat.	Spessore	Stato
		cm	
208	muratura E = 1.024e+05	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
2852	0.37	0.37	0.38	1.249e+04	41.50	0.29	0.04	0.07	0.12	27,38,25
2853	0.37	0.37	0.38	1.249e+04	41.50	0.29	0.04	0.07	0.12	27,38,25
2988	0.37	0.37	0.38	1.249e+04	41.50	0.29	0.04	0.07	0.12	27,38,25
2989	0.37	0.37	0.38	1.249e+04	41.50	0.29	0.04	0.07	0.12	27,38,25
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				1.249e+04	41.50	0.29				
	0.37	0.37	0.38	1.249e+04	41.50	0.29	0.04	0.07	0.12	

Setto	Mat.	Spessore	Stato
		cm	
209	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
1921	0.62	0.61	0.62	9.364e+04	87.50	0.50	0.43	0.10	0.11	27,34,27
1930	0.62	0.61	0.62	9.364e+04	87.50	0.50	0.43	0.10	0.11	27,34,27
1939	0.62	0.61	0.62	9.364e+04	87.50	0.50	0.43	0.10	0.11	27,34,27
2996	0.62	0.36	0.36	9.364e+04	87.50	0.29	0.43	0.11	0.19	27,34,27
2997	0.62	0.36	0.36	9.364e+04	87.50	0.29	0.43	0.11	0.19	27,34,27
2998	0.13	0.36	0.14	1.959e+04	87.50	0.11	0.39	0.11	0.44	30,34,28
2999	0.13	0.36	0.14	1.959e+04	87.50	0.11	0.39	0.11	0.44	30,34,28
3000	0.13	0.14	0.14	1.959e+04	80.88	0.11	0.39	0.07	0.44	30,34,28
3001	0.13	0.14	0.14	1.959e+04	80.88	0.11	0.39	0.07	0.44	30,34,28
3002	0.62	0.36	0.36	9.364e+04	87.50	0.29	0.43	0.11	0.19	27,34,27
3003	0.13	0.36	0.14	1.959e+04	87.50	0.11	0.39	0.11	0.44	30,34,28
3004	0.13	0.14	0.14	1.959e+04	80.88	0.11	0.39	0.07	0.44	30,34,28
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				1.959e+04	80.88	0.11				
	0.62	0.61	0.62	9.364e+04	87.50	0.50	0.43	0.11	0.44	

Setto	Mat.	Spessore	Stato
		cm	
211	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
1795	0.20	0.21	0.20	4.138e+05	323.00	0.16	0.34	0.06	0.62	17,11,30
1804	0.20	0.21	0.20	4.138e+05	323.00	0.16	0.34	0.06	0.62	17,11,30
1813	0.20	0.21	0.20	4.138e+05	323.00	0.16	0.34	0.06	0.62	17,11,30
1822	0.20	0.21	0.20	4.138e+05	323.00	0.16	0.34	0.06	0.62	17,11,30
1831	0.20	0.21	0.20	4.138e+05	323.00	0.16	0.34	0.06	0.62	17,11,30
1840	0.20	0.21	0.20	4.138e+05	323.00	0.16	0.34	0.06	0.62	17,11,30
1849	0.20	0.21	0.20	4.138e+05	323.00	0.16	0.34	0.06	0.62	17,11,30
1858	0.20	0.21	0.20	4.138e+05	323.00	0.16	0.34	0.06	0.62	17,11,30
1867	0.20	0.21	0.20	4.138e+05	323.00	0.16	0.34	0.06	0.62	17,11,30
1876	0.20	0.21	0.20	4.138e+05	323.00	0.16	0.34	0.06	0.62	17,11,30
3017	0.20	0.21	0.20	4.138e+05	323.00	0.16	0.34	0.06	0.62	17,11,30
3018	0.23	0.23	0.22	4.674e+05	323.00	0.18	0.23	0.05	0.47	17,11,30
3019	0.21	0.21	0.20	4.324e+05	323.00	0.16	0.17	0.02	0.33	17,11,30
3020	0.20	0.21	0.20	4.138e+05	323.00	0.16	0.34	0.06	0.62	17,11,30
3021	0.23	0.23	0.22	4.674e+05	323.00	0.18	0.23	0.05	0.47	17,11,30
3022	0.21	0.21	0.20	4.324e+05	323.00	0.16	0.17	0.02	0.33	17,11,30
3023	0.20	0.21	0.20	4.138e+05	323.00	0.16	0.34	0.06	0.62	17,11,30
3024	0.23	0.23	0.22	4.674e+05	323.00	0.18	0.23	0.05	0.47	17,11,30
3025	0.21	0.21	0.20	4.324e+05	323.00	0.16	0.17	0.02	0.33	17,11,30
3026	0.20	0.21	0.20	4.138e+05	323.00	0.16	0.34	0.06	0.62	17,11,30
3027	0.23	0.23	0.22	4.674e+05	323.00	0.18	0.23	0.05	0.47	17,11,30
3028	0.21	0.21	0.20	4.324e+05	323.00	0.16	0.17	0.02	0.33	17,11,30
3029	0.20	0.21	0.20	4.138e+05	323.00	0.16	0.34	0.06	0.62	17,11,30
3030	0.23	0.23	0.22	4.674e+05	323.00	0.18	0.23	0.05	0.47	17,11,30
3031	0.21	0.21	0.20	4.324e+05	323.00	0.16	0.17	0.02	0.33	17,11,30
3032	0.20	0.21	0.20	4.138e+05	323.00	0.16	0.34	0.06	0.62	17,11,30
3033	0.23	0.23	0.22	4.674e+05	323.00	0.18	0.23	0.05	0.47	17,11,30
3034	0.21	0.21	0.20	4.324e+05	323.00	0.16	0.17	0.02	0.33	17,11,30
3035	0.20	0.21	0.20	4.138e+05	323.00	0.16	0.34	0.06	0.62	17,11,30
3036	0.23	0.23	0.22	4.674e+05	323.00	0.18	0.23	0.05	0.47	17,11,30
3037	0.21	0.21	0.20	4.324e+05	323.00	0.16	0.17	0.02	0.33	17,11,30
3038	0.20	0.21	0.20	4.138e+05	323.00	0.16	0.34	0.06	0.62	17,11,30
3039	0.23	0.23	0.22	4.674e+05	323.00	0.18	0.23	0.05	0.47	17,11,30
3040	0.21	0.21	0.20	4.324e+05	323.00	0.16	0.17	0.02	0.33	17,11,30
3041	0.20	0.21	0.20	4.138e+05	323.00	0.16	0.34	0.06	0.62	17,11,30
3042	0.23	0.23	0.22	4.674e+05	323.00	0.18	0.23	0.05	0.47	17,11,30
3043	0.21	0.21	0.20	4.324e+05	323.00	0.16	0.17	0.02	0.33	17,11,30
3044	0.20	0.21	0.20	4.138e+05	323.00	0.16	0.34	0.06	0.62	17,11,30
3045	0.23	0.23	0.22	4.674e+05	323.00	0.18	0.23	0.05	0.47	17,11,30
3046	0.21	0.21	0.20	4.324e+05	323.00	0.16	0.17	0.02	0.33	17,11,30

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				4.138e+05	323.00	0.16			
	0.23	0.23	0.22	4.674e+05	323.00	0.18	0.34	0.06	0.62

Setto	Mat.	Spessore	Stato
		cm	
213	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
1740	0.91	0.95	0.91	1.567e+05	93.50	0.73	0.04	0.26	0.13	15,31,20
1741	0.91	0.95	0.91	1.567e+05	93.50	0.73	0.04	0.26	0.13	15,31,20
1750	0.91	0.95	0.91	1.567e+05	93.50	0.73	0.04	0.26	0.13	15,31,20
3059	0.53	0.95	0.46	9.083e+04	93.50	0.37	0.06	0.26	0.14	14,31,24
3060	0.15	0.51	0.14	2.645e+04	93.50	0.12	0.25	0.24	0.20	22,29,19
3061	0.15	0.15	0.14	2.645e+04	93.50	0.12	0.25	0.16	0.20	22,21,19
3062	0.53	0.95	0.46	9.083e+04	93.50	0.37	0.06	0.26	0.14	14,31,24
3063	0.15	0.51	0.14	2.645e+04	93.50	0.12	0.25	0.24	0.20	22,29,19
3064	0.15	0.15	0.14	2.645e+04	93.50	0.12	0.25	0.16	0.20	22,21,19
3065	0.53	0.95	0.46	9.083e+04	93.50	0.37	0.06	0.26	0.14	14,31,24
3066	0.15	0.51	0.14	2.645e+04	93.50	0.12	0.25	0.24	0.20	22,29,19
3067	0.15	0.15	0.14	2.645e+04	93.50	0.12	0.25	0.16	0.20	22,21,19

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				2.645e+04	93.50	0.12			
	0.91	0.95	0.91	1.567e+05	93.50	0.73	0.25	0.26	0.20

Setto	Mat.	Spessore	Stato
		cm	
214	muratura (consolidata) E = 1.536e+05	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
3066	0.47	0.54	0.52	7.435e+04	89.00	0.27	0.10	0.05	0.15	26,35,32
3067	0.47	0.54	0.52	7.435e+04	89.00	0.27	0.10	0.05	0.15	26,35,32
3069	0.47	0.54	0.52	7.435e+04	89.00	0.27	0.10	0.05	0.15	26,35,32
3070	0.47	0.54	0.52	7.435e+04	89.00	0.27	0.10	0.05	0.15	26,35,32
3072	0.47	0.54	0.52	7.435e+04	89.00	0.27	0.10	0.05	0.15	26,35,32
3073	0.47	0.54	0.52	7.435e+04	89.00	0.27	0.10	0.05	0.15	26,35,32
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	0.47	0.54	0.52	7.435e+04	89.00	0.27				
	0.47	0.54	0.52	7.435e+04	89.00	0.27	0.10	0.05	0.15	

Setto	Mat.	Spessore	Stato
		cm	
217	muratura (consolidata) E = 1.536e+05	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
3081	0.32	0.31	0.32	5.176e+04	90.00	0.17	0.08	0.01	0.05	16,11,12
3082	0.32	0.31	0.32	5.176e+04	90.00	0.17	0.08	0.01	0.05	16,11,12
3084	0.32	0.31	0.32	5.176e+04	90.00	0.17	0.08	0.01	0.05	16,11,12
3085	0.32	0.31	0.32	5.176e+04	90.00	0.17	0.08	0.01	0.05	16,11,12
3087	0.32	0.31	0.32	5.176e+04	90.00	0.17	0.08	0.01	0.05	16,11,12
3088	0.32	0.31	0.32	5.176e+04	90.00	0.17	0.08	0.01	0.05	16,11,12
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
	0.32	0.31	0.32	5.176e+04	90.00	0.17				
	0.32	0.31	0.32	5.176e+04	90.00	0.17	0.08	0.01	0.05	

Setto	Mat.	Spessore	Stato
		cm	
218	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
2669	0.50	0.50	0.51	2.857e+06	536.00	0.59	0.15	0.04	0.25	35,35,20
2678	0.50	0.50	0.51	2.857e+06	536.00	0.59	0.15	0.04	0.25	35,35,20
2687	0.50	0.50	0.51	2.857e+06	536.00	0.59	0.15	0.04	0.25	35,35,20
2696	0.50	0.50	0.51	2.857e+06	536.00	0.59	0.15	0.04	0.25	35,35,20
2705	0.50	0.50	0.51	2.857e+06	536.00	0.59	0.15	0.04	0.25	35,35,20
2714	0.50	0.50	0.51	2.857e+06	536.00	0.59	0.15	0.04	0.25	35,35,20
2723	0.50	0.50	0.51	2.857e+06	536.00	0.59	0.15	0.04	0.25	35,35,20
2732	0.50	0.50	0.51	2.857e+06	536.00	0.59	0.15	0.04	0.25	35,35,20
2741	0.50	0.50	0.51	2.857e+06	536.00	0.59	0.15	0.04	0.25	35,35,20
2750	0.50	0.50	0.51	2.857e+06	536.00	0.59	0.15	0.04	0.25	35,35,20
2759	0.50	0.50	0.51	2.857e+06	536.00	0.59	0.15	0.04	0.25	35,35,20
2768	0.50	0.50	0.51	2.857e+06	536.00	0.59	0.15	0.04	0.25	35,35,20
3086	0.50	0.50	0.51	2.857e+06	536.00	0.59	0.15	0.04	0.25	35,35,20
3087	0.46	0.46	0.47	2.623e+06	536.00	0.54	0.10	0.04	0.23	35,35,20
3089	0.50	0.50	0.51	2.857e+06	536.00	0.59	0.15	0.04	0.25	35,35,20
3090	0.46	0.46	0.47	2.623e+06	536.00	0.54	0.10	0.04	0.23	35,35,20
3092	0.50	0.50	0.51	2.857e+06	536.00	0.59	0.15	0.04	0.25	35,35,20
3093	0.46	0.46	0.47	2.623e+06	536.00	0.54	0.10	0.04	0.23	35,35,20
3095	0.50	0.50	0.51	2.857e+06	536.00	0.59	0.15	0.04	0.25	35,35,20
3096	0.46	0.46	0.47	2.623e+06	536.00	0.54	0.10	0.04	0.23	35,35,20

3098	0.50	0.50	0.51	2.857e+06	536.00	0.59	0.15	0.04	0.25	35,35,20
3099	0.46	0.46	0.47	2.623e+06	536.00	0.54	0.10	0.04	0.23	35,35,20
3101	0.50	0.50	0.51	2.857e+06	536.00	0.59	0.15	0.04	0.25	35,35,20
3102	0.46	0.46	0.47	2.623e+06	536.00	0.54	0.10	0.04	0.23	35,35,20
3104	0.50	0.50	0.51	2.857e+06	536.00	0.59	0.15	0.04	0.25	35,35,20
3105	0.46	0.46	0.47	2.623e+06	536.00	0.54	0.10	0.04	0.23	35,35,20
3107	0.50	0.50	0.51	2.857e+06	536.00	0.59	0.15	0.04	0.25	35,35,20
3108	0.46	0.46	0.47	2.623e+06	536.00	0.54	0.10	0.04	0.23	35,35,20
3110	0.50	0.50	0.51	2.857e+06	536.00	0.59	0.15	0.04	0.25	35,35,20
3111	0.46	0.46	0.47	2.623e+06	536.00	0.54	0.10	0.04	0.23	35,35,20
3113	0.50	0.50	0.51	2.857e+06	536.00	0.59	0.15	0.04	0.25	35,35,20
3114	0.46	0.46	0.47	2.623e+06	536.00	0.54	0.10	0.04	0.23	35,35,20
3116	0.50	0.50	0.51	2.857e+06	536.00	0.59	0.15	0.04	0.25	35,35,20
3117	0.46	0.46	0.47	2.623e+06	536.00	0.54	0.10	0.04	0.23	35,35,20
3119	0.50	0.50	0.51	2.857e+06	536.00	0.59	0.15	0.04	0.25	35,35,20
3120	0.46	0.46	0.47	2.623e+06	536.00	0.54	0.10	0.04	0.23	35,35,20

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				2.623e+06	536.00	0.54			
	0.50	0.50	0.51	2.857e+06	536.00	0.59	0.15	0.04	0.25

Setto	Mat.	Spessore	Stato
		cm	
219	muratura (consolidata) E = 1.536e+05	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
3087	0.35	0.35	0.36	2.024e+06	536.00	0.18	0.06	0.01	0.20	35,35,20
3088	0.35	0.35	0.36	2.024e+06	536.00	0.18	0.06	0.01	0.20	35,35,20
3090	0.35	0.35	0.36	2.024e+06	536.00	0.18	0.06	0.01	0.20	35,35,20
3091	0.35	0.35	0.36	2.024e+06	536.00	0.18	0.06	0.01	0.20	35,35,20
3093	0.35	0.35	0.36	2.024e+06	536.00	0.18	0.06	0.01	0.20	35,35,20
3094	0.35	0.35	0.36	2.024e+06	536.00	0.18	0.06	0.01	0.20	35,35,20
3096	0.35	0.35	0.36	2.024e+06	536.00	0.18	0.06	0.01	0.20	35,35,20
3097	0.35	0.35	0.36	2.024e+06	536.00	0.18	0.06	0.01	0.20	35,35,20
3099	0.35	0.35	0.36	2.024e+06	536.00	0.18	0.06	0.01	0.20	35,35,20
3100	0.35	0.35	0.36	2.024e+06	536.00	0.18	0.06	0.01	0.20	35,35,20
3102	0.35	0.35	0.36	2.024e+06	536.00	0.18	0.06	0.01	0.20	35,35,20
3103	0.35	0.35	0.36	2.024e+06	536.00	0.18	0.06	0.01	0.20	35,35,20
3105	0.35	0.35	0.36	2.024e+06	536.00	0.18	0.06	0.01	0.20	35,35,20
3106	0.35	0.35	0.36	2.024e+06	536.00	0.18	0.06	0.01	0.20	35,35,20
3108	0.35	0.35	0.36	2.024e+06	536.00	0.18	0.06	0.01	0.20	35,35,20
3109	0.35	0.35	0.36	2.024e+06	536.00	0.18	0.06	0.01	0.20	35,35,20
3111	0.35	0.35	0.36	2.024e+06	536.00	0.18	0.06	0.01	0.20	35,35,20
3112	0.35	0.35	0.36	2.024e+06	536.00	0.18	0.06	0.01	0.20	35,35,20
3114	0.35	0.35	0.36	2.024e+06	536.00	0.18	0.06	0.01	0.20	35,35,20
3115	0.35	0.35	0.36	2.024e+06	536.00	0.18	0.06	0.01	0.20	35,35,20
3117	0.35	0.35	0.36	2.024e+06	536.00	0.18	0.06	0.01	0.20	35,35,20
3118	0.35	0.35	0.36	2.024e+06	536.00	0.18	0.06	0.01	0.20	35,35,20
3120	0.35	0.35	0.36	2.024e+06	536.00	0.18	0.06	0.01	0.20	35,35,20
3121	0.35	0.35	0.36	2.024e+06	536.00	0.18	0.06	0.01	0.20	35,35,20

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				2.024e+06	536.00	0.18			
	0.35	0.35	0.36	2.024e+06	536.00	0.18	0.06	0.01	0.20

Setto	Mat.	Spessore	Stato
		cm	
220	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
2768	0.74	0.71	0.71	3.761e+04	50.95	0.57	0.14	0.34	0.34	37,18,21
2786	0.74	0.71	0.71	3.761e+04	50.95	0.57	0.14	0.34	0.34	37,18,21
3119	0.74	0.71	0.32	3.761e+04	50.95	0.26	0.14	0.34	0.50	37,18,21
3120	0.34	0.34	0.32	1.760e+04	50.95	0.26	0.03	0.31	0.50	42,38,21

3122	0.74	0.71	0.32	3.761e+04	50.95	0.26	0.14	0.34	0.50	37,18,21
3123	0.34	0.34	0.32	1.760e+04	50.95	0.26	0.03	0.31	0.50	42,38,21
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				1.760e+04	50.95	0.26				
	0.74	0.71	0.71	3.761e+04	50.95	0.57	0.14	0.34	0.50	

Setto	Mat.	Spessore	Stato
		cm	
224	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
3131	0.08	0.06	0.06	1.596e+04	101.90	0.05	0.38	0.09	0.24	37,24,24
3132	0.08	0.06	0.06	1.596e+04	101.90	0.05	0.38	0.09	0.24	37,24,24
3134	0.08	0.06	0.06	1.596e+04	101.90	0.05	0.38	0.09	0.24	37,24,24
3135	0.08	0.06	0.06	1.596e+04	101.90	0.05	0.38	0.09	0.24	37,24,24
3137	0.08	0.06	0.06	1.596e+04	101.90	0.05	0.38	0.09	0.24	37,24,24
3138	0.08	0.06	0.06	1.596e+04	101.90	0.05	0.38	0.09	0.24	37,24,24
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				1.596e+04	101.90	0.05				
	0.08	0.06	0.06	1.596e+04	101.90	0.05	0.38	0.09	0.24	

Setto	Mat.	Spessore	Stato
		cm	
225	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
3132	0.06	0.06	0.06	1.237e+04	101.90	0.05	0.13	0.04	0.09	37,24,24
3133	0.06	0.06	0.06	1.237e+04	101.90	0.05	0.13	0.04	0.09	37,24,24
3135	0.06	0.06	0.06	1.237e+04	101.90	0.05	0.13	0.04	0.09	37,24,24
3136	0.06	0.06	0.06	1.237e+04	101.90	0.05	0.13	0.04	0.09	37,24,24
3138	0.06	0.06	0.06	1.237e+04	101.90	0.05	0.13	0.04	0.09	37,24,24
3139	0.06	0.06	0.06	1.237e+04	101.90	0.05	0.13	0.04	0.09	37,24,24
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				1.237e+04	101.90	0.05				
	0.06	0.06	0.06	1.237e+04	101.90	0.05	0.13	0.04	0.09	

Setto	Mat.	Spessore	Stato
		cm	
228	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
2574	0.97	0.95	0.95	4.928e+04	50.95	0.76	0.07	0.21	0.05	26,35,35
2801	0.97	0.95	0.95	4.928e+04	50.95	0.76	0.07	0.21	0.05	26,35,35
3146	0.62	0.95	0.64	3.191e+04	50.95	0.51	0.14	0.21	0.09	26,35,41
3147	0.62	0.54	0.64	3.191e+04	50.95	0.51	0.14	0.16	0.09	26,15,41
3149	0.62	0.95	0.64	3.191e+04	50.95	0.51	0.14	0.21	0.09	26,35,41
3150	0.62	0.54	0.64	3.191e+04	50.95	0.51	0.14	0.16	0.09	26,15,41
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				3.191e+04	50.95	0.51				
	0.97	0.95	0.95	4.928e+04	50.95	0.76	0.14	0.21	0.09	

Setto	Mat.	Spessore	Stato
		cm	
229	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
3147	0.17	0.39	0.28	8883.58	22.17	0.22	0.71	0.09	0.17	24,24,33
3148	0.17	0.39	0.28	8883.58	22.17	0.22	0.71	0.09	0.17	24,24,33
3150	0.17	0.39	0.28	8883.58	22.17	0.22	0.71	0.09	0.17	24,24,33
3151	0.17	0.39	0.28	8883.58	22.17	0.22	0.71	0.09	0.17	24,24,33

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				8883.58	22.17	0.22			
	0.17	0.39	0.28	8883.58	22.17	0.22	0.71	0.09	0.17

Setto	Mat.	Spessore	Stato
		cm	
230	mattoni pieni e malta di calce	37.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
2574	0.49	0.54	0.42	6.933e+04	88.17	0.47	0.11	0.05	0.10	35,25,24
2575	0.49	0.54	0.42	6.933e+04	88.17	0.47	0.11	0.05	0.10	35,25,24
2584	0.49	0.54	0.42	6.933e+04	88.17	0.47	0.11	0.05	0.10	35,25,24
3149	0.34	0.54	0.42	4.836e+04	88.17	0.47	0.17	0.05	0.10	41,25,24
3150	0.34	0.36	0.26	4.836e+04	88.17	0.30	0.17	0.04	0.07	41,25,24
3152	0.34	0.54	0.42	4.836e+04	88.17	0.47	0.17	0.05	0.10	41,25,24
3153	0.34	0.36	0.26	4.836e+04	88.17	0.30	0.17	0.04	0.07	41,25,24
3155	0.34	0.54	0.42	4.836e+04	88.17	0.47	0.17	0.05	0.10	41,25,24
3156	0.34	0.36	0.26	4.836e+04	88.17	0.30	0.17	0.04	0.07	41,25,24

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				4.836e+04	88.17	0.30			
	0.49	0.54	0.42	6.933e+04	88.17	0.47	0.17	0.05	0.10

Setto	Mat.	Spessore	Stato
		cm	
231	mattoni pieni e malta di calce	37.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
3150	0.12	0.23	0.12	1.753e+04	46.06	0.18	0.65	0.08	0.12	25,25,25
3151	0.12	0.23	0.12	1.753e+04	46.06	0.18	0.65	0.08	0.12	25,25,25
3153	0.12	0.23	0.12	1.753e+04	46.06	0.18	0.65	0.08	0.12	25,25,25
3154	0.12	0.23	0.12	1.753e+04	46.06	0.18	0.65	0.08	0.12	25,25,25
3156	0.12	0.23	0.12	1.753e+04	46.06	0.18	0.65	0.08	0.12	25,25,25
3157	0.12	0.23	0.12	1.753e+04	46.06	0.18	0.65	0.08	0.12	25,25,25

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				1.753e+04	46.06	0.18			
	0.12	0.23	0.12	1.753e+04	46.06	0.18	0.65	0.08	0.12

Setto	Mat.	Spessore	Stato
		cm	
234	mattoni pieni e malta di calce	37.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
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	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
3162	0.23	0.23	0.23	2.173e+05	224.67	0.26	0.15	0.04	0.81	21,18,39
3163	0.23	0.23	0.23	2.173e+05	224.67	0.26	0.15	0.04	0.81	21,18,39
3165	0.23	0.23	0.23	2.173e+05	224.67	0.26	0.15	0.04	0.81	21,18,39
3166	0.23	0.23	0.23	2.173e+05	224.67	0.26	0.15	0.04	0.81	21,18,39
3168	0.23	0.23	0.23	2.173e+05	224.67	0.26	0.15	0.04	0.81	21,18,39
3169	0.23	0.23	0.23	2.173e+05	224.67	0.26	0.15	0.04	0.81	21,18,39
3171	0.23	0.23	0.23	2.173e+05	224.67	0.26	0.15	0.04	0.81	21,18,39
3172	0.23	0.23	0.23	2.173e+05	224.67	0.26	0.15	0.04	0.81	21,18,39
3174	0.23	0.23	0.23	2.173e+05	224.67	0.26	0.15	0.04	0.81	21,18,39
3175	0.23	0.23	0.23	2.173e+05	224.67	0.26	0.15	0.04	0.81	21,18,39
3177	0.23	0.23	0.23	2.173e+05	224.67	0.26	0.15	0.04	0.81	21,18,39
3178	0.23	0.23	0.23	2.173e+05	224.67	0.26	0.15	0.04	0.81	21,18,39
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				2.173e+05	224.67	0.26				
	0.23	0.23	0.23	2.173e+05	224.67	0.26	0.15	0.04	0.81	

Setto	Mat.	Spessore	Stato
		cm	
235	mattoni pieni e malta di calce	37.0	ok L

	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
3163	0.10	0.10	0.10	8.867e+04	224.67	0.14	0.06	0.03	0.38	21,13,39
3164	0.10	0.10	0.10	8.867e+04	224.67	0.14	0.06	0.03	0.38	21,13,39
3166	0.10	0.10	0.10	8.867e+04	224.67	0.14	0.06	0.03	0.38	21,13,39
3167	0.10	0.10	0.10	8.867e+04	224.67	0.14	0.06	0.03	0.38	21,13,39
3169	0.10	0.10	0.10	8.867e+04	224.67	0.14	0.06	0.03	0.38	21,13,39
3170	0.10	0.10	0.10	8.867e+04	224.67	0.14	0.06	0.03	0.38	21,13,39
3172	0.10	0.10	0.10	8.867e+04	224.67	0.14	0.06	0.03	0.38	21,13,39
3173	0.10	0.10	0.10	8.867e+04	224.67	0.14	0.06	0.03	0.38	21,13,39
3175	0.10	0.10	0.10	8.867e+04	224.67	0.14	0.06	0.03	0.38	21,13,39
3176	0.10	0.10	0.10	8.867e+04	224.67	0.14	0.06	0.03	0.38	21,13,39
3178	0.10	0.10	0.10	8.867e+04	224.67	0.14	0.06	0.03	0.38	21,13,39
3179	0.10	0.10	0.10	8.867e+04	224.67	0.14	0.06	0.03	0.38	21,13,39
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
				8.867e+04	224.67	0.14				
	0.10	0.10	0.10	8.867e+04	224.67	0.14	0.06	0.03	0.38	

Setto	Mat.	Spessore	Stato
		cm	
238	mattoni pieni e malta di calce	37.0	ok L

	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
2493	0.35	0.37	0.37	1.515e+05	153.50	0.41	0.31	0.04	0.57	21,41,31
2494	0.35	0.37	0.37	1.515e+05	153.50	0.41	0.31	0.04	0.57	21,41,31
2503	0.35	0.37	0.37	1.515e+05	153.50	0.41	0.31	0.04	0.57	21,41,31
2512	0.35	0.37	0.37	1.515e+05	153.50	0.41	0.31	0.04	0.57	21,41,31
3183	0.30	0.35	0.37	1.304e+05	131.64	0.41	0.43	0.06	0.57	29,33,31
3184	0.30	0.35	0.31	1.304e+05	131.64	0.34	0.43	0.06	0.54	29,33,31
3186	0.30	0.35	0.37	1.304e+05	131.64	0.41	0.43	0.06	0.57	29,33,31
3187	0.30	0.35	0.31	1.304e+05	131.64	0.34	0.43	0.06	0.54	29,33,31
3189	0.30	0.35	0.37	1.304e+05	131.64	0.41	0.43	0.06	0.57	29,33,31
3190	0.30	0.35	0.31	1.304e+05	131.64	0.34	0.43	0.06	0.54	29,33,31
3192	0.30	0.35	0.37	1.304e+05	131.64	0.41	0.43	0.06	0.57	29,33,31
3193	0.30	0.35	0.31	1.304e+05	131.64	0.34	0.43	0.06	0.54	29,33,31
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				1.304e+05	131.64	0.34				
	0.35	0.37	0.37	1.515e+05	153.50	0.41	0.43	0.06	0.57	

Setto	Mat.	Spessore	Stato
		cm	
239	mattoni pieni e malta di calce	37.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
3184	0.18	0.44	0.17	7.586e+04	61.76	0.25	0.74	0.18	0.27	35,35,27
3185	0.18	0.44	0.17	7.586e+04	61.76	0.25	0.74	0.18	0.27	35,35,27
3187	0.18	0.44	0.17	7.586e+04	61.76	0.25	0.74	0.18	0.27	35,35,27
3188	0.18	0.44	0.17	7.586e+04	61.76	0.25	0.74	0.18	0.27	35,35,27
3190	0.18	0.44	0.17	7.586e+04	61.76	0.25	0.74	0.18	0.27	35,35,27
3191	0.18	0.44	0.17	7.586e+04	61.76	0.25	0.74	0.18	0.27	35,35,27
3193	0.18	0.44	0.17	7.586e+04	61.76	0.25	0.74	0.18	0.27	35,35,27
3194	0.18	0.44	0.17	7.586e+04	61.76	0.25	0.74	0.18	0.27	35,35,27

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				7.586e+04	61.76	0.25			
	0.18	0.44	0.17	7.586e+04	61.76	0.25	0.74	0.18	0.27

Setto	Mat.	Spessore	Stato
		cm	
244	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
2058	0.52	0.50	0.52	2.940e+05	170.00	0.60	0.28	0.09	0.05	32,38,31
2067	0.52	0.50	0.52	2.940e+05	170.00	0.60	0.28	0.09	0.05	32,38,31
2076	0.52	0.50	0.52	2.940e+05	170.00	0.60	0.28	0.09	0.05	32,38,31
2085	0.52	0.50	0.52	2.940e+05	170.00	0.60	0.28	0.09	0.05	32,38,31
2094	0.52	0.50	0.52	2.940e+05	170.00	0.60	0.28	0.09	0.05	32,38,31
3204	0.52	0.50	0.32	2.940e+05	170.00	0.37	0.28	0.09	0.06	32,38,29
3205	0.33	0.32	0.32	1.874e+05	170.00	0.37	0.25	0.08	0.06	32,38,29
3207	0.52	0.50	0.32	2.940e+05	170.00	0.37	0.28	0.09	0.06	32,38,29
3208	0.33	0.32	0.32	1.874e+05	170.00	0.37	0.25	0.08	0.06	32,38,29
3210	0.52	0.50	0.32	2.940e+05	170.00	0.37	0.28	0.09	0.06	32,38,29
3211	0.33	0.32	0.32	1.874e+05	170.00	0.37	0.25	0.08	0.06	32,38,29
3213	0.52	0.50	0.32	2.940e+05	170.00	0.37	0.28	0.09	0.06	32,38,29
3214	0.33	0.32	0.32	1.874e+05	170.00	0.37	0.25	0.08	0.06	32,38,29
3216	0.52	0.50	0.32	2.940e+05	170.00	0.37	0.28	0.09	0.06	32,38,29
3217	0.33	0.32	0.32	1.874e+05	170.00	0.37	0.25	0.08	0.06	32,38,29

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
				1.874e+05	170.00	0.37			
	0.52	0.50	0.52	2.940e+05	170.00	0.60	0.28	0.09	0.06

Setto	Mat.	Spessore	Stato
		cm	
245	muratura (consolidata) E = 1.536e+05	40.0	ok L

Nodo	P / A daN/cm2	P / A daN/cm2	P / A .3 daN/cm2	Mu daN cm	b (h/l)	tc cm	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
3205	0.11	0.11	0.11	6.279e+04	170.00	0.06	0.13	0.02	0.06	32,33,29
3206	0.11	0.11	0.11	6.279e+04	170.00	0.06	0.13	0.02	0.06	32,33,29
3208	0.11	0.11	0.11	6.279e+04	170.00	0.06	0.13	0.02	0.06	32,33,29
3209	0.11	0.11	0.11	6.279e+04	170.00	0.06	0.13	0.02	0.06	32,33,29
3211	0.11	0.11	0.11	6.279e+04	170.00	0.06	0.13	0.02	0.06	32,33,29
3212	0.11	0.11	0.11	6.279e+04	170.00	0.06	0.13	0.02	0.06	32,33,29
3214	0.11	0.11	0.11	6.279e+04	170.00	0.06	0.13	0.02	0.06	32,33,29
3215	0.11	0.11	0.11	6.279e+04	170.00	0.06	0.13	0.02	0.06	32,33,29
3217	0.11	0.11	0.11	6.279e+04	170.00	0.06	0.13	0.02	0.06	32,33,29
3218	0.11	0.11	0.11	6.279e+04	170.00	0.06	0.13	0.02	0.06	32,33,29

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3
	0.11	0.11	0.11	6.279e+04	170.00	0.06			
				6.279e+04	170.00	0.06	0.13	0.02	0.06

Setto	Mat.	Spessore	Stato
		cm	
248	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
2004	0.56	0.56	0.58	3.168e+05	170.00	0.67	0.28	0.08	0.10	27,32,19
2013	0.56	0.56	0.58	3.168e+05	170.00	0.67	0.28	0.08	0.10	27,32,19
2022	0.56	0.56	0.58	3.168e+05	170.00	0.67	0.28	0.08	0.10	27,32,19
2031	0.56	0.56	0.58	3.168e+05	170.00	0.67	0.28	0.08	0.10	27,32,19
2040	0.56	0.56	0.58	3.168e+05	170.00	0.67	0.28	0.08	0.10	27,32,19
3222	0.56	0.56	0.36	3.168e+05	170.00	0.41	0.28	0.08	0.11	27,32,19
3223	0.34	0.35	0.36	1.958e+05	170.00	0.41	0.26	0.08	0.11	27,32,19
3225	0.56	0.56	0.36	3.168e+05	170.00	0.41	0.28	0.08	0.11	27,32,19
3226	0.34	0.35	0.36	1.958e+05	170.00	0.41	0.26	0.08	0.11	27,32,19
3228	0.56	0.56	0.36	3.168e+05	170.00	0.41	0.28	0.08	0.11	27,32,19
3229	0.34	0.35	0.36	1.958e+05	170.00	0.41	0.26	0.08	0.11	27,32,19
3231	0.56	0.56	0.36	3.168e+05	170.00	0.41	0.28	0.08	0.11	27,32,19
3232	0.34	0.35	0.36	1.958e+05	170.00	0.41	0.26	0.08	0.11	27,32,19
3234	0.56	0.56	0.36	3.168e+05	170.00	0.41	0.28	0.08	0.11	27,32,19
3235	0.34	0.35	0.36	1.958e+05	170.00	0.41	0.26	0.08	0.11	27,32,19
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				1.958e+05	170.00	0.41				
	0.56	0.56	0.58	3.168e+05	170.00	0.67	0.28	0.08	0.11	

Setto	Mat.	Spessore	Stato
		cm	
249	muratura (consolidata) E = 1.536e+05	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
3223	0.10	0.10	0.10	5.976e+04	170.00	0.05	0.16	0.02	0.10	27,32,14
3224	0.10	0.10	0.10	5.976e+04	170.00	0.05	0.16	0.02	0.10	27,32,14
3226	0.10	0.10	0.10	5.976e+04	170.00	0.05	0.16	0.02	0.10	27,32,14
3227	0.10	0.10	0.10	5.976e+04	170.00	0.05	0.16	0.02	0.10	27,32,14
3229	0.10	0.10	0.10	5.976e+04	170.00	0.05	0.16	0.02	0.10	27,32,14
3230	0.10	0.10	0.10	5.976e+04	170.00	0.05	0.16	0.02	0.10	27,32,14
3232	0.10	0.10	0.10	5.976e+04	170.00	0.05	0.16	0.02	0.10	27,32,14
3233	0.10	0.10	0.10	5.976e+04	170.00	0.05	0.16	0.02	0.10	27,32,14
3235	0.10	0.10	0.10	5.976e+04	170.00	0.05	0.16	0.02	0.10	27,32,14
3236	0.10	0.10	0.10	5.976e+04	170.00	0.05	0.16	0.02	0.10	27,32,14
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				5.976e+04	170.00	0.05				
	0.10	0.10	0.10	5.976e+04	170.00	0.05	0.16	0.02	0.10	

Setto	Mat.	Spessore	Stato
		cm	
254	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	Rif. cmb
	daN/cm2	daN/cm2	daN/cm2	daN cm		cm				
3088	0.24	0.24	0.24	1.363e+06	536.00	0.27	0.03	9.70e-03	0.22	42,38,20
3091	0.24	0.24	0.24	1.363e+06	536.00	0.27	0.03	9.70e-03	0.22	42,38,20
3094	0.24	0.24	0.24	1.363e+06	536.00	0.27	0.03	9.70e-03	0.22	42,38,20
3097	0.24	0.24	0.24	1.363e+06	536.00	0.27	0.03	9.70e-03	0.22	42,38,20

3100	0.24	0.24	0.24	1.363e+06	536.00	0.27	0.03	9.70e-03	0.22	42,38,20
3103	0.24	0.24	0.24	1.363e+06	536.00	0.27	0.03	9.70e-03	0.22	42,38,20
3106	0.24	0.24	0.24	1.363e+06	536.00	0.27	0.03	9.70e-03	0.22	42,38,20
3109	0.24	0.24	0.24	1.363e+06	536.00	0.27	0.03	9.70e-03	0.22	42,38,20
3112	0.24	0.24	0.24	1.363e+06	536.00	0.27	0.03	9.70e-03	0.22	42,38,20
3115	0.24	0.24	0.24	1.363e+06	536.00	0.27	0.03	9.70e-03	0.22	42,38,20
3118	0.24	0.24	0.24	1.363e+06	536.00	0.27	0.03	9.70e-03	0.22	42,38,20
3121	0.24	0.24	0.24	1.363e+06	536.00	0.27	0.03	9.70e-03	0.22	42,38,20
3251	0.24	0.24	0.24	1.363e+06	536.00	0.27	0.03	9.70e-03	0.22	42,38,20
3252	0.21	0.21	0.20	1.175e+06	536.00	0.24	0.03	6.97e-03	0.17	42,38,20
3253	0.14	0.14	0.14	7.882e+05	536.00	0.16	0.03	3.99e-03	0.08	38,41,20
3254	0.07	0.07	0.07	3.955e+05	536.00	0.08	0.02	2.84e-03	0.03	26,33,20
3255	0.24	0.24	0.24	1.363e+06	536.00	0.27	0.03	9.70e-03	0.22	42,38,20
3256	0.21	0.21	0.20	1.175e+06	536.00	0.24	0.03	6.97e-03	0.17	42,38,20
3257	0.14	0.14	0.14	7.882e+05	536.00	0.16	0.03	3.99e-03	0.08	38,41,20
3258	0.07	0.07	0.07	3.955e+05	536.00	0.08	0.02	2.84e-03	0.03	26,33,20
3259	0.24	0.24	0.24	1.363e+06	536.00	0.27	0.03	9.70e-03	0.22	42,38,20
3260	0.21	0.21	0.20	1.175e+06	536.00	0.24	0.03	6.97e-03	0.17	42,38,20
3261	0.14	0.14	0.14	7.882e+05	536.00	0.16	0.03	3.99e-03	0.08	38,41,20
3262	0.07	0.07	0.07	3.955e+05	536.00	0.08	0.02	2.84e-03	0.03	26,33,20
3263	0.24	0.24	0.24	1.363e+06	536.00	0.27	0.03	9.70e-03	0.22	42,38,20
3264	0.21	0.21	0.20	1.175e+06	536.00	0.24	0.03	6.97e-03	0.17	42,38,20
3265	0.14	0.14	0.14	7.882e+05	536.00	0.16	0.03	3.99e-03	0.08	38,41,20
3266	0.07	0.07	0.07	3.955e+05	536.00	0.08	0.02	2.84e-03	0.03	26,33,20
3267	0.24	0.24	0.24	1.363e+06	536.00	0.27	0.03	9.70e-03	0.22	42,38,20
3268	0.21	0.21	0.20	1.175e+06	536.00	0.24	0.03	6.97e-03	0.17	42,38,20
3269	0.14	0.14	0.14	7.882e+05	536.00	0.16	0.03	3.99e-03	0.08	38,41,20
3270	0.07	0.07	0.07	3.955e+05	536.00	0.08	0.02	2.84e-03	0.03	26,33,20
3271	0.24	0.24	0.24	1.363e+06	536.00	0.27	0.03	9.70e-03	0.22	42,38,20
3272	0.21	0.21	0.20	1.175e+06	536.00	0.24	0.03	6.97e-03	0.17	42,38,20
3273	0.14	0.14	0.14	7.882e+05	536.00	0.16	0.03	3.99e-03	0.08	38,41,20
3274	0.07	0.07	0.07	3.955e+05	536.00	0.08	0.02	2.84e-03	0.03	26,33,20
3276	0.24	0.24	0.24	1.363e+06	536.00	0.27	0.03	9.70e-03	0.22	42,38,20
3277	0.21	0.21	0.20	1.175e+06	536.00	0.24	0.03	6.97e-03	0.17	42,38,20
3278	0.14	0.14	0.14	7.882e+05	536.00	0.16	0.03	3.99e-03	0.08	38,41,20
3279	0.07	0.07	0.07	3.955e+05	536.00	0.08	0.02	2.84e-03	0.03	26,33,20
3280	0.24	0.24	0.24	1.363e+06	536.00	0.27	0.03	9.70e-03	0.22	42,38,20
3281	0.21	0.21	0.20	1.175e+06	536.00	0.24	0.03	6.97e-03	0.17	42,38,20
3282	0.14	0.14	0.14	7.882e+05	536.00	0.16	0.03	3.99e-03	0.08	38,41,20
3283	0.07	0.07	0.07	3.955e+05	536.00	0.08	0.02	2.84e-03	0.03	26,33,20
3284	0.24	0.24	0.24	1.363e+06	536.00	0.27	0.03	9.70e-03	0.22	42,38,20
3285	0.21	0.21	0.20	1.175e+06	536.00	0.24	0.03	6.97e-03	0.17	42,38,20
3286	0.14	0.14	0.14	7.882e+05	536.00	0.16	0.03	3.99e-03	0.08	38,41,20
3287	0.07	0.07	0.07	3.955e+05	536.00	0.08	0.02	2.84e-03	0.03	26,33,20
3288	0.24	0.24	0.24	1.363e+06	536.00	0.27	0.03	9.70e-03	0.22	42,38,20
3289	0.21	0.21	0.20	1.175e+06	536.00	0.24	0.03	6.97e-03	0.17	42,38,20
3290	0.14	0.14	0.14	7.882e+05	536.00	0.16	0.03	3.99e-03	0.08	38,41,20
3291	0.07	0.07	0.07	3.955e+05	536.00	0.08	0.02	2.84e-03	0.03	26,33,20
3292	0.24	0.24	0.24	1.363e+06	536.00	0.27	0.03	9.70e-03	0.22	42,38,20
3293	0.21	0.21	0.20	1.175e+06	536.00	0.24	0.03	6.97e-03	0.17	42,38,20
3294	0.14	0.14	0.14	7.882e+05	536.00	0.16	0.03	3.99e-03	0.08	38,41,20
3295	0.07	0.07	0.07	3.955e+05	536.00	0.08	0.02	2.84e-03	0.03	26,33,20
3296	0.24	0.24	0.24	1.363e+06	536.00	0.27	0.03	9.70e-03	0.22	42,38,20
3297	0.21	0.21	0.20	1.175e+06	536.00	0.24	0.03	6.97e-03	0.17	42,38,20
3298	0.14	0.14	0.14	7.882e+05	536.00	0.16	0.03	3.99e-03	0.08	38,41,20
3299	0.07	0.07	0.07	3.955e+05	536.00	0.08	0.02	2.84e-03	0.03	26,33,20
Nodo	P / A	P / A	P / A .3	Mu	b (h/l)	tc	V. 8.2.2.1	V.11.5.8.1	V. 8.2.2.3	
				3.955e+05	536.00	0.08				
	0.24	0.24	0.24	1.363e+06	536.00	0.27	0.03	9.70e-03	0.22	

Fascia	Mat.	Spessore	Stato
		cm	
25	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
685	0.319.606e+042.625e+04			0.08	5.956e+06	11,11	1707	0.311.191e+052.625e+04			0.07	5.956e+06	11,11
1708	0.341.191e+052.625e+04			0.07	5.956e+06	11,11	1709	0.319.606e+042.625e+04			0.08	5.956e+06	11,11
1716	0.311.191e+052.625e+04			0.07	5.956e+06	11,11	1717	0.341.191e+052.625e+04			0.07	5.956e+06	11,11
1718	0.319.606e+042.625e+04			0.08	5.956e+06	11,11	1722	0.311.191e+052.625e+04			0.07	5.956e+06	11,11
1723	0.341.191e+052.625e+04			0.07	5.956e+06	11,11							

Nodo **Ver. V** **Ver. M**
 0.34 0.08

Fascia	Mat.	Spessore	Stato
		cm	
26	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
432	0.181.191e+052.625e+04			0.04	5.956e+06	11,11	452	0.181.191e+052.625e+04			0.04	5.956e+06	11,11
693	0.201.191e+052.625e+04			0.04	5.956e+06	11,11	694	0.191.191e+052.625e+04			0.04	5.956e+06	11,11
695	0.201.191e+052.625e+04			0.05	5.956e+06	11,11	696	0.231.191e+052.625e+04			0.05	5.956e+06	11,11
1701	0.201.191e+052.625e+04			0.04	5.956e+06	11,11	1702	0.191.191e+052.625e+04			0.04	5.956e+06	11,11
1703	0.201.191e+052.625e+04			0.05	5.956e+06	11,11	1704	0.231.191e+052.625e+04			0.05	5.956e+06	11,11
1705	0.261.191e+052.625e+04			0.06	5.956e+06	11,11	1706	0.281.191e+052.625e+04			0.06	5.956e+06	11,11
1707	0.311.191e+052.625e+04			0.07	5.956e+06	11,11	1710	0.201.191e+052.625e+04			0.04	5.956e+06	11,11
1711	0.191.191e+052.625e+04			0.04	5.956e+06	11,11	1712	0.201.191e+052.625e+04			0.05	5.956e+06	11,11
1713	0.231.191e+052.625e+04			0.05	5.956e+06	11,11	1714	0.261.191e+052.625e+04			0.06	5.956e+06	11,11
1715	0.281.191e+052.625e+04			0.06	5.956e+06	11,11	1716	0.311.191e+052.625e+04			0.07	5.956e+06	11,11
1719	0.261.191e+052.625e+04			0.06	5.956e+06	11,11	1720	0.181.191e+052.625e+04			0.04	5.956e+06	11,11
1721	0.281.191e+052.625e+04			0.06	5.956e+06	11,11	1722	0.311.191e+052.625e+04			0.07	5.956e+06	11,11

Nodo **Ver. V** **Ver. M**
 0.31 0.07

Fascia	Mat.	Spessore	Stato
		cm	
30	mattoni pieni e malta di calce	25.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
22	0.103.541e+04 6937.50			0.02	2.903e+06	20,20	23	0.103.541e+04 6937.50			0.02	2.903e+06	20,20
715	0.123.541e+04 6937.50			0.02	2.903e+06	20,20	716	0.093.541e+04 6937.50			0.02	2.903e+06	20,20
724	0.123.541e+04 6937.50			0.02	2.903e+06	20,20	725	0.103.541e+04 6937.50			0.02	2.903e+06	20,20
726	0.093.541e+04 6937.50			0.02	2.903e+06	20,20	734	0.123.541e+04 6937.50			0.02	2.903e+06	20,20
735	0.103.541e+04 6937.50			0.02	2.903e+06	20,20	736	0.093.541e+04 6937.50			0.02	2.903e+06	20,20
744	0.123.541e+04 6937.50			0.02	2.903e+06	20,20	745	0.093.541e+04 6937.50			0.02	2.903e+06	20,20

Nodo **Ver. V** **Ver. M**
 0.12 0.02

Fascia	Mat.	Spessore	Stato
		cm	
33	mattoni pieni e malta di calce	42.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
721	0.115.948e+041.166e+04			0.02	4.878e+06	21,21	722	0.135.948e+041.166e+04			0.03	4.878e+06	21,21
731	0.115.948e+041.166e+04			0.02	4.878e+06	21,21	732	0.135.948e+041.166e+04			0.03	4.878e+06	21,21
741	0.115.948e+041.166e+04			0.02	4.878e+06	21,21	742	0.135.948e+041.166e+04			0.03	4.878e+06	21,21
750	0.115.948e+041.166e+04			0.02	4.878e+06	21,21	751	0.135.948e+041.166e+04			0.03	4.878e+06	21,21

Nodo **Ver. V** **Ver. M**
 0.13 0.03

Fascia	Mat.	Spessore	Stato
		cm	
34	mattoni pieni e malta di calce	42.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
757	0.188.130e+041.166e+04			0.03	4.878e+06	23,23	758	0.278.130e+041.166e+04			0.04	4.878e+06	23,23
759	0.308.130e+041.166e+04			0.04	4.878e+06	23,23	767	0.188.130e+041.166e+04			0.03	4.878e+06	23,23
768	0.278.130e+041.166e+04			0.04	4.878e+06	23,23	769	0.308.130e+041.166e+04			0.04	4.878e+06	23,23
776	0.188.130e+041.166e+04			0.03	4.878e+06	23,23	777	0.278.130e+041.166e+04			0.04	4.878e+06	23,23
778	0.308.130e+041.166e+04			0.04	4.878e+06	23,23							
Nodo	Ver. V			Ver. M									
	0.30			0.04									

Fascia	Mat.	Spessore	Stato
		cm	
35	mattoni pieni e malta di calce	42.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
759	0.308.130e+041.166e+04			0.04	4.878e+06	23,23	760	0.218.130e+041.166e+04			0.03	4.878e+06	23,23
769	0.308.130e+041.166e+04			0.04	4.878e+06	23,23	770	0.218.130e+041.166e+04			0.03	4.878e+06	23,23
778	0.308.130e+041.166e+04			0.04	4.878e+06	23,23	779	0.218.130e+041.166e+04			0.03	4.878e+06	23,23
Nodo	Ver. V			Ver. M									
	0.30			0.04									

Fascia	Mat.	Spessore	Stato
		cm	
38	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2093	0.159.606e+042.625e+04			0.04	5.956e+06	32,32	2094	0.271.191e+052.625e+04			0.06	5.956e+06	32,32
2102	0.159.606e+042.625e+04			0.04	5.956e+06	32,32	2103	0.271.191e+052.625e+04			0.06	5.956e+06	32,32
2111	0.159.606e+042.625e+04			0.04	5.956e+06	32,32	2112	0.271.191e+052.625e+04			0.06	5.956e+06	32,32
Nodo	Ver. V			Ver. M									
	0.27			0.06									

Fascia	Mat.	Spessore	Stato
		cm	
42	muratura E = 1.024e+05	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
866	0.101.415e+053.150e+04			0.02	8.934e+06	37,37	868	0.151.415e+053.150e+04			0.03	8.934e+06	37,37
885	0.101.415e+053.150e+04			0.02	8.934e+06	37,37	886	0.101.415e+053.150e+04			0.02	8.934e+06	37,37
887	0.151.415e+053.150e+04			0.03	8.934e+06	37,37	888	0.151.415e+053.150e+04			0.03	8.934e+06	37,37
899	0.101.415e+053.150e+04			0.02	8.934e+06	37,37	900	0.151.415e+053.150e+04			0.03	8.934e+06	37,37
Nodo	Ver. V			Ver. M									
	0.15			0.03									

Fascia	Mat.	Spessore	Stato
		cm	
43	muratura E = 1.024e+05	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
868	0.151.415e+053.150e+04			0.03	8.934e+06	37,37	870	0.161.415e+053.150e+04			0.04	8.934e+06	37,37
872	0.121.415e+053.150e+04			0.03	8.934e+06	37,37	887	0.151.415e+053.150e+04			0.03	8.934e+06	37,37
888	0.151.415e+053.150e+04			0.03	8.934e+06	37,37	889	0.161.415e+053.150e+04			0.04	8.934e+06	37,37
890	0.161.415e+053.150e+04			0.04	8.934e+06	37,37	891	0.121.415e+053.150e+04			0.03	8.934e+06	37,37
892	0.121.415e+053.150e+04			0.03	8.934e+06	37,37	900	0.151.415e+053.150e+04			0.03	8.934e+06	37,37
901	0.161.415e+053.150e+04			0.04	8.934e+06	37,37	902	0.121.415e+053.150e+04			0.03	8.934e+06	37,37
Nodo	Ver. V 0.16			Ver. M 0.04									

Fascia	Mat.	Spessore	Stato
		cm	
47	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
932	0.161.161e+051.665e+04			0.02	6.968e+06	20,20	933	0.261.161e+051.665e+04			0.04	6.968e+06	20,20
1036	0.161.161e+051.665e+04			0.02	6.968e+06	20,20	1037	0.261.161e+051.665e+04			0.04	6.968e+06	20,20
1045	0.161.161e+051.665e+04			0.02	6.968e+06	20,20	1046	0.261.161e+051.665e+04			0.04	6.968e+06	20,20
Nodo	Ver. V 0.26			Ver. M 0.04									

Fascia	Mat.	Spessore	Stato
		cm	
48	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
933	0.251.161e+051.665e+04			0.04	6.968e+06	20,20	934	0.311.161e+051.665e+04			0.04	6.968e+06	20,20
935	0.331.161e+051.665e+04			0.05	6.968e+06	20,20	1037	0.251.161e+051.665e+04			0.04	6.968e+06	20,20
1038	0.311.161e+051.665e+04			0.04	6.968e+06	20,20	1039	0.331.161e+051.665e+04			0.05	6.968e+06	20,20
1040	0.311.161e+051.665e+04			0.04	6.968e+06	20,20	1041	0.331.161e+051.665e+04			0.05	6.968e+06	20,20
1046	0.251.161e+051.665e+04			0.04	6.968e+06	20,20							
Nodo	Ver. V 0.33			Ver. M 0.05									

Fascia	Mat.	Spessore	Stato
		cm	
50	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
17	0.063.097e+051.665e+043.08e-03				6.968e+06	26,26	18	0.063.097e+051.665e+043.08e-03				6.968e+06	26,26
926	0.053.097e+051.665e+042.88e-03				6.968e+06	26,26	927	0.295.642e+041.665e+04	0.09			6.968e+06	26,26
936	0.053.097e+051.665e+042.88e-03				6.968e+06	26,26	937	0.295.642e+041.665e+04		0.09		6.968e+06	26,26
940	0.063.097e+051.665e+043.08e-03				6.968e+06	26,26	941	0.063.097e+051.665e+043.07e-03				6.968e+06	26,26
942	0.063.097e+051.665e+043.06e-03				6.968e+06	26,26	943	0.063.097e+051.665e+042.96e-03				6.968e+06	26,26
944	0.053.097e+051.665e+042.95e-03				6.968e+06	26,26	945	0.053.097e+051.665e+042.88e-03				6.968e+06	26,26
946	0.295.642e+041.665e+04			0.09	6.968e+06	26,26	949	0.063.097e+051.665e+043.08e-03				6.968e+06	26,26
950	0.063.097e+051.665e+043.07e-03				6.968e+06	26,26	951	0.063.097e+051.665e+043.06e-03				6.968e+06	26,26
952	0.063.097e+051.665e+042.96e-03				6.968e+06	26,26	953	0.053.097e+051.665e+042.95e-03				6.968e+06	26,26
954	0.053.097e+051.665e+042.88e-03				6.968e+06	26,26	955	0.295.642e+041.665e+04	0.09			6.968e+06	26,26

963	0.053.097e+051.665e+042.88e-03	6.968e+06	26,26	964	0.295.642e+041.665e+04	0.09	6.968e+06	26,26
972	0.053.097e+051.665e+042.88e-03	6.968e+06	26,26	973	0.295.642e+041.665e+04	0.09	6.968e+06	26,26

Nodo	Ver. V	Ver. M
	0.29	0.09

Fascia	Mat.	Spessore	Stato
		cm	
51	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
927	0.315.642e+041.665e+04			0.09	6.968e+06	26,26	928	0.404.523e+041.665e+04			0.15	6.968e+06	26,26
929	0.315.642e+041.665e+04			0.09	6.968e+06	26,26	937	0.315.642e+041.665e+04			0.09	6.968e+06	26,26
938	0.404.523e+041.665e+04			0.15	6.968e+06	26,26	939	0.315.642e+041.665e+04			0.09	6.968e+06	26,26
946	0.315.642e+041.665e+04			0.09	6.968e+06	26,26	947	0.404.523e+041.665e+04			0.15	6.968e+06	26,26
948	0.315.642e+041.665e+04			0.09	6.968e+06	26,26	955	0.315.642e+041.665e+04			0.09	6.968e+06	26,26
956	0.404.523e+041.665e+04			0.15	6.968e+06	26,26	957	0.315.642e+041.665e+04			0.09	6.968e+06	26,26
964	0.315.642e+041.665e+04			0.09	6.968e+06	26,26	965	0.404.523e+041.665e+04			0.15	6.968e+06	26,26
966	0.315.642e+041.665e+04			0.09	6.968e+06	26,26	973	0.315.642e+041.665e+04			0.09	6.968e+06	26,26
974	0.404.523e+041.665e+04			0.15	6.968e+06	26,26	975	0.315.642e+041.665e+04			0.09	6.968e+06	26,26
2405	0.315.642e+041.665e+04			0.09	6.968e+06	26,26							

Nodo	Ver. V	Ver. M
	0.40	0.15

Fascia	Mat.	Spessore	Stato
		cm	
56	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
564	0.118.565e+041.665e+04			0.02	6.968e+06	24,24	571	0.118.565e+041.665e+04			0.02	6.968e+06	24,24
578	0.118.565e+041.665e+04			0.02	6.968e+06	24,24	585	0.118.565e+041.665e+04			0.02	6.968e+06	24,24
985	0.208.909e+041.665e+04			0.04	6.968e+06	24,24	986	0.228.909e+041.665e+04			0.04	6.968e+06	24,24
987	0.258.909e+041.665e+04			0.05	6.968e+06	24,24	988	0.268.909e+041.665e+04			0.05	6.968e+06	20,20
989	0.248.909e+041.665e+04			0.05	6.968e+06	24,24	990	0.208.909e+041.665e+04			0.04	6.968e+06	24,24
991	0.148.909e+041.665e+04			0.03	6.968e+06	20,20	994	0.208.909e+041.665e+04			0.04	6.968e+06	24,24
995	0.228.909e+041.665e+04			0.04	6.968e+06	24,24	996	0.258.909e+041.665e+04			0.05	6.968e+06	24,24
997	0.268.909e+041.665e+04			0.05	6.968e+06	20,20	998	0.248.909e+041.665e+04			0.05	6.968e+06	24,24
999	0.208.909e+041.665e+04			0.04	6.968e+06	24,24	1000	0.148.909e+041.665e+04			0.03	6.968e+06	20,20
1003	0.208.909e+041.665e+04			0.04	6.968e+06	24,24	1004	0.228.909e+041.665e+04			0.04	6.968e+06	24,24
1005	0.258.909e+041.665e+04			0.05	6.968e+06	24,24	1006	0.268.909e+041.665e+04			0.05	6.968e+06	20,20
1007	0.248.909e+041.665e+04			0.05	6.968e+06	24,24	1008	0.208.909e+041.665e+04			0.04	6.968e+06	24,24
1009	0.148.909e+041.665e+04			0.03	6.968e+06	20,20	1012	0.208.909e+041.665e+04			0.04	6.968e+06	24,24
1013	0.228.909e+041.665e+04			0.04	6.968e+06	24,24	1014	0.258.909e+041.665e+04			0.05	6.968e+06	24,24
1015	0.268.909e+041.665e+04			0.05	6.968e+06	20,20	1016	0.248.909e+041.665e+04			0.05	6.968e+06	24,24
1017	0.208.909e+041.665e+04			0.04	6.968e+06	24,24	1018	0.148.909e+041.665e+04			0.03	6.968e+06	20,20

Nodo	Ver. V	Ver. M
	0.26	0.05

Fascia	Mat.	Spessore	Stato
		cm	
57	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
991	0.118.909e+041.665e+04			0.02	6.968e+06	20,20	992	0.118.909e+041.665e+04			0.02	6.968e+06	20,20
993	0.141.083e+051.665e+04			0.02	6.968e+06	20,20	1000	0.118.909e+041.665e+04			0.02	6.968e+06	20,20
1001	0.118.909e+041.665e+04			0.02	6.968e+06	20,20	1002	0.141.083e+051.665e+04			0.02	6.968e+06	20,20

1009	0.118.909e+041.665e+04	0.02	6.968e+06	20,20	1010	0.118.909e+041.665e+04	0.02	6.968e+06	20,20
1011	0.141.083e+051.665e+04	0.02	6.968e+06	20,20	1018	0.118.909e+041.665e+04	0.02	6.968e+06	20,20
1019	0.118.909e+041.665e+04	0.02	6.968e+06	20,20	1020	0.141.083e+051.665e+04	0.02	6.968e+06	20,20

Nodo **Ver. V** **Ver. M**
 0.14 0.02

Fascia	Mat.	Spessore	Stato
		cm	
60	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
929	0.349.409e+041.665e+04			0.06	6.968e+06	21,21	939	0.349.409e+041.665e+04			0.06	6.968e+06	21,21
966	0.349.409e+041.665e+04			0.06	6.968e+06	21,21	975	0.349.409e+041.665e+04			0.06	6.968e+06	21,21
2368	0.349.409e+041.665e+04			0.06	6.968e+06	21,21	2369	0.349.409e+041.665e+04			0.06	6.968e+06	26,26
2370	0.339.409e+041.665e+04			0.06	6.968e+06	26,26	2371	0.349.409e+041.665e+04			0.06	6.968e+06	26,26
2372	0.439.409e+041.665e+04			0.08	6.968e+06	26,26	2373	0.335.642e+041.665e+04			0.10	6.968e+06	26,26
2374	0.345.642e+041.665e+04			0.10	6.968e+06	26,26	2375	0.345.642e+041.665e+04			0.10	6.968e+06	26,26
2377	0.349.409e+041.665e+04			0.06	6.968e+06	21,21	2378	0.349.409e+041.665e+04			0.06	6.968e+06	26,26
2379	0.339.409e+041.665e+04			0.06	6.968e+06	26,26	2380	0.349.409e+041.665e+04			0.06	6.968e+06	26,26
2381	0.439.409e+041.665e+04			0.08	6.968e+06	26,26	2382	0.335.642e+041.665e+04			0.10	6.968e+06	26,26
2383	0.345.642e+041.665e+04			0.10	6.968e+06	26,26	2384	0.345.642e+041.665e+04			0.10	6.968e+06	26,26
2390	0.439.409e+041.665e+04			0.08	6.968e+06	26,26	2391	0.335.642e+041.665e+04			0.10	6.968e+06	26,26
2392	0.345.642e+041.665e+04			0.10	6.968e+06	26,26	2393	0.345.642e+041.665e+04			0.10	6.968e+06	26,26
2399	0.439.409e+041.665e+04			0.08	6.968e+06	26,26	2400	0.335.642e+041.665e+04			0.10	6.968e+06	26,26
2401	0.345.642e+041.665e+04			0.10	6.968e+06	26,26	2402	0.345.642e+041.665e+04			0.10	6.968e+06	26,26
2405	0.349.409e+041.665e+04			0.06	6.968e+06	21,21	2409	0.439.409e+041.665e+04			0.08	6.968e+06	26,26
2410	0.335.642e+041.665e+04			0.10	6.968e+06	26,26	2411	0.345.642e+041.665e+04			0.10	6.968e+06	26,26
2412	0.345.642e+041.665e+04			0.10	6.968e+06	26,26	2414	0.349.409e+041.665e+04			0.06	6.968e+06	21,21
2415	0.349.409e+041.665e+04			0.06	6.968e+06	26,26	2416	0.339.409e+041.665e+04			0.06	6.968e+06	26,26
2417	0.349.409e+041.665e+04			0.06	6.968e+06	26,26	2418	0.439.409e+041.665e+04			0.08	6.968e+06	26,26
2419	0.335.642e+041.665e+04			0.10	6.968e+06	26,26	2420	0.345.642e+041.665e+04			0.10	6.968e+06	26,26
2421	0.345.642e+041.665e+04			0.10	6.968e+06	26,26	2431	0.349.409e+041.665e+04			0.06	6.968e+06	21,21
2432	0.349.409e+041.665e+04			0.06	6.968e+06	21,21	2433	0.349.409e+041.665e+04			0.06	6.968e+06	26,26
2434	0.349.409e+041.665e+04			0.06	6.968e+06	26,26	2435	0.339.409e+041.665e+04			0.06	6.968e+06	26,26
2436	0.339.409e+041.665e+04			0.06	6.968e+06	26,26	2437	0.349.409e+041.665e+04			0.06	6.968e+06	26,26
2438	0.349.409e+041.665e+04			0.06	6.968e+06	26,26	2439	0.439.409e+041.665e+04			0.08	6.968e+06	26,26
2440	0.335.642e+041.665e+04			0.10	6.968e+06	26,26	2441	0.345.642e+041.665e+04			0.10	6.968e+06	26,26
2442	0.345.642e+041.665e+04			0.10	6.968e+06	26,26							

Nodo **Ver. V** **Ver. M**
 0.43 0.10

Fascia	Mat.	Spessore	Stato
		cm	
67	muratura E = 1.024e+05	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
1112	0.161.489e+053.150e+04			0.03	8.934e+06	23,23	1114	0.261.489e+053.150e+04			0.05	8.934e+06	23,23
1116	0.251.489e+053.150e+04			0.05	8.934e+06	23,23	1125	0.161.489e+053.150e+04			0.03	8.934e+06	23,23
1126	0.261.489e+053.150e+04			0.05	8.934e+06	23,23	1127	0.251.489e+053.150e+04			0.05	8.934e+06	23,23
1134	0.161.489e+053.150e+04			0.03	8.934e+06	23,23	1135	0.261.489e+053.150e+04			0.05	8.934e+06	23,23
1136	0.251.489e+053.150e+04			0.05	8.934e+06	23,23	1143	0.161.489e+053.150e+04			0.03	8.934e+06	23,23
1144	0.261.489e+053.150e+04			0.05	8.934e+06	23,23	1145	0.251.489e+053.150e+04			0.05	8.934e+06	23,23

Nodo **Ver. V** **Ver. M**
 0.26 0.05

Fascia	Mat.	Spessore	Stato
		cm	
68	muratura E = 1.024e+05	40.0	ok L

Fascia	Mat.	Spessore	Stato
		cm	
71	muratura E = 1.024e+05	40.0	ok L

Fascia	Mat.	Spessore	Stato
		cm	
72	muratura E = 1.024e+05	40.0	ok L

Fascia	Mat.	Spessore	Stato
		cm	
78	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	Ver. V	Ver. M
	0.20	0.06

Fascia	Mat.	Spessore	Stato
		cm	
79	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
1399	0.178.272e+042.625e+04			0.05	5.956e+06	17,17	1400	0.228.272e+042.625e+04			0.07	5.956e+06	16,16
1401	0.248.272e+042.625e+04			0.08	5.956e+06	16,16	1402	0.168.272e+042.625e+04			0.05	5.956e+06	16,16
1408	0.178.272e+042.625e+04			0.05	5.956e+06	17,17	1409	0.228.272e+042.625e+04			0.07	5.956e+06	16,16
1410	0.248.272e+042.625e+04			0.08	5.956e+06	16,16	1411	0.168.272e+042.625e+04			0.05	5.956e+06	16,16
1417	0.178.272e+042.625e+04			0.05	5.956e+06	17,17	1418	0.228.272e+042.625e+04			0.07	5.956e+06	16,16
1419	0.248.272e+042.625e+04			0.08	5.956e+06	16,16	1420	0.168.272e+042.625e+04			0.05	5.956e+06	16,16
1426	0.178.272e+042.625e+04			0.05	5.956e+06	17,17	1427	0.228.272e+042.625e+04			0.07	5.956e+06	16,16
1428	0.248.272e+042.625e+04			0.08	5.956e+06	16,16	1429	0.168.272e+042.625e+04			0.05	5.956e+06	16,16

Nodo	Ver. V	Ver. M
	0.24	0.08

Fascia	Mat.	Spessore	Stato
		cm	
84	mattoni pieni e malta di calce	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
5	0.275.498e+041.110e+04			0.05	4.645e+06	17,17	6	0.275.498e+041.110e+04			0.05	4.645e+06	17,17
358	0.275.498e+041.110e+04			0.05	4.645e+06	17,17	379	0.275.498e+041.110e+04			0.05	4.645e+06	17,17
1448	0.235.498e+041.110e+04			0.05	4.645e+06	17,17	1449	0.195.498e+041.110e+04			0.04	4.645e+06	17,17
1457	0.235.498e+041.110e+04			0.05	4.645e+06	17,17	1458	0.195.498e+041.110e+04			0.04	4.645e+06	17,17
1466	0.235.498e+041.110e+04			0.05	4.645e+06	17,17	1467	0.275.498e+041.110e+04			0.05	4.645e+06	17,17
1468	0.195.498e+041.110e+04			0.04	4.645e+06	17,17	1476	0.235.498e+041.110e+04			0.05	4.645e+06	17,17
1477	0.275.498e+041.110e+04			0.05	4.645e+06	17,17	1478	0.195.498e+041.110e+04			0.04	4.645e+06	17,17
1486	0.235.498e+041.110e+04			0.05	4.645e+06	17,17	1487	0.195.498e+041.110e+04			0.04	4.645e+06	17,17
1495	0.235.498e+041.110e+04			0.05	4.645e+06	17,17	1496	0.195.498e+041.110e+04			0.04	4.645e+06	17,17

Nodo	Ver. V	Ver. M
	0.27	0.05

Fascia	Mat.	Spessore	Stato
		cm	
87	mattoni pieni e malta di calce	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
1455	0.375.498e+041.110e+04			0.08	4.645e+06	17,17	1456	0.785.498e+041.110e+04			0.16	4.645e+06	17,17
1464	0.375.498e+041.110e+04			0.08	4.645e+06	17,17	1465	0.785.498e+041.110e+04			0.16	4.645e+06	17,17
1474	0.375.498e+041.110e+04			0.08	4.645e+06	17,17	1475	0.785.498e+041.110e+04			0.16	4.645e+06	17,17
1484	0.375.498e+041.110e+04			0.08	4.645e+06	17,17	1485	0.785.498e+041.110e+04			0.16	4.645e+06	17,17
1493	0.375.498e+041.110e+04			0.08	4.645e+06	17,17	1494	0.785.498e+041.110e+04			0.16	4.645e+06	17,17
1502	0.375.498e+041.110e+04			0.08	4.645e+06	17,17	1503	0.785.498e+041.110e+04			0.16	4.645e+06	17,17

Nodo	Ver. V	Ver. M
	0.78	0.16

Fascia	Mat.	Spessore	Stato
		cm	
88	mattoni pieni e malta di calce	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
1151	0.045.498e+041.110e+047.61e-03			4.645e+06	17,17		1520	0.035.498e+041.110e+045.62e-03			4.645e+06	17,17	
1521	0.045.498e+041.110e+047.61e-03			4.645e+06	17,17		1529	0.035.498e+041.110e+045.62e-03			4.645e+06	17,17	
1530	0.045.498e+041.110e+047.61e-03			4.645e+06	17,17		1539	0.035.498e+041.110e+045.62e-03			4.645e+06	17,17	
1540	0.045.498e+041.110e+047.61e-03			4.645e+06	17,17		1549	0.035.498e+041.110e+045.62e-03			4.645e+06	17,17	
1550	0.045.498e+041.110e+047.61e-03			4.645e+06	17,17		1558	0.035.498e+041.110e+045.62e-03			4.645e+06	17,17	
1559	0.045.498e+041.110e+047.61e-03			4.645e+06	17,17		1567	0.035.498e+041.110e+045.62e-03			4.645e+06	17,17	

Nodo	Ver. V	Ver. M
	0.04	7.61e-03

Fascia	Mat.	Spessore	Stato
		cm	
90	mattoni pieni e malta di calce	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
1459	0.615.498e+041.110e+04			0.12	4.645e+06	11,11	1462	0.325.498e+041.110e+04			0.06	4.645e+06	11,11
1463	0.615.498e+041.110e+04			0.12	4.645e+06	11,11	1482	0.325.498e+041.110e+04			0.06	4.645e+06	11,11
1483	0.615.498e+041.110e+04			0.12	4.645e+06	11,11	1527	0.325.498e+041.110e+04			0.06	4.645e+06	11,11
1528	0.615.498e+041.110e+04			0.12	4.645e+06	11,11	1546	0.325.498e+041.110e+04			0.06	4.645e+06	11,11
1547	0.615.498e+041.110e+04			0.12	4.645e+06	11,11	1585	0.325.498e+041.110e+04			0.06	4.645e+06	11,11
1586	0.615.498e+041.110e+04			0.12	4.645e+06	11,11	1590	0.325.498e+041.110e+04			0.06	4.645e+06	11,11

Nodo	Ver. V	Ver. M
	0.61	0.12

Fascia	Mat.	Spessore	Stato
		cm	
91	mattoni pieni e malta di calce	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
9	0.315.498e+041.110e+04			0.06	4.645e+06	11,11	10	0.315.498e+041.110e+04			0.06	4.645e+06	11,11
12	0.315.498e+041.110e+04			0.06	4.645e+06	11,11	414	0.315.498e+041.110e+04			0.06	4.645e+06	11,11
1469	0.275.498e+041.110e+04			0.05	4.645e+06	11,11	1470	0.315.498e+041.110e+04			0.06	4.645e+06	11,11
1471	0.215.498e+041.110e+04			0.04	4.645e+06	11,11	1488	0.275.498e+041.110e+04			0.05	4.645e+06	11,11
1489	0.315.498e+041.110e+04			0.06	4.645e+06	11,11	1490	0.215.498e+041.110e+04			0.04	4.645e+06	11,11
1534	0.275.498e+041.110e+04			0.05	4.645e+06	11,11	1535	0.215.498e+041.110e+04			0.04	4.645e+06	11,11
1548	0.275.498e+041.110e+04			0.05	4.645e+06	11,11	1553	0.215.498e+041.110e+04			0.04	4.645e+06	11,11
1578	0.275.498e+041.110e+04			0.05	4.645e+06	11,11	1579	0.215.498e+041.110e+04			0.04	4.645e+06	11,11
1587	0.275.498e+041.110e+04			0.05	4.645e+06	11,11	1588	0.215.498e+041.110e+04			0.04	4.645e+06	11,11

Nodo	Ver. V	Ver. M
	0.31	0.06

Fascia	Mat.	Spessore	Stato
		cm	
94	mattoni pieni e malta di calce	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
7	0.055.498e+041.110e+04			0.01	4.645e+06	14,14	8	0.055.498e+041.110e+04			0.01	4.645e+06	14,14
386	0.055.498e+041.110e+04			0.01	4.645e+06	14,14	407	0.055.498e+041.110e+04			0.01	4.645e+06	14,14
1513	0.115.498e+041.110e+04			0.02	4.645e+06	14,14	1514	0.065.498e+041.110e+04			0.01	4.645e+06	14,14
1522	0.115.498e+041.110e+04			0.02	4.645e+06	14,14	1523	0.065.498e+041.110e+04			0.01	4.645e+06	14,14
1531	0.115.498e+041.110e+04			0.02	4.645e+06	14,14	1532	0.055.498e+041.110e+04			0.01	4.645e+06	14,14
1533	0.065.498e+041.110e+04			0.01	4.645e+06	14,14	1541	0.115.498e+041.110e+04			0.02	4.645e+06	14,14
1542	0.055.498e+041.110e+04			0.01	4.645e+06	14,14	1543	0.065.498e+041.110e+04			0.01	4.645e+06	14,14
1551	0.115.498e+041.110e+04			0.02	4.645e+06	14,14	1552	0.065.498e+041.110e+04			0.01	4.645e+06	14,14

1560 0.115.498e+041.110e+04 0.02 4.645e+06 14,14 1561 0.065.498e+041.110e+04 0.01 4.645e+06 14,14

Nodo **Ver. V** **Ver. M**
 0.11 0.02

Fascia	Mat.	Spessore	Stato
		cm	
97	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
515	0.191.191e+052.625e+04			0.04	5.956e+06	30,30	533	0.191.191e+052.625e+04			0.04	5.956e+06	30,30
1591	0.231.191e+052.625e+04			0.05	5.956e+06	30,30	1592	0.221.191e+052.625e+04			0.05	5.956e+06	30,30
1593	0.251.191e+052.625e+04			0.05	5.956e+06	30,30	1594	0.271.191e+052.625e+04			0.06	5.956e+06	30,30
1595	0.301.191e+052.625e+04			0.07	5.956e+06	30,30	1596	0.331.191e+052.625e+04			0.07	5.956e+06	30,30
1597	0.361.191e+052.625e+04			0.08	5.956e+06	30,30	1600	0.231.191e+052.625e+04			0.05	5.956e+06	30,30
1601	0.191.191e+052.625e+04			0.04	5.956e+06	30,30	1602	0.221.191e+052.625e+04			0.05	5.956e+06	30,30
1603	0.251.191e+052.625e+04			0.05	5.956e+06	30,30	1604	0.271.191e+052.625e+04			0.06	5.956e+06	30,30
1605	0.301.191e+052.625e+04			0.07	5.956e+06	30,30	1606	0.331.191e+052.625e+04			0.07	5.956e+06	30,30
1607	0.361.191e+052.625e+04			0.08	5.956e+06	30,30	1610	0.231.191e+052.625e+04			0.05	5.956e+06	30,30
1611	0.221.191e+052.625e+04			0.05	5.956e+06	30,30	1612	0.251.191e+052.625e+04			0.05	5.956e+06	30,30
1613	0.271.191e+052.625e+04			0.06	5.956e+06	30,30	1614	0.301.191e+052.625e+04			0.07	5.956e+06	30,30
1615	0.331.191e+052.625e+04			0.07	5.956e+06	30,30	1616	0.361.191e+052.625e+04			0.08	5.956e+06	30,30

Nodo **Ver. V** **Ver. M**
 0.36 0.08

Fascia	Mat.	Spessore	Stato
		cm	
98	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
1597	0.361.191e+052.625e+04			0.08	5.956e+06	30,30	1598	0.381.191e+052.625e+04			0.08	5.956e+06	30,30
1599	0.359.606e+042.625e+04			0.10	5.956e+06	32,32	1607	0.361.191e+052.625e+04			0.08	5.956e+06	30,30
1608	0.381.191e+052.625e+04			0.08	5.956e+06	30,30	1609	0.359.606e+042.625e+04			0.10	5.956e+06	32,32
1616	0.361.191e+052.625e+04			0.08	5.956e+06	30,30	1617	0.381.191e+052.625e+04			0.08	5.956e+06	30,30
1618	0.359.606e+042.625e+04			0.10	5.956e+06	32,32							

Nodo **Ver. V** **Ver. M**
 0.38 0.10

Fascia	Mat.	Spessore	Stato
		cm	
101	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
473	0.121.191e+052.625e+04			0.03	5.956e+06	30,30	487	0.121.191e+052.625e+04			0.03	5.956e+06	30,30
1646	0.121.191e+052.625e+04			0.03	5.956e+06	30,30	1647	0.111.191e+052.625e+04			0.03	5.956e+06	30,30
1648	0.101.191e+052.625e+04			0.02	5.956e+06	30,30	1649	0.101.191e+052.625e+04			0.02	5.956e+06	30,30
1650	0.091.191e+052.625e+04			0.02	5.956e+06	30,30	1651	0.081.191e+052.625e+04			0.02	5.956e+06	30,30
1652	0.071.191e+052.625e+04			0.02	5.956e+06	27,27	1655	0.121.191e+052.625e+04			0.03	5.956e+06	30,30
1656	0.121.191e+052.625e+04			0.03	5.956e+06	30,30	1657	0.111.191e+052.625e+04			0.03	5.956e+06	30,30
1658	0.101.191e+052.625e+04			0.02	5.956e+06	30,30	1659	0.101.191e+052.625e+04			0.02	5.956e+06	30,30
1660	0.091.191e+052.625e+04			0.02	5.956e+06	30,30	1661	0.081.191e+052.625e+04			0.02	5.956e+06	30,30
1662	0.071.191e+052.625e+04			0.02	5.956e+06	27,27	1665	0.121.191e+052.625e+04			0.03	5.956e+06	30,30
1666	0.111.191e+052.625e+04			0.03	5.956e+06	30,30	1667	0.101.191e+052.625e+04			0.02	5.956e+06	30,30
1668	0.101.191e+052.625e+04			0.02	5.956e+06	30,30	1669	0.091.191e+052.625e+04			0.02	5.956e+06	30,30
1670	0.081.191e+052.625e+04			0.02	5.956e+06	30,30	1671	0.071.191e+052.625e+04			0.02	5.956e+06	27,27

Nodo **Ver. V** **Ver. M**
 0.12 0.03

Fascia	Mat.	Spessore	Stato
		cm	
102	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
1652	0.071.191e+052.625e+04			0.02	5.956e+06	27,27	1653	0.091.191e+052.625e+04			0.02	5.956e+06	27,27
1654	0.079.606e+042.625e+04			0.02	5.956e+06	27,27	1662	0.071.191e+052.625e+04			0.02	5.956e+06	27,27
1663	0.091.191e+052.625e+04			0.02	5.956e+06	27,27	1664	0.079.606e+042.625e+04			0.02	5.956e+06	27,27
1671	0.071.191e+052.625e+04			0.02	5.956e+06	27,27	1672	0.091.191e+052.625e+04			0.02	5.956e+06	27,27
1673	0.079.606e+042.625e+04			0.02	5.956e+06	27,27							

Nodo **Ver. V** **Ver. M**
 0.09 0.02

Fascia	Mat.	Spessore	Stato
		cm	
109	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
1743	0.548.246e+041.665e+04			0.11	6.968e+06	17,17	1744	0.405.239e+051.665e+04			0.01	6.968e+06	16,16
1745	0.045.239e+051.665e+041.14e-03				6.968e+06	11,11	1746	0.055.239e+051.665e+041.71e-03				6.968e+06	17,17
1747	0.075.239e+051.665e+042.07e-03				6.968e+06	25,25	1748	0.155.239e+051.665e+044.76e-03				6.968e+06	14,14
1752	0.548.246e+041.665e+04			0.11	6.968e+06	17,17	1753	0.405.239e+051.665e+04			0.01	6.968e+06	16,16
1754	0.045.239e+051.665e+041.14e-03				6.968e+06	11,11	1755	0.055.239e+051.665e+041.71e-03				6.968e+06	17,17
1756	0.075.239e+051.665e+042.07e-03				6.968e+06	25,25	1757	0.155.239e+051.665e+044.76e-03				6.968e+06	14,14
1779	0.548.246e+041.665e+04			0.11	6.968e+06	17,17	1780	0.405.239e+051.665e+04			0.01	6.968e+06	16,16
1781	0.045.239e+051.665e+041.14e-03				6.968e+06	11,11	1782	0.055.239e+051.665e+041.71e-03				6.968e+06	17,17
1783	0.075.239e+051.665e+042.07e-03				6.968e+06	25,25	1784	0.155.239e+051.665e+044.76e-03				6.968e+06	14,14
1788	0.548.246e+041.665e+04			0.11	6.968e+06	17,17	1789	0.405.239e+051.665e+04			0.01	6.968e+06	16,16
1790	0.045.239e+051.665e+041.14e-03				6.968e+06	11,11	1791	0.055.239e+051.665e+041.71e-03				6.968e+06	17,17
1792	0.075.239e+051.665e+042.07e-03				6.968e+06	25,25	1793	0.155.239e+051.665e+044.76e-03				6.968e+06	14,14

Nodo **Ver. V** **Ver. M**
 0.54 0.11

Fascia	Mat.	Spessore	Stato
		cm	
110	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
1749	0.458.246e+041.665e+04			0.09	6.968e+06	17,17	1750	0.818.246e+041.665e+04			0.16	6.968e+06	17,17
1758	0.458.246e+041.665e+04			0.09	6.968e+06	17,17	1759	0.818.246e+041.665e+04			0.16	6.968e+06	17,17
1767	0.458.246e+041.665e+04			0.09	6.968e+06	17,17	1768	0.818.246e+041.665e+04			0.16	6.968e+06	17,17
1776	0.458.246e+041.665e+04			0.09	6.968e+06	17,17	1777	0.818.246e+041.665e+04			0.16	6.968e+06	17,17
1785	0.458.246e+041.665e+04			0.09	6.968e+06	17,17	1786	0.818.246e+041.665e+04			0.16	6.968e+06	17,17
1794	0.458.246e+041.665e+04			0.09	6.968e+06	17,17	1795	0.818.246e+041.665e+04			0.16	6.968e+06	17,17

Nodo **Ver. V** **Ver. M**
 0.81 0.16

Fascia	Mat.	Spessore	Stato
		cm	
113	mattoni pieni e malta di calce	38.0	ok L

Fascia	Mat.	Spessore	Stato
		cm	
120	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
1151	0.058.246e+041.665e+04			0.01	6.968e+06	17,17	1521	0.058.246e+041.665e+04			0.01	6.968e+06	17,17
1530	0.058.246e+041.665e+04			0.01	6.968e+06	17,17	1540	0.058.246e+041.665e+04			0.01	6.968e+06	17,17
1550	0.058.246e+041.665e+04			0.01	6.968e+06	17,17	1559	0.058.246e+041.665e+04			0.01	6.968e+06	17,17
1805	0.058.246e+041.665e+04			0.01	6.968e+06	17,17	1806	0.088.246e+041.665e+04			0.02	6.968e+06	14,14
1807	0.128.246e+041.665e+04			0.02	6.968e+06	14,14	1808	0.158.246e+041.665e+04			0.03	6.968e+06	14,14
1809	0.168.246e+041.665e+04			0.03	6.968e+06	14,14	1810	0.168.246e+041.665e+04			0.03	6.968e+06	14,14
1811	0.148.246e+041.665e+04			0.03	6.968e+06	14,14	1812	0.118.246e+041.665e+04			0.02	6.968e+06	14,14
1814	0.058.246e+041.665e+04			0.01	6.968e+06	17,17	1815	0.088.246e+041.665e+04			0.02	6.968e+06	14,14
1816	0.128.246e+041.665e+04			0.02	6.968e+06	14,14	1817	0.158.246e+041.665e+04			0.03	6.968e+06	14,14
1818	0.168.246e+041.665e+04			0.03	6.968e+06	14,14	1819	0.168.246e+041.665e+04			0.03	6.968e+06	14,14
1820	0.148.246e+041.665e+04			0.03	6.968e+06	14,14	1821	0.118.246e+041.665e+04			0.02	6.968e+06	14,14
1823	0.058.246e+041.665e+04			0.01	6.968e+06	17,17	1824	0.088.246e+041.665e+04			0.02	6.968e+06	14,14
1825	0.128.246e+041.665e+04			0.02	6.968e+06	14,14	1826	0.158.246e+041.665e+04			0.03	6.968e+06	14,14
1827	0.168.246e+041.665e+04			0.03	6.968e+06	14,14	1828	0.168.246e+041.665e+04			0.03	6.968e+06	14,14
1829	0.148.246e+041.665e+04			0.03	6.968e+06	14,14	1830	0.118.246e+041.665e+04			0.02	6.968e+06	14,14
1832	0.058.246e+041.665e+04			0.01	6.968e+06	17,17	1833	0.088.246e+041.665e+04			0.02	6.968e+06	14,14
1834	0.128.246e+041.665e+04			0.02	6.968e+06	14,14	1835	0.158.246e+041.665e+04			0.03	6.968e+06	14,14
1836	0.168.246e+041.665e+04			0.03	6.968e+06	14,14	1837	0.168.246e+041.665e+04			0.03	6.968e+06	14,14
1838	0.148.246e+041.665e+04			0.03	6.968e+06	14,14	1839	0.118.246e+041.665e+04			0.02	6.968e+06	14,14
1841	0.058.246e+041.665e+04			0.01	6.968e+06	17,17	1842	0.088.246e+041.665e+04			0.02	6.968e+06	14,14
1843	0.128.246e+041.665e+04			0.02	6.968e+06	14,14	1844	0.158.246e+041.665e+04			0.03	6.968e+06	14,14
1845	0.168.246e+041.665e+04			0.03	6.968e+06	14,14	1846	0.168.246e+041.665e+04			0.03	6.968e+06	14,14
1847	0.148.246e+041.665e+04			0.03	6.968e+06	14,14	1848	0.118.246e+041.665e+04			0.02	6.968e+06	14,14
1850	0.058.246e+041.665e+04			0.01	6.968e+06	17,17	1851	0.088.246e+041.665e+04			0.02	6.968e+06	14,14
1852	0.128.246e+041.665e+04			0.02	6.968e+06	14,14	1853	0.158.246e+041.665e+04			0.03	6.968e+06	14,14
1854	0.168.246e+041.665e+04			0.03	6.968e+06	14,14	1855	0.168.246e+041.665e+04			0.03	6.968e+06	14,14
1856	0.148.246e+041.665e+04			0.03	6.968e+06	14,14	1857	0.118.246e+041.665e+04			0.02	6.968e+06	14,14

Nodo Ver. V Ver. M
0.16 0.03

Fascia	Mat.	Spessore	Stato
		cm	
121	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
1812	0.068.246e+041.665e+04			0.01	6.968e+06	14,14	1813	0.068.246e+041.665e+04			0.01	6.968e+06	14,14
1821	0.068.246e+041.665e+04			0.01	6.968e+06	14,14	1822	0.068.246e+041.665e+04			0.01	6.968e+06	14,14
1830	0.068.246e+041.665e+04			0.01	6.968e+06	14,14	1831	0.068.246e+041.665e+04			0.01	6.968e+06	14,14
1839	0.068.246e+041.665e+04			0.01	6.968e+06	14,14	1840	0.068.246e+041.665e+04			0.01	6.968e+06	14,14
1848	0.068.246e+041.665e+04			0.01	6.968e+06	14,14	1849	0.068.246e+041.665e+04			0.01	6.968e+06	14,14
1857	0.068.246e+041.665e+04			0.01	6.968e+06	14,14	1858	0.068.246e+041.665e+04			0.01	6.968e+06	14,14

Nodo Ver. V Ver. M
0.06 0.01

Fascia	Mat.	Spessore	Stato
		cm	
124	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
1459	0.798.246e+041.665e+04			0.16	6.968e+06	11,11	1463	0.798.246e+041.665e+04			0.16	6.968e+06	11,11
1483	0.798.246e+041.665e+04			0.16	6.968e+06	11,11	1528	0.798.246e+041.665e+04			0.16	6.968e+06	11,11
1547	0.798.246e+041.665e+04			0.16	6.968e+06	11,11	1586	0.798.246e+041.665e+04			0.16	6.968e+06	11,11

1868	0.848.246e+041.665e+04	0.17	6.968e+06	11,11	1869	0.488.246e+041.665e+04	0.10	6.968e+06	11,11
1870	0.355.239e+051.665e+04	0.01	6.968e+06	14,14	1871	0.055.239e+051.665e+041.53e-03	6.968e+06	17,17	
1872	0.085.239e+051.665e+042.50e-03	6.968e+06	11,11	1873	0.085.239e+051.665e+042.62e-03	6.968e+06	11,11		
1874	0.145.239e+051.665e+044.44e-03	6.968e+06	15,15	1875	0.995.239e+051.665e+04	0.03	6.968e+06	11,11	
1877	0.848.246e+041.665e+04	0.17	6.968e+06	11,11	1878	0.488.246e+041.665e+04	0.10	6.968e+06	11,11
1879	0.355.239e+051.665e+04	0.01	6.968e+06	14,14	1880	0.055.239e+051.665e+041.53e-03	6.968e+06	17,17	
1881	0.085.239e+051.665e+042.50e-03	6.968e+06	11,11	1882	0.085.239e+051.665e+042.62e-03	6.968e+06	11,11		
1883	0.145.239e+051.665e+044.44e-03	6.968e+06	15,15	1884	0.995.239e+051.665e+04	0.03	6.968e+06	11,11	
1886	0.848.246e+041.665e+04	0.17	6.968e+06	11,11	1887	0.488.246e+041.665e+04	0.10	6.968e+06	11,11
1895	0.848.246e+041.665e+04	0.17	6.968e+06	11,11	1896	0.488.246e+041.665e+04	0.10	6.968e+06	11,11
1904	0.848.246e+041.665e+04	0.17	6.968e+06	11,11	1905	0.488.246e+041.665e+04	0.10	6.968e+06	11,11
1906	0.355.239e+051.665e+04	0.01	6.968e+06	14,14	1907	0.055.239e+051.665e+041.53e-03	6.968e+06	17,17	
1908	0.085.239e+051.665e+042.50e-03	6.968e+06	11,11	1909	0.085.239e+051.665e+042.62e-03	6.968e+06	11,11		
1910	0.145.239e+051.665e+044.44e-03	6.968e+06	15,15	1911	0.995.239e+051.665e+04	0.03	6.968e+06	11,11	
1913	0.848.246e+041.665e+04	0.17	6.968e+06	11,11	1914	0.488.246e+041.665e+04	0.10	6.968e+06	11,11
1915	0.355.239e+051.665e+04	0.01	6.968e+06	14,14	1916	0.055.239e+051.665e+041.53e-03	6.968e+06	17,17	
1917	0.085.239e+051.665e+042.50e-03	6.968e+06	11,11	1918	0.085.239e+051.665e+042.62e-03	6.968e+06	11,11		
1919	0.145.239e+051.665e+044.44e-03	6.968e+06	15,15	1920	0.995.239e+051.665e+04	0.03	6.968e+06	11,11	

Nodo **Ver. V** **Ver. M**
 0.99 0.17

Fascia	Mat.	Spessore	Stato
		cm	
125	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
1875	0.398.246e+041.665e+04			0.08	6.968e+06	11,11	1876	0.668.246e+041.665e+04			0.13	6.968e+06	11,11
1884	0.398.246e+041.665e+04			0.08	6.968e+06	11,11	1885	0.668.246e+041.665e+04			0.13	6.968e+06	11,11
1893	0.398.246e+041.665e+04			0.08	6.968e+06	11,11	1894	0.668.246e+041.665e+04			0.13	6.968e+06	11,11
1902	0.398.246e+041.665e+04			0.08	6.968e+06	11,11	1903	0.668.246e+041.665e+04			0.13	6.968e+06	11,11
1911	0.398.246e+041.665e+04			0.08	6.968e+06	11,11	1912	0.668.246e+041.665e+04			0.13	6.968e+06	11,11
1920	0.398.246e+041.665e+04			0.08	6.968e+06	11,11	1921	0.668.246e+041.665e+04			0.13	6.968e+06	11,11

Nodo **Ver. V** **Ver. M**
 0.66 0.13

Fascia	Mat.	Spessore	Stato
		cm	
126	mattoni pieni e malta di calce	38.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
1892	0.141.038e+051.055e+04			0.01	4.413e+06	32,32	1989	0.091.038e+051.055e+048.77e-03			4.413e+06	32,32	
2124	0.141.038e+051.055e+04			0.01	4.413e+06	32,32	2125	0.091.038e+051.055e+048.77e-03			4.413e+06	32,32	
2135	0.141.038e+051.055e+04			0.01	4.413e+06	32,32	2136	0.091.038e+051.055e+048.77e-03			4.413e+06	32,32	

Nodo **Ver. V** **Ver. M**
 0.14 0.01

Fascia	Mat.	Spessore	Stato
		cm	
127	mattoni pieni e malta di calce	25.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
1901	0.124.893e+04	6937.50		0.02	2.903e+06	37,37	1990	0.084.893e+04	6937.50		0.01	2.903e+06	37,37
2043	0.134.893e+04	6937.50		0.02	2.903e+06	37,37	2044	0.124.893e+04	6937.50		0.02	2.903e+06	37,37
2122	0.084.893e+04	6937.50		0.01	2.903e+06	37,37	2143	0.134.893e+04	6937.50		0.02	2.903e+06	37,37
2158	0.124.893e+04	6937.50		0.02	2.903e+06	37,37	2160	0.134.893e+04	6937.50		0.02	2.903e+06	37,37

2193	0.084.893e+04	6937.50	0.01	2.903e+06	37,37	2201	0.084.893e+04	6937.50	0.01	2.903e+06	37,37
2202	0.124.893e+04	6937.50	0.02	2.903e+06	37,37	2210	0.134.893e+04	6937.50	0.02	2.903e+06	37,37

Nodo	Ver. V	Ver. M
	0.13	0.02

Fascia	Mat.	Spessore	Stato
		cm	
130	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
685	0.259.606e+04	2.625e+04	0.07	5.956e+06	27,27		1709	0.259.606e+04	2.625e+04	0.07	5.956e+06	27,27	
1718	0.259.606e+04	2.625e+04	0.07	5.956e+06	27,27		1978	0.239.606e+04	2.625e+04	0.06	5.956e+06	27,27	
1979	0.149.606e+04	2.625e+04	0.04	5.956e+06	27,27		1987	0.239.606e+04	2.625e+04	0.06	5.956e+06	27,27	
1988	0.149.606e+04	2.625e+04	0.04	5.956e+06	27,27		1996	0.239.606e+04	2.625e+04	0.06	5.956e+06	27,27	
1997	0.149.606e+04	2.625e+04	0.04	5.956e+06	27,27								

Nodo	Ver. V	Ver. M
	0.25	0.07

Fascia	Mat.	Spessore	Stato
		cm	
131	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
1985	0.169.606e+04	2.625e+04	0.04	5.956e+06	15,15		1986	0.311.191e+05	2.625e+04	0.07	5.956e+06	15,15	
1994	0.169.606e+04	2.625e+04	0.04	5.956e+06	15,15		1995	0.311.191e+05	2.625e+04	0.07	5.956e+06	15,15	
2003	0.169.606e+04	2.625e+04	0.04	5.956e+06	15,15		2004	0.311.191e+05	2.625e+04	0.07	5.956e+06	15,15	

Nodo	Ver. V	Ver. M
	0.31	0.07

Fascia	Mat.	Spessore	Stato
		cm	
135	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
1654	0.079.606e+04	2.625e+04	0.02	5.956e+06	27,27		1664	0.079.606e+04	2.625e+04	0.02	5.956e+06	27,27	
1673	0.079.606e+04	2.625e+04	0.02	5.956e+06	27,27		2032	0.079.606e+04	2.625e+04	0.02	5.956e+06	27,27	
2033	0.059.606e+04	2.625e+04	0.01	5.956e+06	27,27		2041	0.079.606e+04	2.625e+04	0.02	5.956e+06	27,27	
2042	0.059.606e+04	2.625e+04	0.01	5.956e+06	27,27		2050	0.079.606e+04	2.625e+04	0.02	5.956e+06	27,27	
2051	0.059.606e+04	2.625e+04	0.01	5.956e+06	27,27								

Nodo	Ver. V	Ver. M
	0.07	0.02

Fascia	Mat.	Spessore	Stato
		cm	
138	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	

2039	0.049.606e+042.625e+04	0.01	5.956e+06	30,30	2040	0.061.191e+052.625e+04	0.01	5.956e+06	30,30
2048	0.049.606e+042.625e+04	0.01	5.956e+06	30,30	2049	0.061.191e+052.625e+04	0.01	5.956e+06	30,30
2057	0.049.606e+042.625e+04	0.01	5.956e+06	30,30	2058	0.061.191e+052.625e+04	0.01	5.956e+06	30,30

Nodo **Ver. V** **Ver. M**
 0.06 0.01

Fascia	Mat.	Spessore	Stato
		cm	
141	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
1599	0.349.606e+042.625e+04			0.09	5.956e+06	32,32	1609	0.349.606e+042.625e+04			0.09	5.956e+06	32,32
1618	0.349.606e+042.625e+04			0.09	5.956e+06	32,32	2086	0.329.606e+042.625e+04			0.09	5.956e+06	32,32
2087	0.199.606e+042.625e+04			0.05	5.956e+06	32,32	2095	0.329.606e+042.625e+04			0.09	5.956e+06	32,32
2096	0.199.606e+042.625e+04			0.05	5.956e+06	32,32	2104	0.329.606e+042.625e+04			0.09	5.956e+06	32,32
2105	0.199.606e+042.625e+04			0.05	5.956e+06	32,32							

Nodo **Ver. V** **Ver. M**
 0.34 0.09

Fascia	Mat.	Spessore	Stato
		cm	
144	mattoni pieni e malta di calce	25.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
2153	0.236.832e+04 6937.50			0.02	2.903e+06	39,39	2154	0.236.832e+04 6937.50			0.02	2.903e+06	39,39
2175	0.266.832e+04 6937.50			0.03	2.903e+06	39,39	2176	0.296.832e+04 6937.50			0.03	2.903e+06	39,39
2184	0.266.832e+04 6937.50			0.03	2.903e+06	39,39	2185	0.236.832e+04 6937.50			0.02	2.903e+06	39,39
2186	0.296.832e+04 6937.50			0.03	2.903e+06	39,39	2194	0.266.832e+04 6937.50			0.03	2.903e+06	39,39
2195	0.296.832e+04 6937.50			0.03	2.903e+06	39,39							

Nodo **Ver. V** **Ver. M**
 0.29 0.03

Fascia	Mat.	Spessore	Stato
		cm	
145	mattoni pieni e malta di calce	38.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
2190	0.212.077e+051.055e+04			0.01	4.413e+06	39,39	2191	0.202.077e+051.055e+04			0.01	4.413e+06	39,39
2199	0.212.077e+051.055e+04			0.01	4.413e+06	39,39	2200	0.202.077e+051.055e+04			0.01	4.413e+06	39,39

Nodo **Ver. V** **Ver. M**
 0.21 0.01

Fascia	Mat.	Spessore	Stato
		cm	
148	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	

2295	0.091.133e+051.665e+04	0.01	6.968e+06	11,11	2304	0.091.133e+051.665e+04	0.01	6.968e+06	11,11
2313	0.091.133e+051.665e+04	0.01	6.968e+06	11,11	3323	0.051.133e+051.665e+047.66e-03	6.968e+06	11,11	
3325	0.041.133e+051.665e+045.40e-03	6.968e+06	11,11	3327	0.051.133e+051.665e+047.66e-03	6.968e+06	11,11		
3328	0.041.133e+051.665e+045.40e-03	6.968e+06	11,11	3330	0.051.133e+051.665e+047.66e-03	6.968e+06	11,11		
3331	0.041.133e+051.665e+045.40e-03	6.968e+06	11,11						

Nodo **Ver. V** **Ver. M**
 0.09 0.01

Fascia	Mat.	Spessore	Stato
		cm	
149	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
3325	0.031.133e+051.665e+043.99e-03			6.968e+06	27,27		3326	0.021.133e+051.665e+042.86e-03			6.968e+06	27,27	
3328	0.031.133e+051.665e+043.99e-03			6.968e+06	27,27		3329	0.021.133e+051.665e+042.86e-03			6.968e+06	27,27	
3331	0.031.133e+051.665e+043.99e-03			6.968e+06	27,27		3332	0.021.133e+051.665e+042.86e-03			6.968e+06	27,27	

Nodo **Ver. V** **Ver. M**
 0.03 3.99e-03

Fascia	Mat.	Spessore	Stato
		cm	
152	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2254	0.131.394e+051.665e+04			0.02	6.968e+06	21,21	2255	0.081.394e+051.665e+049.41e-03			6.968e+06	21,21	
2259	0.131.394e+051.665e+04			0.02	6.968e+06	21,21	2260	0.081.394e+051.665e+049.41e-03			6.968e+06	21,21	
2262	0.131.394e+051.665e+04			0.02	6.968e+06	21,21	2263	0.081.394e+051.665e+049.41e-03			6.968e+06	21,21	
2268	0.131.394e+051.665e+04			0.02	6.968e+06	21,21	2331	0.231.394e+051.665e+04	0.03		6.968e+06	21,21	
2340	0.231.394e+051.665e+04			0.03	6.968e+06	21,21	2349	0.231.394e+051.665e+04	0.03		6.968e+06	21,21	
2398	0.231.394e+051.665e+04			0.03	6.968e+06	21,21	3322	0.081.394e+051.665e+049.41e-03			6.968e+06	21,21	

Nodo **Ver. V** **Ver. M**
 0.23 0.03

Fascia	Mat.	Spessore	Stato
		cm	
153	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2255	0.121.394e+051.665e+04			0.01	6.968e+06	26,26	2256	0.141.394e+051.665e+04			0.02	6.968e+06	26,26
2260	0.121.394e+051.665e+04			0.01	6.968e+06	26,26	2261	0.141.394e+051.665e+04			0.02	6.968e+06	26,26
2263	0.121.394e+051.665e+04			0.01	6.968e+06	26,26	2265	0.141.394e+051.665e+04			0.02	6.968e+06	26,26
3275	0.141.394e+051.665e+04			0.02	6.968e+06	26,26	3322	0.121.394e+051.665e+04			0.01	6.968e+06	26,26

Nodo **Ver. V** **Ver. M**
 0.14 0.02

Fascia	Mat.	Spessore	Stato
		cm	
158	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
935	0.391.161e+051.665e+04			0.06	6.968e+06	20,20	1039	0.391.161e+051.665e+04			0.06	6.968e+06	20,20
1041	0.391.161e+051.665e+04			0.06	6.968e+06	20,20	2287	0.411.161e+051.665e+04			0.06	6.968e+06	20,20
2288	0.411.161e+051.665e+04			0.06	6.968e+06	20,20	2289	0.401.161e+051.665e+04			0.06	6.968e+06	20,20
2290	0.381.161e+051.665e+04			0.05	6.968e+06	20,20	2291	0.351.161e+051.665e+04			0.05	6.968e+06	20,20
2292	0.331.161e+051.665e+04			0.05	6.968e+06	20,20	2293	0.311.161e+051.665e+04			0.04	6.968e+06	20,20
2294	0.281.161e+051.665e+04			0.04	6.968e+06	20,20	2296	0.411.161e+051.665e+04			0.06	6.968e+06	20,20
2297	0.411.161e+051.665e+04			0.06	6.968e+06	20,20	2298	0.401.161e+051.665e+04			0.06	6.968e+06	20,20
2299	0.381.161e+051.665e+04			0.05	6.968e+06	20,20	2300	0.351.161e+051.665e+04			0.05	6.968e+06	20,20
2301	0.331.161e+051.665e+04			0.05	6.968e+06	20,20	2302	0.311.161e+051.665e+04			0.04	6.968e+06	20,20
2303	0.281.161e+051.665e+04			0.04	6.968e+06	20,20	2305	0.411.161e+051.665e+04			0.06	6.968e+06	20,20
2306	0.411.161e+051.665e+04			0.06	6.968e+06	20,20	2307	0.401.161e+051.665e+04			0.06	6.968e+06	20,20
2308	0.381.161e+051.665e+04			0.05	6.968e+06	20,20	2309	0.351.161e+051.665e+04			0.05	6.968e+06	20,20
2310	0.331.161e+051.665e+04			0.05	6.968e+06	20,20	2311	0.311.161e+051.665e+04			0.04	6.968e+06	20,20
2312	0.281.161e+051.665e+04			0.04	6.968e+06	20,20							

Nodo Ver. V Ver. M
0.41 0.06

Fascia	Mat.	Spessore	Stato
		cm	
159	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2294	0.271.161e+051.665e+04			0.04	6.968e+06	12,12	2295	0.221.133e+051.665e+04			0.03	6.968e+06	12,12
2303	0.271.161e+051.665e+04			0.04	6.968e+06	12,12	2304	0.221.133e+051.665e+04			0.03	6.968e+06	12,12
2312	0.271.161e+051.665e+04			0.04	6.968e+06	12,12	2313	0.221.133e+051.665e+04			0.03	6.968e+06	12,12

Nodo Ver. V Ver. M
0.27 0.04

Fascia	Mat.	Spessore	Stato
		cm	
162	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2375	0.355.642e+041.665e+04			0.10	6.968e+06	26,26	2376	0.315.642e+041.665e+04			0.09	6.968e+06	26,26
2384	0.355.642e+041.665e+04			0.10	6.968e+06	26,26	2385	0.315.642e+041.665e+04			0.09	6.968e+06	26,26
2393	0.355.642e+041.665e+04			0.10	6.968e+06	26,26	2394	0.315.642e+041.665e+04			0.09	6.968e+06	26,26
2402	0.355.642e+041.665e+04			0.10	6.968e+06	26,26	2403	0.315.642e+041.665e+04			0.09	6.968e+06	26,26
2412	0.355.642e+041.665e+04			0.10	6.968e+06	26,26	2413	0.315.642e+041.665e+04			0.09	6.968e+06	26,26
2421	0.355.642e+041.665e+04			0.10	6.968e+06	26,26	2422	0.315.642e+041.665e+04			0.09	6.968e+06	26,26
2442	0.355.642e+041.665e+04			0.10	6.968e+06	26,26	2443	0.315.642e+041.665e+04			0.09	6.968e+06	26,26

Nodo Ver. V Ver. M
0.35 0.10

Fascia	Mat.	Spessore	Stato
		cm	
164	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2327	0.121.394e+051.665e+04			0.01	6.968e+06	20,20	2328	0.181.394e+051.665e+04			0.02	6.968e+06	20,20
2329	0.181.394e+051.665e+04			0.02	6.968e+06	20,20	2330	0.161.394e+051.665e+04			0.02	6.968e+06	20,20
2336	0.121.394e+051.665e+04			0.01	6.968e+06	20,20	2337	0.181.394e+051.665e+04			0.02	6.968e+06	20,20
2338	0.181.394e+051.665e+04			0.02	6.968e+06	20,20	2339	0.161.394e+051.665e+04			0.02	6.968e+06	20,20
2345	0.121.394e+051.665e+04			0.01	6.968e+06	20,20	2346	0.181.394e+051.665e+04			0.02	6.968e+06	20,20

2347	0.181.394e+051.665e+04	0.02	6.968e+06	20,20	2348	0.161.394e+051.665e+04	0.02	6.968e+06	20,20
2389	0.181.394e+051.665e+04	0.02	6.968e+06	20,20	2395	0.121.394e+051.665e+04	0.01	6.968e+06	20,20
2396	0.181.394e+051.665e+04	0.02	6.968e+06	20,20	2397	0.161.394e+051.665e+04	0.02	6.968e+06	20,20

Nodo **Ver. V** **Ver. M**
 0.18 0.02

Fascia	Mat.	Spessore	Stato
		cm	
165	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
2330	0.151.394e+051.665e+04			0.02	6.968e+06	23,23	2331	0.151.394e+051.665e+04			0.02	6.968e+06	23,23
2339	0.151.394e+051.665e+04			0.02	6.968e+06	23,23	2340	0.151.394e+051.665e+04			0.02	6.968e+06	23,23
2348	0.151.394e+051.665e+04			0.02	6.968e+06	23,23	2349	0.151.394e+051.665e+04			0.02	6.968e+06	23,23
2397	0.151.394e+051.665e+04			0.02	6.968e+06	23,23	2398	0.151.394e+051.665e+04			0.02	6.968e+06	23,23

Nodo **Ver. V** **Ver. M**
 0.15 0.02

Fascia	Mat.	Spessore	Stato
		cm	
171	mattoni pieni e malta di calce	25.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
810	0.164.133e+04	6937.50		0.03	2.903e+06	26,26	820	0.164.133e+04	6937.50		0.03	2.903e+06	26,26
829	0.164.133e+04	6937.50		0.03	2.903e+06	26,26	2504	0.154.133e+04	6937.50		0.03	2.903e+06	26,26
2505	0.104.133e+04	6937.50		0.02	2.903e+06	26,26	2513	0.154.133e+04	6937.50		0.03	2.903e+06	26,26
2514	0.104.133e+04	6937.50		0.02	2.903e+06	26,26	2522	0.154.133e+04	6937.50		0.03	2.903e+06	26,26
2523	0.104.133e+04	6937.50		0.02	2.903e+06	26,26							

Nodo **Ver. V** **Ver. M**
 0.16 0.03

Fascia	Mat.	Spessore	Stato
		cm	
174	mattoni pieni e malta di calce	37.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
2511	0.126.117e+041.027e+04			0.02	4.297e+06	21,21	2512	0.146.117e+041.027e+04			0.02	4.297e+06	21,21
2520	0.126.117e+041.027e+04			0.02	4.297e+06	21,21	2521	0.146.117e+041.027e+04			0.02	4.297e+06	21,21
2529	0.126.117e+041.027e+04			0.02	4.297e+06	21,21	2530	0.146.117e+041.027e+04			0.02	4.297e+06	21,21

Nodo **Ver. V** **Ver. M**
 0.14 0.02

Fascia	Mat.	Spessore	Stato
		cm	
179	mattoni pieni e malta di calce	25.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	

1075	0.164.085e+04	6937.50	0.03	2.903e+06	21,21	1085	0.164.085e+04	6937.50	0.03	2.903e+06	21,21
1095	0.164.085e+04	6937.50	0.03	2.903e+06	21,21	2576	0.194.085e+04	6937.50	0.03	2.903e+06	21,21
2577	0.114.085e+04	6937.50	0.02	2.903e+06	21,21	2585	0.194.085e+04	6937.50	0.03	2.903e+06	21,21
2586	0.114.085e+04	6937.50	0.02	2.903e+06	21,21	2594	0.194.085e+04	6937.50	0.03	2.903e+06	21,21
2595	0.114.085e+04	6937.50	0.02	2.903e+06	21,21						

Nodo **Ver. V** **Ver. M**
 0.19 0.03

Fascia	Mat.	Spessore	Stato
		cm	
180	mattoni pieni e malta di calce	37.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2583	0.076.045e+04	1.027e+04		0.01	4.297e+06	21,21	2584	0.106.045e+04	1.027e+04		0.02	4.297e+06	21,21
2592	0.076.045e+04	1.027e+04		0.01	4.297e+06	21,21	2593	0.106.045e+04	1.027e+04		0.02	4.297e+06	21,21
2601	0.076.045e+04	1.027e+04		0.01	4.297e+06	21,21	2602	0.106.045e+04	1.027e+04		0.02	4.297e+06	21,21

Nodo **Ver. V** **Ver. M**
 0.10 0.02

Fascia	Mat.	Spessore	Stato
		cm	
181	muratura E = 1.024e+05	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
2631	0.212.153e+05	3.150e+04		0.03	8.934e+06	42,42	2639	0.062.153e+05	3.150e+04	8.34e-03	8.934e+06	42,42	
2981	0.212.153e+05	3.150e+04		0.03	8.934e+06	42,42	2982	0.062.153e+05	3.150e+04	8.34e-03	8.934e+06	42,42	
2988	0.212.153e+05	3.150e+04		0.03	8.934e+06	42,42	2989	0.062.153e+05	3.150e+04	8.34e-03	8.934e+06	42,42	

Nodo **Ver. V** **Ver. M**
 0.21 0.03

Fascia	Mat.	Spessore	Stato
		cm	
183	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2618	0.088.272e+04	2.625e+04		0.03	5.956e+06	14,14	2619	0.128.272e+04	2.625e+04		0.04	5.956e+06	14,14
2620	0.108.272e+04	2.625e+04		0.03	5.956e+06	14,14	2627	0.088.272e+04	2.625e+04		0.03	5.956e+06	14,14
2628	0.128.272e+04	2.625e+04		0.04	5.956e+06	14,14	2629	0.108.272e+04	2.625e+04		0.03	5.956e+06	14,14
2636	0.088.272e+04	2.625e+04		0.03	5.956e+06	14,14	2637	0.128.272e+04	2.625e+04		0.04	5.956e+06	14,14
2638	0.108.272e+04	2.625e+04		0.03	5.956e+06	14,14	2645	0.088.272e+04	2.625e+04		0.03	5.956e+06	14,14
2646	0.128.272e+04	2.625e+04		0.04	5.956e+06	14,14	2647	0.108.272e+04	2.625e+04		0.03	5.956e+06	14,14

Nodo **Ver. V** **Ver. M**
 0.12 0.04

Fascia	Mat.	Spessore	Stato
		cm	
184	muratura E = 1.024e+05	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2852	0.172.414e+053.150e+04			0.02	8.934e+06	35,35	2853	0.212.414e+053.150e+04			0.03	8.934e+06	35,35
2970	0.172.414e+053.150e+04			0.02	8.934e+06	35,35	2971	0.212.414e+053.150e+04			0.03	8.934e+06	35,35
2979	0.172.414e+053.150e+04			0.02	8.934e+06	35,35	2980	0.212.414e+053.150e+04			0.03	8.934e+06	35,35

Nodo	Ver. V	Ver. M
	0.21	0.03

Fascia	Mat.	Spessore	Stato
		cm	
185	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2623	0.038.272e+042.625e+048.05e-03			5.956e+06	14,14		2624	0.078.272e+042.625e+04			0.02	5.956e+06	11,11
2632	0.038.272e+042.625e+048.05e-03			5.956e+06	14,14		2633	0.078.272e+042.625e+04			0.02	5.956e+06	11,11
2641	0.038.272e+042.625e+048.05e-03			5.956e+06	14,14		2642	0.078.272e+042.625e+04			0.02	5.956e+06	11,11
2650	0.038.272e+042.625e+048.05e-03			5.956e+06	14,14		2651	0.078.272e+042.625e+04			0.02	5.956e+06	11,11

Nodo	Ver. V	Ver. M
	0.07	0.02

Fascia	Mat.	Spessore	Stato
		cm	
187	muratura E = 1.024e+05	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2630	0.542.153e+053.150e+04			0.08	8.934e+06	42,42	2631	0.402.153e+053.150e+04			0.06	8.934e+06	42,42
2635	0.322.153e+053.150e+04			0.05	8.934e+06	42,42	2981	0.402.153e+053.150e+04			0.06	8.934e+06	42,42
2983	0.322.153e+053.150e+04			0.05	8.934e+06	42,42	2984	0.572.153e+053.150e+04			0.08	8.934e+06	42,42
2985	0.322.153e+053.150e+04			0.05	8.934e+06	42,42	2986	0.572.153e+053.150e+04			0.08	8.934e+06	42,42
2987	0.542.153e+053.150e+04			0.08	8.934e+06	42,42	2988	0.402.153e+053.150e+04			0.06	8.934e+06	42,42
2990	0.572.153e+053.150e+04			0.08	8.934e+06	42,42	2991	0.542.153e+053.150e+04			0.08	8.934e+06	42,42

Nodo	Ver. V	Ver. M
	0.57	0.08

Fascia	Mat.	Spessore	Stato
		cm	
192	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2769	0.709.118e+041.665e+04			0.13	6.968e+06	36,36	2770	0.709.118e+041.665e+04			0.13	6.968e+06	36,36
2771	0.709.118e+041.665e+04			0.13	6.968e+06	36,36	2772	0.709.118e+041.665e+04			0.13	6.968e+06	36,36
2778	0.679.118e+041.665e+04			0.12	6.968e+06	36,36	2779	0.269.118e+041.665e+04			0.05	6.968e+06	36,36
2787	0.679.118e+041.665e+04			0.12	6.968e+06	36,36	2788	0.269.118e+041.665e+04			0.05	6.968e+06	36,36
2796	0.679.118e+041.665e+04			0.12	6.968e+06	36,36	2797	0.269.118e+041.665e+04			0.05	6.968e+06	36,36
2805	0.679.118e+041.665e+04			0.12	6.968e+06	36,36	2806	0.269.118e+041.665e+04			0.05	6.968e+06	36,36

Nodo	Ver. V	Ver. M
	0.70	0.13

Fascia	Mat.	Spessore	Stato
		cm	
193	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Fascia	Mat.	Spessore	Stato
		cm	
195	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Fascia	Mat.	Spessore	Stato
		cm	
196	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Fascia	Mat.	Spessore	Stato
		cm	
201	muratura E = 1.024e+05	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2836	0.151.489e+053.150e+04			0.03	8.934e+06	23,23
2838	0.221.489e+053.150e+04			0.05	8.934e+06	23,23
2845	0.151.489e+053.150e+04			0.03	8.934e+06	23,23
2847	0.221.489e+053.150e+04			0.05	8.934e+06	23,23
2854	0.151.489e+053.150e+04			0.03	8.934e+06	23,23
2856	0.221.489e+053.150e+04			0.05	8.934e+06	23,23
2863	0.151.489e+053.150e+04			0.03	8.934e+06	23,23
2865	0.221.489e+053.150e+04			0.05	8.934e+06	23,23

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2837	0.261.489e+053.150e+04			0.05	8.934e+06	23,23
2839	0.181.489e+053.150e+04			0.04	8.934e+06	23,23
2846	0.261.489e+053.150e+04			0.05	8.934e+06	23,23
2848	0.181.489e+053.150e+04			0.04	8.934e+06	23,23
2855	0.261.489e+053.150e+04			0.05	8.934e+06	23,23
2857	0.181.489e+053.150e+04			0.04	8.934e+06	23,23
2864	0.261.489e+053.150e+04			0.05	8.934e+06	23,23
2866	0.181.489e+053.150e+04			0.04	8.934e+06	23,23

Nodo	Ver. V	Ver. M
	0.26	0.05

Fascia	Mat.	Spessore	Stato
		cm	
202	muratura E = 1.024e+05	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
2839	0.161.489e+053.150e+04			0.03	8.934e+06	23,23	2840	0.041.489e+053.150e+048.51e-03			8.934e+06	23,23	
2848	0.161.489e+053.150e+04			0.03	8.934e+06	23,23	2849	0.041.489e+053.150e+048.51e-03			8.934e+06	23,23	
2857	0.161.489e+053.150e+04			0.03	8.934e+06	23,23	2858	0.041.489e+053.150e+048.51e-03			8.934e+06	23,23	
2866	0.161.489e+053.150e+04			0.03	8.934e+06	23,23	2867	0.041.489e+053.150e+048.51e-03			8.934e+06	23,23	

Nodo	Ver. V	Ver. M
	0.16	0.03

Fascia	Mat.	Spessore	Stato
		cm	
206	muratura E = 1.024e+05	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
1142	0.142.414e+053.150e+04			0.02	8.934e+06	36,36	1294	0.142.414e+053.150e+04			0.02	8.934e+06	36,36
1303	0.142.414e+053.150e+04			0.02	8.934e+06	36,36	2841	0.192.414e+053.150e+04			0.02	8.934e+06	36,36
2842	0.222.414e+053.150e+04			0.03	8.934e+06	36,36	2843	0.262.414e+053.150e+04			0.03	8.934e+06	36,36
2844	0.222.414e+053.150e+04			0.03	8.934e+06	36,36	2850	0.052.414e+053.150e+046.62e-03			8.934e+06	40,40	
2851	0.062.414e+053.150e+047.38e-03			8.934e+06	41,41		2852	0.132.414e+053.150e+04			0.02	8.934e+06	41,41
2886	0.182.414e+053.150e+04			0.02	8.934e+06	36,36	2963	0.182.414e+053.150e+04			0.02	8.934e+06	36,36
2964	0.192.414e+053.150e+04			0.02	8.934e+06	36,36	2965	0.222.414e+053.150e+04			0.03	8.934e+06	36,36
2966	0.262.414e+053.150e+04			0.03	8.934e+06	36,36	2967	0.222.414e+053.150e+04			0.03	8.934e+06	36,36
2968	0.052.414e+053.150e+046.62e-03			8.934e+06	40,40		2969	0.062.414e+053.150e+047.38e-03			8.934e+06	41,41	
2970	0.132.414e+053.150e+04			0.02	8.934e+06	41,41	2972	0.182.414e+053.150e+04			0.02	8.934e+06	36,36
2973	0.192.414e+053.150e+04			0.02	8.934e+06	36,36	2974	0.222.414e+053.150e+04			0.03	8.934e+06	36,36
2975	0.262.414e+053.150e+04			0.03	8.934e+06	36,36	2976	0.222.414e+053.150e+04			0.03	8.934e+06	36,36
2977	0.052.414e+053.150e+046.62e-03			8.934e+06	40,40		2978	0.062.414e+053.150e+047.38e-03			8.934e+06	41,41	
2979	0.132.414e+053.150e+04			0.02	8.934e+06	41,41							

Nodo	Ver. V	Ver. M
	0.26	0.03

Fascia	Mat.	Spessore	Stato
		cm	
210	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
1876	0.678.246e+041.665e+04			0.14	6.968e+06	11,11	1885	0.678.246e+041.665e+04			0.14	6.968e+06	11,11
1894	0.678.246e+041.665e+04			0.14	6.968e+06	11,11	1903	0.678.246e+041.665e+04			0.14	6.968e+06	11,11
1912	0.678.246e+041.665e+04			0.14	6.968e+06	11,11	1921	0.678.246e+041.665e+04			0.14	6.968e+06	11,11
3002	0.618.246e+041.665e+04			0.12	6.968e+06	11,11	3003	0.428.246e+041.665e+04			0.08	6.968e+06	11,11
3004	0.058.246e+041.665e+04			0.01	6.968e+06	11,11	3005	0.618.246e+041.665e+04			0.12	6.968e+06	11,11
3006	0.428.246e+041.665e+04			0.08	6.968e+06	11,11	3007	0.058.246e+041.665e+04			0.01	6.968e+06	11,11
3008	0.618.246e+041.665e+04			0.12	6.968e+06	11,11	3009	0.428.246e+041.665e+04			0.08	6.968e+06	11,11
3010	0.058.246e+041.665e+04			0.01	6.968e+06	11,11	3011	0.618.246e+041.665e+04			0.12	6.968e+06	11,11
3012	0.428.246e+041.665e+04			0.08	6.968e+06	11,11	3013	0.058.246e+041.665e+04			0.01	6.968e+06	11,11
3014	0.618.246e+041.665e+04			0.12	6.968e+06	11,11	3015	0.428.246e+041.665e+04			0.08	6.968e+06	11,11
3016	0.058.246e+041.665e+04			0.01	6.968e+06	11,11	3017	0.618.246e+041.665e+04			0.12	6.968e+06	11,11
3018	0.428.246e+041.665e+04			0.08	6.968e+06	11,11	3019	0.058.246e+041.665e+04			0.01	6.968e+06	11,11

Nodo	Ver. V	Ver. M
	0.67	0.14

Fascia	Mat.	Spessore	Stato
		cm	
212	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
1750	0.878.246e+041.665e+04			0.18	6.968e+06	17,17	1759	0.878.246e+041.665e+04			0.18	6.968e+06	17,17
1768	0.878.246e+041.665e+04			0.18	6.968e+06	17,17	1777	0.878.246e+041.665e+04			0.18	6.968e+06	17,17
1786	0.878.246e+041.665e+04			0.18	6.968e+06	17,17	1795	0.878.246e+041.665e+04			0.18	6.968e+06	17,17
3044	0.818.246e+041.665e+04			0.16	6.968e+06	17,17	3045	0.578.246e+041.665e+04			0.12	6.968e+06	17,17
3046	0.078.246e+041.665e+04			0.01	6.968e+06	17,17	3047	0.818.246e+041.665e+04			0.16	6.968e+06	17,17
3048	0.578.246e+041.665e+04			0.12	6.968e+06	17,17	3049	0.078.246e+041.665e+04			0.01	6.968e+06	17,17
3050	0.818.246e+041.665e+04			0.16	6.968e+06	17,17	3051	0.578.246e+041.665e+04			0.12	6.968e+06	17,17
3052	0.078.246e+041.665e+04			0.01	6.968e+06	17,17	3053	0.818.246e+041.665e+04			0.16	6.968e+06	17,17
3054	0.578.246e+041.665e+04			0.12	6.968e+06	17,17	3055	0.078.246e+041.665e+04			0.01	6.968e+06	17,17
3056	0.818.246e+041.665e+04			0.16	6.968e+06	17,17	3057	0.578.246e+041.665e+04			0.12	6.968e+06	17,17
3058	0.078.246e+041.665e+04			0.01	6.968e+06	17,17	3059	0.818.246e+041.665e+04			0.16	6.968e+06	17,17
3060	0.578.246e+041.665e+04			0.12	6.968e+06	17,17	3061	0.078.246e+041.665e+04			0.01	6.968e+06	17,17
Nodo	Ver. V 0.87			Ver. M 0.18									

Fascia	Mat.	Spessore	Stato
		cm	
215	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2624	0.138.272e+042.625e+04			0.04	5.956e+06	15,15	2633	0.138.272e+042.625e+04			0.04	5.956e+06	15,15
2642	0.138.272e+042.625e+04			0.04	5.956e+06	15,15	2651	0.138.272e+042.625e+04			0.04	5.956e+06	15,15
3071	0.158.272e+042.625e+04			0.05	5.956e+06	15,15	3072	0.138.272e+042.625e+04			0.04	5.956e+06	15,15
3074	0.158.272e+042.625e+04			0.05	5.956e+06	15,15	3075	0.138.272e+042.625e+04			0.04	5.956e+06	15,15
3077	0.158.272e+042.625e+04			0.05	5.956e+06	15,15	3078	0.138.272e+042.625e+04			0.04	5.956e+06	15,15
3080	0.158.272e+042.625e+04			0.05	5.956e+06	15,15	3081	0.138.272e+042.625e+04			0.04	5.956e+06	15,15
Nodo	Ver. V 0.15			Ver. M 0.05									

Fascia	Mat.	Spessore	Stato
		cm	
216	muratura (consolidata) E = 1.536e+05	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
3072	0.071.861e+054.725e+04			0.02	1.340e+07	15,15	3073	0.031.861e+054.725e+047.14e-03			1.340e+07	15,15	
3075	0.071.861e+054.725e+04			0.02	1.340e+07	15,15	3076	0.031.861e+054.725e+047.14e-03			1.340e+07	15,15	
3078	0.071.861e+054.725e+04			0.02	1.340e+07	15,15	3079	0.031.861e+054.725e+047.14e-03			1.340e+07	15,15	
3081	0.071.861e+054.725e+04			0.02	1.340e+07	15,15	3082	0.031.861e+054.725e+047.14e-03			1.340e+07	15,15	
Nodo	Ver. V			Ver. M									
	0.07			0.02									

Fascia	Mat.	Spessore	Stato
		cm	
222	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
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	daN	daN		daN cm			daN	daN		daN cm	
2786	0.499.118e+041.665e+04	0.09	6.968e+06	36,36	2795	0.499.118e+041.665e+04	0.09	6.968e+06	36,36		
2804	0.499.118e+041.665e+04	0.09	6.968e+06	36,36	2813	0.499.118e+041.665e+04	0.09	6.968e+06	36,36		
3122	0.489.118e+041.665e+04	0.09	6.968e+06	36,36	3123	0.359.118e+041.665e+04	0.06	6.968e+06	36,36		
3125	0.489.118e+041.665e+04	0.09	6.968e+06	36,36	3126	0.359.118e+041.665e+04	0.06	6.968e+06	36,36		
3128	0.489.118e+041.665e+04	0.09	6.968e+06	36,36	3129	0.359.118e+041.665e+04	0.06	6.968e+06	36,36		
3131	0.489.118e+041.665e+04	0.09	6.968e+06	36,36	3132	0.359.118e+041.665e+04	0.06	6.968e+06	36,36		

Nodo **Ver. V** **Ver. M**
 0.49 0.09

Fascia	Mat.	Spessore	Stato
		cm	
223	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
3123	0.349.118e+041.665e+04	0.06	6.968e+06	36,36	3124	0.049.118e+041.665e+047.09e-03	6.968e+06	36,36					
3126	0.349.118e+041.665e+04	0.06	6.968e+06	36,36	3127	0.049.118e+041.665e+047.09e-03	6.968e+06	36,36					
3129	0.349.118e+041.665e+04	0.06	6.968e+06	36,36	3130	0.049.118e+041.665e+047.09e-03	6.968e+06	36,36					
3132	0.349.118e+041.665e+04	0.06	6.968e+06	36,36	3133	0.049.118e+041.665e+047.09e-03	6.968e+06	36,36					

Nodo **Ver. V** **Ver. M**
 0.34 0.06

Fascia	Mat.	Spessore	Stato
		cm	
226	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
2515	0.379.118e+041.665e+04	0.07	6.968e+06	37,37	2790	0.379.118e+041.665e+04	0.07	6.968e+06	37,37				
2801	0.379.118e+041.665e+04	0.07	6.968e+06	37,37	2831	0.379.118e+041.665e+04	0.07	6.968e+06	37,37				
3137	0.359.118e+041.665e+04	0.06	6.968e+06	37,37	3138	0.269.118e+041.665e+04	0.05	6.968e+06	37,37				
3140	0.359.118e+041.665e+04	0.06	6.968e+06	37,37	3141	0.269.118e+041.665e+04	0.05	6.968e+06	37,37				
3143	0.359.118e+041.665e+04	0.06	6.968e+06	37,37	3144	0.269.118e+041.665e+04	0.05	6.968e+06	37,37				
3146	0.359.118e+041.665e+04	0.06	6.968e+06	37,37	3147	0.269.118e+041.665e+04	0.05	6.968e+06	37,37				

Nodo **Ver. V** **Ver. M**
 0.37 0.07

Fascia	Mat.	Spessore	Stato
		cm	
227	mattoni pieni e malta di calce INTONACO ARMATO	40.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
3138	0.269.118e+041.665e+04	0.05	6.968e+06	25,25	3139	0.049.118e+041.665e+047.11e-03	6.968e+06	25,25					
3141	0.269.118e+041.665e+04	0.05	6.968e+06	25,25	3142	0.049.118e+041.665e+047.11e-03	6.968e+06	25,25					
3144	0.269.118e+041.665e+04	0.05	6.968e+06	25,25	3145	0.049.118e+041.665e+047.11e-03	6.968e+06	25,25					
3147	0.269.118e+041.665e+04	0.05	6.968e+06	25,25	3148	0.049.118e+041.665e+047.11e-03	6.968e+06	25,25					

Nodo **Ver. V** **Ver. M**
 0.26 0.05

Fascia	Mat.	Spessore	Stato
		cm	
232	mattoni pieni e malta di calce	37.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2584	0.146.045e+041.027e+04			0.02	4.297e+06	21,21	2593	0.146.045e+041.027e+04			0.02	4.297e+06	21,21
2602	0.146.045e+041.027e+04			0.02	4.297e+06	21,21	3155	0.156.045e+041.027e+04			0.02	4.297e+06	21,21
3156	0.126.045e+041.027e+04			0.02	4.297e+06	21,21	3158	0.156.045e+041.027e+04			0.02	4.297e+06	21,21
3160	0.126.045e+041.027e+04			0.02	4.297e+06	21,21	3162	0.156.045e+041.027e+04			0.02	4.297e+06	21,21
3163	0.126.045e+041.027e+04			0.02	4.297e+06	21,21							
Nodo	Ver. V			Ver. M									
	0.15			0.02									

Fascia	Mat.	Spessore	Stato
		cm	
233	mattoni pieni e malta di calce	37.0	ok L

Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
3156	0.124.650e+04	7908.75		0.02	3.305e+06	25,25	3157	0.054.650e+04	7908.75	8.29e-03	3.305e+06	25,25	
3160	0.124.650e+04	7908.75		0.02	3.305e+06	25,25	3161	0.054.650e+04	7908.75	8.29e-03	3.305e+06	25,25	
3163	0.124.650e+04	7908.75		0.02	3.305e+06	25,25	3164	0.054.650e+04	7908.75	8.29e-03	3.305e+06	25,25	
Nodo	Ver. V			Ver. M									
	0.12			0.02									

Fascia	Mat.	Spessore	Stato
		cm	
236	mattoni pieni e malta di calce	37.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2512	0.106.117e+041.027e+04			0.02	4.297e+06	21,21	2521	0.106.117e+041.027e+04			0.02	4.297e+06	21,21
2530	0.106.117e+041.027e+04			0.02	4.297e+06	21,21	3177	0.096.117e+041.027e+04			0.02	4.297e+06	21,21
3178	0.066.117e+041.027e+04			0.01	4.297e+06	21,21	3180	0.096.117e+041.027e+04			0.02	4.297e+06	21,21
3181	0.066.117e+041.027e+04			0.01	4.297e+06	21,21	3183	0.096.117e+041.027e+04			0.02	4.297e+06	21,21
3184	0.066.117e+041.027e+04			0.01	4.297e+06	21,21							
Nodo	Ver. V			Ver. M									
	0.10			0.02									

Fascia	Mat.	Spessore	Stato
		cm	
237	mattoni pieni e malta di calce	37.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
3178	0.044.705e+04	7908.75	7.45e-03	3.305e+06		21,21	3179	0.044.705e+04	7908.75	6.34e-03	3.305e+06		21,21
3181	0.044.705e+04	7908.75	7.45e-03	3.305e+06		21,21	3182	0.044.705e+04	7908.75	6.34e-03	3.305e+06		21,21
3184	0.044.705e+04	7908.75	7.45e-03	3.305e+06		21,21	3185	0.044.705e+04	7908.75	6.34e-03	3.305e+06		21,21
Nodo	Ver. V			Ver. M									
	0.04			7.45e-03									

Fascia	Mat.	Spessore	Stato
		cm	
242	muratura (consolidata) E =	6.825e+04	40.0 ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2094	0.311.191e+052.625e+04			0.07	5.956e+06	32,32
2112	0.311.191e+052.625e+04			0.07	5.956e+06	32,32
3198	0.261.191e+052.625e+04			0.06	5.956e+06	32,32
3202	0.261.191e+052.625e+04			0.06	5.956e+06	32,32
3205	0.261.191e+052.625e+04			0.06	5.956e+06	32,32

Nodo	Ver. V	Ver. M
	0.31	0.07

Fascia	Mat.	Spessore	Stato
		cm	
243	muratura (consolidata) E = 1.536e+05	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2103	0.311.191e+052.625e+04			0.07	5.956e+06	32,32
3196	0.311.191e+052.625e+04			0.07	5.956e+06	32,32
3201	0.311.191e+052.625e+04			0.07	5.956e+06	32,32
3204	0.311.191e+052.625e+04			0.07	5.956e+06	32,32

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
3198	0.152.680e+054.725e+04			0.03	1.340e+07	28,28
3202	0.152.680e+054.725e+04			0.03	1.340e+07	28,28
3205	0.152.680e+054.725e+04			0.03	1.340e+07	28,28

Nodo	Ver. V	Ver. M
	0.15	0.03

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
3200	0.032.680e+054.725e+044.65e-03			1.340e+07	28,28	
3203	0.032.680e+054.725e+044.65e-03			1.340e+07	28,28	
3206	0.032.680e+054.725e+044.65e-03			1.340e+07	28,28	

Fascia	Mat.	Spessore	Stato
		cm	
246	muratura (consolidata) E = 6.825e+04	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2040	0.061.191e+052.625e+04			0.01	5.956e+06	30,30
2058	0.061.191e+052.625e+04			0.01	5.956e+06	30,30
3217	0.051.191e+052.625e+04			0.01	5.956e+06	30,30
3220	0.051.191e+052.625e+04			0.01	5.956e+06	30,30
3223	0.051.191e+052.625e+04			0.01	5.956e+06	30,30

Nodo	Ver. V	Ver. M
	0.06	0.01

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
2049	0.061.191e+052.625e+04			0.01	5.956e+06	30,30
3216	0.061.191e+052.625e+04			0.01	5.956e+06	30,30
3219	0.061.191e+052.625e+04			0.01	5.956e+06	30,30
3222	0.061.191e+052.625e+04			0.01	5.956e+06	30,30

Fascia	Mat.	Spessore	Stato
		cm	
247	muratura (consolidata) E = 1.536e+05	40.0	ok L

Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
3217	0.022.680e+054.725e+044.02e-03			1.340e+07	30,30	
3220	0.022.680e+054.725e+044.02e-03			1.340e+07	30,30	
3223	0.022.680e+054.725e+044.02e-03			1.340e+07	30,30	

Nodo	Ver. V	Ver. M
	0.02	4.02e-03

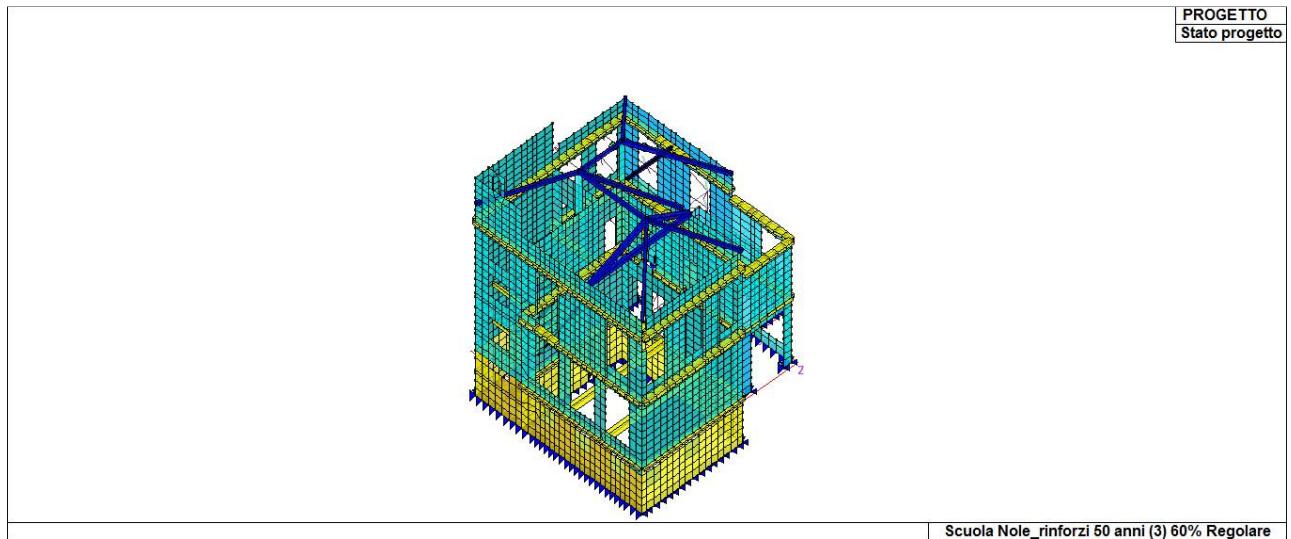
Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
3218	0.012.680e+054.725e+041.93e-03			1.340e+07	30,30	
3221	0.012.680e+054.725e+041.93e-03			1.340e+07	30,30	
3224	0.012.680e+054.725e+041.93e-03			1.340e+07	30,30	

Fascia	Mat.	Spessore	Stato
		cm	
250	muratura (consolidata) E = 6.825e+04	40.0	ok L

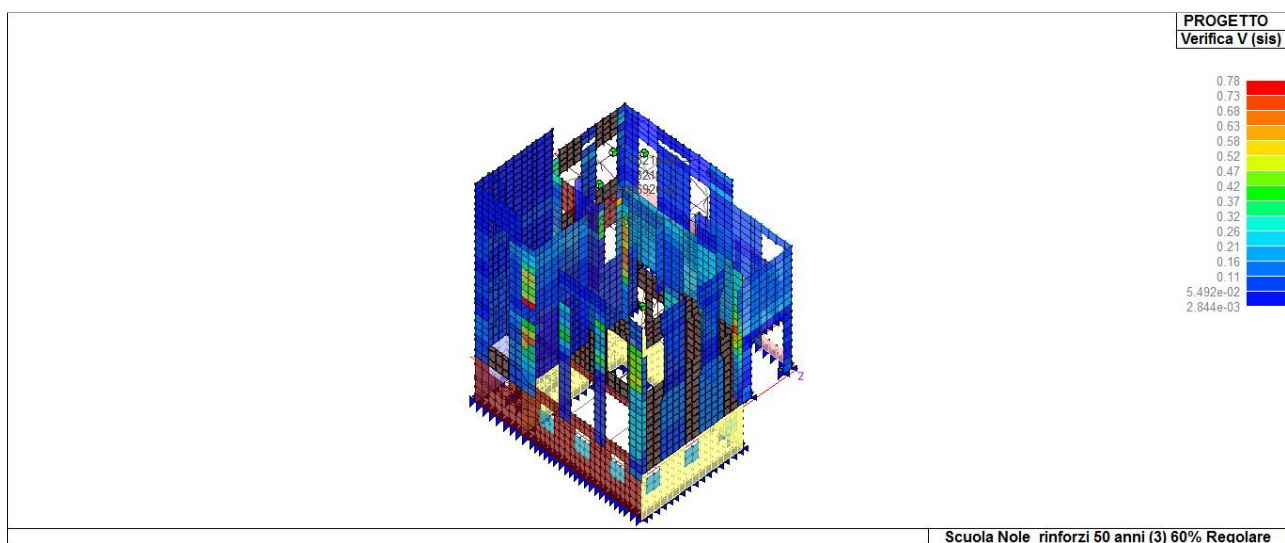
Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb	Nodo	Ver. V	Vp daN	Vt daN	Ver. M	Mu daN cm	Rif. cmb
1986	0.331.191e+052.625e+04			0.07	5.956e+06	11,11	1995	0.331.191e+052.625e+04			0.07	5.956e+06	11,11
2004	0.331.191e+052.625e+04			0.07	5.956e+06	11,11	3234	0.321.191e+052.625e+04			0.07	5.956e+06	11,11
3235	0.261.191e+052.625e+04			0.06	5.956e+06	11,11	3237	0.321.191e+052.625e+04			0.07	5.956e+06	11,11
3238	0.261.191e+052.625e+04			0.06	5.956e+06	11,11	3240	0.321.191e+052.625e+04			0.07	5.956e+06	11,11
3241	0.261.191e+052.625e+04			0.06	5.956e+06	11,11							
Nodo	Ver. V			Ver. M									
	0.33			0.07									

Fascia	Mat.	Spessore	Stato
		cm	
251	muratura (consolidata) E = 1.536e+05	40.0	ok L

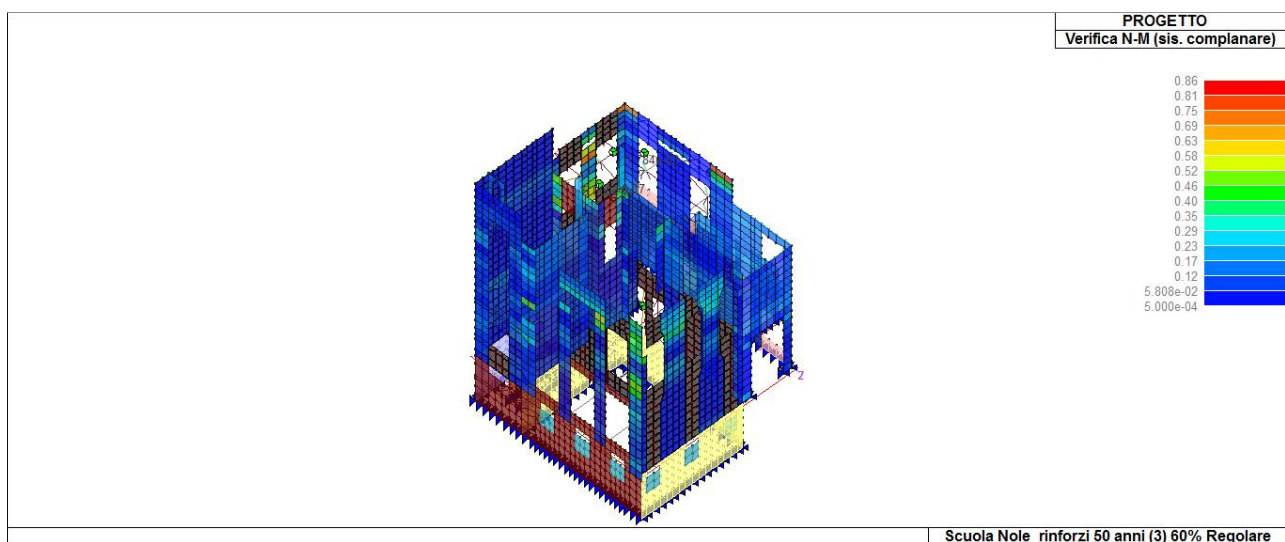
Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb	Nodo	Ver. V	Vp	Vt	Ver. M	Mu	Rif. cmb
		daN	daN		daN cm				daN	daN		daN cm	
3235	0.152.680e+054.725e+04			0.03	1.340e+07	35,35	3236	0.022.680e+054.725e+043.02e-03			1.340e+07	35,35	
3238	0.152.680e+054.725e+04			0.03	1.340e+07	35,35	3239	0.022.680e+054.725e+043.02e-03			1.340e+07	35,35	
3241	0.152.680e+054.725e+04			0.03	1.340e+07	35,35	3242	0.022.680e+054.725e+043.02e-03			1.340e+07	35,35	
Nodo	Ver. V			Ver. M									
	0.15			0.03									



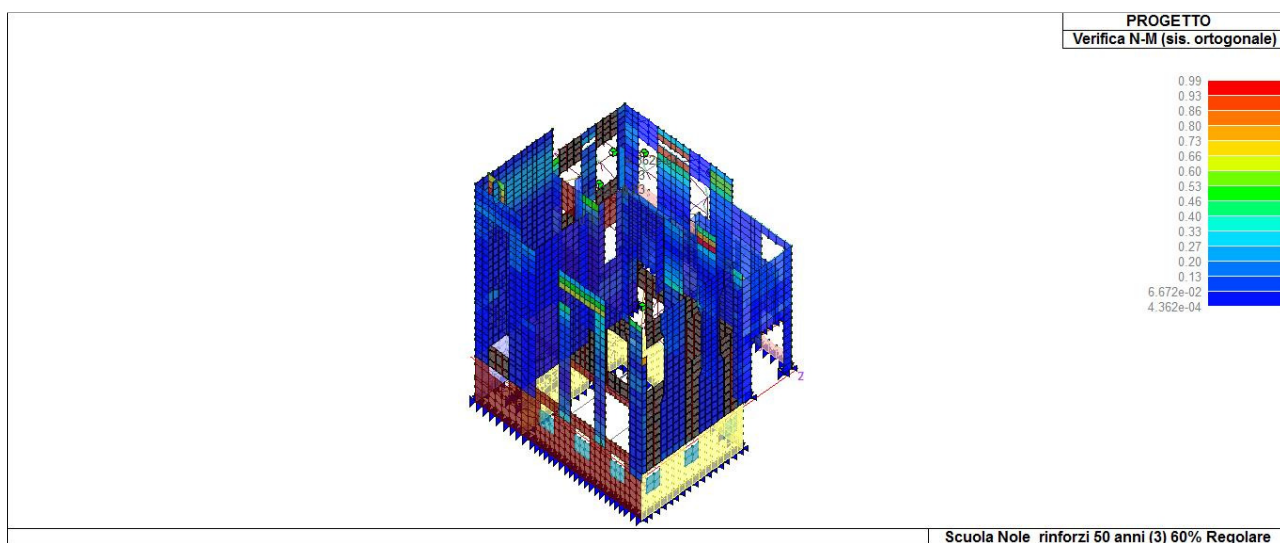
Verifiche sismiche compressive murature. Risultano tutte positive per un'accelerazione attesa al suolo pari al 60%



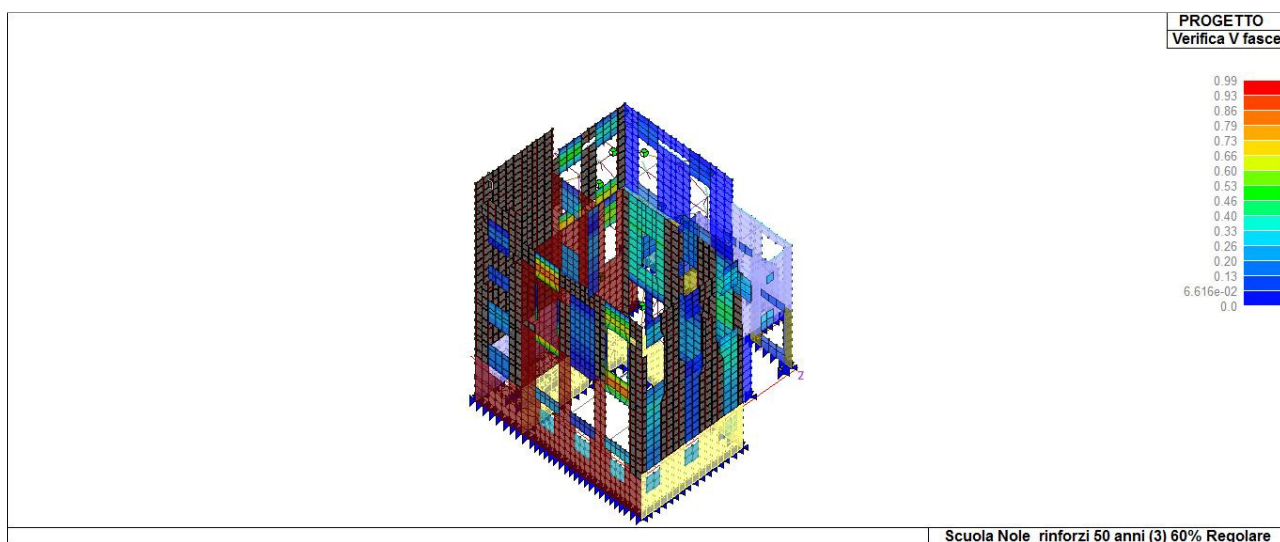
Verifica positiva (<1) muratura a taglio per un'accelerazione attesa al suolo pari al 60%



Verifica positiva (<1) muratura a pressoflessione nel piano per un'accelerazione attesa al suolo pari al 60%

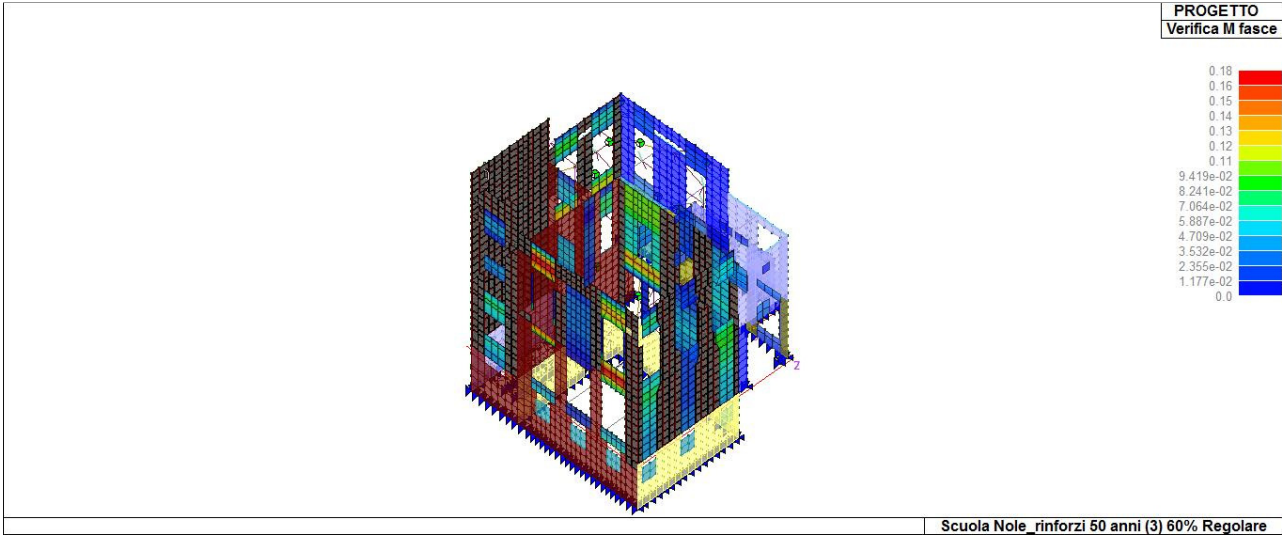


Verifica positiva (<1) muratura a pressoflessione fuori dal piano per un'accelerazione attesa al suolo pari al 60%



Verifica positiva (<1) a taglio travi muratura per un'accelerazione attesa al suolo pari al 60%

Verifica positiva (<1) a momento flettente travi muratura per un'accelerazione attesa al suolo pari al 60%



Relazione di calcolo Analisi lineare e non lineare dei cinematismi nella muratura

PARETE NORD EST – Stato di fatto

Relazione di calcolo sulla struttura impostata e redatta secondo le modalità previste dal DM 17/01/2018 NTC cap. 10 'Redazione dei progetti strutturali esecutivi e delle relazioni di calcolo'.

Di seguito si indicano l'origine e le caratteristiche dei codici di calcolo utilizzati riportando titolo, produttore e distributore, versione, estremi della licenza d'uso:

Nome del software:

PRO_CINEm Analisi lineare e non lineare dei cinematismi nella muratura

Versione del software:

v. 2018.04.0044b

Produttore del software:

2 S.I. Software e Servizi per l'Ingegneria s.r.l., Ferrara

Distributore del software:

2 S.I. Software e Servizi per l'Ingegneria s.r.l., Ferrara

Dati utente finale:

.....

Normativa di Riferimento

NTC 2018 e Circolare 617 del 2009

Parametri sismici

Località: NOLE (TO)

Altezza totale dell'edificio: 13,00 m

Vita nominale dell'edificio: 50,00 anni

Coefficiente di struttura: 2,00

Periodo del modo per principale di vibrare (T_1): 0,342 sec

Coefficiente di partecipazione modale: γ : 1,20

Categoria di sottosuolo: Tipo B

SLV

Periodo di ritorno per lo SLV (T_r): 712 anni

Probabilità di superamento per lo SLV (P_{ver}): 10 %

Periodo di inizio del tratto a velocità costante per lo SLV (T_{c^*}): 0,280 sec

Accelerazione orizzontale massima al sito per lo SLV (a_g): 0,065 g

Fattore di amplificazione dello spettro in accelerazione orizzontale per lo SLV (F_0): 2,77

Periodo dello spettro T_b : 0,13 sec

Periodo dello spettro T_c : 0,40 sec

Periodo dello spettro T_d : 1,86 sec

Coefficiente di sottosuolo S : 1,20

SLD

Periodo di ritorno per lo SLD (T_r): 75 anni

Probabilità di superamento per lo SLD (P_{ver}): 63 %

Periodo di inizio del tratto a velocità costante per lo SLD (T_c^*): 0,210 sec
Accelerazione orizzontale massima al sito per lo SLD (a_g): 0,035 g
Fattore di amplificazione dello spettro in accelerazione orizzontale per lo SLD (F_0) 2,62
Periodo dello spettro T_b : 0,11 sec
Periodo dello spettro T_c : 0,32 sec
Periodo dello spettro T_d : 1,74 sec
Coefficiente di sottosuolo S : 1,20

Livello di conoscenza e coefficiente di sicurezza

In relazione alle indagini svolte e alla documentazione acquisita il livello di conoscenza è di tipo LC2 (Adeguito), il fattore di confidenza adottato è: 1,20

Nelle verifiche di sicurezza viene considerato un coefficiente di sicurezza sulle proprietà meccaniche pari a: 2

Nel calcolo dei cinematismi viene considerato l'arretramento del punto di contatto tra i blocchi nei seguenti casi:

- Cinematismi di ribaltamento fuori piano
- Cinematismi di flessione verticale
- Cinematismi di flessione orizzontale

Proprietà meccaniche caratteristiche delle pareti e coefficienti correttivi

Parete n°: 1

Tipologia muraria: Muratura in mattoni semipieni e malta cementizia (es. doppio UNI perc. for.<40%)

Resistenza media a compressione [MPa]: 6,500

Resistenza a taglio [MPa]: 0,280

Peso specifico [kN/mc]: 15,00

Alla muratura della parete n° 1 vengono applicati i seguenti fattori correttivi definiti nella Tab. C8A.2.2 della Circolare 617 del 2009:

- Fattore correttivo dovuto a Malta buona: 1,50
- Fattore correttivo dovuto a Giunti sottili: 1,50

Fattore correttivo complessivo delle proprietà meccaniche: 2,25

Parete n°: 2

Tipologia muraria: Muratura in mattoni semipieni e malta cementizia (es. doppio UNI perc. for.<40%)

Resistenza media a compressione [MPa]: 6,500

Resistenza a taglio [MPa]: 0,280

Peso specifico [kN/mc]: 15,00

Alla muratura della parete n° 2 vengono applicati i seguenti fattori correttivi definiti nella Tab. C8A.2.2 della Circolare 617 del 2009:

- Fattore correttivo dovuto a Malta buona: 1,50
- Fattore correttivo dovuto a Giunti sottili: 1,50

Fattore correttivo complessivo delle proprietà meccaniche: 2,25

Parete n°: 3

Tipologia muraria: Muratura in mattoni semipieni e malta cementizia (es. doppio UNI perc. for.<40%)

Resistenza media a compressione [MPa]: 6,500

Resistenza a taglio [MPa]: 0,280

Peso specifico [kN/mc]: 15,00

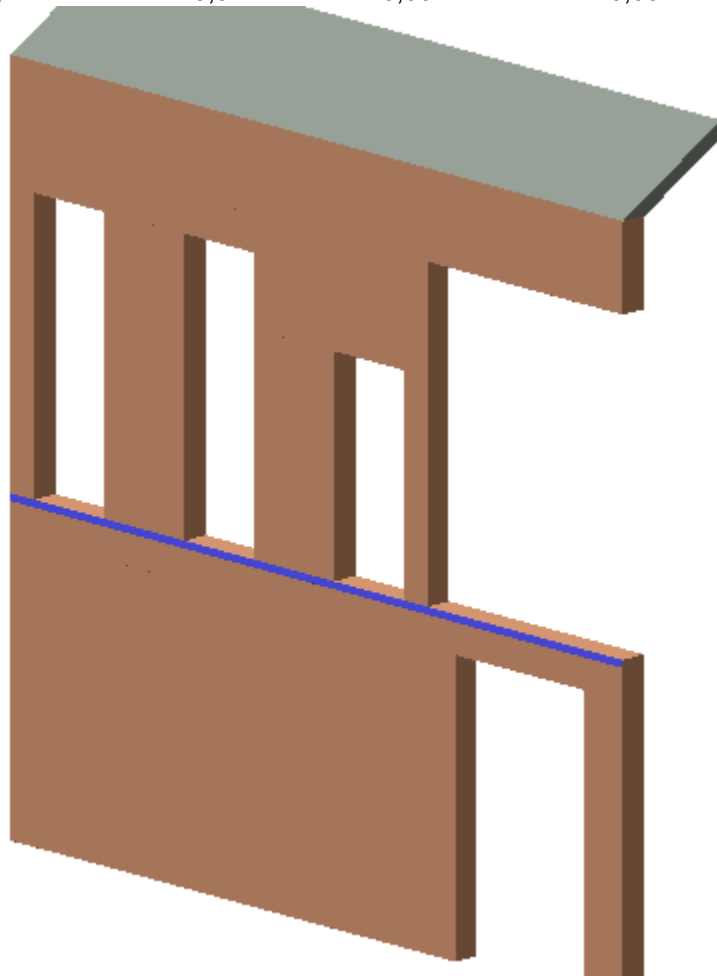
Proprietà meccaniche delle pareti, valori di progetto:

n°	γ [kN/m ³]	f_{cd} [MPa]	f_{vd} [MPa]
1	15,00	6,094	0,263
2	15,00	6,094	0,263
3	15,00	2,708	0,117

Geometria delle pareti:

n°	Larghezza [m]	Altezza [m]	Spessore [m]	$d_{y_timpano}$ [m]	$d_{z_timpano}$ [m]
1	10,88	4,5	0,37	0,00	0,00

2	10,88	4,5	0,37	0,00	0,00
3	10,88	1,2	0,37	0,00	0,00



Carichi sulle pareti:

Legenda:

P_p : peso proprio della parete
 G_k : carico permanente gravante sul solaio della parete
 Q_k : carico variabile gravante sul solaio della parete
 φ_2 : carico variabile gravante sul solaio della parete
 i_s : interasse del solaio
 $G_{k\text{timp}}$: carico permanente gravante sul solaio del timpano
 $Q_{k\text{timp}}$: carico variabile gravante sul solaio del timpano
 $\varphi_{2\text{timp}}$: carico variabile gravante sul solaio del timpano
 i_t : interasse del timpano
 $G_{k\text{falda}}$: carico permanente gravante sul solaio della falda inclinata
 $Q_{k\text{falda}}$: carico variabile gravante sul solaio della falda inclinata
 $\varphi_{2\text{falda}}$: carico variabile gravante sul solaio della falda inclinata
 i_f : interasse della falda

n°	P_p [kN]	G_k [kN/m ²]	Q_k [kN/m ²]	φ_2	i_s [m]	$G_{k\text{timp}}$ [kN/m ²]	$Q_{k\text{timp}}$ [kN/m ²]	$\varphi_{2\text{timp}}$	i_t [m]	$G_{k\text{falda}}$ [kN/m ²]	$Q_{k\text{falda}}$ [kN/m ²]	$\varphi_{2\text{falda}}$	i_f [m]
1	222,92	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
2	109,61	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
3	73,67	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	1,20	1,90	0,00	2,00

Carichi sulle pareti ortogonali:

Legenda:

G_{korto} : carico permanente gravante sul solaio delle pareti ortogonali

Q_{korto} : carico variabile gravante sul solaio delle pareti ortogonali

φ_{2orto} : carico variabile gravante sul solaio delle pareti ortogonali

n°:	G_{korto} [kN/m ²]	Q_{korto} [kN/m ²]	φ_{2orto}
1	6,40	3,00	0,60
2	6,40	3,00	0,60
3	6,40	3,00	0,60

Cinematismi:

Cinematismo n°: 1

Tipo: Fles. Verticale singola

Pareti coinvolte: 1,

Quota: 0,00[m]

PGA relativa al cinematismo nel caso di analisi cinematica lineare: 1,1212 [g]

PGA relativa al cinematismo nel caso di analisi cinematica non lineare: 0,4253 [g]

Moltiplicatore di collasso dei carichi orizzontali α_0 : 0,722

accelerazione spettrale di attivazione del cinematismo a_0^* : 0,673 [g]

Massa partecipante al cinematismo M^* : 23 [kN]

Frazione di massa partecipante della struttura e^* : 0,895

Risultati della verifica con analisi cinematica lineare allo SLD

Accelerazione di riferimento allo SLD per cinematismo a quota zero: 0,042 [g]

Stato di verifica dell'analisi cinematica lineare allo SLD: **Verificato**

Risultati della verifica con analisi cinematica lineare allo SLV

Accelerazione di riferimento allo SLV per cinematismo a quota zero: 0,039 [g]

Stato di verifica dell'analisi cinematica lineare allo SLV: **Verificato**

Risultati della verifica con analisi cinematica non lineare allo SLV

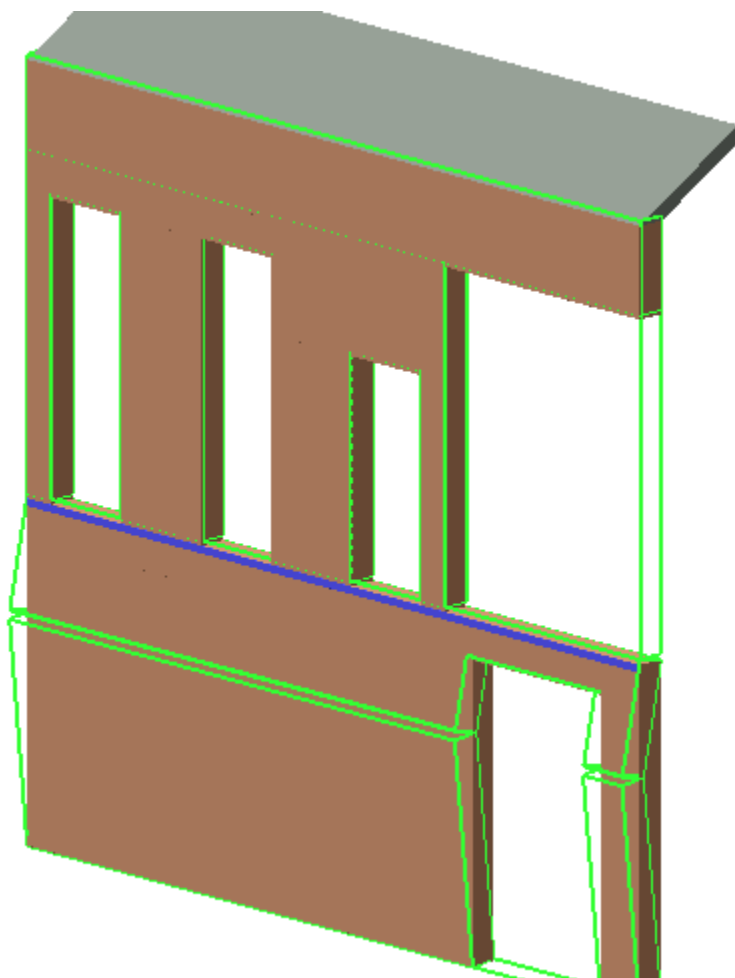
Periodo secante T_s : 0,392[sec]

Spostamento spettrale d_u^* : 0,054[m]

Domanda di spostamento nel caso di cinematismo a quota zero $\Delta_{d, \text{ quota zero}}$: 0,008 [m]

Domanda di spostamento nel caso di cinematismo a quota maggiore di zero $\Delta_{d, \text{ quota sopraelev.}}$: 0,000 [m]

Stato di verifica dell'analisi cinematica non lineare allo SLV: **Verificato**



Cinematismo n°: 2

Tipo: Rib. Multi

Pareti coinvolte: 2, 3,

Quota: 4,53[m]

Primo modo di vibrare normalizzato ad 1 in sommità dell'edificio $\Psi(Z)$: 0,348

PGA relativa al cinematismo nel caso di analisi cinematica lineare: 0,0000 [g]

PGA relativa al cinematismo nel caso di analisi cinematica non lineare: 0,0000 [g]

Moltiplicatore di collasso dei carichi orizzontali α_0 : -0,112

accelerazione spettrale di attivazione del cinematismo a_0^* : -0,106 [g]

Massa partecipante al cinematismo M^* : 19 [kN]

Frazione di massa partecipante della struttura e^* : 0,884

Risultati della verifica con analisi cinematica lineare allo SLD

Accelerazione di riferimento allo SLD (a quota zero): 0,042 [g]

Accelerazione di riferimento allo SLD (a quota diversa da zero): 0,042 [g]

Stato di verifica dell'analisi cinematica lineare allo SLD: **Non Verificato**

Risultati della verifica con analisi cinematica lineare allo SLV

Accelerazione di riferimento allo SLV (a quota zero): 0,039[g]

Accelerazione di riferimento allo SLV (a quota diversa da zero): 0,045 [g]

Stato di verifica dell'analisi cinematica lineare allo SLV: **Non Verificato**

Risultati della verifica con analisi cinematica non lineare allo SLV

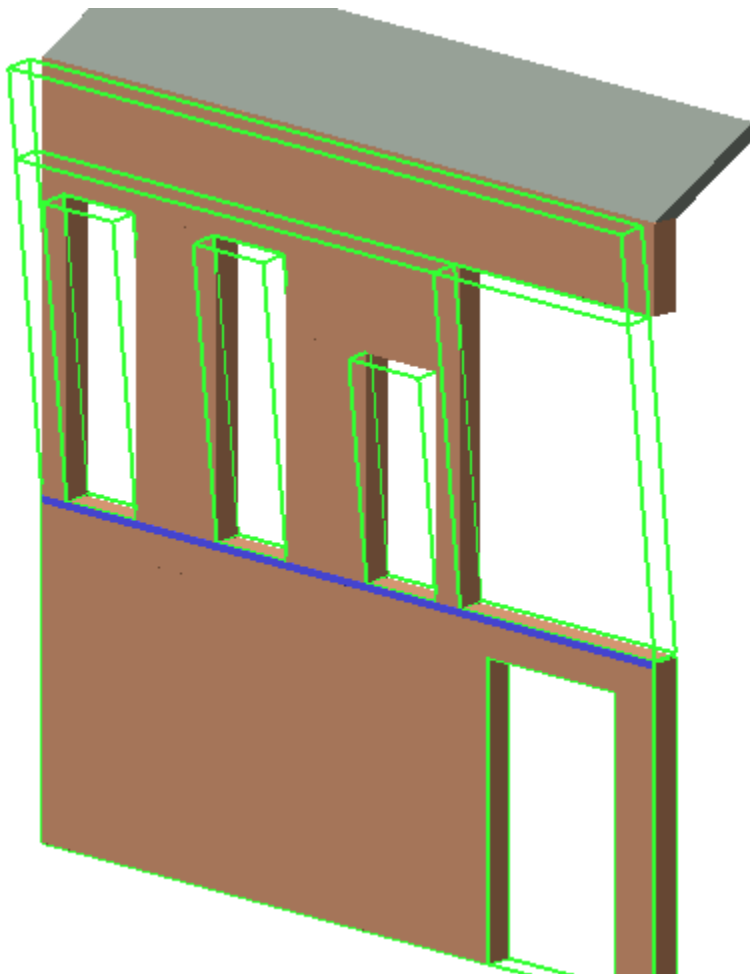
Periodo secante T_s : 0,000[sec]

Spostamento spettrale d_u^* : 0,002[m]

Domanda di spostamento nel caso di cinematismo a quota zero $\Delta_{d, \text{quota zero}}$: 0,000 [m]

Domanda di spostamento nel caso di cinematismo a quota maggiore di zero $\Delta_{d, \text{quota sopraelev}}$: 0,000 [m]

Stato di verifica dell'analisi cinematica non lineare allo SLV: **Verificato**



Cinematismo n°: 3

Tipo: Rib. Singolo

Pareti coinvolte: 3,

Quota: 9,03[m]

Primo modo di vibrare normalizzato ad 1 in sommità dell'edificio $\psi(Z)$: 0,695

PGA relativa al cinematismo nel caso di analisi cinematica lineare: 0,0000 [g]

PGA relativa al cinematismo nel caso di analisi cinematica non lineare: 0,0000 [g]

Moltiplicatore di collasso dei carichi orizzontali α_0 : -0,114

accelerazione spettrale di attivazione del cinematismo a_0^* : -0,106 [g]

Massa partecipante al cinematismo M^* : 9 [kN]

Frazione di massa partecipante della struttura e^* : 0,892

Risultati della verifica con analisi cinematica lineare allo SLD

Accelerazione di riferimento allo SLD (a quota zero): 0,042 [g]

Accelerazione di riferimento allo SLD (a quota diversa da zero): 0,084 [g]

Stato di verifica dell'analisi cinematica lineare allo SLD: **Non Verificato**

Risultati della verifica con analisi cinematica lineare allo SLV

Accelerazione di riferimento allo SLV (a quota zero): 0,039[g]

Accelerazione di riferimento allo SLV (a quota diversa da zero): 0,090 [g]

Stato di verifica dell'analisi cinematica lineare allo SLV: **Non Verificato**

Risultati della verifica con analisi cinematica non lineare allo SLV

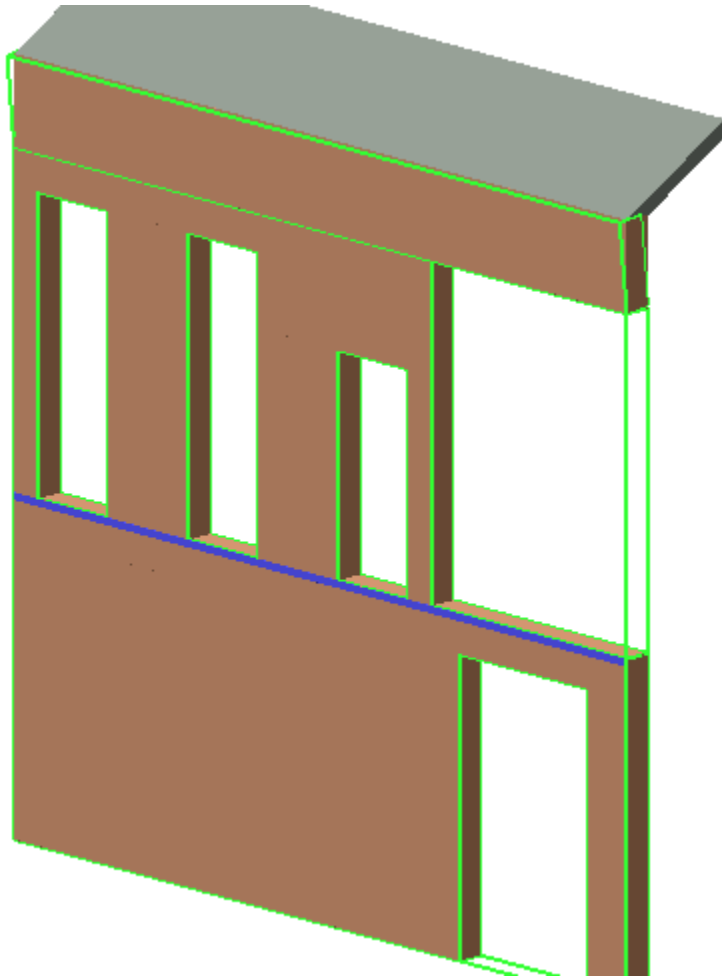
Periodo secante T_s : 0,000[sec]

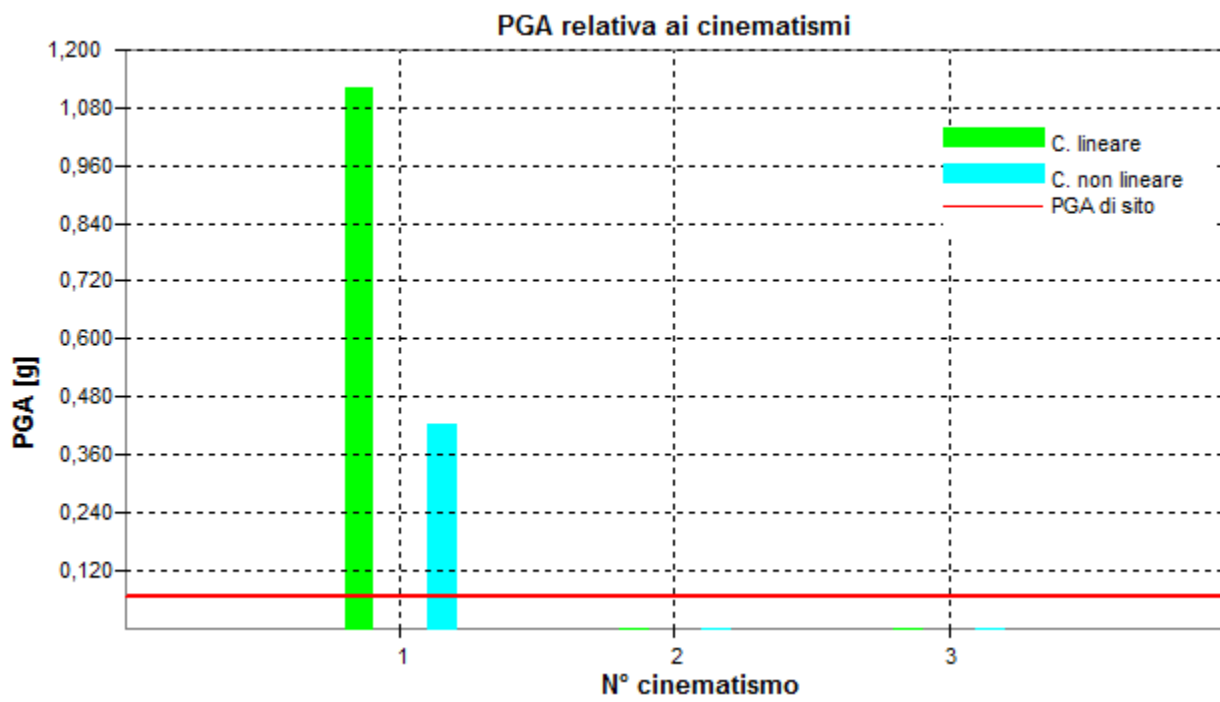
Spostamento spettrale d_u^* : 0,000[m]

Domanda di spostamento nel caso di cinematismo a quota zero $\Delta_{d, \text{ quota zero}}$: 0,000 [m]

Domanda di spostamento nel caso di cinematismo a quota maggiore di zero $\Delta_{d, \text{ quota sopraelev}}$: 0,000 [m]

Stato di verifica dell'analisi cinematica non lineare allo SLV: **Verificato**





Relazione di calcolo Analisi lineare e non lineare dei cinematismi nella muratura

PARETE NORD OVEST – Stato di fatto

Relazione di calcolo sulla struttura impostata e redatta secondo le modalità previste dal DM 17/01/2018 NTC cap. 10 'Redazione dei progetti strutturali esecutivi e delle relazioni di calcolo'.

Di seguito si indicano l'origine e le caratteristiche dei codici di calcolo utilizzati riportando titolo, produttore e distributore, versione, estremi della licenza d'uso:

Nome del software:

PRO_CINEm Analisi lineare e non lineare dei cinematismi nella muratura

Versione del software:

v. 2018.04.0044b

Produttore del software:

2 S.I. Software e Servizi per l'Ingegneria s.r.l., Ferrara

Distributore del software:

2 S.I. Software e Servizi per l'Ingegneria s.r.l., Ferrara

Dati utente finale:

.....

Normativa di Riferimento

NTC 2018 e Circolare 617 del 2009

Parametri sismici

Località: NOLE (TO)

Altezza totale dell'edificio: 13,00 m

Vita nominale dell'edificio: 50,00 anni

Coefficiente di struttura: 2,00

Periodo del modo per principale di vibrare (T1): 0,342 sec

Coefficiente di partecipazione modale: γ : 1,20

Categoria di sottosuolo: Tipo B

SLV

Periodo di ritorno per lo SLV (Tr): 712 anni

Probabilità di superamento per lo SLV (Pver): 10 %

Periodo di inizio del tratto a velocità costante per lo SLV (Tc*): 0,280 sec

Accelerazione orizzontale massima al sito per lo SLV (ag): 0,065 g

Fattore di amplificazione dello spettro in accelerazione orizzontale per lo SLV (F0): 2,77

Periodo dello spettro Tb: 0,13 sec

Periodo dello spettro Tc: 0,40 sec

Periodo dello spettro Td: 1,86 sec

Coefficiente di sottosuolo S: 1,20

SLD

Periodo di ritorno per lo SLD (Tr): 75 anni

Probabilità di superamento per lo SLD (Pver): 63 %

Periodo di inizio del tratto a velocità costante per lo SLD (T_c^*): 0,210 sec
Accelerazione orizzontale massima al sito per lo SLD (a_g): 0,035 g
Fattore di amplificazione dello spettro in accelerazione orizzontale per lo SLD (F_0) 2,62
Periodo dello spettro T_b : 0,11 sec
Periodo dello spettro T_c : 0,32 sec
Periodo dello spettro T_d : 1,74 sec
Coefficiente di sottosuolo S : 1,20

Livello di conoscenza e coefficiente di sicurezza

In relazione alle indagini svolte e alla documentazione acquisita il livello di conoscenza è di tipo LC2 (Adeguito), il fattore di confidenza adottato è: 1,20

Nelle verifiche di sicurezza viene considerato un coefficiente di sicurezza sulle proprietà meccaniche pari a: 2

Nel calcolo dei cinematismi viene considerato l'arretramento del punto di contatto tra i blocchi nei seguenti casi:

- Cinematismi di ribaltamento fuori piano
- Cinematismi di flessione verticale
- Cinematismi di flessione orizzontale

Proprietà meccaniche caratteristiche delle pareti e coefficienti correttivi

Parete n°: 1

Tipologia muraria: Muratura in mattoni pieni e malta di calce

Resistenza media a compressione [MPa]: 3,200

Resistenza a taglio [MPa]: 0,076

Peso specifico [kN/mc]: 18,00

Alla muratura della parete n° 1 vengono applicati i seguenti fattori correttivi definiti nella Tab. C8A.2.2 della Circolare 617 del 2009:

- Fattore correttivo dovuto a Malta buona: 1,50
- Fattore correttivo dovuto a Giunti sottili: 1,50
- Fattore correttivo dovuto a Connessione trasversale: 1,30

Fattore correttivo complessivo delle proprietà meccaniche: 2,93

Parete n°: 2

Tipologia muraria: Muratura in mattoni pieni e malta di calce

Resistenza media a compressione [MPa]: 3,200

Resistenza a taglio [MPa]: 0,076

Peso specifico [kN/mc]: 18,00

Alla muratura della parete n° 2 vengono applicati i seguenti fattori correttivi definiti nella Tab. C8A.2.2 della Circolare 617 del 2009:

- Fattore correttivo dovuto a Malta buona: 1,50
- Fattore correttivo dovuto a Giunti sottili: 1,50
- Fattore correttivo dovuto a Connessione trasversale: 1,30

Fattore correttivo complessivo delle proprietà meccaniche: 2,93

Parete n°: 3

Tipologia muraria: Muratura in mattoni pieni e malta di calce

Resistenza media a compressione [MPa]: 3,200

Resistenza a taglio [MPa]: 0,076

Peso specifico [kN/mc]: 18,00

Alla muratura della parete n° 3 vengono applicati i seguenti fattori correttivi definiti nella Tab. C8A.2.2 della Circolare 617 del 2009:

- Fattore correttivo dovuto a Malta buona: 1,50
- Fattore correttivo dovuto a Giunti sottili: 1,50
- Fattore correttivo dovuto a Connessione trasversale: 1,30

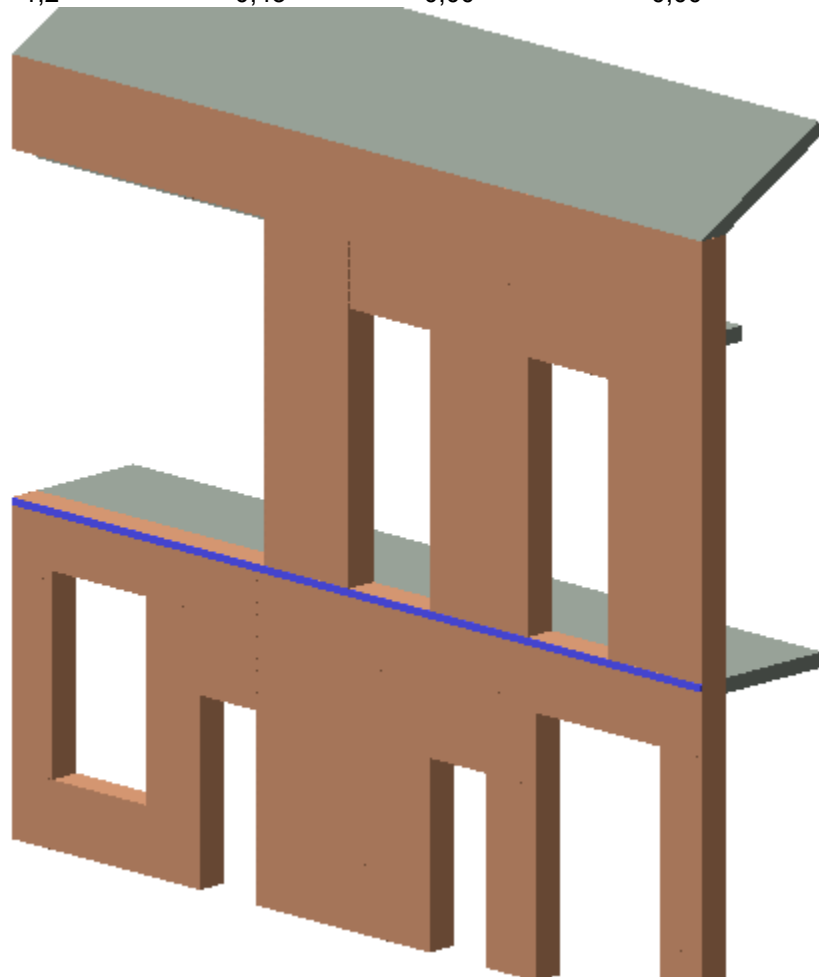
Fattore correttivo complessivo delle proprietà meccaniche: 2,93

Proprietà meccaniche delle pareti, valori di progetto:

n°	γ [kN/m ³]	f_{cd} [MPa]	f_{vd} [MPa]
1	18,00	3,900	0,093
2	18,00	3,900	0,093
3	18,00	3,900	0,093

Geometria delle pareti:

n°	Larghezza [m]	Altezza [m]	Spessore [m]	dy_timpano [m]	dz_timpano [m]
1	12,05	4,4	0,43	0,00	0,00
2	12,05	4,5	0,43	0,00	0,00
3	12,05	1,2	0,43	0,00	0,00



Carichi sulle pareti:

Legenda:

- P_p : peso proprio della parete
- G_k : carico permanente gravante sul solaio della parete
- Q_k : carico variabile gravante sul solaio della parete
- ϕ_2 : carico variabile gravante sul solaio della parete
- i_s : interasse del solaio
- $G_{k\text{timpano}}$: carico permanente gravante sul solaio del timpano
- $Q_{k\text{timpano}}$: carico variabile gravante sul solaio del timpano
- $\phi_{2\text{timpano}}$: carico variabile gravante sul solaio del timpano
- i_t : interasse del timpano
- G_{kfalda} : carico permanente gravante sul solaio della falda inclinata
- Q_{kfalda} : carico variabile gravante sul solaio della falda inclinata

φ_{2falda} : carico variabile gravante sul solaio della falda inclinata
 if: interasse della falda

n°	P _P [kN]	G _k [kN/m ²]	Q _k [kN/m ²]	φ_2	is [m]	G _k _{temp} [kN/m ²]	Q _k _{temp} [kN/m ²]	φ_{2temp}	it [m]	G _k _{falda} [kN/m ²]	Q _k _{falda} [kN/m ²]	φ_{2falda}	if
1	278,78	5,90	3,00	0,60	1,90	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
2	107,91	3,00	0,50	0,00	0,50	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
3	113,79	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	1,20	1,90	0,00	2,35

Carichi sulle pareti ortogonali:

Legenda:

G_{korto}: carico permanente gravante sul solaio delle pareti ortogonali

Q_{korto}: carico variabile gravante sul solaio delle pareti ortogonali

φ_{2orto} : carico variabile gravante sul solaio delle pareti ortogonali

n°:	G _{korto} [kN/m ²]	Q _{korto} [kN/m ²]	φ_{2orto}
1	6,40	3,00	0,60
2	6,40	3,00	0,60
3	6,40	3,00	0,60

Cinematismi:

Cinematismo n°: 1

Tipo: Fles. Verticale singola

Pareti coinvolte: 1,

Quota: 0,00[m]

PGA relativa al cinematismo nel caso di analisi cinematica lineare: 3,3595 [g]

PGA relativa al cinematismo nel caso di analisi cinematica non lineare: 1,2846 [g]

Moltiplicatore di collasso dei carichi orizzontali α_0 : 1,328

accelerazione spettrale di attivazione del cinematismo a_0^* : 2,016 [g]

Massa partecipante al cinematismo M*: 28 [kN]

Frazione di massa partecipante della struttura e^* : 0,549

Risultati della verifica con analisi cinematica lineare allo SLD

Accelerazione di riferimento allo SLD per cinematismo a quota zero: 0,042 [g]

Stato di verifica dell'analisi cinematica lineare allo SLD: **Verificato**

Risultati della verifica con analisi cinematica lineare allo SLV

Accelerazione di riferimento allo SLV per cinematismo a quota zero: 0,039 [g]

Stato di verifica dell'analisi cinematica lineare allo SLV: **Verificato**

Risultati della verifica con analisi cinematica non lineare allo SLV

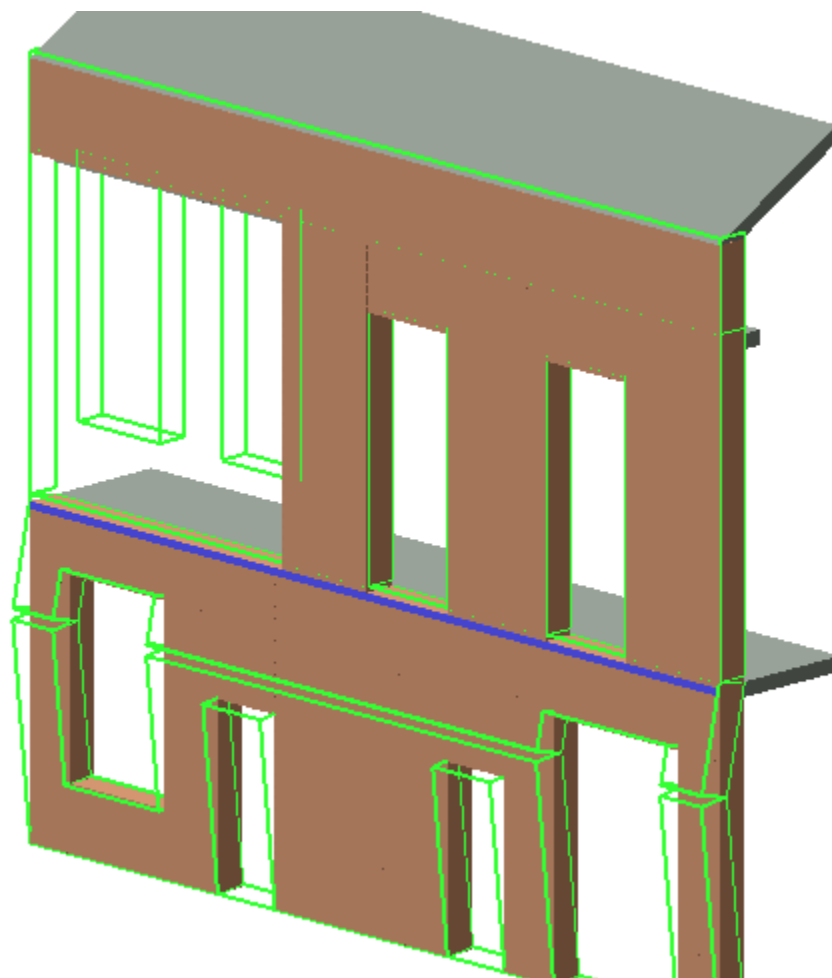
Periodo secante T_s: 0,232[sec]

Spostamento spettrale d_u^* : 0,057[m]

Domanda di spostamento nel caso di cinematismo a quota zero $\Delta_{d, \text{ quota zero}}$: 0,003 [m]

Domanda di spostamento nel caso di cinematismo a quota maggiore di zero $\Delta_{d, \text{ quota sopraelev.}}$: 0,000 [m]

Stato di verifica dell'analisi cinematica non lineare allo SLV: **Verificato**



Cinematismo n°: 2

Tipo: Rib. Multi

Pareti coinvolte: 2, 3,

Quota: 4,39[m]

Primo modo di vibrare normalizzato ad 1 in sommità dell'edificio $\Psi(Z)$: 0,338

PGA relativa al cinematismo nel caso di analisi cinematica lineare: 0,0000 [g]

PGA relativa al cinematismo nel caso di analisi cinematica non lineare: 0,0000 [g]

Moltiplicatore di collasso dei carichi orizzontali α_0 : -0,104

accelerazione spettrale di attivazione del cinematismo a_0^* : -0,099 [g]

Massa partecipante al cinematismo M^* : 24 [kN]

Frazione di massa partecipante della struttura e^* : 0,874

Risultati della verifica con analisi cinematica lineare allo SLD

Accelerazione di riferimento allo SLD (a quota zero): 0,042 [g]

Accelerazione di riferimento allo SLD (a quota diversa da zero): 0,041 [g]

Stato di verifica dell'analisi cinematica lineare allo SLD: **Non Verificato**

Risultati della verifica con analisi cinematica lineare allo SLV

Accelerazione di riferimento allo SLV (a quota zero): 0,039[g]

Accelerazione di riferimento allo SLV (a quota diversa da zero): 0,044 [g]

Stato di verifica dell'analisi cinematica lineare allo SLV: **Non Verificato**

Risultati della verifica con analisi cinematica non lineare allo SLV

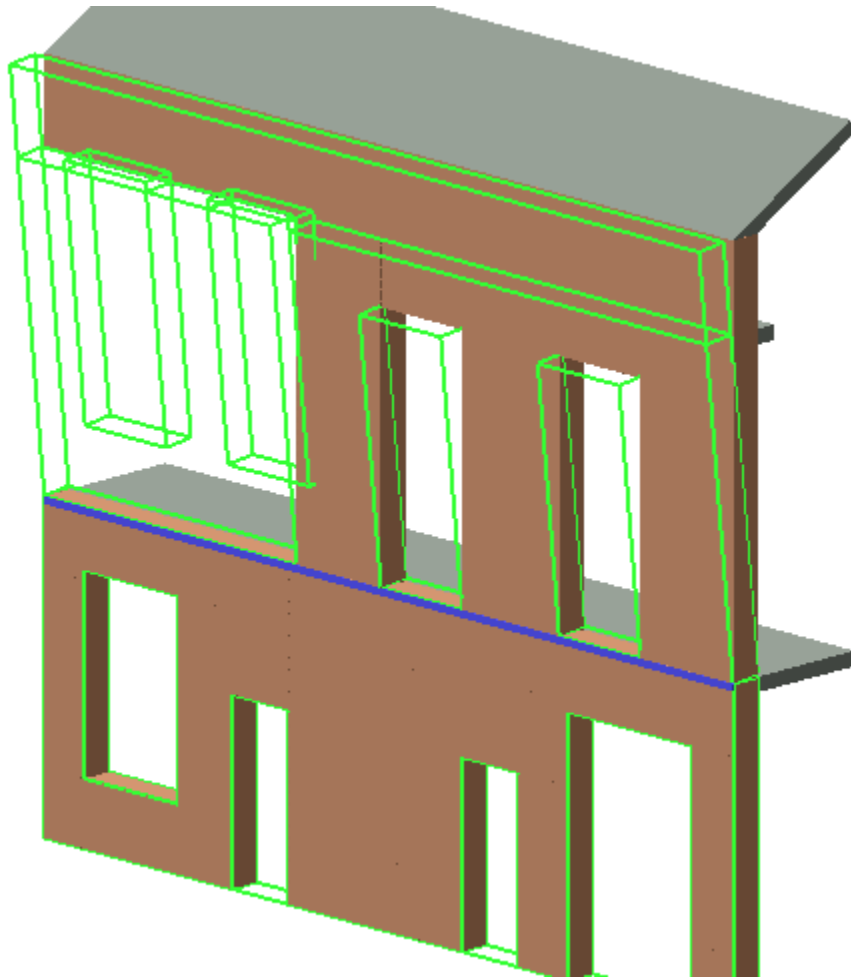
Periodo secante T_s : 0,000[sec]

Spostamento spettrale d_u^* : 0,002[m]

Domanda di spostamento nel caso di cinematisimo a quota zero $\Delta_{d, \text{quota zero}}$: 0,000 [m]

Domanda di spostamento nel caso di cinematisimo a quota maggiore di zero $\Delta_{d, \text{quota sopraelev}}$: 0,000 [m]

Stato di verifica dell'analisi cinematica non lineare allo SLV: **Verificato**



Cinematisimo n°: 3

Tipo: Rib. Singolo

Pareti coinvolte: 3,

Quota: 8,86[m]

Primo modo di vibrare normalizzato ad 1 in sommità dell'edificio $\psi(Z)$: 0,682

PGA relativa al cinematisimo nel caso di analisi cinematica lineare: 0,0000 [g]

PGA relativa al cinematisimo nel caso di analisi cinematica non lineare: 0,0000 [g]

Moltiplicatore di collasso dei carichi orizzontali α_0 : -0,063

accelerazione spettrale di attivazione del cinematisimo a_0^* : -0,059 [g]

Massa partecipante al cinematisimo M^* : 13 [kN]

Frazione di massa partecipante della struttura e^* : 0,895

Risultati della verifica con analisi cinematica lineare allo SLD

Accelerazione di riferimento allo SLD (a quota zero): 0,042 [g]

Accelerazione di riferimento allo SLD (a quota diversa da zero): 0,082 [g]

Stato di verifica dell'analisi cinematica lineare allo SLD: **Non Verificato**

Risultati della verifica con analisi cinematica lineare allo SLV

Accelerazione di riferimento allo SLV (a quota zero): 0,039[g]

Accelerazione di riferimento allo SLV (a quota diversa da zero): 0,088 [g]

Stato di verifica dell'analisi cinematica lineare allo SLV: **Non Verificato**

Risultati della verifica con analisi cinematica non lineare allo SLV

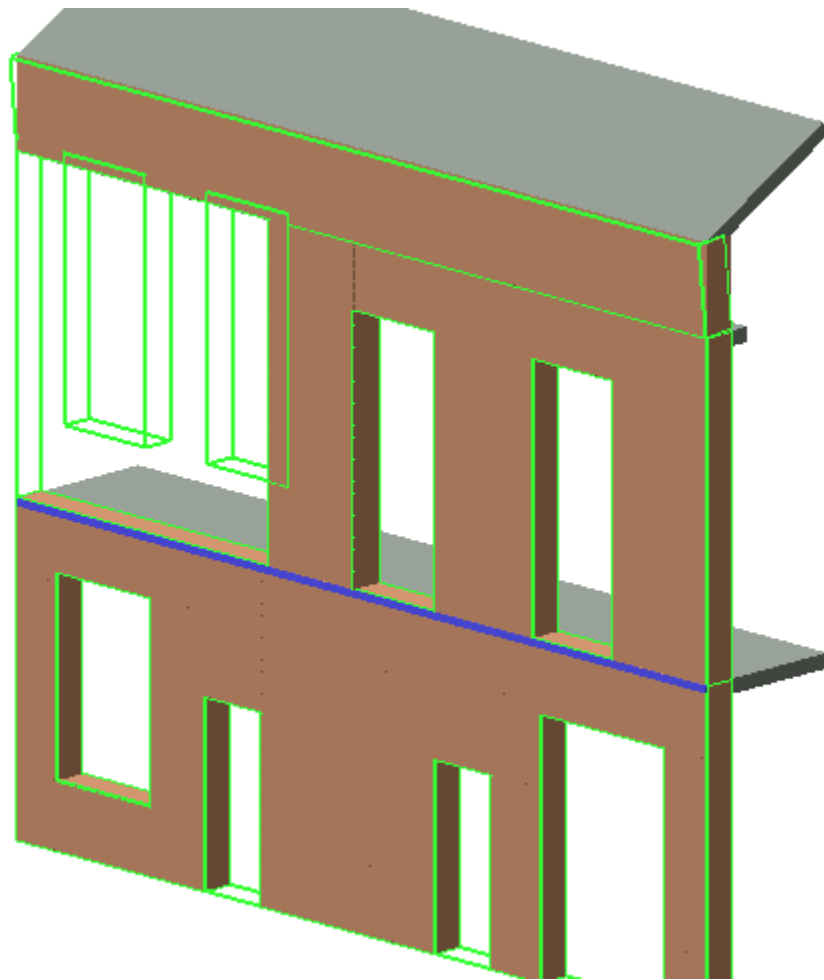
Periodo secante T_s : 0,000[sec]

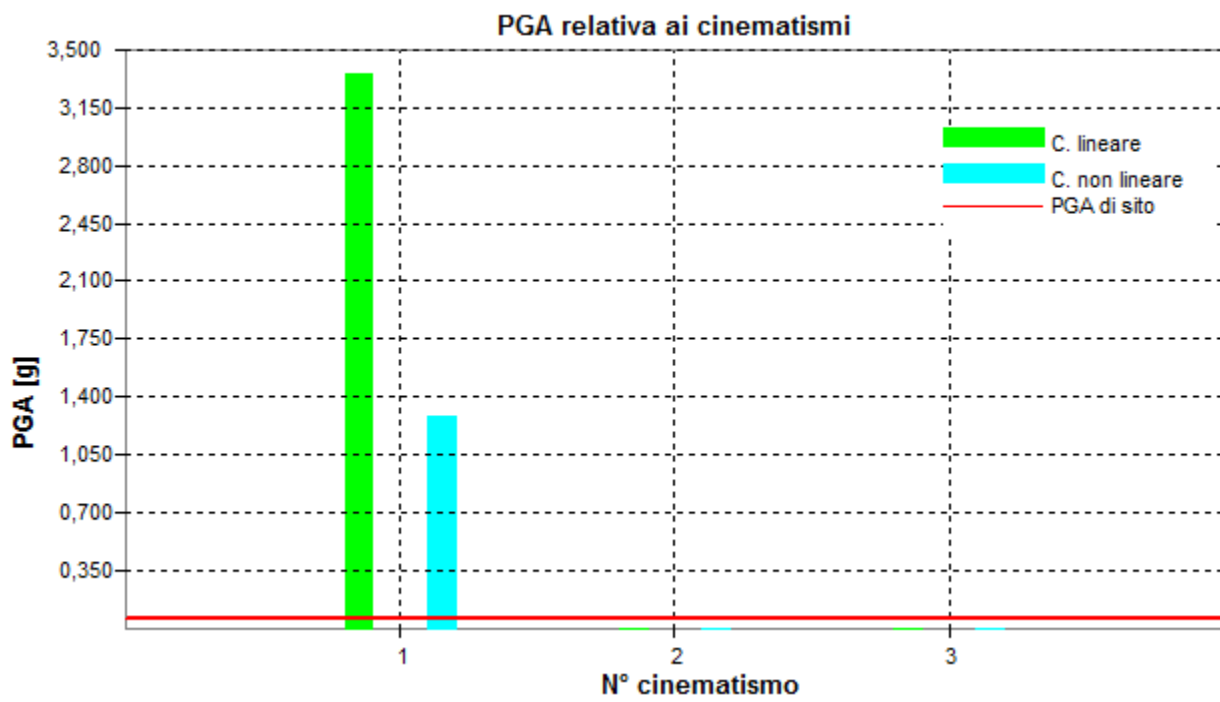
Spostamento spettrale d_u^* : 0,000[m]

Domanda di spostamento nel caso di cinetismo a quota zero $\Delta_{d, \text{ quota zero}}$: 0,000 [m]

Domanda di spostamento nel caso di cinetismo a quota maggiore di zero $\Delta_{d, \text{ quota sopraelev}}$: 0,000 [m]

Stato di verifica dell'analisi cinematica non lineare allo SLV: **Verificato**





Relazione di calcolo Analisi lineare e non lineare dei cinematismi nella muratura

PARETE SUD EST – Stato di fatto

Relazione di calcolo sulla struttura impostata e redatta secondo le modalità previste dal DM 17/01/2018 NTC cap. 10 'Redazione dei progetti strutturali esecutivi e delle relazioni di calcolo'.

Di seguito si indicano l'origine e le caratteristiche dei codici di calcolo utilizzati riportando titolo, produttore e distributore, versione, estremi della licenza d'uso:

Nome del software:

PRO_CINEm Analisi lineare e non lineare dei cinematismi nella muratura

Versione del software:

v. 2018.04.0044b

Produttore del software:

2 S.I. Software e Servizi per l'Ingegneria s.r.l., Ferrara

Distributore del software:

2 S.I. Software e Servizi per l'Ingegneria s.r.l., Ferrara

Dati utente finale:

.....

Normativa di Riferimento

NTC 2018 e Circolare 617 del 2009

Parametri sismici

Località: NOLE (TO)

Altezza totale dell'edificio: 13,00 m

Vita nominale dell'edificio: 50,00 anni

Coefficiente di struttura: 2,00

Periodo del modo per principale di vibrare (T_1): 0,342 sec

Coefficiente di partecipazione modale: γ : 1,20

Categoria di sottosuolo: Tipo B

SLV

Periodo di ritorno per lo SLV (T_r): 712 anni

Probabilità di superamento per lo SLV (P_{ver}): 10 %

Periodo di inizio del tratto a velocità costante per lo SLV (T_{c^*}): 0,280 sec

Accelerazione orizzontale massima al sito per lo SLV (a_g): 0,065 g

Fattore di amplificazione dello spettro in accelerazione orizzontale per lo SLV (F_0): 2,77

Periodo dello spettro T_b : 0,13 sec

Periodo dello spettro T_c : 0,40 sec

Periodo dello spettro T_d : 1,86 sec

Coefficiente di sottosuolo S : 1,20

SLD

Periodo di ritorno per lo SLD (T_r): 75 anni

Probabilità di superamento per lo SLD (P_{ver}): 63 %

Periodo di inizio del tratto a velocità costante per lo SLD (T_c^*): 0,210 sec
Accelerazione orizzontale massima al sito per lo SLD (a_g): 0,035 g
Fattore di amplificazione dello spettro in accelerazione orizzontale per lo SLD (F_0) 2,62
Periodo dello spettro T_b : 0,11 sec
Periodo dello spettro T_c : 0,32 sec
Periodo dello spettro T_d : 1,74 sec
Coefficiente di sottosuolo S : 1,20

Livello di conoscenza e coefficiente di sicurezza

In relazione alle indagini svolte e alla documentazione acquisita il livello di conoscenza è di tipo LC2 (Adeguito), il fattore di confidenza adottato è: 1,20

Nelle verifiche di sicurezza viene considerato un coefficiente di sicurezza sulle proprietà meccaniche pari a: 2

Nel calcolo dei cinematismi viene considerato l'arretramento del punto di contatto tra i blocchi nei seguenti casi:

- Cinematismi di ribaltamento fuori piano
- Cinematismi di flessione verticale
- Cinematismi di flessione orizzontale

Proprietà meccaniche caratteristiche delle pareti e coefficienti correttivi

Parete n°: 1

Tipologia muraria: Muratura in mattoni pieni e malta di calce

Resistenza media a compressione [MPa]: 3,200

Resistenza a taglio [MPa]: 0,076

Peso specifico [kN/mc]: 18,00

Alla muratura della parete n° 1 vengono applicati i seguenti fattori correttivi definiti nella Tab. C8A.2.2 della Circolare 617 del 2009:

- Fattore correttivo dovuto a Malta buona: 1,50
- Fattore correttivo dovuto a Giunti sottili: 1,50
- Fattore correttivo dovuto a Connessione trasversale: 1,30

Fattore correttivo complessivo delle proprietà meccaniche: 2,93

Parete n°: 2

Tipologia muraria: Muratura in mattoni pieni e malta di calce

Resistenza media a compressione [MPa]: 3,200

Resistenza a taglio [MPa]: 0,076

Peso specifico [kN/mc]: 18,00

Alla muratura della parete n° 2 vengono applicati i seguenti fattori correttivi definiti nella Tab. C8A.2.2 della Circolare 617 del 2009:

- Fattore correttivo dovuto a Malta buona: 1,50
- Fattore correttivo dovuto a Giunti sottili: 1,50
- Fattore correttivo dovuto a Connessione trasversale: 1,30

Fattore correttivo complessivo delle proprietà meccaniche: 2,93

Parete n°: 3

Tipologia muraria: Muratura in mattoni pieni e malta di calce

Resistenza media a compressione [MPa]: 3,200

Resistenza a taglio [MPa]: 0,076

Peso specifico [kN/mc]: 18,00

Alla muratura della parete n° 3 vengono applicati i seguenti fattori correttivi definiti nella Tab. C8A.2.2 della Circolare 617 del 2009:

- Fattore correttivo dovuto a Malta buona: 1,50
- Fattore correttivo dovuto a Giunti sottili: 1,50
- Fattore correttivo dovuto a Connessione trasversale: 1,30

Fattore correttivo complessivo delle proprietà meccaniche: 2,93

Parete n°: 4

Tipologia muraria: Muratura in mattoni pieni e malta di calce

Resistenza media a compressione [MPa]: 3,200

Resistenza a taglio [MPa]: 0,076

Peso specifico [kN/mc]: 18,00

Alla muratura della parete n° 4 vengono applicati i seguenti fattori correttivi definiti nella Tab. C8A.2.2 della Circolare 617 del 2009:

- Fattore correttivo dovuto a Malta buona: 1,50

- Fattore correttivo dovuto a Giunti sottili: 1,50

- Fattore correttivo dovuto a Connessione trasversale: 1,30

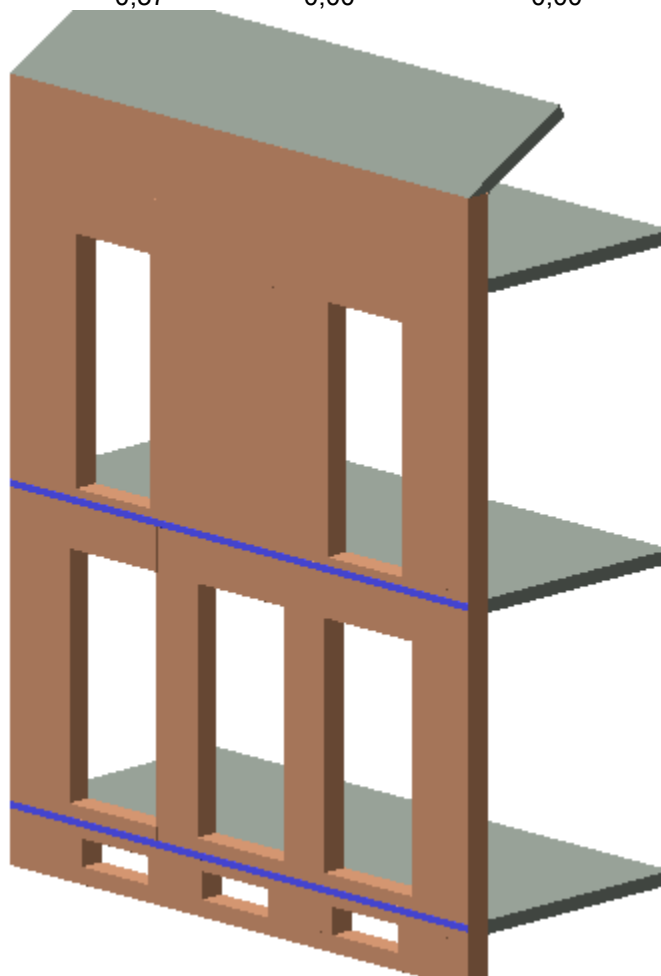
Fattore correttivo complessivo delle proprietà meccaniche: 2,93

Proprietà meccaniche delle pareti, valori di progetto:

n°	γ [kN/m ³]	f_{cd} [MPa]	f_{vd} [MPa]
1	18,00	3,900	0,093
2	18,00	3,900	0,093
3	18,00	3,900	0,093
4	18,00	3,900	0,093

Geometria delle pareti:

n°	Larghezza [m]	Altezza [m]	Spessore [m]	dy_timpano [m]	dz_timpano [m]
1	8,82	0,9	0,37	0,00	0,00
2	8,82	4,5	0,37	0,00	0,00
3	8,82	4,5	0,37	0,00	0,00
4	8,82	1,2	0,37	0,00	0,00



Carichi sulle pareti:

Legenda:

P_p : peso proprio della parete
 G_k : carico permanente gravante sul solaio della parete
 Q_k : carico variabile gravante sul solaio della parete
 φ_2 : carico variabile gravante sul solaio della parete
 i_s : interasse del solaio
 G_{ktemp} : carico permanente gravante sul solaio del timpano
 Q_{ktemp} : carico variabile gravante sul solaio del timpano
 φ_{2temp} : carico variabile gravante sul solaio del timpano
 i_t : interasse del timpano
 G_{kfalda} : carico permanente gravante sul solaio della falda inclinata
 Q_{kfalda} : carico variabile gravante sul solaio della falda inclinata
 φ_{2falda} : carico variabile gravante sul solaio della falda inclinata
 i_f : interasse della falda

n°	P_p [kN]	G_k [kN/m ²]	Q_k [kN/m ²]	φ_2	i_s [m]	G_{ktemp} [kN/m ²]	Q_{ktemp} [kN/m ²]	φ_{2temp}	i_t [m]	G_{kfalda} [kN/m ²]	Q_{kfalda} [kN/m ²]	φ_{2falda}	i_f [m]
1	43,30	4,40	3,00	0,60	3,70	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
2	145,13	5,90	3,00	0,60	3,70	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
3	196,83	3,00	0,05	0,00	3,70	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
4	71,66	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	1,20	1,90	0,00	2,00

Carichi sulle pareti ortogonali:**Legenda:**

G_{korto} : carico permanente gravante sul solaio delle pareti ortogonali
 Q_{korto} : carico variabile gravante sul solaio delle pareti ortogonali
 φ_{2orto} : carico variabile gravante sul solaio delle pareti ortogonali

n°:	G_{korto} [kN/m ²]	Q_{korto} [kN/m ²]	φ_{2orto}
1	6,40	3,00	0,60
2	3,10	0,50	0,00
3	3,10	0,50	0,00
4	3,10	0,50	0,00

Cinematismi:**Cinematismo n°: 1**

Tipo: Fles. Verticale singola

Pareti coinvolte: 1,

Quota: 0,00[m]

PGA relativa al cinematismo nel caso di analisi cinematica lineare: 1238,0350 [g]

PGA relativa al cinematismo nel caso di analisi cinematica non lineare: 1330,9140 [g]

Moltiplicatore di collasso dei carichi orizzontali α_0 : 62,704

accelerazione spettrale di attivazione del cinematismo a_0^* : 742,821 [g]

Massa partecipante al cinematismo M^* : 4 [kN]

Frazione di massa partecipante della struttura e^* : 0,070

Risultati della verifica con analisi cinematica lineare allo SLD

Accelerazione di riferimento allo SLD per cinematismo a quota zero: 0,042 [g]

Stato di verifica dell'analisi cinematica lineare allo SLD: **Verificato**

Risultati della verifica con analisi cinematica lineare allo SLV

Accelerazione di riferimento allo SLV per cinematismo a quota zero: 0,039 [g]

Stato di verifica dell'analisi cinematica lineare allo SLV: **Verificato**

Risultati della verifica con analisi cinematica non lineare allo SLV

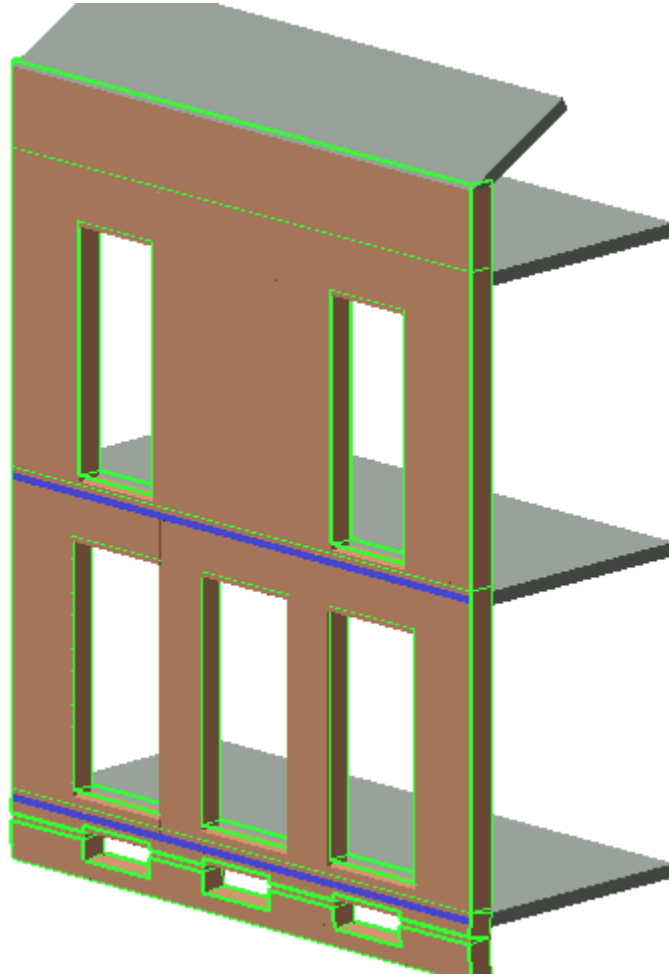
Periodo secante T_s : 0,011[sec]

Spostamento spettrale d_u^* : 0,052[m]

Domanda di spostamento nel caso di cinematismo a quota zero $\Delta_{d, \text{quota zero}}$: 0,000 [m]

Domanda di spostamento nel caso di cinematismo a quota maggiore di zero $\Delta_{d, \text{quota sopraelev}}$: 0,000 [m]

Stato di verifica dell'analisi cinematica non lineare allo SLV: **Verificato**



Cinematismo n°: 2

Tipo: Fles. Verticale singola

Pareti coinvolte: 2,

Quota: 0,91[m]

Primo modo di vibrare normalizzato ad 1 in sommità dell'edificio $\psi(Z)$: 0,070

PGA relativa al cinematismo nel caso di analisi cinematica lineare: 19,1038 [g]

PGA relativa al cinematismo nel caso di analisi cinematica non lineare: 9,3270 [g]

Moltiplicatore di collasso dei carichi orizzontali α_0 : 2,768

accelerazione spettrale di attivazione del cinematismo a_0^* : 11,462 [g]

Massa partecipante al cinematismo M^* : 15 [kN]

Frazione di massa partecipante della struttura e^* : 0,201

Risultati della verifica con analisi cinematica lineare allo SLD

Accelerazione di riferimento allo SLD (a quota zero): 0,042 [g]

Accelerazione di riferimento allo SLD (a quota diversa da zero): 0,008 [g]

Stato di verifica dell'analisi cinematica lineare allo SLD: **Verificato**

Risultati della verifica con analisi cinematica lineare allo SLV

Accelerazione di riferimento allo SLV (a quota zero): 0,039[g]

Accelerazione di riferimento allo SLV (a quota diversa da zero): 0,009 [g]

Stato di verifica dell'analisi cinematica lineare allo SLV: **Verificato**

Risultati della verifica con analisi cinematica non lineare allo SLV

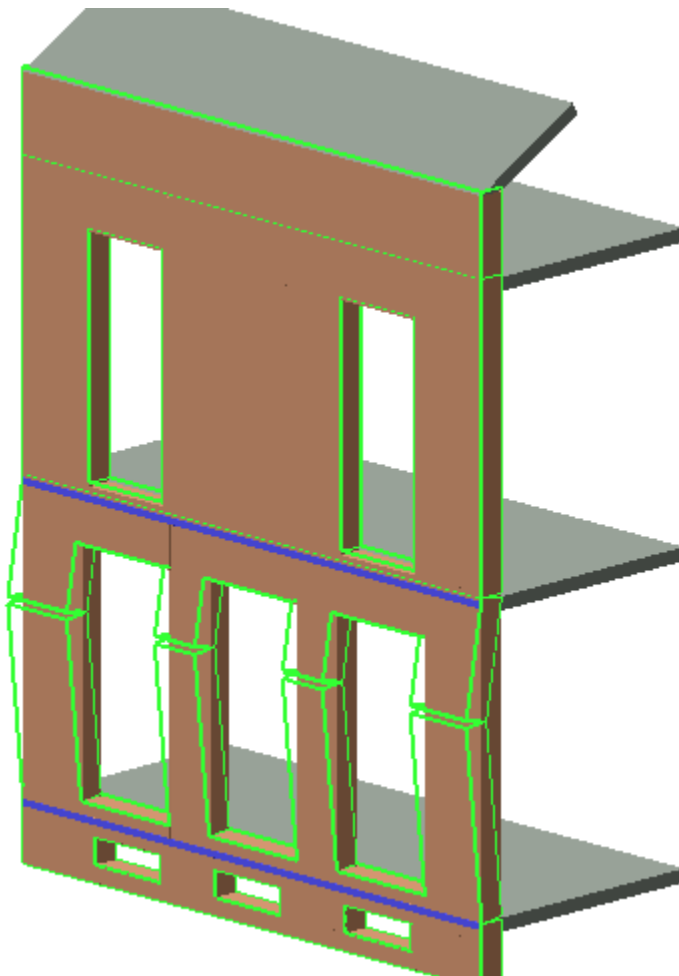
Periodo secante T_s : 0,087[sec]

Spostamento spettrale d_u^* : 0,045[m]

Domanda di spostamento nel caso di cinematismo a quota zero $\Delta_{d, \text{quota zero}}$: 0,000 [m]

Domanda di spostamento nel caso di cinematismo a quota maggiore di zero $\Delta_{d, \text{quota sopraelev}}$: 0,000 [m]

Stato di verifica dell'analisi cinematica non lineare allo SLV: **Verificato**



Cinematismo n°: 3

Tipo: Rib. Multi

Pareti coinvolte: 3, 4,

Quota: 5,45[m]

Primo modo di vibrare normalizzato ad 1 in sommità dell'edificio $\psi(Z)$: 0,419

PGA relativa al cinematismo nel caso di analisi cinematica lineare: 0,0000 [g]
PGA relativa al cinematismo nel caso di analisi cinematica non lineare: 0,0000 [g]

Moltiplicatore di collasso dei carichi orizzontali α_0 : -0,035
accelerazione spettrale di attivazione del cinematismo a_0^* : -0,033 [g]
Massa partecipante al cinematismo M^* : 35 [kN]
Frazione di massa partecipante della struttura e^* : 0,887

Risultati della verifica con analisi cinematica lineare allo SLD

Accelerazione di riferimento allo SLD (a quota zero): 0,042 [g]
Accelerazione di riferimento allo SLD (a quota diversa da zero): 0,051 [g]
Stato di verifica dell'analisi cinematica lineare allo SLD: **Non Verificato**

Risultati della verifica con analisi cinematica lineare allo SLV

Accelerazione di riferimento allo SLV (a quota zero): 0,039[g]
Accelerazione di riferimento allo SLV (a quota diversa da zero): 0,054 [g]
Stato di verifica dell'analisi cinematica lineare allo SLV: **Non Verificato**

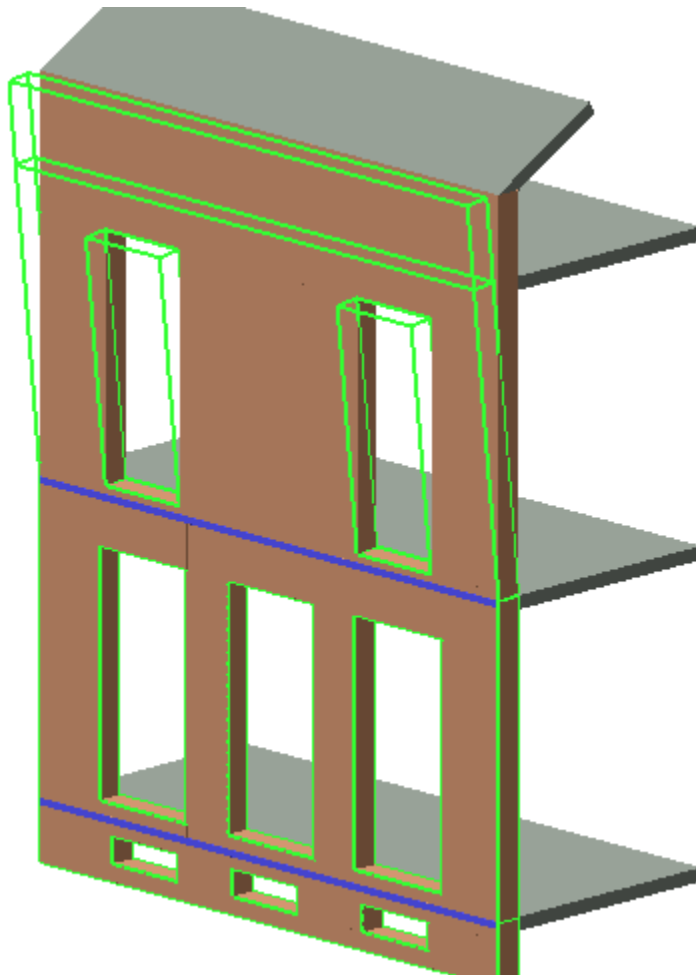
Risultati della verifica con analisi cinematica non lineare allo SLV

Periodo secante T_s : 0,000[sec]
Spostamento spettrale d_u^* : 0,002[m]

Domanda di spostamento nel caso di cinematismo a quota zero $\Delta_{d, \text{quota zero}}$: 0,000 [m]

Domanda di spostamento nel caso di cinematismo a quota maggiore di zero $\Delta_{d, \text{quota sopraelev}}$: 0,000 [m]

Stato di verifica dell'analisi cinematica non lineare allo SLV: **Verificato**



Cinematismo n°: 4

Tipo: Rib. Singolo
Pareti coinvolte: 4,
Quota: 9,96[m]

Primo modo di vibrare normalizzato ad 1 in sommità dell'edificio $\psi(Z)$: 0,766
PGA relativa al cinematismo nel caso di analisi cinematica lineare: 0,0000 [g]
PGA relativa al cinematismo nel caso di analisi cinematica non lineare: 0,0000 [g]

Moltiplicatore di collasso dei carichi orizzontali α_0 : -0,092
accelerazione spettrale di attivazione del cinematismo a_0^* : -0,086 [g]
Massa partecipante al cinematismo M^* : 8 [kN]
Frazione di massa partecipante della struttura e^* : 0,895

Risultati della verifica con analisi cinematica lineare allo SLD

Accelerazione di riferimento allo SLD (a quota zero): 0,042 [g]
Accelerazione di riferimento allo SLD (a quota diversa da zero): 0,092 [g]
Stato di verifica dell'analisi cinematica lineare allo SLD: **Non Verificato**

Risultati della verifica con analisi cinematica lineare allo SLV

Accelerazione di riferimento allo SLV (a quota zero): 0,039[g]
Accelerazione di riferimento allo SLV (a quota diversa da zero): 0,099 [g]
Stato di verifica dell'analisi cinematica lineare allo SLV: **Non Verificato**

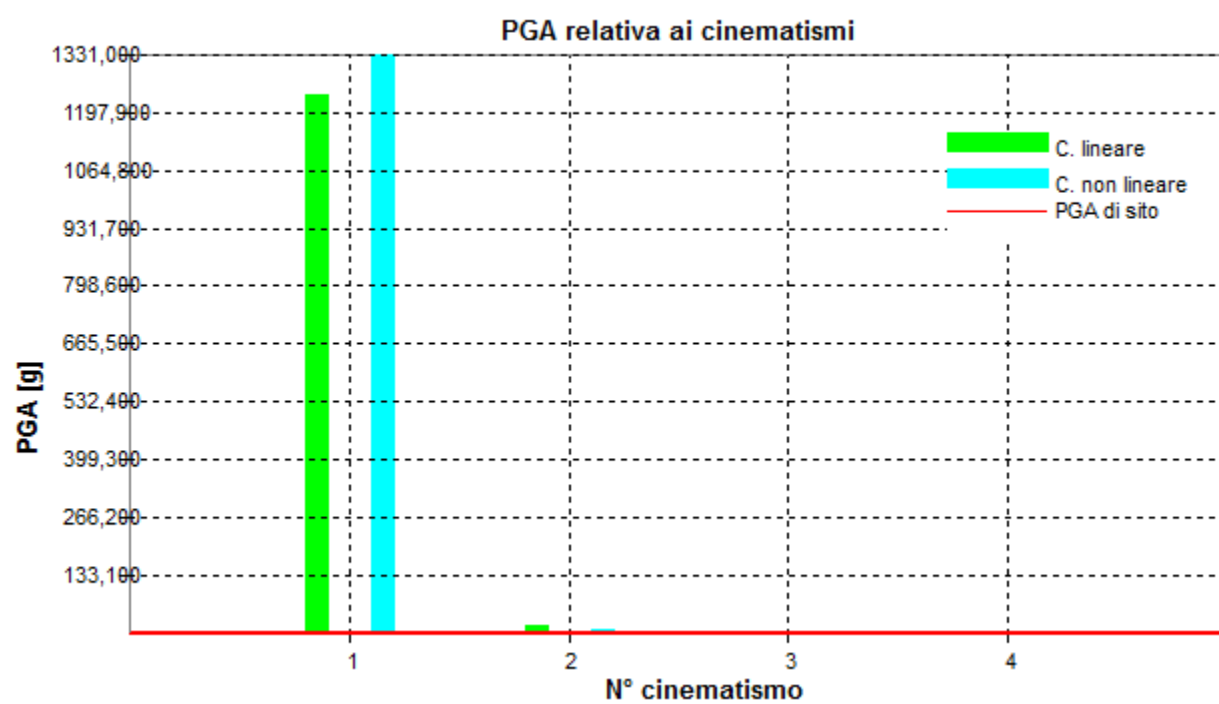
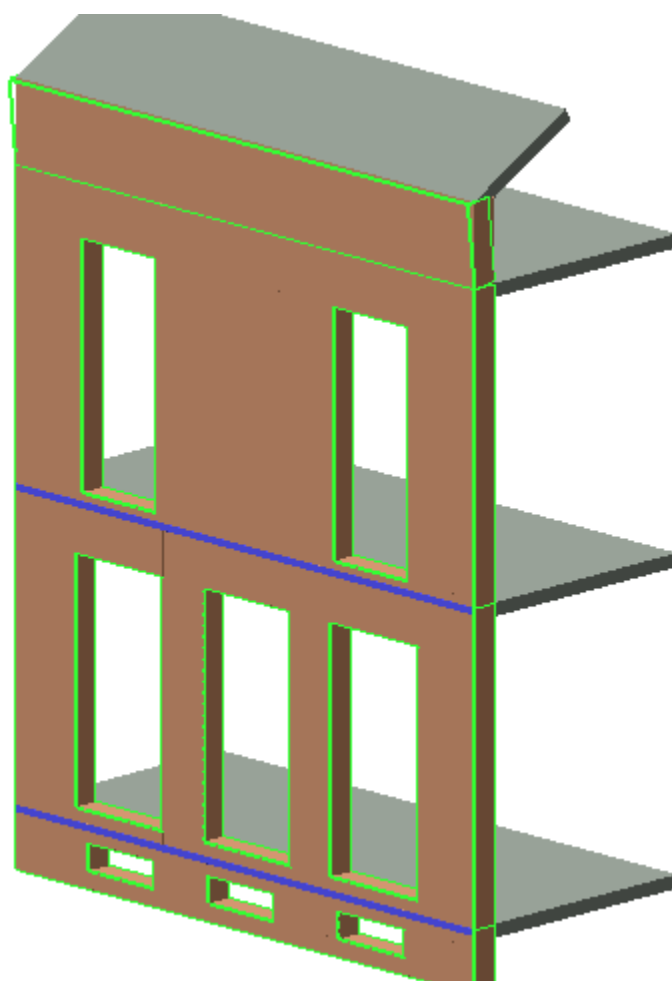
Risultati della verifica con analisi cinematica non lineare allo SLV

Periodo secante T_s : 0,000[sec]
Spostamento spettrale d_u^* : 0,000[m]

Domanda di spostamento nel caso di cinematismo a quota zero $\Delta_{d, \text{quota zero}}$: 0,000 [m]

Domanda di spostamento nel caso di cinematismo a quota maggiore di zero $\Delta_{d, \text{quota sopraelev}}$: 0,000 [m]

Stato di verifica dell'analisi cinematica non lineare allo SLV: **Verificato**



Relazione di calcolo Analisi lineare e non lineare dei cinematismi nella muratura

PARETE SUD EST VANO SCALA – Stato di fatto

Relazione di calcolo sulla struttura impostata e redatta secondo le modalità previste dal DM 17/01/2018 NTC cap. 10 'Redazione dei progetti strutturali esecutivi e delle relazioni di calcolo'.

Di seguito si indicano l'origine e le caratteristiche dei codici di calcolo utilizzati riportando titolo, produttore e distributore, versione, estremi della licenza d'uso:

Nome del software:

PRO_CINEm Analisi lineare e non lineare dei cinematismi nella muratura

Versione del software:

v. 2018.04.0044b

Produttore del software:

2 S.I. Software e Servizi per l'Ingegneria s.r.l., Ferrara

Distributore del software:

2 S.I. Software e Servizi per l'Ingegneria s.r.l., Ferrara

Dati utente finale:

.....

Normativa di Riferimento

NTC 2018 e Circolare 617 del 2009

Parametri sismici

Località: NOLE (TO)

Altezza totale dell'edificio: 13,00 m

Vita nominale dell'edificio: 50,00 anni

Coefficiente di struttura: 2,00

Periodo del modo per principale di vibrare (T1): 0,342 sec

Coefficiente di partecipazione modale: γ : 1,20

Categoria di sottosuolo: Tipo B

SLV

Periodo di ritorno per lo SLV (Tr): 712 anni

Probabilità di superamento per lo SLV (Pver): 10 %

Periodo di inizio del tratto a velocità costante per lo SLV (Tc*): 0,280 sec

Accelerazione orizzontale massima al sito per lo SLV (ag): 0,065 g

Fattore di amplificazione dello spettro in accelerazione orizzontale per lo SLV (F0): 2,77

Periodo dello spettro Tb: 0,13 sec

Periodo dello spettro Tc: 0,40 sec

Periodo dello spettro Td: 1,86 sec

Coefficiente di sottosuolo S: 1,20

SLD

Periodo di ritorno per lo SLD (Tr): 75 anni

Probabilità di superamento per lo SLD (Pver): 63 %

Periodo di inizio del tratto a velocità costante per lo SLD (T_c^*): 0,210 sec
 Accelerazione orizzontale massima al sito per lo SLD (a_g): 0,035 g
 Fattore di amplificazione dello spettro in accelerazione orizzontale per lo SLD (F_0) 2,62
 Periodo dello spettro T_b : 0,11 sec
 Periodo dello spettro T_c : 0,32 sec
 Periodo dello spettro T_d : 1,74 sec
 Coefficiente di sottosuolo S : 1,20

Livello di conoscenza e coefficiente di sicurezza

In relazione alle indagini svolte e alla documentazione acquisita il livello di conoscenza è di tipo LC2 (Adeguito), il fattore di confidenza adottato è: 1,20

Nelle verifiche di sicurezza viene considerato un coefficiente di sicurezza sulle proprietà meccaniche pari a: 2

Nel calcolo dei cinematismi viene considerato l'arretramento del punto di contatto tra i blocchi nei seguenti casi:

- Cinematismi di ribaltamento fuori piano
- Cinematismi di flessione verticale
- Cinematismi di flessione orizzontale

Proprietà meccaniche caratteristiche delle pareti e coefficienti correttivi

Parete n°: 1

Tipologia muraria: Muratura in mattoni semipieni e malta cementizia (es. doppio UNI perc. for.<40%)

Resistenza media a compressione [MPa]: 6,500

Resistenza a taglio [MPa]: 0,280

Peso specifico [kN/mc]: 15,00

Parete n°: 2

Tipologia muraria: Muratura in mattoni semipieni e malta cementizia (es. doppio UNI perc. for.<40%)

Resistenza media a compressione [MPa]: 6,500

Resistenza a taglio [MPa]: 0,280

Peso specifico [kN/mc]: 15,00

Parete n°: 3

Tipologia muraria: Muratura in mattoni semipieni e malta cementizia (es. doppio UNI perc. for.<40%)

Resistenza media a compressione [MPa]: 6,500

Resistenza a taglio [MPa]: 0,280

Peso specifico [kN/mc]: 15,00

Parete n°: 4

Tipologia muraria: Muratura in mattoni semipieni e malta cementizia (es. doppio UNI perc. for.<40%)

Resistenza media a compressione [MPa]: 6,500

Resistenza a taglio [MPa]: 0,280

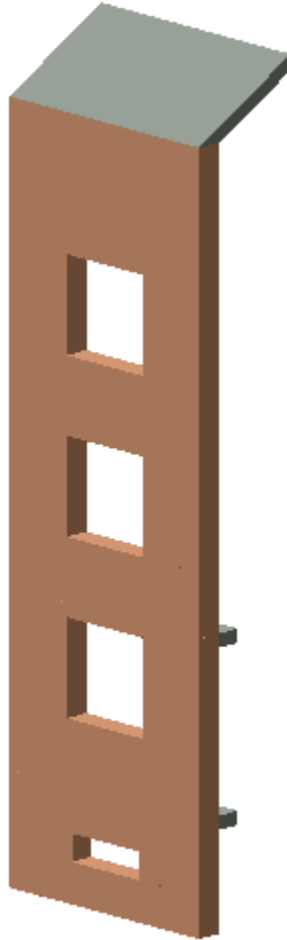
Peso specifico [kN/mc]: 15,00

Proprietà meccaniche delle pareti, valori di progetto:

n°	γ [kN/m ³]	f_{cd} [MPa]	f_{vd} [MPa]
1	15,00	2,708	0,117
2	15,00	2,708	0,117
3	15,00	2,708	0,117
4	15,00	2,708	0,117

Geometria delle pareti:

n°	Larghezza [m]	Altezza [m]	Spessore [m]	dy_timpano [m]	dz_timpano [m]
1	3,63	1,7	0,37	0,00	0,00
2	3,63	2,6	0,37	0,00	0,00
3	3,63	5,7	0,37	0,00	0,00
4	3,63	1,2	0,37	0,00	0,00



Carichi sulle pareti:

Legenda:

P_p : peso proprio della parete

G_k : carico permanente gravante sul solaio della parete

Q_k : carico variabile gravante sul solaio della parete

φ_2 : carico variabile gravante sul solaio della parete

i_s : interasse del solaio

$G_{k\text{timp}}$: carico permanente gravante sul solaio del timpano

$Q_{k\text{timp}}$: carico variabile gravante sul solaio del timpano

$\varphi_{2\text{timp}}$: carico variabile gravante sul solaio del timpano

i_t : interasse del timpano

$G_{k\text{falda}}$: carico permanente gravante sul solaio della falda inclinata

$Q_{k\text{falda}}$: carico variabile gravante sul solaio della falda inclinata

$\varphi_{2\text{falda}}$: carico variabile gravante sul solaio della falda inclinata

i_f : interasse della falda

n°	P_p [kN]	G_k [kN/m ²]	Q_k [kN/m ²]	φ_2	i_s [m]	$G_{k\text{timp}}$ [kN/m ²]	$Q_{k\text{timp}}$ [kN/m ²]	$\varphi_{2\text{timp}}$	i_t [m]	$G_{k\text{falda}}$ [kN/m ²]	$Q_{k\text{falda}}$ [kN/m ²]	$\varphi_{2\text{falda}}$	i_f [m]
1	30,62	5,20	4,00	0,60	0,55	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
2	40,23	5,20	4,00	0,60	0,55	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
3	92,14	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
4	24,18	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	1,20	1,90	0,00	2,00

Carichi sulle pareti ortogonali:

Legenda:

G_{korto} : carico permanente gravante sul solaio delle pareti ortogonali

Q_{korto} : carico variabile gravante sul solaio delle pareti ortogonali

φ_{2orto} : carico variabile gravante sul solaio delle pareti ortogonali

n°:	G_{korto} [kN/m ²]	Q_{korto} [kN/m ²]	φ_{2orto}
1	6,40	3,00	0,60
2	6,40	3,00	0,60
3	6,40	3,00	0,60
4	6,40	3,00	0,60

Cinematismi:**Cinematismo n°: 1**

Tipo: Rib. Multi

Pareti coinvolte: 1, 2, 3, 4,

Quota: 0,00[m]

PGA relativa al cinematismo nel caso di analisi cinematica lineare: 0,0000 [g]

PGA relativa al cinematismo nel caso di analisi cinematica non lineare: 0,0000 [g]

Moltiplicatore di collasso dei carichi orizzontali α_0 : -0,007

accelerazione spettrale di attivazione del cinematismo a_0^* : -0,008 [g]

Massa partecipante al cinematismo M^* : 17 [kN]

Frazione di massa partecipante della struttura e^* : 0,743

Risultati della verifica con analisi cinematica lineare allo SLD

Accelerazione di riferimento allo SLD per cinematismo a quota zero: 0,042 [g]

Stato di verifica dell'analisi cinematica lineare allo SLD: **Non Verificato**

Risultati della verifica con analisi cinematica lineare allo SLV

Accelerazione di riferimento allo SLV per cinematismo a quota zero: 0,039 [g]

Stato di verifica dell'analisi cinematica lineare allo SLV: **Non Verificato**

Risultati della verifica con analisi cinematica non lineare allo SLV

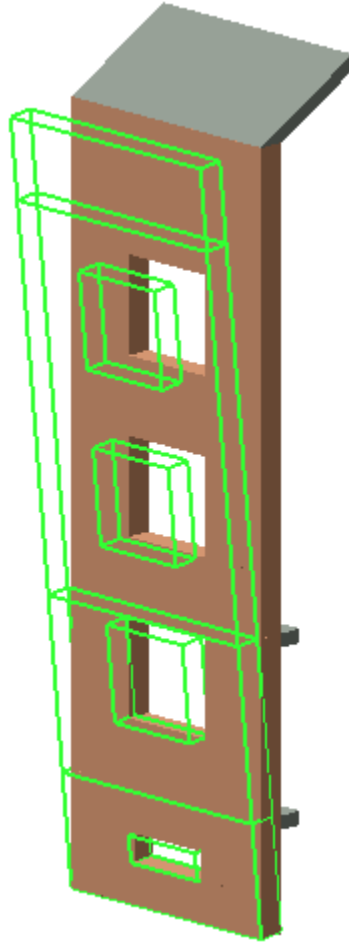
Periodo secante T_s : 0,000[sec]

Spostamento spettrale d_u^* : 0,003[m]

Domanda di spostamento nel caso di cinematismo a quota zero $\Delta_{d, \text{ quota zero}}$: 0,000 [m]

Domanda di spostamento nel caso di cinematismo a quota maggiore di zero $\Delta_{d, \text{ quota sopraelev}}$: 0,000 [m]

Stato di verifica dell'analisi cinematica non lineare allo SLV: **Verificato**



Cinematismo n°: 2

Tipo: Rib. Multi

Pareti coinvolte: 2, 3, 4,

Quota: 1,66[m]

Primo modo di vibrare normalizzato ad 1 in sommità dell'edificio $\Psi(Z)$: 0,128

PGA relativa al cinematismo nel caso di analisi cinematica lineare: 0,0000 [g]

PGA relativa al cinematismo nel caso di analisi cinematica non lineare: 0,0000 [g]

Moltiplicatore di collasso dei carichi orizzontali α_0 : -0,010

accelerazione spettrale di attivazione del cinematismo a_0^* : -0,011 [g]

Massa partecipante al cinematismo M^* : 14 [kN]

Frazione di massa partecipante della struttura e^* : 0,778

Risultati della verifica con analisi cinematica lineare allo SLD

Accelerazione di riferimento allo SLD (a quota zero): 0,042 [g]

Accelerazione di riferimento allo SLD (a quota diversa da zero): 0,015 [g]

Stato di verifica dell'analisi cinematica lineare allo SLD: **Non Verificato**

Risultati della verifica con analisi cinematica lineare allo SLV

Accelerazione di riferimento allo SLV (a quota zero): 0,039[g]

Accelerazione di riferimento allo SLV (a quota diversa da zero): 0,017 [g]

Stato di verifica dell'analisi cinematica lineare allo SLV: **Non Verificato**

Risultati della verifica con analisi cinematica non lineare allo SLV

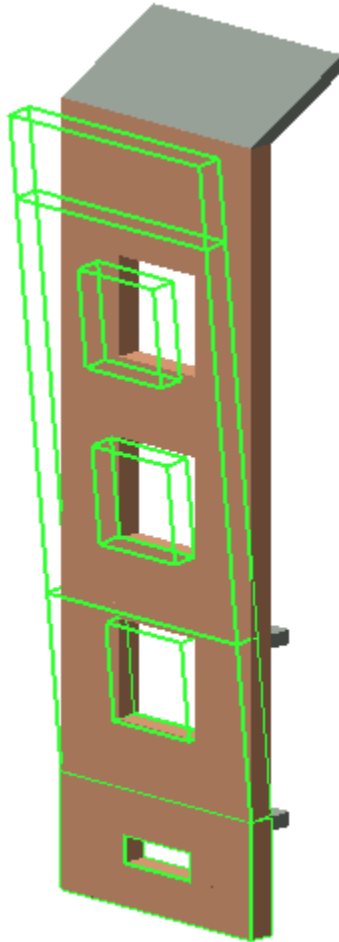
Periodo secante T_s : 0,000[sec]

Spostamento spettrale d_u^* : 0,003[m]

Domanda di spostamento nel caso di cinematisimo a quota zero $\Delta_{d, \text{quota zero}}$: 0,000 [m]

Domanda di spostamento nel caso di cinematisimo a quota maggiore di zero $\Delta_{d, \text{quota sopraelev}}$: 0,000 [m]

Stato di verifica dell'analisi cinematica non lineare allo SLV: **Verificato**



Cinematisimo n°: 3

Tipo: Rib. Multi

Pareti coinvolte: 3, 4,

Quota: 4,22[m]

Primo modo di vibrare normalizzato ad 1 in sommità dell'edificio $\psi(Z)$: 0,325

PGA relativa al cinematisimo nel caso di analisi cinematica lineare: 0,0000 [g]

PGA relativa al cinematisimo nel caso di analisi cinematica non lineare: 0,0000 [g]

Moltiplicatore di collasso dei carichi orizzontali α_0 : -0,015

accelerazione spettrale di attivazione del cinematisimo a_0^* : -0,015 [g]

Massa partecipante al cinematisimo M^* : 11 [kN]

Frazione di massa partecipante della struttura e^* : 0,848

Risultati della verifica con analisi cinematica lineare allo SLD

Accelerazione di riferimento allo SLD (a quota zero): 0,042 [g]

Accelerazione di riferimento allo SLD (a quota diversa da zero): 0,039 [g]

Stato di verifica dell'analisi cinematica lineare allo SLD: **Non Verificato**

Risultati della verifica con analisi cinematica lineare allo SLV

Accelerazione di riferimento allo SLV (a quota zero): 0,039[g]

Accelerazione di riferimento allo SLV (a quota diversa da zero): 0,042 [g]

Stato di verifica dell'analisi cinematica lineare allo SLV: **Non Verificato**

Risultati della verifica con analisi cinematica non lineare allo SLV

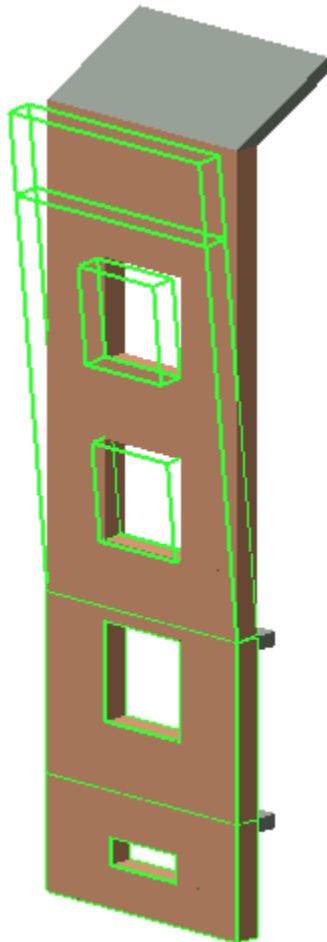
Periodo secante T_s : 0,000[sec]

Spostamento spettrale d_u^* : 0,002[m]

Domanda di spostamento nel caso di cinematismo a quota zero $\Delta_{d, \text{ quota zero}}$: 0,000 [m]

Domanda di spostamento nel caso di cinematismo a quota maggiore di zero $\Delta_{d, \text{ quota sopraelev}}$: 0,000 [m]

Stato di verifica dell'analisi cinematica non lineare allo SLV: **Verificato**



Cinematismo n°: 4

Tipo: Rib. Singolo

Pareti coinvolte: 4,

Quota: 9,92[m]

Primo modo di vibrare normalizzato ad 1 in sommità dell'edificio $\psi(Z)$: 0,763

PGA relativa al cinematismo nel caso di analisi cinematica lineare: 0,0124 [g]

PGA relativa al cinematismo nel caso di analisi cinematica non lineare: 0,0220 [g]

Moltiplicatore di collasso dei carichi orizzontali α_0 : 0,020

accelerazione spettrale di attivazione del cinematismo a_0^* : 0,019 [g]

Massa partecipante al cinematismo M^* : 3 [kN]
Frazione di massa partecipante della struttura e^* : 0,891

Risultati della verifica con analisi cinematica lineare allo SLD

Accelerazione di riferimento allo SLD (a quota zero): 0,042 [g]

Accelerazione di riferimento allo SLD (a quota diversa da zero): 0,092 [g]

Stato di verifica dell'analisi cinematica lineare allo SLD: **Non Verificato**

Risultati della verifica con analisi cinematica lineare allo SLV

Accelerazione di riferimento allo SLV (a quota zero): 0,039[g]

Accelerazione di riferimento allo SLV (a quota diversa da zero): 0,099 [g]

Stato di verifica dell'analisi cinematica lineare allo SLV: **Non Verificato**

Risultati della verifica con analisi cinematica non lineare allo SLV

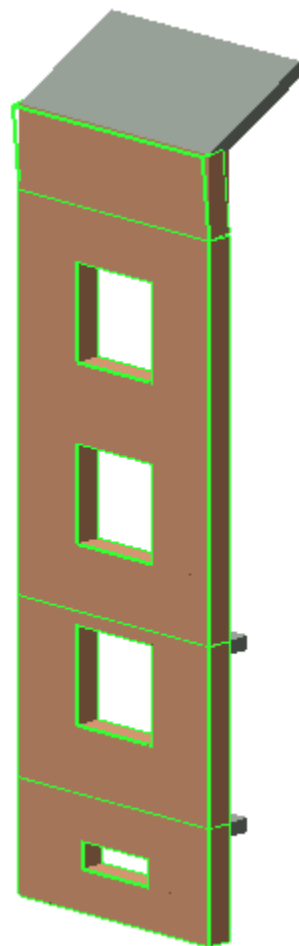
Periodo secante T_s : 0,900[sec]

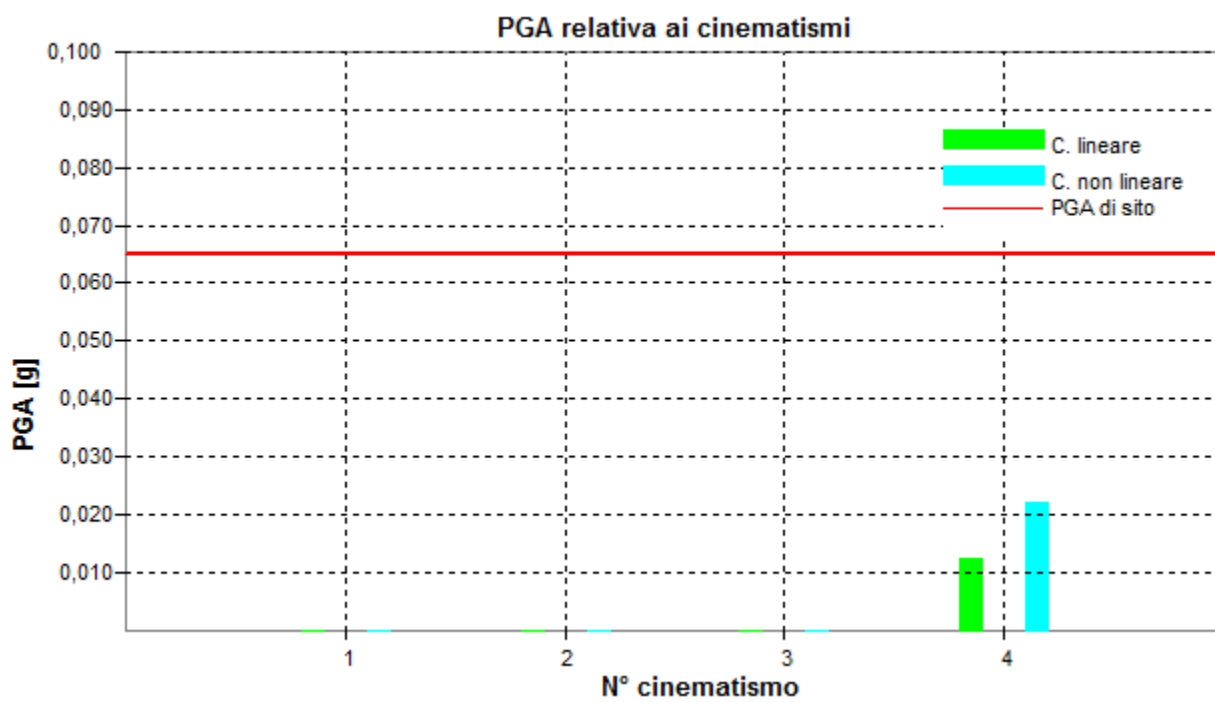
Spostamento spettrale d_u^* : 0,008[m]

Domanda di spostamento nel caso di cinematismo a quota zero $\Delta_{d, \text{quota zero}}$: 0,019 [m]

Domanda di spostamento nel caso di cinematismo a quota maggiore di zero $\Delta_{d, \text{quota sopraelev}}$: 0,024 [m]

Stato di verifica dell'analisi cinematica non lineare allo SLV: **Non Verificato**





Relazione di calcolo Analisi lineare e non lineare dei cinematismi nella muratura

PARETE SUD OVEST – Stato di fatto

Relazione di calcolo sulla struttura impostata e redatta secondo le modalità previste dal DM 17/01/2018 NTC cap. 10 'Redazione dei progetti strutturali esecutivi e delle relazioni di calcolo'.

Di seguito si indicano l'origine e le caratteristiche dei codici di calcolo utilizzati riportando titolo, produttore e distributore, versione, estremi della licenza d'uso:

Nome del software:

PRO_CINEm Analisi lineare e non lineare dei cinematismi nella muratura

Versione del software:

v. 2018.04.0044b

Produttore del software:

2 S.I. Software e Servizi per l'Ingegneria s.r.l., Ferrara

Distributore del software:

2 S.I. Software e Servizi per l'Ingegneria s.r.l., Ferrara

Dati utente finale:

.....

Normativa di Riferimento

NTC 2018 e Circolare 617 del 2009

Parametri sismici

Località: NOLE (TO)

Altezza totale dell'edificio: 13,00 m

Vita nominale dell'edificio: 50,00 anni

Coefficiente di struttura: 2,00

Periodo del modo per principale di vibrare (T1): 0,342 sec

Coefficiente di partecipazione modale: γ : 1,20

Categoria di sottosuolo: Tipo B

SLV

Periodo di ritorno per lo SLV (Tr): 712 anni

Probabilità di superamento per lo SLV (Pver): 10 %

Periodo di inizio del tratto a velocità costante per lo SLV (Tc*): 0,280 sec

Accelerazione orizzontale massima al sito per lo SLV (ag): 0,065 g

Fattore di amplificazione dello spettro in accelerazione orizzontale per lo SLV (F0): 2,77

Periodo dello spettro Tb: 0,13 sec

Periodo dello spettro Tc: 0,40 sec

Periodo dello spettro Td: 1,86 sec

Coefficiente di sottosuolo S: 1,20

SLD

Periodo di ritorno per lo SLD (Tr): 75 anni

Probabilità di superamento per lo SLD (Pver): 63 %

Periodo di inizio del tratto a velocità costante per lo SLD (T_c^*): 0,210 sec
Accelerazione orizzontale massima al sito per lo SLD (a_g): 0,035 g
Fattore di amplificazione dello spettro in accelerazione orizzontale per lo SLD (F_0) 2,62
Periodo dello spettro T_b : 0,11 sec
Periodo dello spettro T_c : 0,32 sec
Periodo dello spettro T_d : 1,74 sec
Coefficiente di sottosuolo S : 1,20

Livello di conoscenza e coefficiente di sicurezza

In relazione alle indagini svolte e alla documentazione acquisita il livello di conoscenza è di tipo LC2 (Adeguate), il fattore di confidenza adottato è: 1,20

Nelle verifiche di sicurezza viene considerato un coefficiente di sicurezza sulle proprietà meccaniche pari a: 2

Nel calcolo dei cinematismi viene considerato l'arretramento del punto di contatto tra i blocchi nei seguenti casi:

- Cinematismi di ribaltamento fuori piano
- Cinematismi di flessione verticale
- Cinematismi di flessione orizzontale

Proprietà meccaniche caratteristiche delle pareti e coefficienti correttivi

Parete n°: 1

Tipologia muraria: Muratura in mattoni pieni e malta di calce

Resistenza media a compressione [MPa]: 3,200

Resistenza a taglio [MPa]: 0,076

Peso specifico [kN/mc]: 18,00

Alla muratura della parete n° 1 vengono applicati i seguenti fattori correttivi definiti nella Tab. C8A.2.2 della Circolare 617 del 2009:

- Fattore correttivo dovuto a Malta buona: 1,50
- Fattore correttivo dovuto a Giunti sottili: 1,50
- Fattore correttivo dovuto a Connessione trasversale: 1,30

Fattore correttivo complessivo delle proprietà meccaniche: 2,93

Parete n°: 2

Tipologia muraria: Muratura in mattoni pieni e malta di calce

Resistenza media a compressione [MPa]: 3,200

Resistenza a taglio [MPa]: 0,076

Peso specifico [kN/mc]: 18,00

Alla muratura della parete n° 2 vengono applicati i seguenti fattori correttivi definiti nella Tab. C8A.2.2 della Circolare 617 del 2009:

- Fattore correttivo dovuto a Malta buona: 1,50
- Fattore correttivo dovuto a Giunti sottili: 1,50
- Fattore correttivo dovuto a Connessione trasversale: 1,30

Fattore correttivo complessivo delle proprietà meccaniche: 2,93

Parete n°: 3

Tipologia muraria: Muratura in mattoni pieni e malta di calce

Resistenza media a compressione [MPa]: 3,200

Resistenza a taglio [MPa]: 0,076

Peso specifico [kN/mc]: 18,00

Alla muratura della parete n° 3 vengono applicati i seguenti fattori correttivi definiti nella Tab. C8A.2.2 della Circolare 617 del 2009:

- Fattore correttivo dovuto a Malta buona: 1,50
- Fattore correttivo dovuto a Giunti sottili: 1,50
- Fattore correttivo dovuto a Connessione trasversale: 1,30

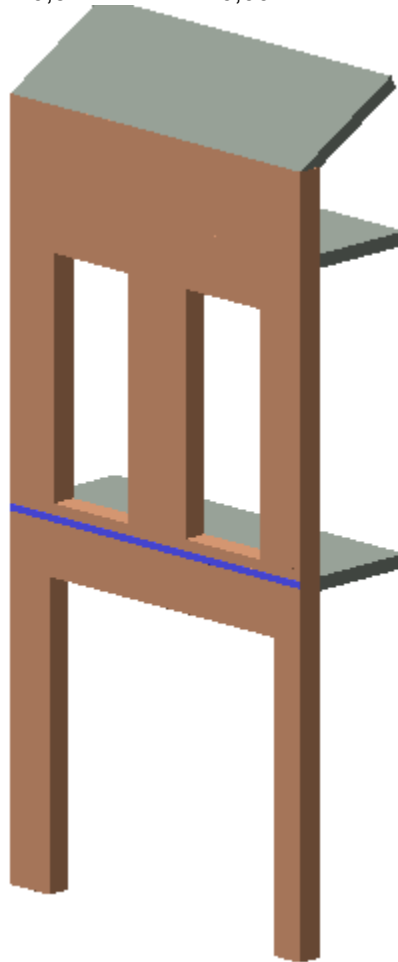
Fattore correttivo complessivo delle proprietà meccaniche: 2,93

Proprietà meccaniche delle pareti, valori di progetto:

n°	γ [kN/m ³]	f_{cd} [MPa]	f_{vd} [MPa]
1	18,00	3,900	0,093
2	18,00	3,900	0,093
3	18,00	3,900	0,093

Geometria delle pareti:

n°	Larghezza [m]	Altezza [m]	Spessore [m]	dy_timpano [m]	dz_timpano [m]
1	5,52	5,3	0,37	0,00	0,00
2	5,52	4,5	0,37	0,00	0,00
3	5,52	1,2	0,37	0,00	0,00



Carichi sulle pareti:

Legenda:

- P_p : peso proprio della parete
- G_k : carico permanente gravante sul solaio della parete
- Q_k : carico variabile gravante sul solaio della parete
- ϕ_2 : carico variabile gravante sul solaio della parete
- i_s : interasse del solaio
- $G_{k\text{timpano}}$: carico permanente gravante sul solaio del timpano
- $Q_{k\text{timpano}}$: carico variabile gravante sul solaio del timpano
- $\phi_{2\text{timpano}}$: carico variabile gravante sul solaio del timpano
- i_t : interasse del timpano
- G_{kfalda} : carico permanente gravante sul solaio della falda inclinata
- Q_{kfalda} : carico variabile gravante sul solaio della falda inclinata

φ_{2fald} : carico variabile gravante sul solaio della falda inclinata
 i_f : interasse della falda

n°	P_P [kN]	G_k [kN/m ²]	Q_k [kN/m ²]	φ_2	i_s [m]	G_{ktemp} [kN/m ²]	Q_{ktemp} [kN/m ²]	φ_{2temp}	i_t [m]	G_{kfalda} [kN/m ²]	Q_{kfalda} [kN/m ²]	φ_{2falda}	i_f [m]
1	69,40	7,75	3,00	0,60	1,80	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
2	99,60	3,00	0,50	0,00	1,80	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
3	44,85	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	1,20	1,90	0,00	2,00

Carichi sulle pareti ortogonali:

Legenda:

G_{korto} : carico permanente gravante sul solaio delle pareti ortogonali

Q_{korto} : carico variabile gravante sul solaio delle pareti ortogonali

φ_{2orto} : carico variabile gravante sul solaio delle pareti ortogonali

n°:	G_{korto} [kN/m ²]	Q_{korto} [kN/m ²]	φ_{2orto}
1	6,40	3,00	0,60
2	6,40	3,00	0,60
3	6,40	3,00	0,60

Cinematismi:

Cinematismo n°: 1

Tipo: Fles. Verticale singola

Pareti coinvolte: 1,

Quota: 0,00[m]

PGA relativa al cinematismo nel caso di analisi cinematica lineare: 10,4438 [g]

PGA relativa al cinematismo nel caso di analisi cinematica non lineare: 4,3580 [g]

Moltiplicatore di collasso dei carichi orizzontali α_0 : 2,426

accelerazione spettrale di attivazione del cinematismo a_0^* : 6,266 [g]

Massa partecipante al cinematismo M^* : 7 [kN]

Frazione di massa partecipante della struttura e^* : 0,323

Risultati della verifica con analisi cinematica lineare allo SLD

Accelerazione di riferimento allo SLD per cinematismo a quota zero: 0,042 [g]

Stato di verifica dell'analisi cinematica lineare allo SLD: **Verificato**

Risultati della verifica con analisi cinematica lineare allo SLV

Accelerazione di riferimento allo SLV per cinematismo a quota zero: 0,039 [g]

Stato di verifica dell'analisi cinematica lineare allo SLV: **Verificato**

Risultati della verifica con analisi cinematica non lineare allo SLV

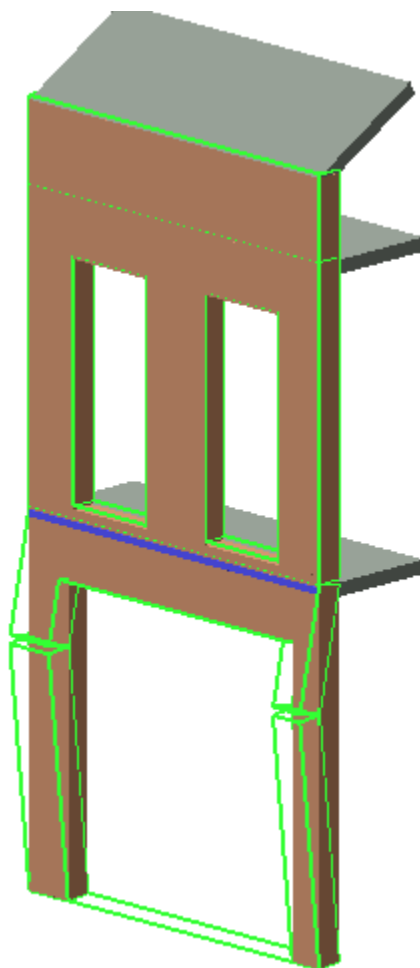
Periodo secante T_s : 0,114[sec]

Spostamento spettrale d_u^* : 0,043[m]

Domanda di spostamento nel caso di cinematismo a quota zero $\Delta_{d, \text{ quota zero}}$: 0,001 [m]

Domanda di spostamento nel caso di cinematismo a quota maggiore di zero $\Delta_{d, \text{ quota sopraelev.}}$: 0,000 [m]

Stato di verifica dell'analisi cinematica non lineare allo SLV: **Verificato**



Cinematismo n°: 2

Tipo: Rib. Multi

Pareti coinvolte: 2, 3,

Quota: 5,33[m]

Primo modo di vibrare normalizzato ad 1 in sommità dell'edificio $\Psi(Z)$: 0,410

PGA relativa al cinematismo nel caso di analisi cinematica lineare: 0,0000 [g]

PGA relativa al cinematismo nel caso di analisi cinematica non lineare: 0,0000 [g]

Moltiplicatore di collasso dei carichi orizzontali α_0 : -0,057

accelerazione spettrale di attivazione del cinematismo a_0^* : -0,053 [g]

Massa partecipante al cinematismo M^* : 17 [kN]

Frazione di massa partecipante della struttura e^* : 0,890

Risultati della verifica con analisi cinematica lineare allo SLD

Accelerazione di riferimento allo SLD (a quota zero): 0,042 [g]

Accelerazione di riferimento allo SLD (a quota diversa da zero): 0,049 [g]

Stato di verifica dell'analisi cinematica lineare allo SLD: **Non Verificato**

Risultati della verifica con analisi cinematica lineare allo SLV

Accelerazione di riferimento allo SLV (a quota zero): 0,039[g]

Accelerazione di riferimento allo SLV (a quota diversa da zero): 0,053 [g]

Stato di verifica dell'analisi cinematica lineare allo SLV: **Non Verificato**

Risultati della verifica con analisi cinematica non lineare allo SLV

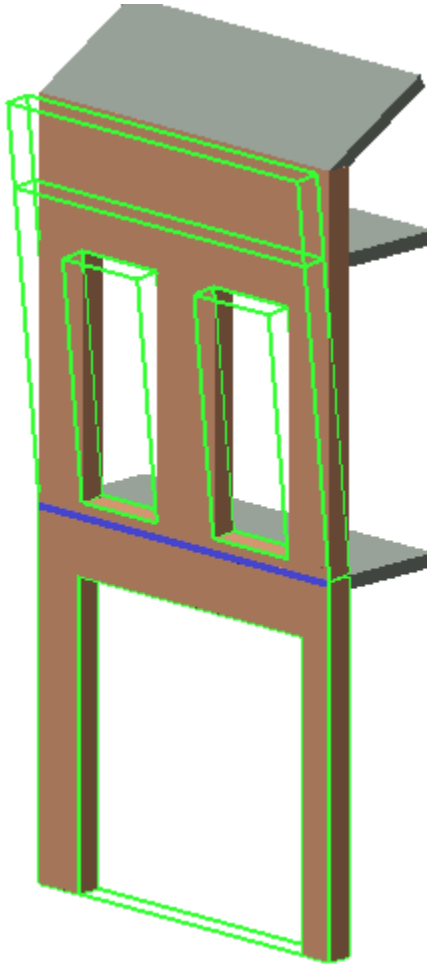
Periodo secante T_s : 0,000[sec]

Spostamento spettrale d_u^* : 0,002[m]

Domanda di spostamento nel caso di cinematismo a quota zero $\Delta_{d, \text{quota zero}}$: 0,000 [m]

Domanda di spostamento nel caso di cinematismo a quota maggiore di zero $\Delta_{d, \text{quota sopraelev}}$: 0,000 [m]

Stato di verifica dell'analisi cinematica non lineare allo SLV: **Verificato**



Cinematismo n°: 3

Tipo: Rib. Singolo

Pareti coinvolte: 3,

Quota: 9,84[m]

Primo modo di vibrare normalizzato ad 1 in sommità dell'edificio $\psi(Z)$: 0,757

PGA relativa al cinematismo nel caso di analisi cinematica lineare: 0,0000 [g]

PGA relativa al cinematismo nel caso di analisi cinematica non lineare: 0,0000 [g]

Moltiplicatore di collasso dei carichi orizzontali α_0 : -0,099

accelerazione spettrale di attivazione del cinematismo a_0^* : -0,092 [g]

Massa partecipante al cinematismo M^* : 5 [kN]

Frazione di massa partecipante della struttura e^* : 0,895

Risultati della verifica con analisi cinematica lineare allo SLD

Accelerazione di riferimento allo SLD (a quota zero): 0,042 [g]

Accelerazione di riferimento allo SLD (a quota diversa da zero): 0,091 [g]

Stato di verifica dell'analisi cinematica lineare allo SLD: **Non Verificato**

Risultati della verifica con analisi cinematica lineare allo SLV

Accelerazione di riferimento allo SLV (a quota zero): 0,039[g]

Accelerazione di riferimento allo SLV (a quota diversa da zero): 0,098 [g]

Stato di verifica dell'analisi cinematica lineare allo SLV: **Non Verificato**

Risultati della verifica con analisi cinematica non lineare allo SLV

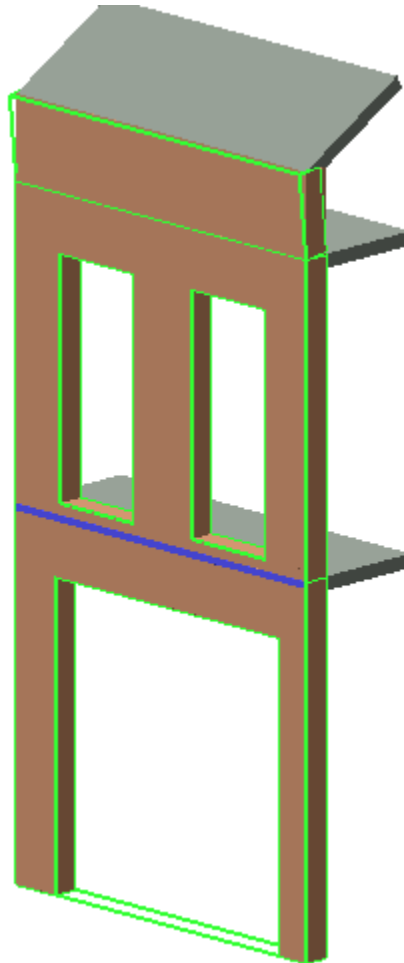
Periodo secante T_s : 0,000[sec]

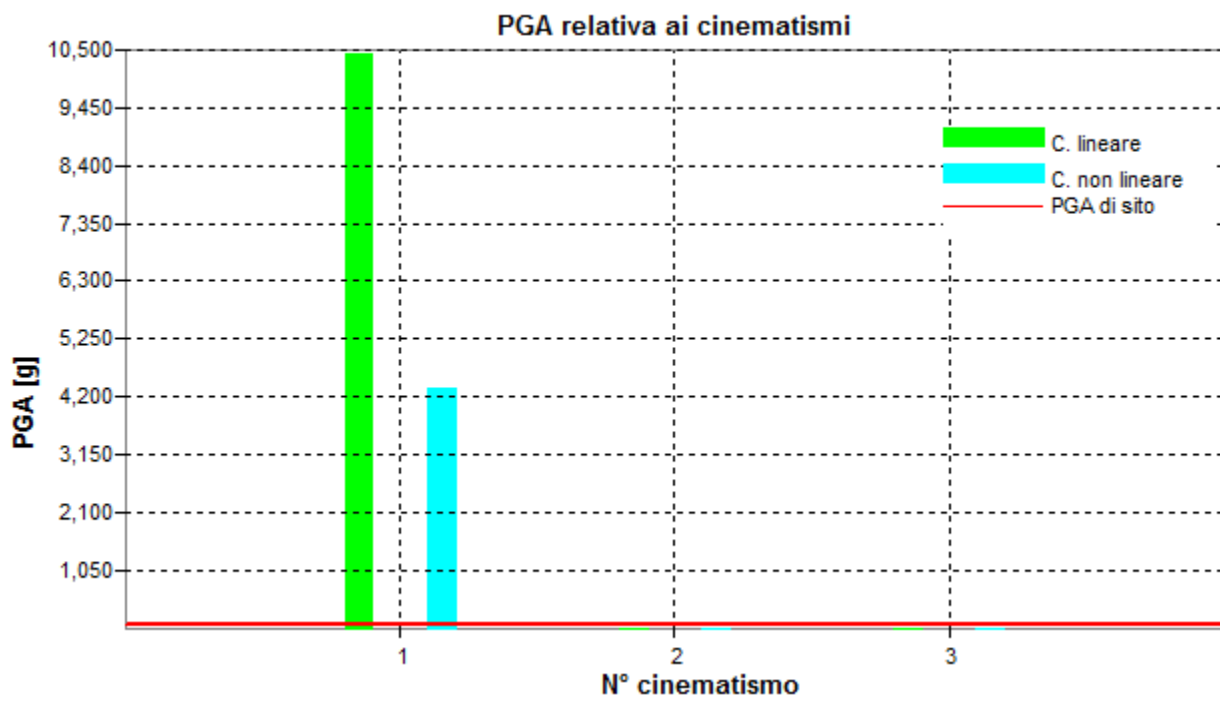
Spostamento spettrale d_u^* : 0,000[m]

Domanda di spostamento nel caso di cinematismo a quota zero $\Delta_{d, \text{ quota zero}}$: 0,000 [m]

Domanda di spostamento nel caso di cinematismo a quota maggiore di zero $\Delta_{d, \text{ quota sopraelev}}$: 0,000 [m]

Stato di verifica dell'analisi cinematica non lineare allo SLV: **Verificato**





Relazione di calcolo Analisi lineare e non lineare dei cinematismi nella muratura

PARETE SUD OVEST VANO SCALA – Stato di fatto

Relazione di calcolo sulla struttura impostata e redatta secondo le modalità previste dal DM 17/01/2018 NTC cap. 10 'Redazione dei progetti strutturali esecutivi e delle relazioni di calcolo'.

Di seguito si indicano l'origine e le caratteristiche dei codici di calcolo utilizzati riportando titolo, produttore e distributore, versione, estremi della licenza d'uso:

Nome del software:

PRO_CINEm Analisi lineare e non lineare dei cinematismi nella muratura

Versione del software:

v. 2018.04.0044b

Produttore del software:

2 S.I. Software e Servizi per l'Ingegneria s.r.l., Ferrara

Distributore del software:

2 S.I. Software e Servizi per l'Ingegneria s.r.l., Ferrara

Dati utente finale:

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Normativa di Riferimento

NTC 2018 e Circolare 617 del 2009

Parametri sismici

Località: NOLE (TO)

Altezza totale dell'edificio: 13,00 m

Vita nominale dell'edificio: 50,00 anni

Coefficiente di struttura: 2,00

Periodo del modo per principale di vibrare (T_1): 0,342 sec

Coefficiente di partecipazione modale: γ : 1,20

Categoria di sottosuolo: Tipo B

SLV

Periodo di ritorno per lo SLV (T_r): 712 anni

Probabilità di superamento per lo SLV (P_{ver}): 10 %

Periodo di inizio del tratto a velocità costante per lo SLV (T_{c^*}): 0,280 sec

Accelerazione orizzontale massima al sito per lo SLV (a_g): 0,065 g

Fattore di amplificazione dello spettro in accelerazione orizzontale per lo SLV (F_0): 2,77

Periodo dello spettro T_b : 0,13 sec

Periodo dello spettro T_c : 0,40 sec

Periodo dello spettro T_d : 1,86 sec

Coefficiente di sottosuolo S : 1,20

SLD

Periodo di ritorno per lo SLD (T_r): 75 anni

Probabilità di superamento per lo SLD (P_{ver}): 63 %

Periodo di inizio del tratto a velocità costante per lo SLD (T_c^*): 0,210 sec
 Accelerazione orizzontale massima al sito per lo SLD (a_g): 0,035 g
 Fattore di amplificazione dello spettro in accelerazione orizzontale per lo SLD (F_0) 2,62
 Periodo dello spettro T_b : 0,11 sec
 Periodo dello spettro T_c : 0,32 sec
 Periodo dello spettro T_d : 1,74 sec
 Coefficiente di sottosuolo S : 1,20

Livello di conoscenza e coefficiente di sicurezza

In relazione alle indagini svolte e alla documentazione acquisita il livello di conoscenza è di tipo LC2 (Adeguate), il fattore di confidenza adottato è: 1,20

Nelle verifiche di sicurezza viene considerato un coefficiente di sicurezza sulle proprietà meccaniche pari a: 2

Nel calcolo dei cinematismi viene considerato l'arretramento del punto di contatto tra i blocchi nei seguenti casi:

- Cinematismi di ribaltamento fuori piano
- Cinematismi di flessione verticale
- Cinematismi di flessione orizzontale

Proprietà meccaniche caratteristiche delle pareti e coefficienti correttivi

Parete n°: 1

Tipologia muraria: Muratura in mattoni semipieni e malta cementizia (es. doppio UNI perc. for.<40%)

Resistenza media a compressione [MPa]: 6,500

Resistenza a taglio [MPa]: 0,280

Peso specifico [kN/mc]: 15,00

Parete n°: 2

Tipologia muraria: Muratura in mattoni semipieni e malta cementizia (es. doppio UNI perc. for.<40%)

Resistenza media a compressione [MPa]: 6,500

Resistenza a taglio [MPa]: 0,280

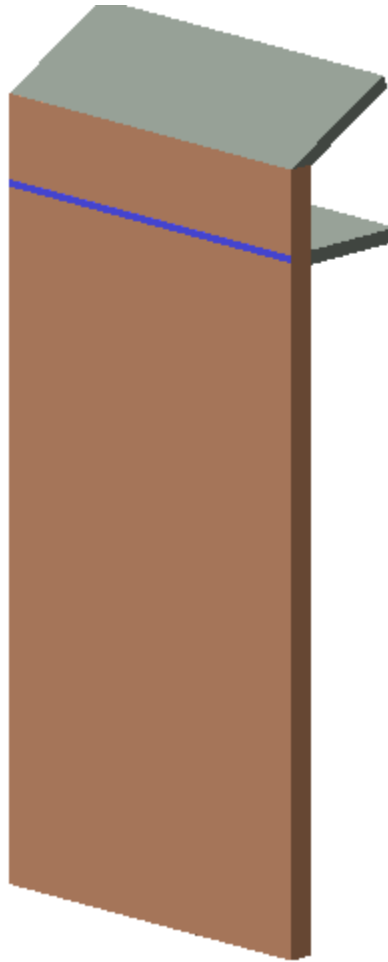
Peso specifico [kN/mc]: 15,00

Proprietà meccaniche delle pareti, valori di progetto:

n°	γ [kN/m ³]	f_{cd} [MPa]	f_{vd} [MPa]
1	15,00	2,708	0,117
2	15,00	2,708	0,117

Geometria delle pareti:

n°	Larghezza [m]	Altezza [m]	Spessore [m]	$d_{y_timpano}$ [m]	$d_{z_timpano}$ [m]
1	5,36	9,9	0,37	0,00	0,00
2	5,36	1,2	0,37	0,00	0,00



Carichi sulle pareti:

Legenda:

P_p : peso proprio della parete
 G_k : carico permanente gravante sul solaio della parete
 Q_k : carico variabile gravante sul solaio della parete
 φ_2 : carico variabile gravante sul solaio della parete
 i_s : interasse del solaio
 $G_{k\text{timp}}$: carico permanente gravante sul solaio del timpano
 $Q_{k\text{timp}}$: carico variabile gravante sul solaio del timpano
 $\varphi_{2\text{timp}}$: carico variabile gravante sul solaio del timpano
 i_t : interasse del timpano
 $G_{k\text{falda}}$: carico permanente gravante sul solaio della falda inclinata
 $Q_{k\text{falda}}$: carico variabile gravante sul solaio della falda inclinata
 $\varphi_{2\text{falda}}$: carico variabile gravante sul solaio della falda inclinata
 i_f : interasse della falda

n°	P_p [kN]	G_k [kN/m ²]	Q_k [kN/m ²]	φ_2	i_s [m]	$G_{k\text{timp}}$ [kN/m ²]	$Q_{k\text{timp}}$ [kN/m ²]	$\varphi_{2\text{timp}}$	i_t [m]	$G_{k\text{falda}}$ [kN/m ²]	$Q_{k\text{falda}}$ [kN/m ²]	$\varphi_{2\text{falda}}$	i_f [m]
1	293,02	3,70	0,50	0,00	1,80	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
2	35,70	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	1,20	1,90	0,00	2,00

Carichi sulle pareti ortogonali:

Legenda:

G_{korto} : carico permanente gravante sul solaio delle pareti ortogonali

Q_{korto} : carico variabile gravante sul solaio delle pareti ortogonali

φ_{2orto} : carico variabile gravante sul solaio delle pareti ortogonali

n°:	G_{korto} [kN/m ²]	Q_{korto} [kN/m ²]	φ_{2orto}
1	6,40	3,00	0,60
2	6,40	3,00	0,60

Cinematismi:

Cinematismo n°: 1

Tipo: Fles. Verticale singola

Pareti coinvolte: 1,

Quota: 0,00[m]

PGA relativa al cinematismo nel caso di analisi cinematica lineare: 0,2554 [g]

PGA relativa al cinematismo nel caso di analisi cinematica non lineare: 0,1998 [g]

Moltiplicatore di collasso dei carichi orizzontali α_0 : 0,158

accelerazione spettrale di attivazione del cinematismo a_0^* : 0,153 [g]

Massa partecipante al cinematismo M^* : 30 [kN]

Frazione di massa partecipante della struttura e^* : 0,858

Risultati della verifica con analisi cinematica lineare allo SLD

Accelerazione di riferimento allo SLD per cinematismo a quota zero: 0,042 [g]

Stato di verifica dell'analisi cinematica lineare allo SLD: **Verificato**

Risultati della verifica con analisi cinematica lineare allo SLV

Accelerazione di riferimento allo SLV per cinematismo a quota zero: 0,039 [g]

Stato di verifica dell'analisi cinematica lineare allo SLV: **Verificato**

Risultati della verifica con analisi cinematica non lineare allo SLV

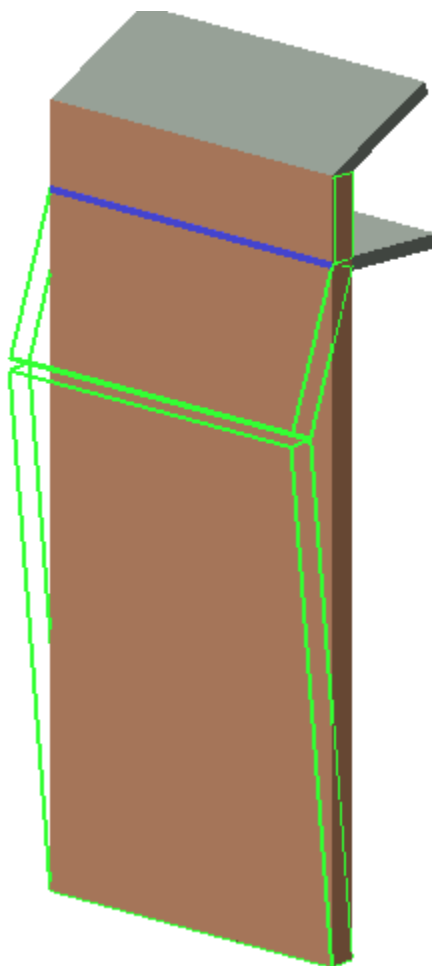
Periodo secante T_s : 0,819[sec]

Spostamento spettrale d_u^* : 0,054[m]

Domanda di spostamento nel caso di cinematismo a quota zero $\Delta_{d, \text{ quota zero}}$: 0,017 [m]

Domanda di spostamento nel caso di cinematismo a quota maggiore di zero $\Delta_{d, \text{ quota sopraelev}}$: 0,000 [m]

Stato di verifica dell'analisi cinematica non lineare allo SLV: **Verificato**



Cinematismo n°: 2

Tipo: Rib. Singolo
 Pareti coinvolte: 2,
 Quota: 9,85[m]

Primo modo di vibrare normalizzato ad 1 in sommità dell'edificio $\Psi(Z)$: 0,758
 PGA relativa al cinematismo nel caso di analisi cinematica lineare: 0,0000 [g]
 PGA relativa al cinematismo nel caso di analisi cinematica non lineare: 0,0000 [g]

Moltiplicatore di collasso dei carichi orizzontali α_0 : -0,127
 accelerazione spettrale di attivazione del cinematismo a_0^* : -0,119 [g]
 Massa partecipante al cinematismo M^* : 4 [kN]
 Frazione di massa partecipante della struttura e^* : 0,891

Risultati della verifica con analisi cinematica lineare allo SLD

Accelerazione di riferimento allo SLD (a quota zero): 0,042 [g]
 Accelerazione di riferimento allo SLD (a quota diversa da zero): 0,091 [g]
 Stato di verifica dell'analisi cinematica lineare allo SLD: **Non Verificato**

Risultati della verifica con analisi cinematica lineare allo SLV

Accelerazione di riferimento allo SLV (a quota zero): 0,039[g]
 Accelerazione di riferimento allo SLV (a quota diversa da zero): 0,098 [g]
 Stato di verifica dell'analisi cinematica lineare allo SLV: **Non Verificato**

Risultati della verifica con analisi cinematica non lineare allo SLV

Periodo secante T_s : 0,000[sec]

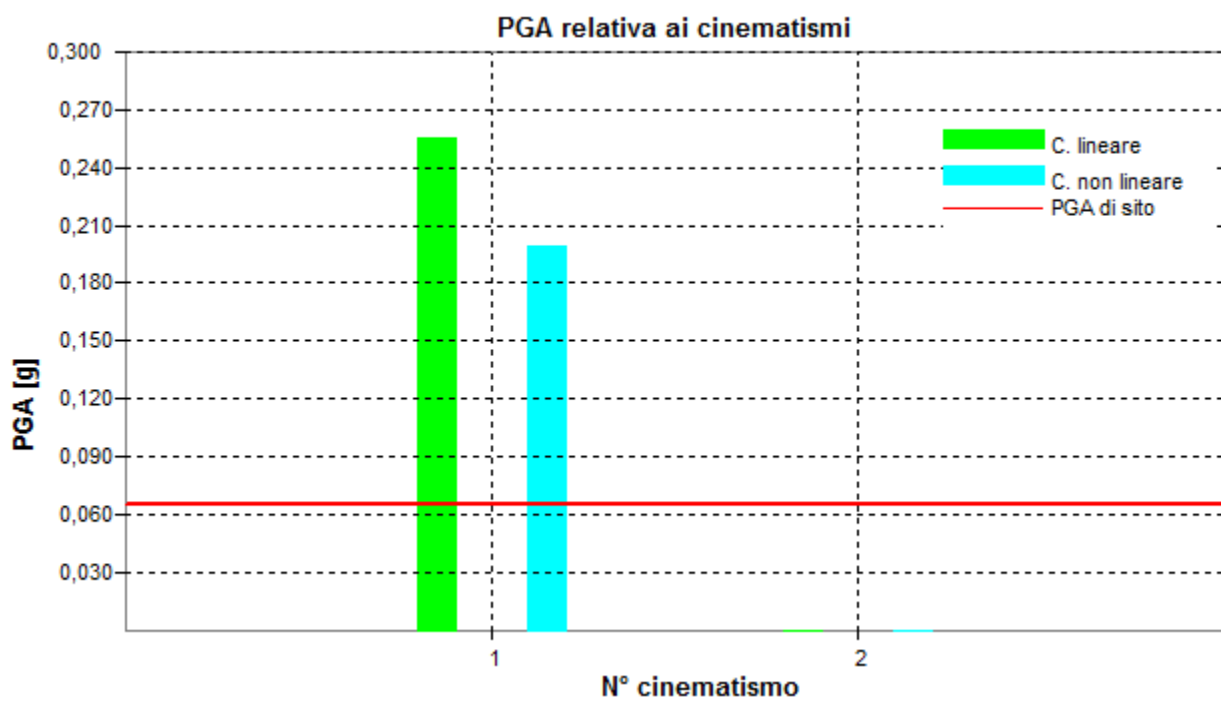
Spostamento spettrale d_u^* : 0,000[m]

Domanda di spostamento nel caso di cinematisimo a quota zero $\Delta_{d, \text{ quota zero}}$: 0,000 [m]

Domanda di spostamento nel caso di cinematisimo a quota maggiore di zero $\Delta_{d, \text{ quota sopraelev}}$: 0,000 [m]

Stato di verifica dell'analisi cinematica non lineare allo SLV: **Verificato**





Relazione di calcolo Analisi lineare e non lineare dei cinematismi nella muratura

PARETE NORD EST – Consolidata con intonaco armato e fascia FRP sommitale

Relazione di calcolo sulla struttura impostata e redatta secondo le modalità previste dal DM 17/01/2018 NTC cap. 10 'Redazione dei progetti strutturali esecutivi e delle relazioni di calcolo'.

Di seguito si indicano l'origine e le caratteristiche dei codici di calcolo utilizzati riportando titolo, produttore e distributore, versione, estremi della licenza d'uso:

Nome del software:

PRO_CINEm Analisi lineare e non lineare dei cinematismi nella muratura

Versione del software:

v. 2018.04.0044b

Produttore del software:

2 S.I. Software e Servizi per l'Ingegneria s.r.l., Ferrara

Distributore del software:

2 S.I. Software e Servizi per l'Ingegneria s.r.l., Ferrara

Dati utente finale:

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Normativa di Riferimento

NTC 2018 e Circolare 617 del 2009

Parametri sismici

Località: NOLE (TO)

Altezza totale dell'edificio: 13,00 m

Vita nominale dell'edificio: 50,00 anni

Coefficiente di struttura: 2,00

Periodo del modo per principale di vibrare (T1): 0,342 sec

Coefficiente di partecipazione modale: γ : 1,20

Categoria di sottosuolo: Tipo B

SLV

Periodo di ritorno per lo SLV (Tr): 712 anni

Probabilità di superamento per lo SLV (Pver): 10 %

Periodo di inizio del tratto a velocità costante per lo SLV (Tc*): 0,280 sec

Accelerazione orizzontale massima al sito per lo SLV (ag): 0,065 g

Fattore di amplificazione dello spettro in accelerazione orizzontale per lo SLV (F0): 2,77

Periodo dello spettro Tb: 0,13 sec

Periodo dello spettro Tc: 0,40 sec

Periodo dello spettro Td: 1,86 sec

Coefficiente di sottosuolo S: 1,20

SLD

Periodo di ritorno per lo SLD (Tr): 75 anni

Probabilità di superamento per lo SLD (Pver): 63 %

Periodo di inizio del tratto a velocità costante per lo SLD (T_c^*): 0,210 sec
 Accelerazione orizzontale massima al sito per lo SLD (a_g): 0,035 g
 Fattore di amplificazione dello spettro in accelerazione orizzontale per lo SLD (F_0) 2,62
 Periodo dello spettro T_b : 0,11 sec
 Periodo dello spettro T_c : 0,32 sec
 Periodo dello spettro T_d : 1,74 sec
 Coefficiente di sottosuolo S : 1,20

Livello di conoscenza e coefficiente di sicurezza

In relazione alle indagini svolte e alla documentazione acquisita il livello di conoscenza è di tipo LC2 (Adeguito), il fattore di confidenza adottato è: 1,20

Nelle verifiche di sicurezza viene considerato un coefficiente di sicurezza sulle proprietà meccaniche pari a: 2

Nel calcolo dei cinematismi viene considerato l'arretramento del punto di contatto tra i blocchi nei seguenti casi:

- Cinematismi di ribaltamento fuori piano
- Cinematismi di flessione verticale
- Cinematismi di flessione orizzontale

Proprietà meccaniche caratteristiche delle pareti e coefficienti correttivi

Parete n°: 1

Tipologia muraria: Muratura in mattoni pieni e malta di calce

Resistenza media a compressione [MPa]: 3,200

Resistenza a taglio [MPa]: 0,076

Peso specifico [kN/mc]: 18,00

Parete n°: 2

Tipologia muraria: Muratura in mattoni semipieni e malta cementizia (es. doppio UNI perc. for.<40%)

Resistenza media a compressione [MPa]: 6,500

Resistenza a taglio [MPa]: 0,280

Peso specifico [kN/mc]: 15,00

Parete n°: 3

Tipologia muraria: Muratura in mattoni semipieni e malta cementizia (es. doppio UNI perc. for.<40%)

Resistenza media a compressione [MPa]: 6,500

Resistenza a taglio [MPa]: 0,280

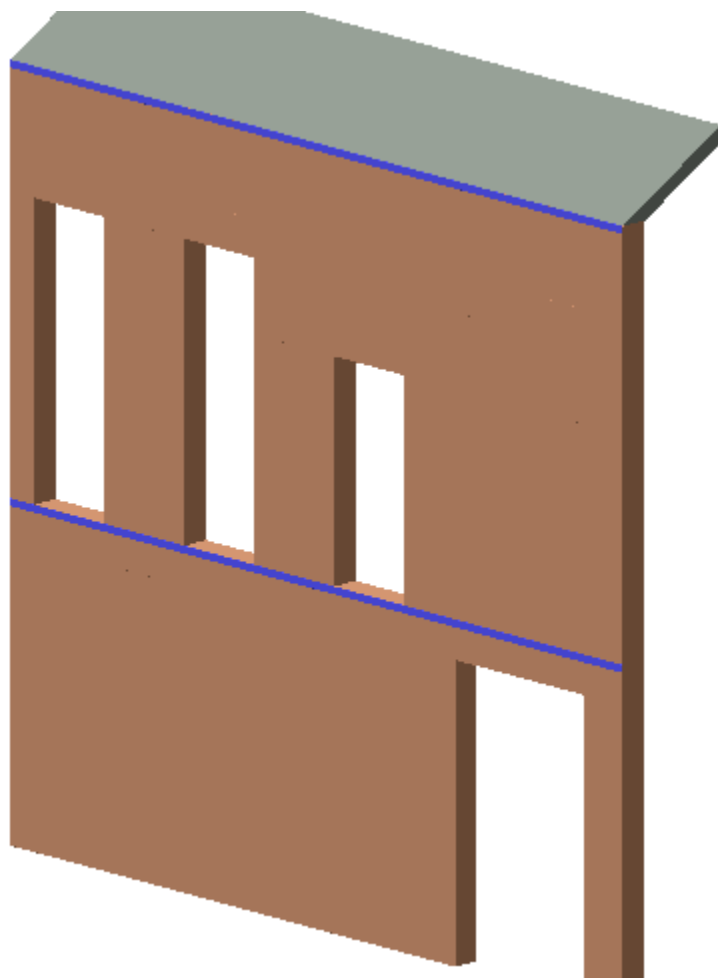
Peso specifico [kN/mc]: 15,00

Proprietà meccaniche delle pareti, valori di progetto:

n°	γ [kN/m ³]	f_{cd} [MPa]	f_{vd} [MPa]
1	18,00	1,333	0,032
2	15,00	2,708	0,117
3	15,00	2,708	0,117

Geometria delle pareti:

n°	Larghezza [m]	Altezza [m]	Spessore [m]	$dy_{timpano}$ [m]	$dz_{timpano}$ [m]
1	10,88	4,5	0,37	0,00	0,00
2	10,88	4,5	0,37	0,00	0,00
3	10,88	1,2	0,37	0,00	0,00



Carichi sulle pareti:

Legenda:

P_p : peso proprio della parete

G_k : carico permanente gravante sul solaio della parete

Q_k : carico variabile gravante sul solaio della parete

φ_2 : carico variabile gravante sul solaio della parete

i_s : interasse del solaio

$G_{k\text{timp}}$: carico permanente gravante sul solaio del timpano

$Q_{k\text{timp}}$: carico variabile gravante sul solaio del timpano

$\varphi_{2\text{timp}}$: carico variabile gravante sul solaio del timpano

i_t : interasse del timpano

$G_{k\text{falda}}$: carico permanente gravante sul solaio della falda inclinata

$Q_{k\text{falda}}$: carico variabile gravante sul solaio della falda inclinata

$\varphi_{2\text{falda}}$: carico variabile gravante sul solaio della falda inclinata

i_f : interasse della falda

n°	P_p [kN]	G_k [kN/m ²]	Q_k [kN/m ²]	φ_2	i_s [m]	$G_{k\text{timp}}$ [kN/m ²]	$Q_{k\text{timp}}$ [kN/m ²]	$\varphi_{2\text{timp}}$	i_t [m]	$G_{k\text{falda}}$ [kN/m ²]	$Q_{k\text{falda}}$ [kN/m ²]	$\varphi_{2\text{falda}}$	i_f [m]
1	267,51	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
2	196,03	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
3	73,67	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	1,20	1,90	0,00	2,00

Carichi sulle pareti ortogonali:

Legenda:

G_{korto} : carico permanente gravante sul solaio delle pareti ortogonali

Q_{korto} : carico variabile gravante sul solaio delle pareti ortogonali

φ_{2orto} : carico variabile gravante sul solaio delle pareti ortogonali

n°:	G_{korto} [kN/m ²]	Q_{korto} [kN/m ²]	φ_{2orto}
1	6,40	3,00	0,60
2	6,40	3,00	0,60
3	6,40	3,00	0,60

Cinematismi:**Cinematismo n°: 1**

Tipo: Fles. Verticale singola

Pareti coinvolte: 1,

Quota: 0,00[m]

PGA relativa al cinematismo nel caso di analisi cinematica lineare: 1,1894 [g]

PGA relativa al cinematismo nel caso di analisi cinematica non lineare: 0,4510 [g]

Moltiplicatore di collasso dei carichi orizzontali α_0 : 0,780

accelerazione spettrale di attivazione del cinematismo a_0^* : 0,714 [g]

Massa partecipante al cinematismo M^* : 27 [kN]

Frazione di massa partecipante della struttura e^* : 0,910

Risultati della verifica con analisi cinematica lineare allo SLD

Accelerazione di riferimento allo SLD per cinematismo a quota zero: 0,042 [g]

Stato di verifica dell'analisi cinematica lineare allo SLD: **Verificato**

Risultati della verifica con analisi cinematica lineare allo SLV

Accelerazione di riferimento allo SLV per cinematismo a quota zero: 0,039 [g]

Stato di verifica dell'analisi cinematica lineare allo SLV: **Verificato**

Risultati della verifica con analisi cinematica non lineare allo SLV

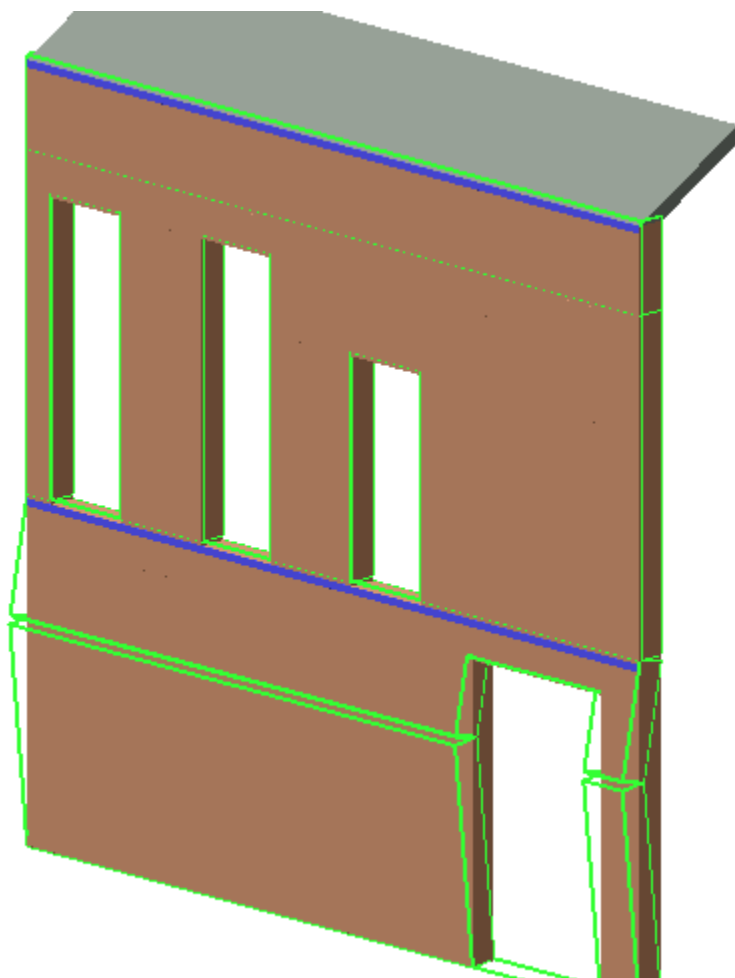
Periodo secante T_s : 0,374[sec]

Spostamento spettrale d_u^* : 0,052[m]

Domanda di spostamento nel caso di cinematismo a quota zero $\Delta_{d, \text{ quota zero}}$: 0,007 [m]

Domanda di spostamento nel caso di cinematismo a quota maggiore di zero $\Delta_{d, \text{ quota sopraelev.}}$: 0,000 [m]

Stato di verifica dell'analisi cinematica non lineare allo SLV: **Verificato**



Cinematismo n°: 2

Tipo: Fles. Verticale multi

Pareti coinvolte: 2, 3,

Quota: 4,53[m]

Primo modo di vibrare normalizzato ad 1 in sommità dell'edificio $\Psi(Z)$: 0,348

PGA relativa al cinematismo nel caso di analisi cinematica lineare: 0,0913 [g]

PGA relativa al cinematismo nel caso di analisi cinematica non lineare: 0,1620 [g]

Moltiplicatore di collasso dei carichi orizzontali α_0 : 0,069

accelerazione spettrale di attivazione del cinematismo a_0^* : 0,063 [g]

Massa partecipante al cinematismo M^* : 28 [kN]

Frazione di massa partecipante della struttura e^* : 0,912

Risultati della verifica con analisi cinematica lineare allo SLD

Accelerazione di riferimento allo SLD (a quota zero): 0,042 [g]

Accelerazione di riferimento allo SLD (a quota diversa da zero): 0,042 [g]

Stato di verifica dell'analisi cinematica lineare allo SLD: **Verificato**

Risultati della verifica con analisi cinematica lineare allo SLV

Accelerazione di riferimento allo SLV (a quota zero): 0,039[g]

Accelerazione di riferimento allo SLV (a quota diversa da zero): 0,045 [g]

Stato di verifica dell'analisi cinematica lineare allo SLV: **Verificato**

Risultati della verifica con analisi cinematica non lineare allo SLV

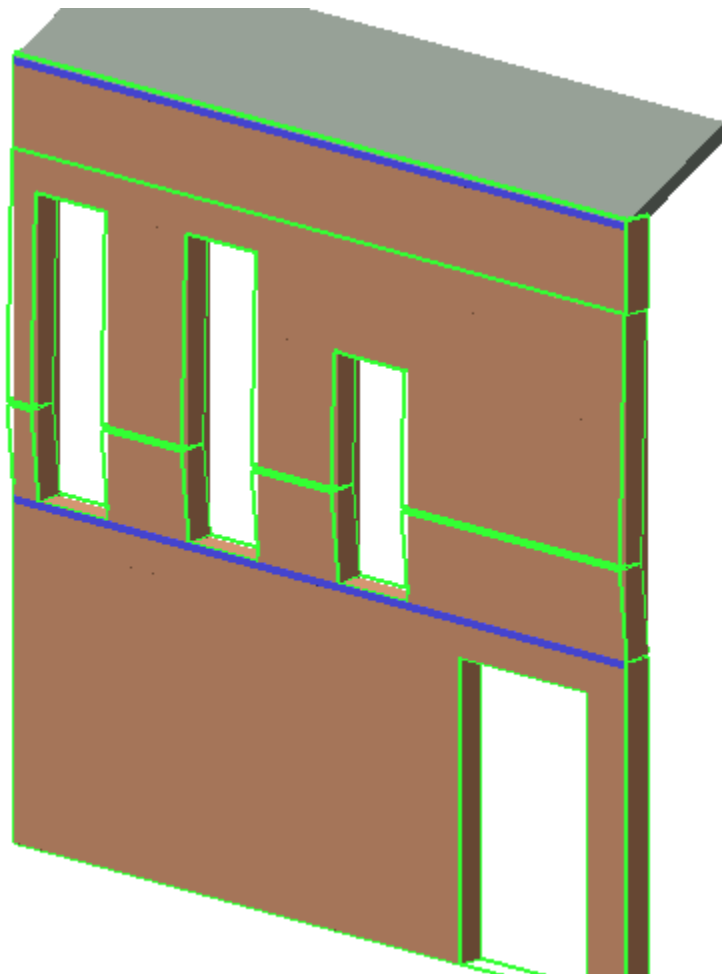
Periodo secante T_s : 1,612[sec]

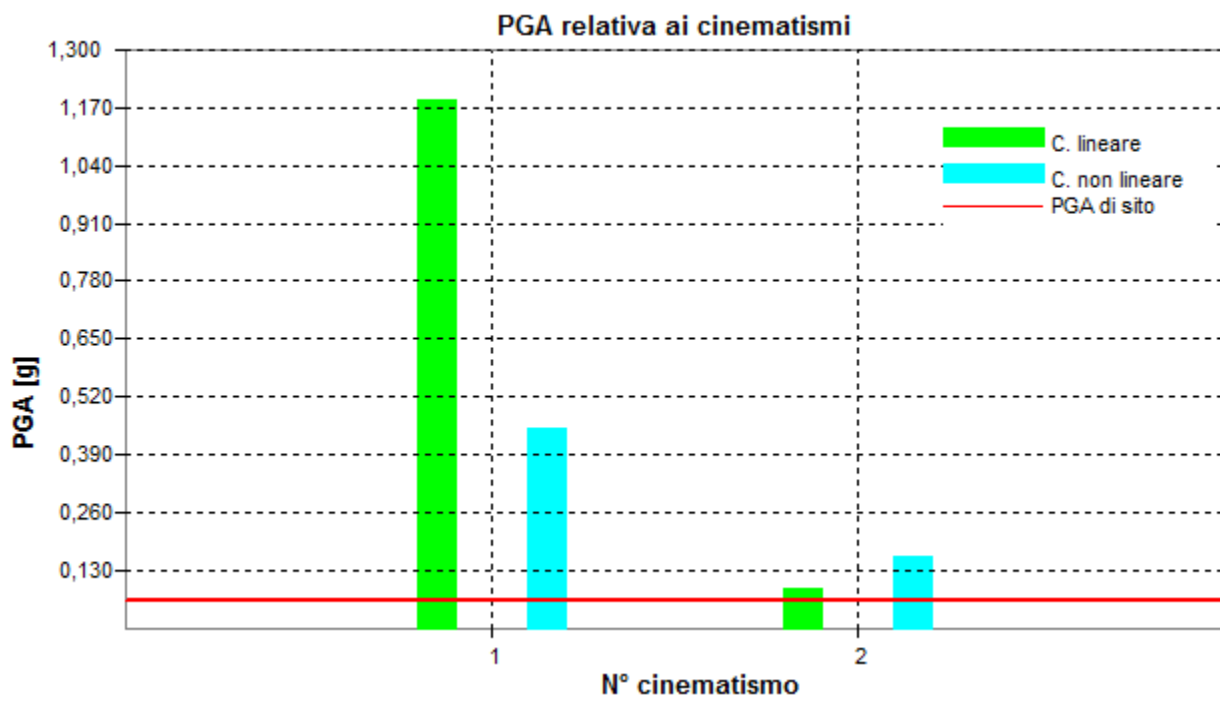
Spostamento spettrale d_u^* : 0,086[m]

Domanda di spostamento nel caso di cinematiso a quota zero $\Delta_{d, \text{ quota zero}}$: 0,034 [m]

Domanda di spostamento nel caso di cinematiso a quota maggiore di zero $\Delta_{d, \text{ quota sopraelev}}$: 0,016 [m]

Stato di verifica dell'analisi cinematica non lineare allo SLV: **Verificato**





Relazione di calcolo Analisi lineare e non lineare dei cinematismi nella muratura

PARETE NORD OVEST – Consolidata con fascia FRP sommitale

Relazione di calcolo sulla struttura impostata e redatta secondo le modalità previste dal DM 17/01/2018 NTC cap. 10 'Redazione dei progetti strutturali esecutivi e delle relazioni di calcolo'.

Di seguito si indicano l'origine e le caratteristiche dei codici di calcolo utilizzati riportando titolo, produttore e distributore, versione, estremi della licenza d'uso:

Nome del software:

PRO_CINEm Analisi lineare e non lineare dei cinematismi nella muratura

Versione del software:

v. 2018.04.0044b

Produttore del software:

2 S.I. Software e Servizi per l'Ingegneria s.r.l., Ferrara

Distributore del software:

2 S.I. Software e Servizi per l'Ingegneria s.r.l., Ferrara

Dati utente finale:

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Normativa di Riferimento

NTC 2018 e Circolare 617 del 2009

Parametri sismici

Località: NOLE (TO)

Altezza totale dell'edificio: 13,00 m

Vita nominale dell'edificio: 100,00 anni

Coefficiente di struttura: 2,00

Periodo del modo per principale di vibrare (T1): 0,342 sec

Coefficiente di partecipazione modale: γ : 1,20

Categoria di sottosuolo: Tipo B

SLV

Periodo di ritorno per lo SLV (Tr): 1424 anni

Probabilità di superamento per lo SLV (Pver): 10 %

Periodo di inizio del tratto a velocità costante per lo SLV (Tc*): 0,290 sec

Accelerazione orizzontale massima al sito per lo SLV (ag): 0,076 g

Fattore di amplificazione dello spettro in accelerazione orizzontale per lo SLV (F0): 2,82

Periodo dello spettro Tb: 0,14 sec

Periodo dello spettro Tc: 0,41 sec

Periodo dello spettro Td: 1,90 sec

Coefficiente di sottosuolo S: 1,20

SLD

Periodo di ritorno per lo SLD (Tr): 151 anni

Probabilità di superamento per lo SLD (Pver): 63 %

Periodo di inizio del tratto a velocità costante per lo SLD (T_c^*): 0,230 sec
Accelerazione orizzontale massima al sito per lo SLD (a_g): 0,043 g
Fattore di amplificazione dello spettro in accelerazione orizzontale per lo SLD (F_0) 2,66
Periodo dello spettro T_b : 0,11 sec
Periodo dello spettro T_c : 0,34 sec
Periodo dello spettro T_d : 1,77 sec
Coefficiente di sottosuolo S : 1,20

Livello di conoscenza e coefficiente di sicurezza

In relazione alle indagini svolte e alla documentazione acquisita il livello di conoscenza è di tipo LC2 (Adeguate), il fattore di confidenza adottato è: 1,20

Nelle verifiche di sicurezza viene considerato un coefficiente di sicurezza sulle proprietà meccaniche pari a: 2

Nel calcolo dei cinematismi viene considerato l'arretramento del punto di contatto tra i blocchi nei seguenti casi:

- Cinematismi di ribaltamento fuori piano
- Cinematismi di flessione verticale
- Cinematismi di flessione orizzontale

Proprietà meccaniche caratteristiche delle pareti e coefficienti correttivi

Parete n°: 1

Tipologia muraria: Muratura in mattoni pieni e malta di calce

Resistenza media a compressione [MPa]: 3,200

Resistenza a taglio [MPa]: 0,076

Peso specifico [kN/mc]: 18,00

Alla muratura della parete n° 1 vengono applicati i seguenti fattori correttivi definiti nella Tab. C8A.2.2 della Circolare 617 del 2009:

- Fattore correttivo dovuto a Malta buona: 1,50
- Fattore correttivo dovuto a Giunti sottili: 1,50
- Fattore correttivo dovuto a Connessione trasversale: 1,30

Fattore correttivo complessivo delle proprietà meccaniche: 2,93

Parete n°: 2

Tipologia muraria: Muratura in mattoni pieni e malta di calce

Resistenza media a compressione [MPa]: 3,200

Resistenza a taglio [MPa]: 0,076

Peso specifico [kN/mc]: 18,00

Alla muratura della parete n° 2 vengono applicati i seguenti fattori correttivi definiti nella Tab. C8A.2.2 della Circolare 617 del 2009:

- Fattore correttivo dovuto a Malta buona: 1,50
- Fattore correttivo dovuto a Giunti sottili: 1,50
- Fattore correttivo dovuto a Connessione trasversale: 1,30

Fattore correttivo complessivo delle proprietà meccaniche: 2,93

Parete n°: 3

Tipologia muraria: Muratura in mattoni pieni e malta di calce

Resistenza media a compressione [MPa]: 3,200

Resistenza a taglio [MPa]: 0,076

Peso specifico [kN/mc]: 18,00

Alla muratura della parete n° 3 vengono applicati i seguenti fattori correttivi definiti nella Tab. C8A.2.2 della Circolare 617 del 2009:

- Fattore correttivo dovuto a Malta buona: 1,50
- Fattore correttivo dovuto a Giunti sottili: 1,50
- Fattore correttivo dovuto a Connessione trasversale: 1,30

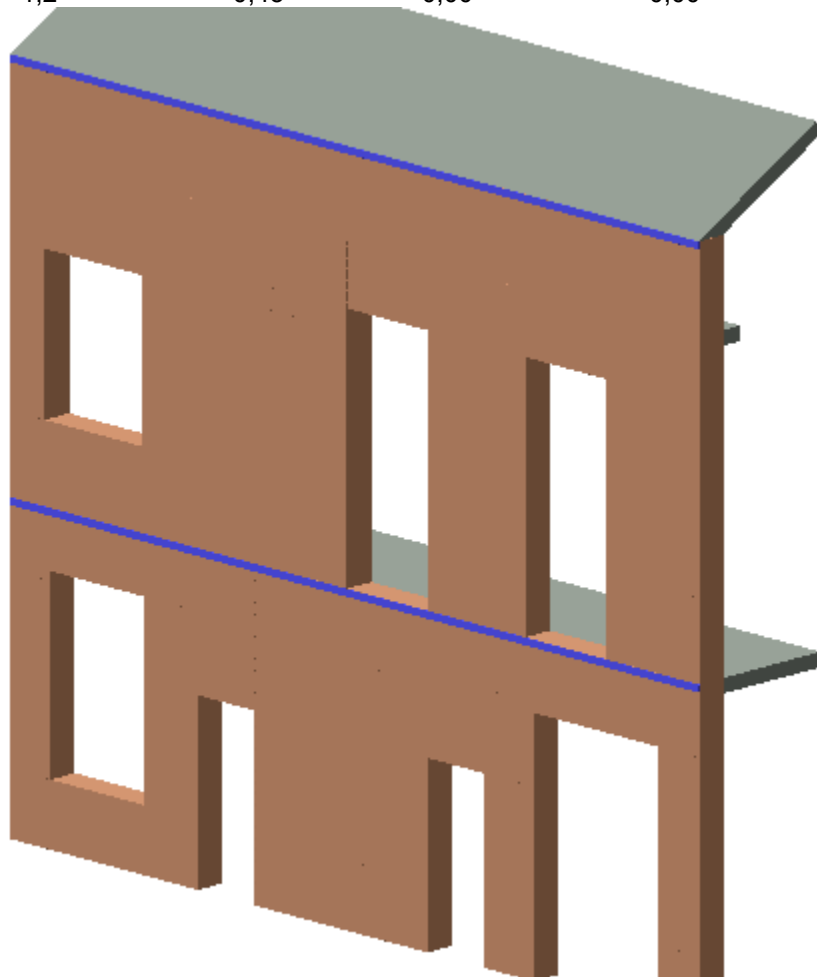
Fattore correttivo complessivo delle proprietà meccaniche: 2,93

Proprietà meccaniche delle pareti, valori di progetto:

n°	γ [kN/m ³]	f_{cd} [MPa]	f_{vd} [MPa]
1	18,00	3,900	0,093
2	18,00	3,900	0,093
3	18,00	3,900	0,093

Geometria delle pareti:

n°	Larghezza [m]	Altezza [m]	Spessore [m]	dy_timpano [m]	dz_timpano [m]
1	12,05	4,4	0,43	0,00	0,00
2	12,05	4,5	0,43	0,00	0,00
3	12,05	1,2	0,43	0,00	0,00



Carichi sulle pareti:

Legenda:

- P_p : peso proprio della parete
- G_k : carico permanente gravante sul solaio della parete
- Q_k : carico variabile gravante sul solaio della parete
- ϕ_2 : carico variabile gravante sul solaio della parete
- i_s : interasse del solaio
- $G_{k\text{timpano}}$: carico permanente gravante sul solaio del timpano
- $Q_{k\text{timpano}}$: carico variabile gravante sul solaio del timpano
- $\phi_{2\text{timpano}}$: carico variabile gravante sul solaio del timpano
- i_t : interasse del timpano
- G_{kfalda} : carico permanente gravante sul solaio della falda inclinata
- Q_{kfalda} : carico variabile gravante sul solaio della falda inclinata

$\varphi_{2\text{falda}}$: carico variabile gravante sul solaio della falda inclinata
 i_f : interasse della falda

n°	P _P [kN]	G _k [kN/m ²]	Q _k [kN/m ²]	φ_2	i _s [m]	G _k _{temp} [kN/m ²]	Q _k _{temp} [kN/m ²]	$\varphi_{2\text{temp}}$	i _t [m]	G _k _{falda} [kN/m ²]	Q _k _{falda} [kN/m ²]	$\varphi_{2\text{falda}}$	i _f [m]
1	278,78	5,90	3,00	0,60	1,90	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
2	231,89	3,00	0,50	0,00	0,50	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
3	113,79	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	1,20	1,90	0,00	2,35

Carichi sulle pareti ortogonali:

Legenda:

G_{korto}: carico permanente gravante sul solaio delle pareti ortogonali

Q_{korto}: carico variabile gravante sul solaio delle pareti ortogonali

$\varphi_{2\text{orto}}$: carico variabile gravante sul solaio delle pareti ortogonali

n°:	G _{korto} [kN/m ²]	Q _{korto} [kN/m ²]	$\varphi_{2\text{orto}}$
1	6,40	3,00	0,60
2	6,40	3,00	0,60
3	6,40	3,00	0,60

Cinematismi:

Cinematismo n°: 1

Tipo: Fles. Verticale singola

Pareti coinvolte: 1,

Quota: 0,00[m]

PGA relativa al cinematismo nel caso di analisi cinematica lineare: 4,0362 [g]

PGA relativa al cinematismo nel caso di analisi cinematica non lineare: 1,5145 [g]

Moltiplicatore di collasso dei carichi orizzontali α_0 : 1,596

accelerazione spettrale di attivazione del cinematismo a_0^* : 2,422 [g]

Massa partecipante al cinematismo M*: 28 [kN]

Frazione di massa partecipante della struttura e^* : 0,549

Risultati della verifica con analisi cinematica lineare allo SLD

Accelerazione di riferimento allo SLD per cinematismo a quota zero: 0,051 [g]

Stato di verifica dell'analisi cinematica lineare allo SLD: **Verificato**

Risultati della verifica con analisi cinematica lineare allo SLV

Accelerazione di riferimento allo SLV per cinematismo a quota zero: 0,045 [g]

Stato di verifica dell'analisi cinematica lineare allo SLV: **Verificato**

Risultati della verifica con analisi cinematica non lineare allo SLV

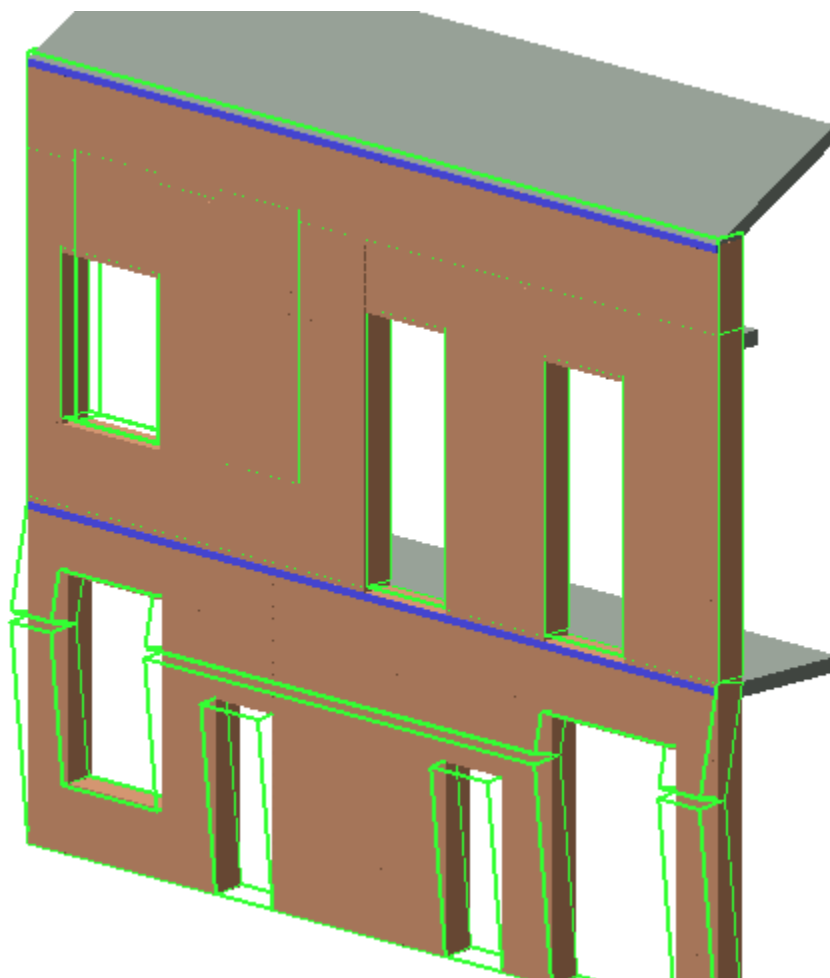
Periodo secante T_s: 0,211[sec]

Spostamento spettrale d_u^* : 0,056[m]

Domanda di spostamento nel caso di cinematismo a quota zero $\Delta_{d, \text{quota zero}}$: 0,003 [m]

Domanda di spostamento nel caso di cinematismo a quota maggiore di zero $\Delta_{d, \text{quota sopraelev.}}$: 0,000 [m]

Stato di verifica dell'analisi cinematica non lineare allo SLV: **Verificato**



Cinematismo n°: 2

Tipo: Fles. Verticale multi

Pareti coinvolte: 2, 3,

Quota: 4,39[m]

Primo modo di vibrare normalizzato ad 1 in sommità dell'edificio $\Psi(Z)$: 0,338

PGA relativa al cinematismo nel caso di analisi cinematica lineare: 0,1791 [g]

PGA relativa al cinematismo nel caso di analisi cinematica non lineare: 0,2425 [g]

Moltiplicatore di collasso dei carichi orizzontali α_0 : 0,090

accelerazione spettrale di attivazione del cinematismo a_0^* : 0,123 [g]

Massa partecipante al cinematismo M^* : 36 [kN]

Frazione di massa partecipante della struttura e^* : 0,609

Risultati della verifica con analisi cinematica lineare allo SLD

Accelerazione di riferimento allo SLD (a quota zero): 0,051 [g]

Accelerazione di riferimento allo SLD (a quota diversa da zero): 0,055 [g]

Stato di verifica dell'analisi cinematica lineare allo SLD: **Verificato**

Risultati della verifica con analisi cinematica lineare allo SLV

Accelerazione di riferimento allo SLV (a quota zero): 0,045[g]

Accelerazione di riferimento allo SLV (a quota diversa da zero): 0,052 [g]

Stato di verifica dell'analisi cinematica lineare allo SLV: **Verificato**

Risultati della verifica con analisi cinematica non lineare allo SLV

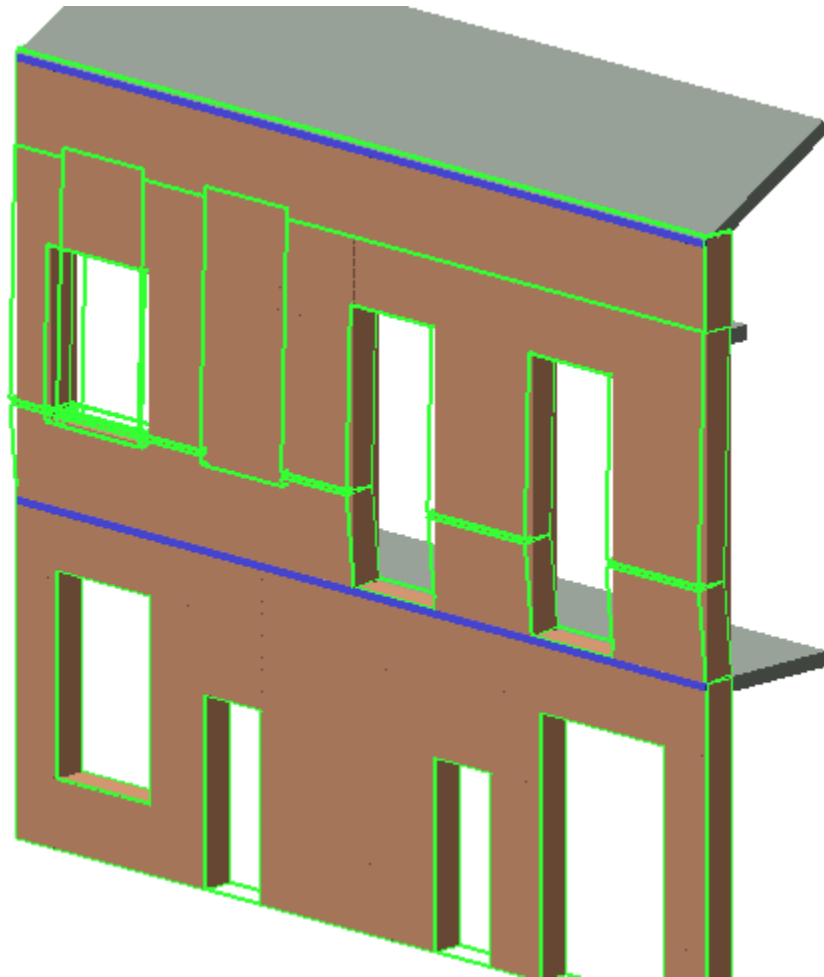
Periodo secante T_s : 1,312[sec]

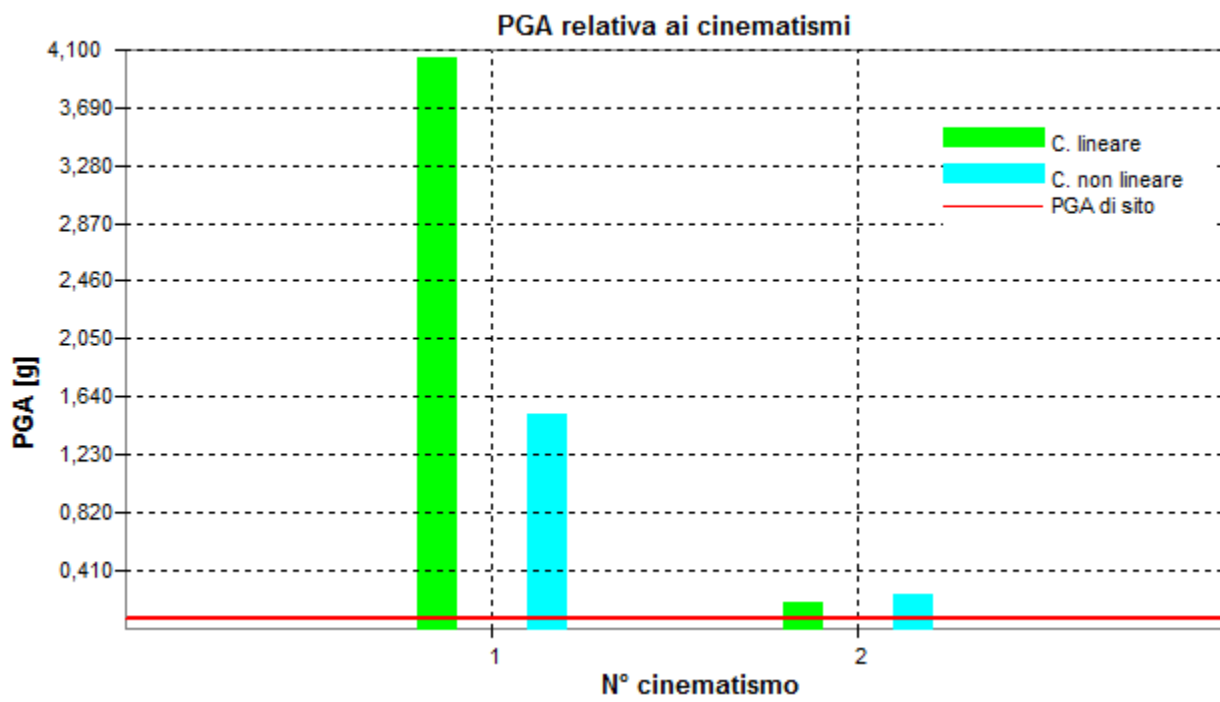
Spostamento spettrale d_u^* : 0,109[m]

Domanda di spostamento nel caso di cinematiso a quota zero $\Delta_{d, \text{quota zero}}$: 0,034 [m]

Domanda di spostamento nel caso di cinematiso a quota maggiore di zero $\Delta_{d, \text{quota sopraelev}}$: 0,016 [m]

Stato di verifica dell'analisi cinematica non lineare allo SLV: **Verificato**





Relazione di calcolo Analisi lineare e non lineare dei cinematismi nella muratura

PARETE SUD EST – Consolidata con intonaco armato (piano 1°) e fascia sommitale in FRP

Relazione di calcolo sulla struttura impostata e redatta secondo le modalità previste dal DM 17/01/2018 NTC cap. 10 'Redazione dei progetti strutturali esecutivi e delle relazioni di calcolo'.

Di seguito si indicano l'origine e le caratteristiche dei codici di calcolo utilizzati riportando titolo, produttore e distributore, versione, estremi della licenza d'uso:

Nome del software:

PRO_CINEm Analisi lineare e non lineare dei cinematismi nella muratura

Versione del software:

v. 2018.04.0044b

Produttore del software:

2 S.I. Software e Servizi per l'Ingegneria s.r.l., Ferrara

Distributore del software:

2 S.I. Software e Servizi per l'Ingegneria s.r.l., Ferrara

Dati utente finale:

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Normativa di Riferimento

NTC 2018 e Circolare 617 del 2009

Parametri sismici

Località: NOLE (TO)

Altezza totale dell'edificio: 13,00 m

Vita nominale dell'edificio: 50,00 anni

Coefficiente di struttura: 2,00

Periodo del modo per principale di vibrare (T1): 0,342 sec

Coefficiente di partecipazione modale: γ : 1,20

Categoria di sottosuolo: Tipo B

SLV

Periodo di ritorno per lo SLV (Tr): 712 anni

Probabilità di superamento per lo SLV (Pver): 10 %

Periodo di inizio del tratto a velocità costante per lo SLV (Tc*): 0,280 sec

Accelerazione orizzontale massima al sito per lo SLV (ag): 0,065 g

Fattore di amplificazione dello spettro in accelerazione orizzontale per lo SLV (F0): 2,77

Periodo dello spettro Tb: 0,13 sec

Periodo dello spettro Tc: 0,40 sec

Periodo dello spettro Td: 1,86 sec

Coefficiente di sottosuolo S: 1,20

SLD

Periodo di ritorno per lo SLD (Tr): 75 anni

Probabilità di superamento per lo SLD (P_{ver}): 63 %
Periodo di inizio del tratto a velocità costante per lo SLD (T_c^{*}): 0,210 sec
Accelerazione orizzontale massima al sito per lo SLD (a_g): 0,035 g
Fattore di amplificazione dello spettro in accelerazione orizzontale per lo SLD (F₀) 2,62
Periodo dello spettro T_b: 0,11 sec
Periodo dello spettro T_c: 0,32 sec
Periodo dello spettro T_d: 1,74 sec
Coefficiente di sottosuolo S: 1,20

Livello di conoscenza e coefficiente di sicurezza

In relazione alle indagini svolte e alla documentazione acquisita il livello di conoscenza è di tipo LC2 (Adeguito), il fattore di confidenza adottato è: 1,20

Nelle verifiche di sicurezza viene considerato un coefficiente di sicurezza sulle proprietà meccaniche pari a: 2
Nel calcolo dei cinematismi viene considerato l'arretramento del punto di contatto tra i blocchi nei seguenti casi:

- Cinematismi di ribaltamento fuori piano
- Cinematismi di flessione verticale
- Cinematismi di flessione orizzontale

Proprietà meccaniche caratteristiche delle pareti e coefficienti correttivi

Parete n°: 1

Tipologia muraria: Muratura in mattoni pieni e malta di calce

Resistenza media a compressione [MPa]: 3,200

Resistenza a taglio [MPa]: 0,076

Peso specifico [kN/mc]: 18,00

Alla muratura della parete n° 1 vengono applicati i seguenti fattori correttivi definiti nella Tab. C8A.2.2 della Circolare 617 del 2009:

- Fattore correttivo dovuto a Malta buona: 1,50
- Fattore correttivo dovuto a Giunti sottili: 1,50
- Fattore correttivo dovuto a Connessione trasversale: 1,30

Fattore correttivo complessivo delle proprietà meccaniche: 2,93

Parete n°: 2

Tipologia muraria: Muratura in mattoni pieni e malta di calce

Resistenza media a compressione [MPa]: 3,200

Resistenza a taglio [MPa]: 0,076

Peso specifico [kN/mc]: 18,00

Alla muratura della parete n° 2 vengono applicati i seguenti fattori correttivi definiti nella Tab. C8A.2.2 della Circolare 617 del 2009:

- Fattore correttivo dovuto a Malta buona: 1,50
- Fattore correttivo dovuto a Giunti sottili: 1,50
- Fattore correttivo dovuto a Connessione trasversale: 1,30

Fattore correttivo complessivo delle proprietà meccaniche: 2,93

Parete n°: 3

Tipologia muraria: Muratura in mattoni pieni e malta di calce

Resistenza media a compressione [MPa]: 3,200

Resistenza a taglio [MPa]: 0,076

Peso specifico [kN/mc]: 18,00

Alla muratura della parete n° 3 vengono applicati i seguenti fattori correttivi definiti nella Tab. C8A.2.2 della Circolare 617 del 2009:

- Fattore correttivo dovuto a Malta buona: 1,50
- Fattore correttivo dovuto a Giunti sottili: 1,50
- Fattore correttivo dovuto a Connessione trasversale: 1,30
- Fattore correttivo dovuto a Intonaco armato: 1,50

Fattore correttivo complessivo delle proprietà meccaniche: 4,39

Parete n°: 4

Tipologia muraria: Muratura in mattoni pieni e malta di calce

Resistenza media a compressione [MPa]: 3,200

Resistenza a taglio [MPa]: 0,076

Peso specifico [kN/mc]: 18,00

Alla muratura della parete n° 4 vengono applicati i seguenti fattori correttivi definiti nella Tab. C8A.2.2 della Circolare 617 del 2009:

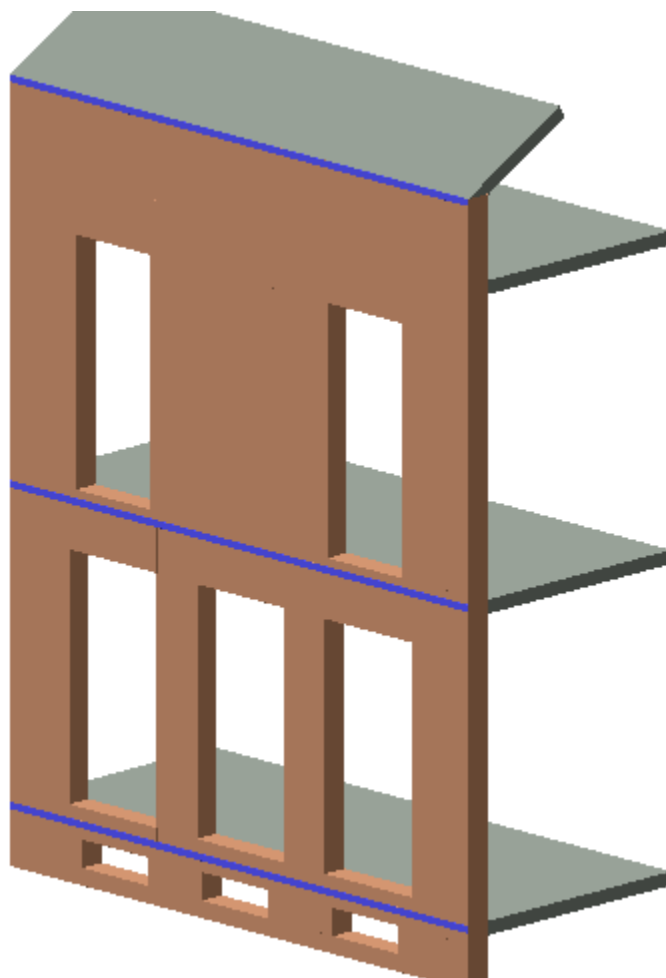
- Fattore correttivo dovuto a Malta buona: 1,50
 - Fattore correttivo dovuto a Giunti sottili: 1,50
 - Fattore correttivo dovuto a Connessione trasversale: 1,30
 - Fattore correttivo dovuto a Intonaco armato: 1,50
- Fattore correttivo complessivo delle proprietà meccaniche: 4,39

Proprietà meccaniche delle pareti, valori di progetto:

n°	γ [kN/m ³]	f_{cd} [MPa]	f_{vd} [MPa]
1	18,00	3,900	0,093
2	18,00	3,900	0,093
3	18,00	5,850	0,139
4	18,00	5,850	0,139

Geometria delle pareti:

n°	Larghezza [m]	Altezza [m]	Spessore [m]	dy_timpano [m]	dz_timpano [m]
1	8,82	0,9	0,37	0,00	0,00
2	8,82	4,5	0,37	0,00	0,00
3	8,82	4,5	0,37	0,00	0,00
4	8,82	1,2	0,37	0,00	0,00



Carichi sulle pareti:

Legenda:

P_p : peso proprio della parete

G_k : carico permanente gravante sul solaio della parete

Q_k : carico variabile gravante sul solaio della parete

φ_2 : carico variabile gravante sul solaio della parete

i_s : interasse del solaio

$G_{k\text{timp}}$: carico permanente gravante sul solaio del timpano

$Q_{k\text{timp}}$: carico variabile gravante sul solaio del timpano

$\varphi_{2\text{timp}}$: carico variabile gravante sul solaio del timpano

i_t : interasse del timpano

$G_{k\text{falda}}$: carico permanente gravante sul solaio della falda inclinata

$Q_{k\text{falda}}$: carico variabile gravante sul solaio della falda inclinata

$\varphi_{2\text{falda}}$: carico variabile gravante sul solaio della falda inclinata

i_f : interasse della falda

n°	P_p [kN]	G_k [kN/m ²]	Q_k [kN/m ²]	φ_2	i_s [m]	$G_{k\text{timp}}$ [kN/m ²]	$Q_{k\text{timp}}$ [kN/m ²]	$\varphi_{2\text{timp}}$	i_t [m]	$G_{k\text{falda}}$ [kN/m ²]	$Q_{k\text{falda}}$ [kN/m ²]	$\varphi_{2\text{falda}}$	i_f [m]
1	43,30	4,40	3,00	0,60	3,70	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
2	145,13	5,90	3,00	0,60	3,70	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
3	196,83	3,00	0,05	0,00	3,70	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
4	71,66	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	1,20	1,90	0,00	2,00

Carichi sulle pareti ortogonali:

Legenda:

G_{korto} : carico permanente gravante sul solaio delle pareti ortogonali

Q_{korto} : carico variabile gravante sul solaio delle pareti ortogonali

φ_{2orto} : carico variabile gravante sul solaio delle pareti ortogonali

n°:	G_{korto} [kN/m ²]	Q_{korto} [kN/m ²]	φ_{2orto}
1	6,40	3,00	0,60
2	3,10	0,50	0,00
3	3,10	0,50	0,00
4	3,10	0,50	0,00

Cinematismi:**Cinematismo n°: 1**

Tipo: Fles. Verticale singola

Pareti coinvolte: 1,

Quota: 0,00[m]

PGA relativa al cinematismo nel caso di analisi cinematica lineare: 1238,0350 [g]

PGA relativa al cinematismo nel caso di analisi cinematica non lineare: 1330,9140 [g]

Moltiplicatore di collasso dei carichi orizzontali α_0 : 62,704

accelerazione spettrale di attivazione del cinematismo a_0^* : 742,821 [g]

Massa partecipante al cinematismo M^* : 4 [kN]

Frazione di massa partecipante della struttura e^* : 0,070

Risultati della verifica con analisi cinematica lineare allo SLD

Accelerazione di riferimento allo SLD per cinematismo a quota zero: 0,042 [g]

Stato di verifica dell'analisi cinematica lineare allo SLD: **Verificato**

Risultati della verifica con analisi cinematica lineare allo SLV

Accelerazione di riferimento allo SLV per cinematismo a quota zero: 0,039 [g]

Stato di verifica dell'analisi cinematica lineare allo SLV: **Verificato**

Risultati della verifica con analisi cinematica non lineare allo SLV

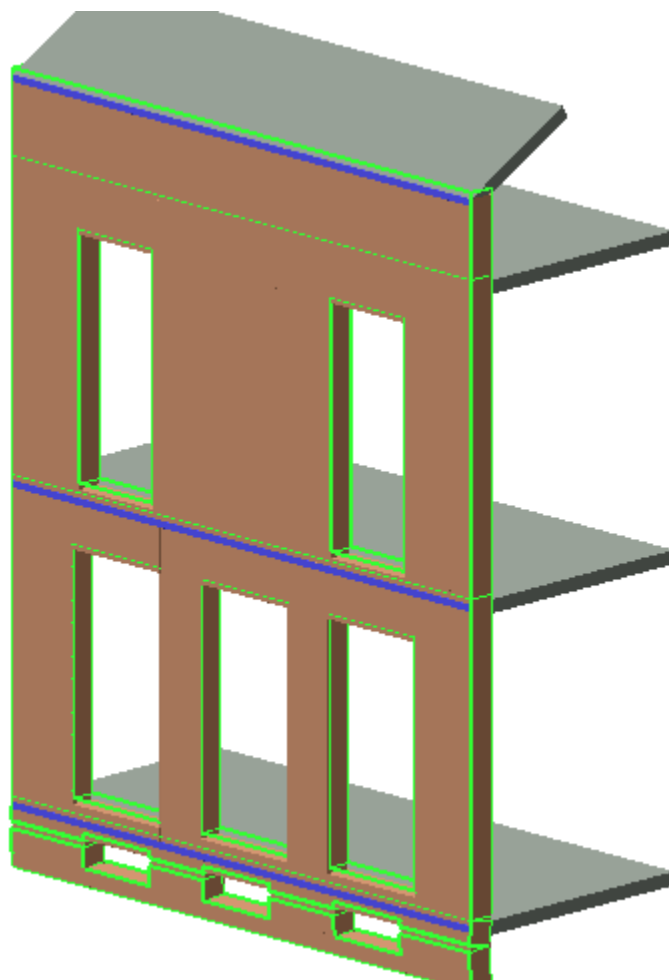
Periodo secante T_s : 0,011[sec]

Spostamento spettrale d_u^* : 0,052[m]

Domanda di spostamento nel caso di cinematismo a quota zero $\Delta_{d, \text{ quota zero}}$: 0,000 [m]

Domanda di spostamento nel caso di cinematismo a quota maggiore di zero $\Delta_{d, \text{ quota sopraelev}}$: 0,000 [m]

Stato di verifica dell'analisi cinematica non lineare allo SLV: **Verificato**



Cinematismo n°: 2

Tipo: Fles. Verticale singola

Pareti coinvolte: 2,

Quota: 0,91[m]

Primo modo di vibrare normalizzato ad 1 in sommità dell'edificio $\Psi(Z)$: 0,070

PGA relativa al cinematismo nel caso di analisi cinematica lineare: 19,1038 [g]

PGA relativa al cinematismo nel caso di analisi cinematica non lineare: 9,3270 [g]

Moltiplicatore di collasso dei carichi orizzontali α_0 : 2,768

accelerazione spettrale di attivazione del cinematismo a_0^* : 11,462 [g]

Massa partecipante al cinematismo M^* : 15 [kN]

Frazione di massa partecipante della struttura e^* : 0,201

Risultati della verifica con analisi cinematica lineare allo SLD

Accelerazione di riferimento allo SLD (a quota zero): 0,042 [g]

Accelerazione di riferimento allo SLD (a quota diversa da zero): 0,008 [g]

Stato di verifica dell'analisi cinematica lineare allo SLD: **Verificato**

Risultati della verifica con analisi cinematica lineare allo SLV

Accelerazione di riferimento allo SLV (a quota zero): 0,039[g]

Accelerazione di riferimento allo SLV (a quota diversa da zero): 0,009 [g]

Stato di verifica dell'analisi cinematica lineare allo SLV: **Verificato**

Risultati della verifica con analisi cinematica non lineare allo SLV

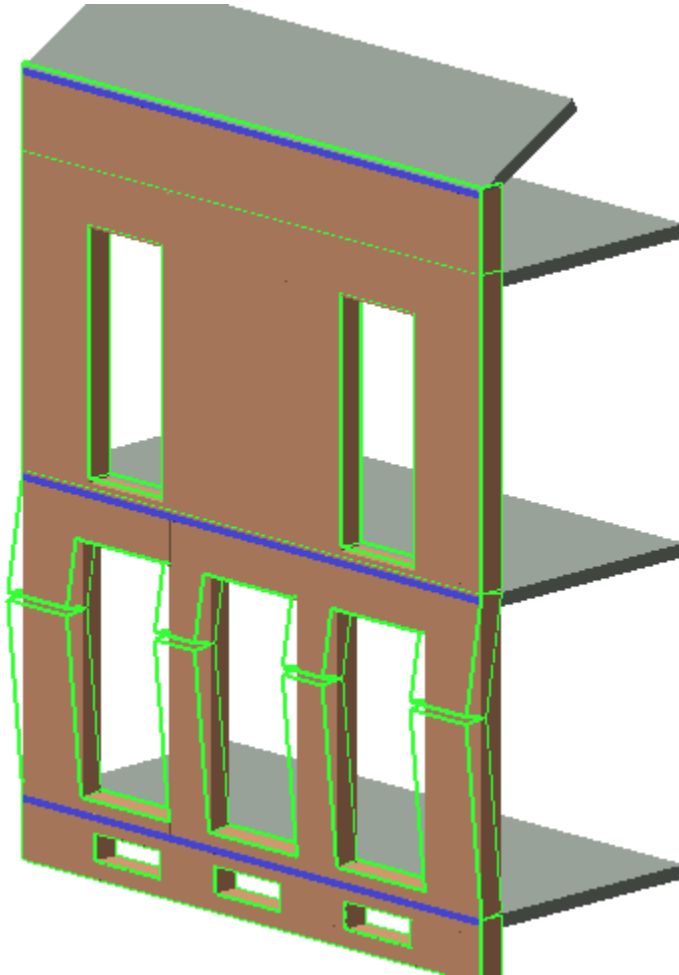
Periodo secante T_s : 0,087[sec]

Spostamento spettrale d_u^* : 0,045[m]

Domanda di spostamento nel caso di cinematisimo a quota zero $\Delta_{d, \text{quota zero}}$: 0,000 [m]

Domanda di spostamento nel caso di cinematisimo a quota maggiore di zero $\Delta_{d, \text{quota sopraelev}}$: 0,000 [m]

Stato di verifica dell'analisi cinematica non lineare allo SLV: **Verificato**



Cinematisimo n°: 3

Tipo: Fles. Verticale multi

Pareti coinvolte: 3, 4,

Quota: 5,45[m]

Primo modo di vibrare normalizzato ad 1 in sommità dell'edificio $\psi(Z)$: 0,419

PGA relativa al cinematisimo nel caso di analisi cinematica lineare: 0,3307 [g]

PGA relativa al cinematisimo nel caso di analisi cinematica non lineare: 0,4036 [g]

Moltiplicatore di collasso dei carichi orizzontali α_0 : 0,114

accelerazione spettrale di attivazione del cinematisimo a_0^* : 0,276 [g]

Massa partecipante al cinematisimo M^* : 29 [kN]

Frazione di massa partecipante della struttura e^* : 0,343

Risultati della verifica con analisi cinematica lineare allo SLD

Accelerazione di riferimento allo SLD (a quota zero): 0,042 [g]

Accelerazione di riferimento allo SLD (a quota diversa da zero): 0,051 [g]

Stato di verifica dell'analisi cinematica lineare allo SLD: **Verificato**

Risultati della verifica con analisi cinematica lineare allo SLV

Accelerazione di riferimento allo SLV (a quota zero): 0,039[g]

Accelerazione di riferimento allo SLV (a quota diversa da zero): 0,054 [g]

Stato di verifica dell'analisi cinematica lineare allo SLV: **Verificato**

Risultati della verifica con analisi cinematica non lineare allo SLV

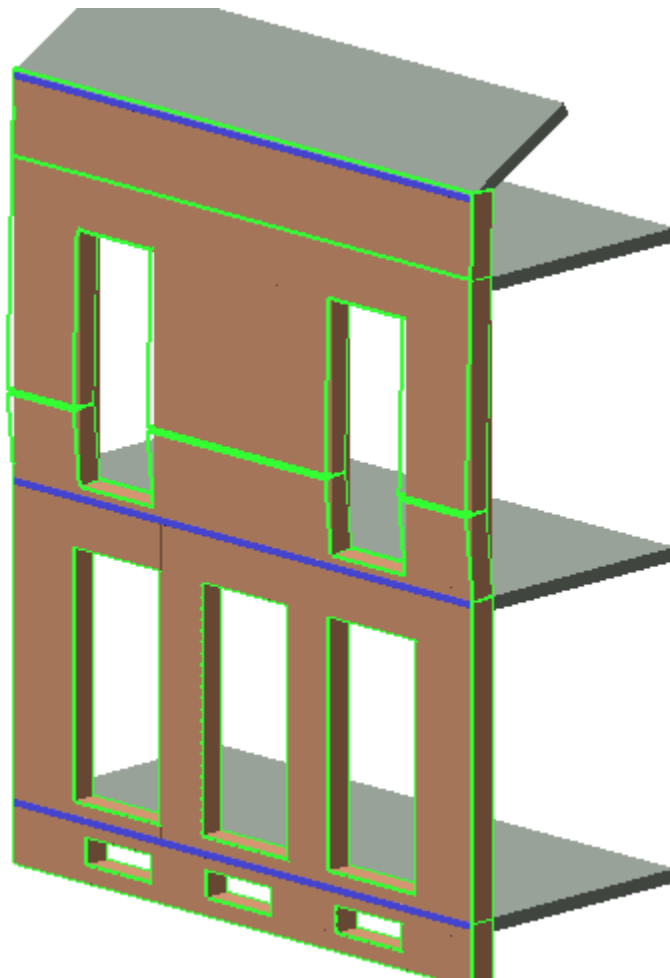
Periodo secante T_s : 0,925[sec]

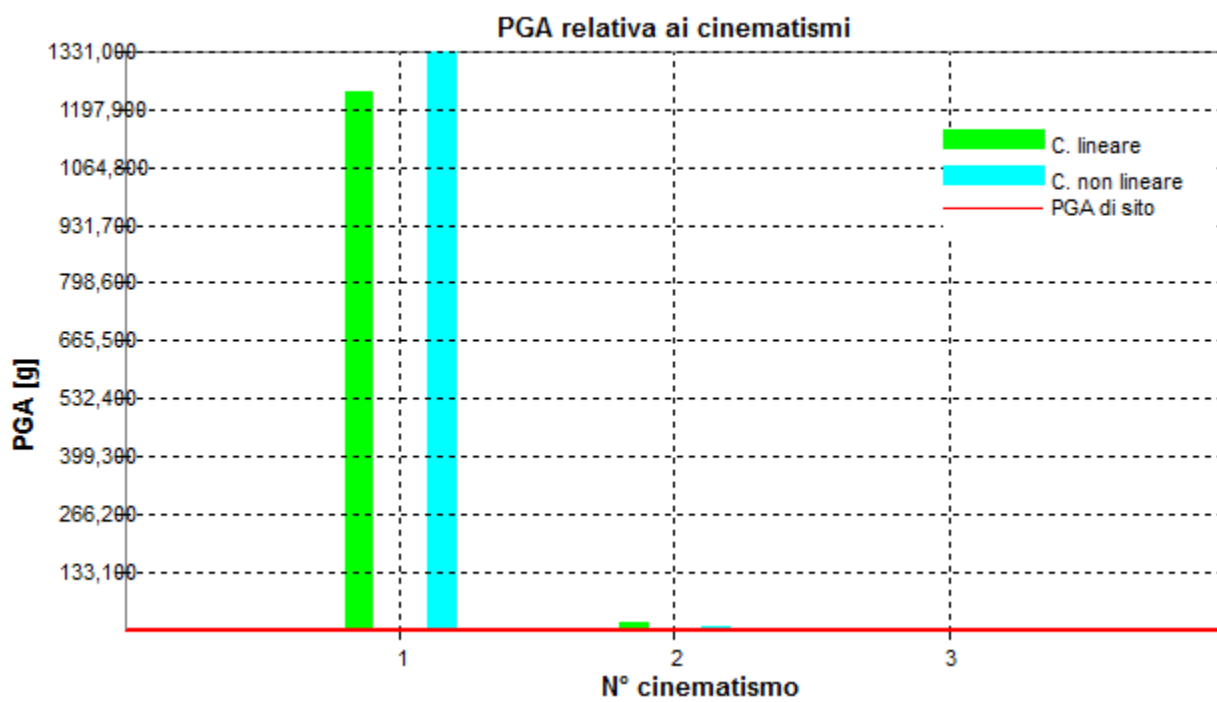
Spostamento spettrale d_u^* : 0,122[m]

Domanda di spostamento nel caso di cinetismo a quota zero $\Delta_{d, \text{ quota zero}}$: 0,020 [m]

Domanda di spostamento nel caso di cinetismo a quota maggiore di zero $\Delta_{d, \text{ quota sopraelev}}$: 0,013 [m]

Stato di verifica dell'analisi cinematica non lineare allo SLV: **Verificato**





Relazione di calcolo Analisi lineare e non lineare dei cinematismi nella muratura

PARETE SUD EST – Consolidata con intonaco armato e fascia sommitale in FRP

Relazione di calcolo sulla struttura impostata e redatta secondo le modalità previste dal DM 17/01/2018 NTC cap. 10 'Redazione dei progetti strutturali esecutivi e delle relazioni di calcolo'.

Di seguito si indicano l'origine e le caratteristiche dei codici di calcolo utilizzati riportando titolo, produttore e distributore, versione, estremi della licenza d'uso:

Nome del software:

PRO_CINEm Analisi lineare e non lineare dei cinematismi nella muratura

Versione del software:

v. 2018.04.0044b

Produttore del software:

2 S.I. Software e Servizi per l'Ingegneria s.r.l., Ferrara

Distributore del software:

2 S.I. Software e Servizi per l'Ingegneria s.r.l., Ferrara

Dati utente finale:

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Normativa di Riferimento

NTC 2018 e Circolare 617 del 2009

Parametri sismici

Località: NOLE (TO)

Altezza totale dell'edificio: 13,00 m

Vita nominale dell'edificio: 50,00 anni

Coefficiente di struttura: 2,00

Periodo del modo per principale di vibrare (T1): 0,342 sec

Coefficiente di partecipazione modale: γ : 1,20

Categoria di sottosuolo: Tipo B

SLV

Periodo di ritorno per lo SLV (Tr): 712 anni

Probabilità di superamento per lo SLV (Pver): 10 %

Periodo di inizio del tratto a velocità costante per lo SLV (Tc*): 0,280 sec

Accelerazione orizzontale massima al sito per lo SLV (ag): 0,065 g

Fattore di amplificazione dello spettro in accelerazione orizzontale per lo SLV (F0): 2,77

Periodo dello spettro Tb: 0,13 sec

Periodo dello spettro Tc: 0,40 sec

Periodo dello spettro Td: 1,86 sec

Coefficiente di sottosuolo S: 1,20

SLD

Periodo di ritorno per lo SLD (Tr): 75 anni

Probabilità di superamento per lo SLD (Pver): 63 %

Periodo di inizio del tratto a velocità costante per lo SLD (T_c^*): 0,210 sec
 Accelerazione orizzontale massima al sito per lo SLD (a_g): 0,035 g
 Fattore di amplificazione dello spettro in accelerazione orizzontale per lo SLD (F_0) 2,62
 Periodo dello spettro T_b : 0,11 sec
 Periodo dello spettro T_c : 0,32 sec
 Periodo dello spettro T_d : 1,74 sec
 Coefficiente di sottosuolo S : 1,20

Livello di conoscenza e coefficiente di sicurezza

In relazione alle indagini svolte e alla documentazione acquisita il livello di conoscenza è di tipo LC2 (Adeguito), il fattore di confidenza adottato è: 1,20

Nelle verifiche di sicurezza viene considerato un coefficiente di sicurezza sulle proprietà meccaniche pari a: 2

Nel calcolo dei cinematismi viene considerato l'arretramento del punto di contatto tra i blocchi nei seguenti casi:

- Cinematismi di ribaltamento fuori piano
- Cinematismi di flessione verticale
- Cinematismi di flessione orizzontale

Proprietà meccaniche caratteristiche delle pareti e coefficienti correttivi

Parete n°: 1

Tipologia muraria: Muratura in mattoni semipieni e malta cementizia (es. doppio UNI perc. for.<40%)

Resistenza media a compressione [MPa]: 6,500

Resistenza a taglio [MPa]: 0,280

Peso specifico [kN/mc]: 15,00

Parete n°: 2

Tipologia muraria: Muratura in mattoni semipieni e malta cementizia (es. doppio UNI perc. for.<40%)

Resistenza media a compressione [MPa]: 6,500

Resistenza a taglio [MPa]: 0,280

Peso specifico [kN/mc]: 15,00

Parete n°: 3

Tipologia muraria: Muratura in mattoni semipieni e malta cementizia (es. doppio UNI perc. for.<40%)

Resistenza media a compressione [MPa]: 6,500

Resistenza a taglio [MPa]: 0,280

Peso specifico [kN/mc]: 15,00

Parete n°: 4

Tipologia muraria: Muratura in mattoni semipieni e malta cementizia (es. doppio UNI perc. for.<40%)

Resistenza media a compressione [MPa]: 6,500

Resistenza a taglio [MPa]: 0,280

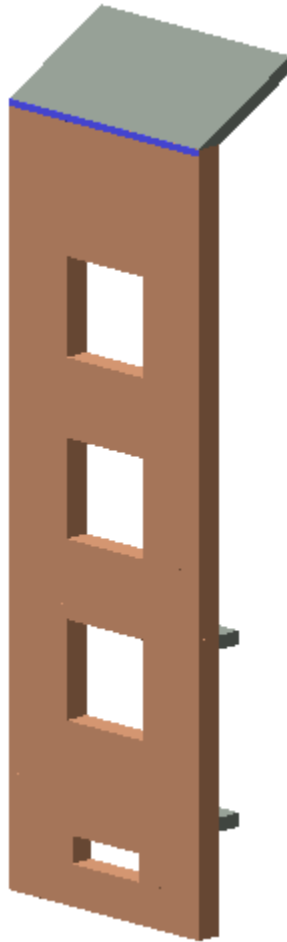
Peso specifico [kN/mc]: 15,00

Proprietà meccaniche delle pareti, valori di progetto:

n°	γ [kN/m ³]	f_{cd} [MPa]	f_{vd} [MPa]
1	15,00	2,708	0,117
2	15,00	2,708	0,117
3	15,00	2,708	0,117
4	15,00	2,708	0,117

Geometria delle pareti:

n°	Larghezza [m]	Altezza [m]	Spessore [m]	dy_timpano [m]	dz_timpano [m]
1	3,63	1,7	0,37	0,00	0,00
2	3,63	2,6	0,37	0,00	0,00
3	3,63	5,7	0,37	0,00	0,00
4	3,63	1,2	0,37	0,00	0,00



Carichi sulle pareti:

Legenda:

P_p : peso proprio della parete

G_k : carico permanente gravante sul solaio della parete

Q_k : carico variabile gravante sul solaio della parete

φ_2 : carico variabile gravante sul solaio della parete

i_s : interasse del solaio

$G_{k\text{timp}}$: carico permanente gravante sul solaio del timpano

$Q_{k\text{timp}}$: carico variabile gravante sul solaio del timpano

$\varphi_{2\text{timp}}$: carico variabile gravante sul solaio del timpano

i_t : interasse del timpano

$G_{k\text{falda}}$: carico permanente gravante sul solaio della falda inclinata

$Q_{k\text{falda}}$: carico variabile gravante sul solaio della falda inclinata

$\varphi_{2\text{falda}}$: carico variabile gravante sul solaio della falda inclinata

i_f : interasse della falda

n°	P_p [kN]	G_k [kN/m²]	Q_k [kN/m²]	φ_2	i_s [m]	$G_{k\text{timp}}$ [kN/m²]	$Q_{k\text{timp}}$ [kN/m²]	$\varphi_{2\text{timp}}$	i_t [m]	$G_{k\text{falda}}$ [kN/m²]	$Q_{k\text{falda}}$ [kN/m²]	$\varphi_{2\text{falda}}$	i_f [m]
1	30,62	5,20	4,00	0,60	0,56	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
2	40,23	5,20	4,00	0,60	0,56	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
3	92,14	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
4	24,18	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	1,20	1,90	0,00	2,00

Carichi sulle pareti ortogonali:

Legenda:

G_{korto} : carico permanente gravante sul solaio delle pareti ortogonali

Q_{korto} : carico variabile gravante sul solaio delle pareti ortogonali

φ_{2orto} : carico variabile gravante sul solaio delle pareti ortogonali

n°:	G_{korto} [kN/m ²]	Q_{korto} [kN/m ²]	φ_{2orto}
1	6,40	3,00	0,60
2	6,40	3,00	0,60
3	6,40	3,00	0,60
4	6,40	3,00	0,60

Cinematismi:**Cinematismo n°: 1**

Tipo: Fles. Verticale multi

Pareti coinvolte: 1, 2, 3, 4,

Quota: 0,00[m]

PGA relativa al cinematismo nel caso di analisi cinematica lineare: 0,0692 [g]

PGA relativa al cinematismo nel caso di analisi cinematica non lineare: 0,1550 [g]

Moltiplicatore di collasso dei carichi orizzontali α_0 : 0,043

accelerazione spettrale di attivazione del cinematismo a_0^* : 0,042 [g]

Massa partecipante al cinematismo M^* : 20 [kN]

Frazione di massa partecipante della struttura e^* : 0,870

Risultati della verifica con analisi cinematica lineare allo SLD

Accelerazione di riferimento allo SLD per cinematismo a quota zero: 0,042 [g]

Stato di verifica dell'analisi cinematica lineare allo SLD: **Verificato**

Risultati della verifica con analisi cinematica lineare allo SLV

Accelerazione di riferimento allo SLV per cinematismo a quota zero: 0,039 [g]

Stato di verifica dell'analisi cinematica lineare allo SLV: **Verificato**

Risultati della verifica con analisi cinematica non lineare allo SLV

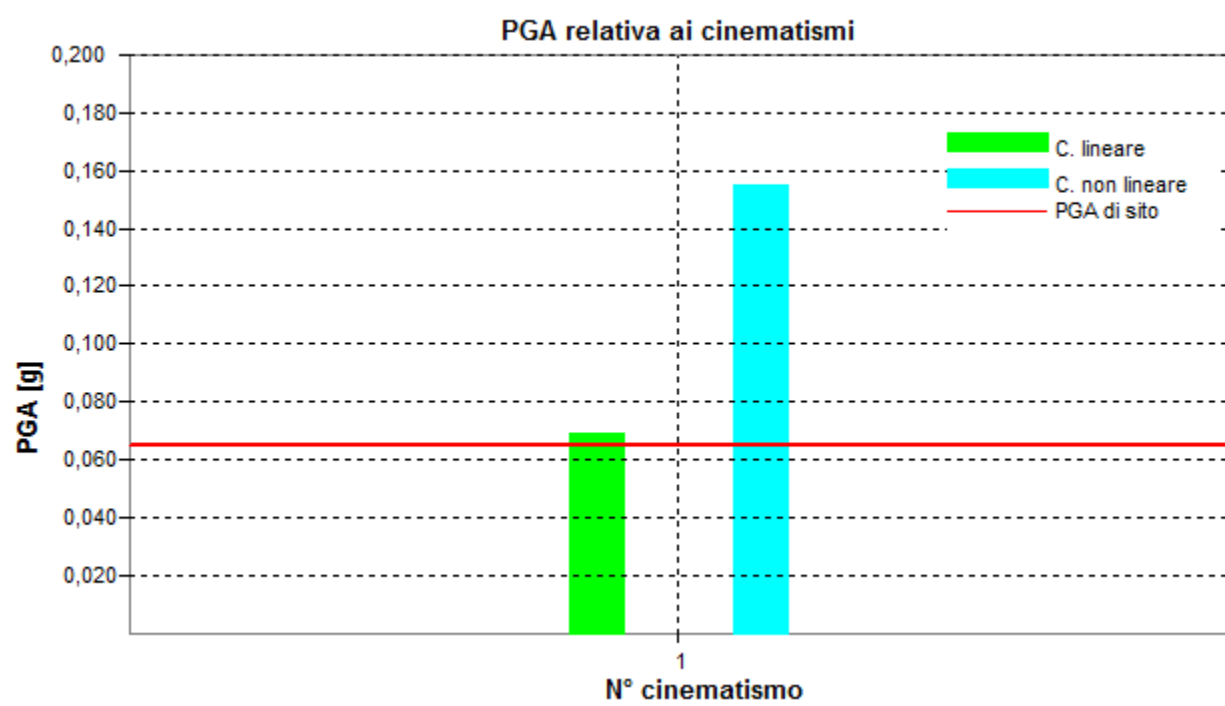
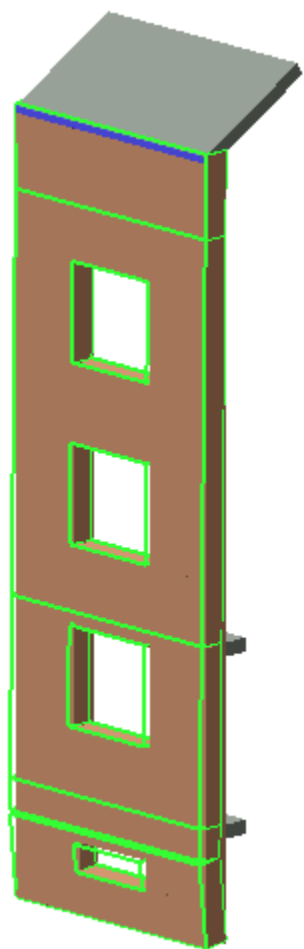
Periodo secante T_s : 2,092[sec]

Spostamento spettrale d_u^* : 0,095[m]

Domanda di spostamento nel caso di cinematismo a quota zero $\Delta_{d, \text{ quota zero}}$: 0,040 [m]

Domanda di spostamento nel caso di cinematismo a quota maggiore di zero $\Delta_{d, \text{ quota sopraelev}}$: 0,000 [m]

Stato di verifica dell'analisi cinematica non lineare allo SLV: **Verificato**



Relazione di calcolo Analisi lineare e non lineare dei cinematismi nella muratura

PARETE SUD EST VANO SCALA – Consolidata con intonaco armato e fascia sommitale in FRP

Relazione di calcolo sulla struttura impostata e redatta secondo le modalità previste dal DM 17/01/2018 NTC cap. 10 'Redazione dei progetti strutturali esecutivi e delle relazioni di calcolo'.

Di seguito si indicano l'origine e le caratteristiche dei codici di calcolo utilizzati riportando titolo, produttore e distributore, versione, estremi della licenza d'uso:

Nome del software:

PRO_CINEm Analisi lineare e non lineare dei cinematismi nella muratura

Versione del software:

v. 2018.04.0044b

Produttore del software:

2 S.I. Software e Servizi per l'Ingegneria s.r.l., Ferrara

Distributore del software:

2 S.I. Software e Servizi per l'Ingegneria s.r.l., Ferrara

Dati utente finale:

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Normativa di Riferimento

NTC 2018 e Circolare 617 del 2009

Parametri sismici

Località: NOLE (TO)

Altezza totale dell'edificio: 13,00 m

Vita nominale dell'edificio: 50,00 anni

Coefficiente di struttura: 2,00

Periodo del modo per principale di vibrare (T1): 0,342 sec

Coefficiente di partecipazione modale: γ : 1,20

Categoria di sottosuolo: Tipo B

SLV

Periodo di ritorno per lo SLV (Tr): 712 anni

Probabilità di superamento per lo SLV (Pver): 10 %

Periodo di inizio del tratto a velocità costante per lo SLV (Tc*): 0,280 sec

Accelerazione orizzontale massima al sito per lo SLV (ag): 0,065 g

Fattore di amplificazione dello spettro in accelerazione orizzontale per lo SLV (F0): 2,77

Periodo dello spettro Tb: 0,13 sec

Periodo dello spettro Tc: 0,40 sec

Periodo dello spettro Td: 1,86 sec

Coefficiente di sottosuolo S: 1,20

SLD

Periodo di ritorno per lo SLD (Tr): 75 anni

Probabilità di superamento per lo SLD (P_{ver}): 63 %
Periodo di inizio del tratto a velocità costante per lo SLD (T_c^{*}): 0,210 sec
Accelerazione orizzontale massima al sito per lo SLD (a_g): 0,035 g
Fattore di amplificazione dello spettro in accelerazione orizzontale per lo SLD (F₀) 2,62
Periodo dello spettro T_b: 0,11 sec
Periodo dello spettro T_c: 0,32 sec
Periodo dello spettro T_d: 1,74 sec
Coefficiente di sottosuolo S: 1,20

Livello di conoscenza e coefficiente di sicurezza

In relazione alle indagini svolte e alla documentazione acquisita il livello di conoscenza è di tipo LC2 (Adeguito), il fattore di confidenza adottato è: 1,20

Nelle verifiche di sicurezza viene considerato un coefficiente di sicurezza sulle proprietà meccaniche pari a: 2
Nel calcolo dei cinematismi viene considerato l'arretramento del punto di contatto tra i blocchi nei seguenti casi:

- Cinematismi di ribaltamento fuori piano
- Cinematismi di flessione verticale
- Cinematismi di flessione orizzontale

Proprietà meccaniche caratteristiche delle pareti e coefficienti correttivi

Parete n°: 1

Tipologia muraria: Muratura in mattoni pieni e malta di calce

Resistenza media a compressione [MPa]: 3,200

Resistenza a taglio [MPa]: 0,076

Peso specifico [kN/mc]: 18,00

Alla muratura della parete n° 1 vengono applicati i seguenti fattori correttivi definiti nella Tab. C8A.2.2 della Circolare 617 del 2009:

- Fattore correttivo dovuto a Malta buona: 1,50
- Fattore correttivo dovuto a Giunti sottili: 1,50
- Fattore correttivo dovuto a Connessione trasversale: 1,30

Fattore correttivo complessivo delle proprietà meccaniche: 2,93

Parete n°: 2

Tipologia muraria: Muratura in mattoni pieni e malta di calce

Resistenza media a compressione [MPa]: 3,200

Resistenza a taglio [MPa]: 0,076

Peso specifico [kN/mc]: 18,00

Alla muratura della parete n° 2 vengono applicati i seguenti fattori correttivi definiti nella Tab. C8A.2.2 della Circolare 617 del 2009:

- Fattore correttivo dovuto a Malta buona: 1,50
- Fattore correttivo dovuto a Giunti sottili: 1,50
- Fattore correttivo dovuto a Connessione trasversale: 1,30
- Fattore correttivo dovuto a Intonaco armato: 1,50

Fattore correttivo complessivo delle proprietà meccaniche: 4,39

Parete n°: 3

Tipologia muraria: Muratura in mattoni pieni e malta di calce

Resistenza media a compressione [MPa]: 3,200

Resistenza a taglio [MPa]: 0,076

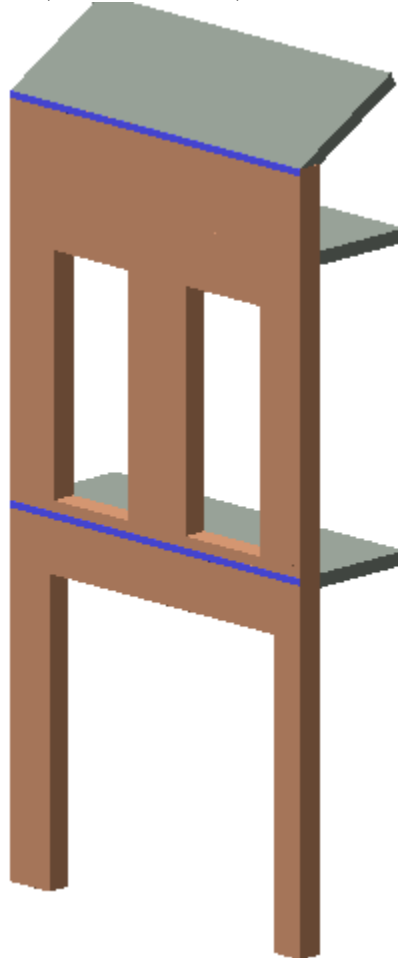
Peso specifico [kN/mc]: 18,00

Proprietà meccaniche delle pareti, valori di progetto:

n°	γ [kN/m ³]	f_{cd} [MPa]	f_{vd} [MPa]
1	18,00	3,900	0,093
2	18,00	5,850	0,139
3	18,00	1,333	0,032

Geometria delle pareti:

n°	Larghezza [m]	Altezza [m]	Spessore [m]	dy_timpano [m]	dz_timpano [m]
1	5,52	5,3	0,37	0,00	0,00
2	5,52	4,5	0,37	0,00	0,00
3	5,52	1,2	0,37	0,00	0,00

**Carichi sulle pareti:****Legenda:**

P_p : peso proprio della parete
 G_k : carico permanente gravante sul solaio della parete
 Q_k : carico variabile gravante sul solaio della parete
 φ_2 : carico variabile gravante sul solaio della parete
 i_s : interasse del solaio
 $G_{k\text{timpano}}$: carico permanente gravante sul solaio del timpano
 $Q_{k\text{timpano}}$: carico variabile gravante sul solaio del timpano
 $\varphi_{2\text{timpano}}$: carico variabile gravante sul solaio del timpano
 i_t : interasse del timpano
 $G_{k\text{falda}}$: carico permanente gravante sul solaio della falda inclinata
 $Q_{k\text{falda}}$: carico variabile gravante sul solaio della falda inclinata
 $\varphi_{2\text{falda}}$: carico variabile gravante sul solaio della falda inclinata
 i_f : interasse della falda

n°	P_p	G_k	Q_k	φ_2	i_s	$G_{k\text{timpano}}$	$Q_{k\text{timpano}}$	$\varphi_{2\text{timpano}}$	i_t	$G_{k\text{falda}}$	$Q_{k\text{falda}}$	$\varphi_{2\text{falda}}$	i_f
----	-------	-------	-------	-------------	-------	-----------------------	-----------------------	-----------------------------	-------	---------------------	---------------------	---------------------------	-------

	[kN]	[kN/m ²]	[kN/m ²]		[m]	[kN/m ²]	[kN/m ²]		[m]	[kN/m ²]	[kN/m ²]		[m]
1	69,40	7,75	3,00	0,60	1,80	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
2	99,60	3,00	0,50	0,00	1,80	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
3	44,85	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	1,20	1,90	0,00	2,00

Carichi sulle pareti ortogonali:

Legenda:

G_{korto}: carico permanente gravante sul solaio delle pareti ortogonali

Q_{korto}: carico variabile gravante sul solaio delle pareti ortogonali

φ_{2orto}: carico variabile gravante sul solaio delle pareti ortogonali

n°:	G _{korto} [kN/m ²]	Q _{korto} [kN/m ²]	φ _{2orto}
1	6,40	3,00	0,60
2	6,40	3,00	0,60
3	6,40	3,00	0,60

Cinematismi:

Cinematismo n°: 1

Tipo: Fles. Verticale singola

Pareti coinvolte: 1,

Quota: 0,00[m]

PGA relativa al cinematismo nel caso di analisi cinematica lineare: 10,4438 [g]

PGA relativa al cinematismo nel caso di analisi cinematica non lineare: 4,3580 [g]

Moltiplicatore di collasso dei carichi orizzontali α₀: 2,426

accelerazione spettrale di attivazione del cinematismo a₀*: 6,266 [g]

Massa partecipante al cinematismo M*: 7 [kN]

Frazione di massa partecipante della struttura e*: 0,323

Risultati della verifica con analisi cinematica lineare allo SLD

Accelerazione di riferimento allo SLD per cinematismo a quota zero: 0,042 [g]

Stato di verifica dell'analisi cinematica lineare allo SLD: **Verificato**

Risultati della verifica con analisi cinematica lineare allo SLV

Accelerazione di riferimento allo SLV per cinematismo a quota zero: 0,039 [g]

Stato di verifica dell'analisi cinematica lineare allo SLV: **Verificato**

Risultati della verifica con analisi cinematica non lineare allo SLV

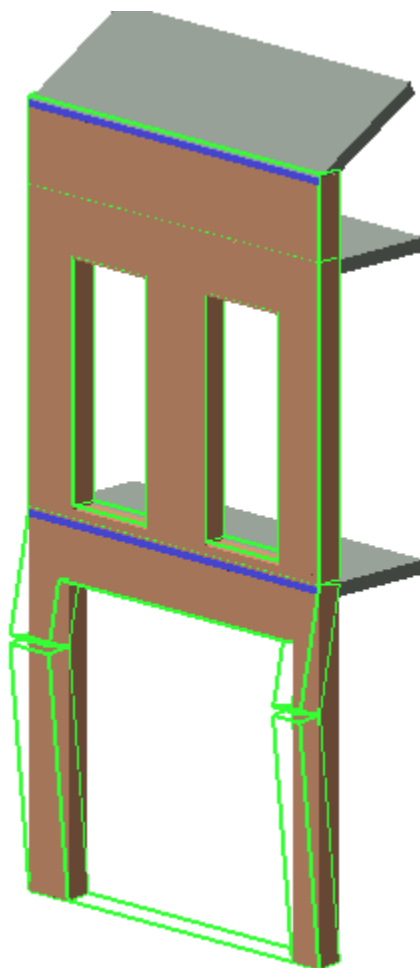
Periodo secante T_s: 0,114[sec]

Spostamento spettrale d_u*: 0,043[m]

Domanda di spostamento nel caso di cinematismo a quota zero Δ_{d, quota zero}: 0,001 [m]

Domanda di spostamento nel caso di cinematismo a quota maggiore di zero Δ_{d, quota sopraelev.}: 0,000 [m]

Stato di verifica dell'analisi cinematica non lineare allo SLV: **Verificato**



Cinematismo n°: 2

Tipo: Fles. Verticale multi

Pareti coinvolte: 2, 3,

Quota: 5,33[m]

Primo modo di vibrare normalizzato ad 1 in sommità dell'edificio $\Psi(Z)$: 0,410

PGA relativa al cinematismo nel caso di analisi cinematica lineare: 0,1742 [g]

PGA relativa al cinematismo nel caso di analisi cinematica non lineare: 0,2751 [g]

Moltiplicatore di collasso dei carichi orizzontali α_0 : 0,091

accelerazione spettrale di attivazione del cinematismo a_0^* : 0,142 [g]

Massa partecipante al cinematismo M^* : 15 [kN]

Frazione di massa partecipante della struttura e^* : 0,532

Risultati della verifica con analisi cinematica lineare allo SLD

Accelerazione di riferimento allo SLD (a quota zero): 0,042 [g]

Accelerazione di riferimento allo SLD (a quota diversa da zero): 0,049 [g]

Stato di verifica dell'analisi cinematica lineare allo SLD: **Verificato**

Risultati della verifica con analisi cinematica lineare allo SLV

Accelerazione di riferimento allo SLV (a quota zero): 0,039[g]

Accelerazione di riferimento allo SLV (a quota diversa da zero): 0,053 [g]

Stato di verifica dell'analisi cinematica lineare allo SLV: **Verificato**

Risultati della verifica con analisi cinematica non lineare allo SLV

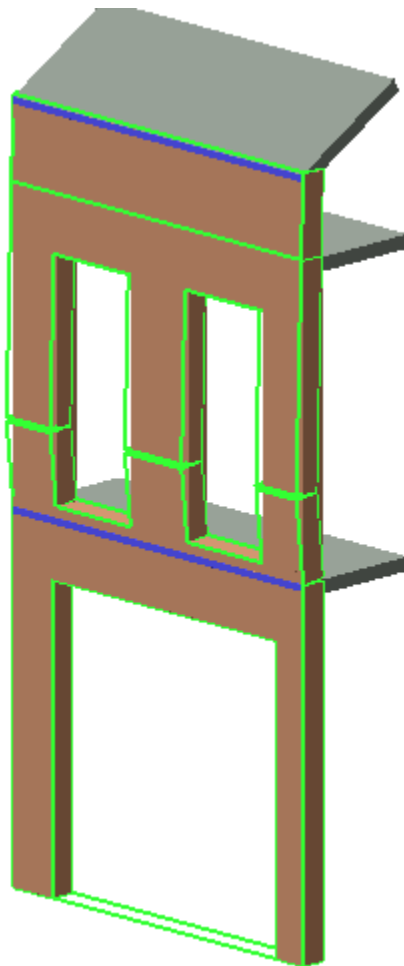
Periodo secante T_s : 1,223[sec]

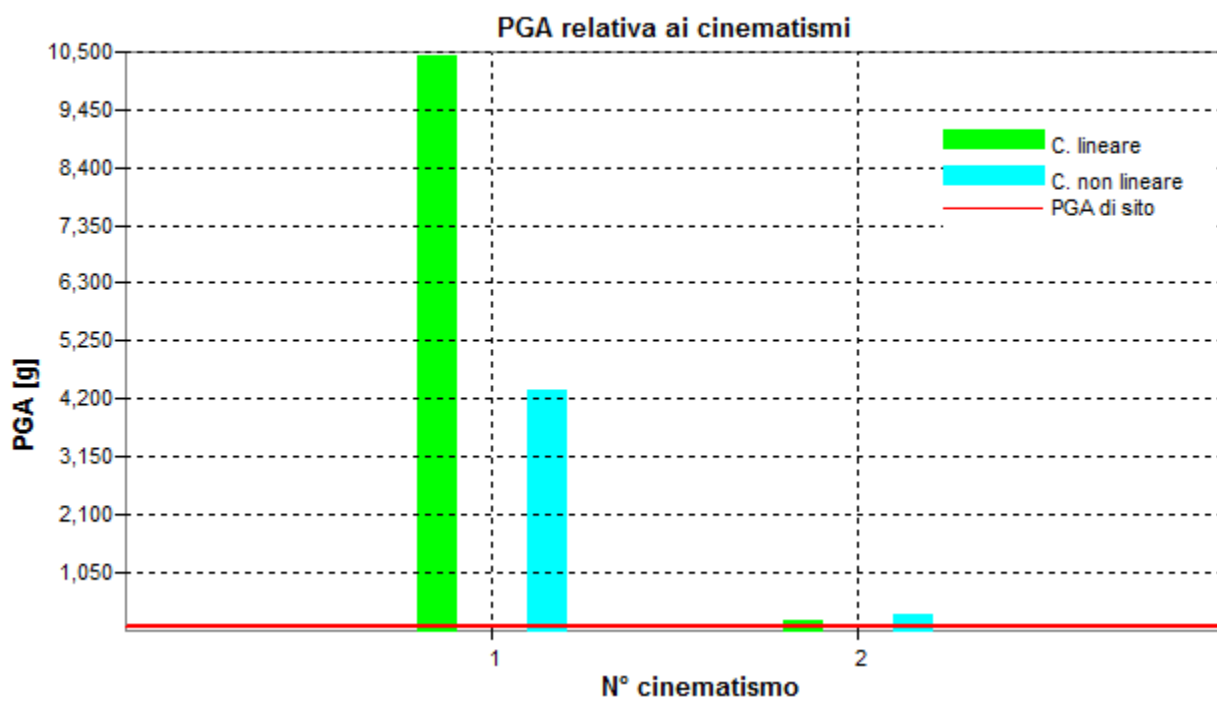
Spostamento spettrale d_u^* : 0,110[m]

Domanda di spostamento nel caso di cinematiso a quota zero $\Delta_{d, \text{ quota zero}}$: 0,026 [m]

Domanda di spostamento nel caso di cinematiso a quota maggiore di zero $\Delta_{d, \text{ quota sopraelev}}$: 0,015 [m]

Stato di verifica dell'analisi cinematica non lineare allo SLV: **Verificato**





Relazione di calcolo Analisi lineare e non lineare dei cinematismi nella muratura

PARETE SUD OVST VANO SCALA – Consolidata con intonaco armato e fascia sommitale in FRP

Relazione di calcolo sulla struttura impostata e redatta secondo le modalità previste dal DM 17/01/2018 NTC cap. 10 'Redazione dei progetti strutturali esecutivi e delle relazioni di calcolo'.

Di seguito si indicano l'origine e le caratteristiche dei codici di calcolo utilizzati riportando titolo, produttore e distributore, versione, estremi della licenza d'uso:

Nome del software:

PRO_CINEm Analisi lineare e non lineare dei cinematismi nella muratura

Versione del software:

v. 2018.04.0044b

Produttore del software:

2 S.I. Software e Servizi per l'Ingegneria s.r.l., Ferrara

Distributore del software:

2 S.I. Software e Servizi per l'Ingegneria s.r.l., Ferrara

Dati utente finale:

.....

Normativa di Riferimento

NTC 2018 e Circolare 617 del 2009

Parametri sismici

Località: NOLE (TO)

Altezza totale dell'edificio: 13,00 m

Vita nominale dell'edificio: 50,00 anni

Coefficiente di struttura: 2,00

Periodo del modo per principale di vibrare (T1): 0,342 sec

Coefficiente di partecipazione modale: γ : 1,20

Categoria di sottosuolo: Tipo B

SLV

Periodo di ritorno per lo SLV (Tr): 712 anni

Probabilità di superamento per lo SLV (Pver): 10 %

Periodo di inizio del tratto a velocità costante per lo SLV (Tc*): 0,280 sec

Accelerazione orizzontale massima al sito per lo SLV (ag): 0,065 g

Fattore di amplificazione dello spettro in accelerazione orizzontale per lo SLV (F0): 2,77

Periodo dello spettro Tb: 0,13 sec

Periodo dello spettro Tc: 0,40 sec

Periodo dello spettro Td: 1,86 sec

Coefficiente di sottosuolo S: 1,20

SLD

Periodo di ritorno per lo SLD (Tr): 75 anni

Probabilità di superamento per lo SLD (P_{ver}): 63 %
 Periodo di inizio del tratto a velocità costante per lo SLD (T_c^{*}): 0,210 sec
 Accelerazione orizzontale massima al sito per lo SLD (a_g): 0,035 g
 Fattore di amplificazione dello spettro in accelerazione orizzontale per lo SLD (F₀) 2,62
 Periodo dello spettro T_b: 0,11 sec
 Periodo dello spettro T_c: 0,32 sec
 Periodo dello spettro T_d: 1,74 sec
 Coefficiente di sottosuolo S: 1,20

Livello di conoscenza e coefficiente di sicurezza

In relazione alle indagini svolte e alla documentazione acquisita il livello di conoscenza è di tipo LC2 (Adeguito), il fattore di confidenza adottato è: 1,20

Nelle verifiche di sicurezza viene considerato un coefficiente di sicurezza sulle proprietà meccaniche pari a: 2

Nel calcolo dei cinematismi viene considerato l'arretramento del punto di contatto tra i blocchi nei seguenti casi:

- Cinematismi di ribaltamento fuori piano
- Cinematismi di flessione verticale
- Cinematismi di flessione orizzontale

Proprietà meccaniche caratteristiche delle pareti e coefficienti correttivi

Parete n°: 1

Tipologia muraria: Muratura in mattoni semipieni e malta cementizia (es. doppio UNI perc. for.<40%)

Resistenza media a compressione [MPa]: 6,500

Resistenza a taglio [MPa]: 0,280

Peso specifico [kN/mc]: 15,00

Parete n°: 2

Tipologia muraria: Muratura in mattoni semipieni e malta cementizia (es. doppio UNI perc. for.<40%)

Resistenza media a compressione [MPa]: 6,500

Resistenza a taglio [MPa]: 0,280

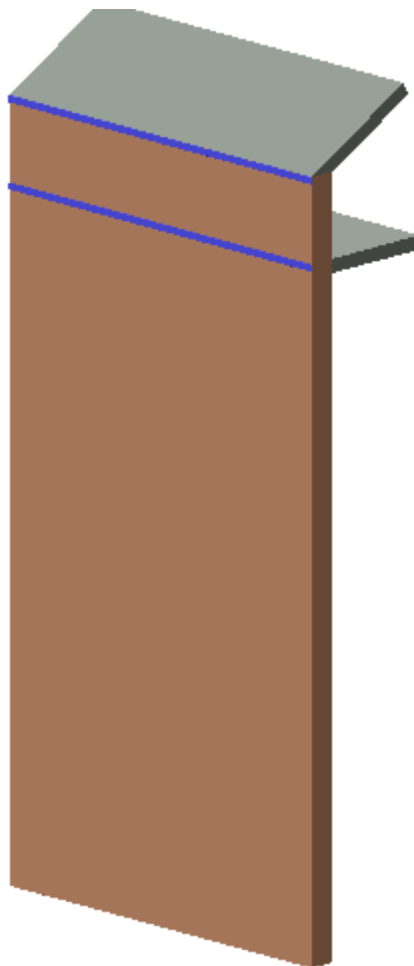
Peso specifico [kN/mc]: 15,00

Proprietà meccaniche delle pareti, valori di progetto:

n°	γ [kN/m ³]	f_{cd} [MPa]	f_{vd} [MPa]
1	15,00	2,708	0,117
2	15,00	2,708	0,117

Geometria delle pareti:

n°	Larghezza [m]	Altezza [m]	Spessore [m]	dy_timpano [m]	dz_timpano [m]
1	5,76	9,8	0,40	0,00	0,00
2	5,76	1,2	0,40	0,00	0,00



Carichi sulle pareti:

Legenda:

P_p : peso proprio della parete

G_k : carico permanente gravante sul solaio della parete

Q_k : carico variabile gravante sul solaio della parete

φ_2 : carico variabile gravante sul solaio della parete

i_s : interasse del solaio

$G_{k\text{timp}}$: carico permanente gravante sul solaio del timpano

$Q_{k\text{timp}}$: carico variabile gravante sul solaio del timpano

$\varphi_{2\text{timp}}$: carico variabile gravante sul solaio del timpano

i_t : interasse del timpano

$G_{k\text{falda}}$: carico permanente gravante sul solaio della falda inclinata

$Q_{k\text{falda}}$: carico variabile gravante sul solaio della falda inclinata

$\varphi_{2\text{falda}}$: carico variabile gravante sul solaio della falda inclinata

i_f : interasse della falda

n°	P_p [kN]	G_k [kN/m²]	Q_k [kN/m²]	φ_2	i_s [m]	$G_{k\text{timp}}$ [kN/m²]	$Q_{k\text{timp}}$ [kN/m²]	$\varphi_{2\text{timp}}$	i_t [m]	$G_{k\text{falda}}$ [kN/m²]	$Q_{k\text{falda}}$ [kN/m²]	$\varphi_{2\text{falda}}$	i_f [m]
1	340,07	3,00	0,50	0,00	1,85	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00
2	42,16	0,00	0,00	0,00	0,00	0,00	0,00	0,00	0,00	1,20	1,90	0,00	2,00

Carichi sulle pareti ortogonali:

Legenda:

G_{korto} : carico permanente gravante sul solaio delle pareti ortogonali

Q_{korto} : carico variabile gravante sul solaio delle pareti ortogonali

ϕ_{2orto} : carico variabile gravante sul solaio delle pareti ortogonali

n°:	G_{korto} [kN/m ²]	Q_{korto} [kN/m ²]	ϕ_{2orto}
1	0,00	0,00	0,00
2	0,00	0,00	0,00

Cinematismi:

Cinematismo n°: 1

Tipo: Fles. Verticale singola

Pareti coinvolte: 1,

Quota: 0,00[m]

PGA relativa al cinematismo nel caso di analisi cinematica lineare: 0,2743 [g]

PGA relativa al cinematismo nel caso di analisi cinematica non lineare: 0,2250 [g]

Moltiplicatore di collasso dei carichi orizzontali α_0 : 0,174

accelerazione spettrale di attivazione del cinematismo a_0^* : 0,165 [g]

Massa partecipante al cinematismo M^* : 35 [kN]

Frazione di massa partecipante della struttura e^* : 0,881

Risultati della verifica con analisi cinematica lineare allo SLD

Accelerazione di riferimento allo SLD per cinematismo a quota zero: 0,042 [g]

Stato di verifica dell'analisi cinematica lineare allo SLD: **Verificato**

Risultati della verifica con analisi cinematica lineare allo SLV

Accelerazione di riferimento allo SLV per cinematismo a quota zero: 0,039 [g]

Stato di verifica dell'analisi cinematica lineare allo SLV: **Verificato**

Risultati della verifica con analisi cinematica non lineare allo SLV

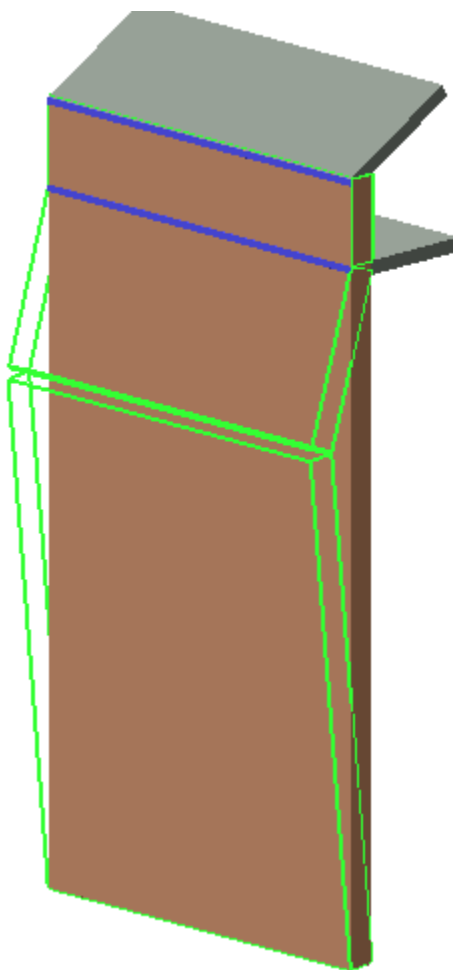
Periodo secante T_s : 0,858[sec]

Spostamento spettrale d_u^* : 0,063[m]

Domanda di spostamento nel caso di cinematismo a quota zero $\Delta_{d, \text{ quota zero}}$: 0,018 [m]

Domanda di spostamento nel caso di cinematismo a quota maggiore di zero $\Delta_{d, \text{ quota sopraelev}}$: 0,000 [m]

Stato di verifica dell'analisi cinematica non lineare allo SLV: **Verificato**



Cinematismo n°: 2

Tipo: Fles. Verticale singola

Pareti coinvolte: 2,

Quota: 9,84[m]

Primo modo di vibrare normalizzato ad 1 in sommità dell'edificio $\Psi(Z)$: 0,757

PGA relativa al cinematismo nel caso di analisi cinematica lineare: 1,9317 [g]

PGA relativa al cinematismo nel caso di analisi cinematica non lineare: 0,9844 [g]

Moltiplicatore di collasso dei carichi orizzontali α_0 : 1,678

accelerazione spettrale di attivazione del cinematismo a_0^* : 2,916 [g]

Massa partecipante al cinematismo M^* : 4 [kN]

Frazione di massa partecipante della struttura e^* : 0,480

Risultati della verifica con analisi cinematica lineare allo SLD

Accelerazione di riferimento allo SLD (a quota zero): 0,042 [g]

Accelerazione di riferimento allo SLD (a quota diversa da zero): 0,091 [g]

Stato di verifica dell'analisi cinematica lineare allo SLD: **Verificato**

Risultati della verifica con analisi cinematica lineare allo SLV

Accelerazione di riferimento allo SLV (a quota zero): 0,039[g]

Accelerazione di riferimento allo SLV (a quota diversa da zero): 0,098 [g]

Stato di verifica dell'analisi cinematica lineare allo SLV: **Verificato**

Risultati della verifica con analisi cinematica non lineare allo SLV

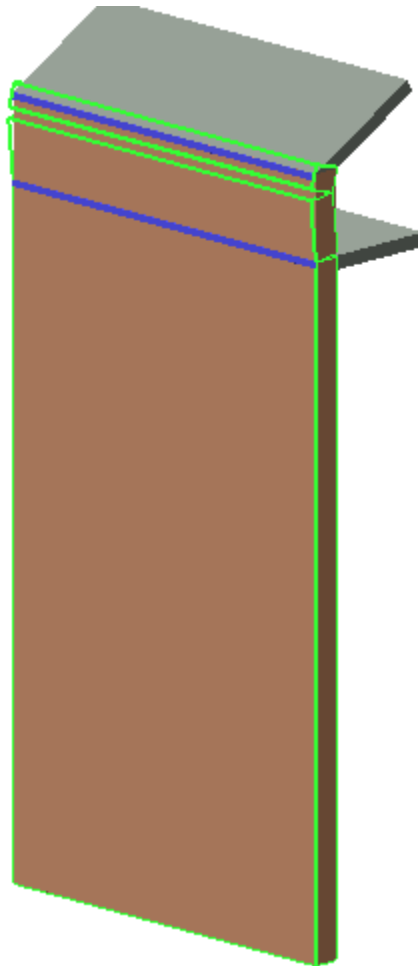
Periodo secante T_s : 0,192[sec]

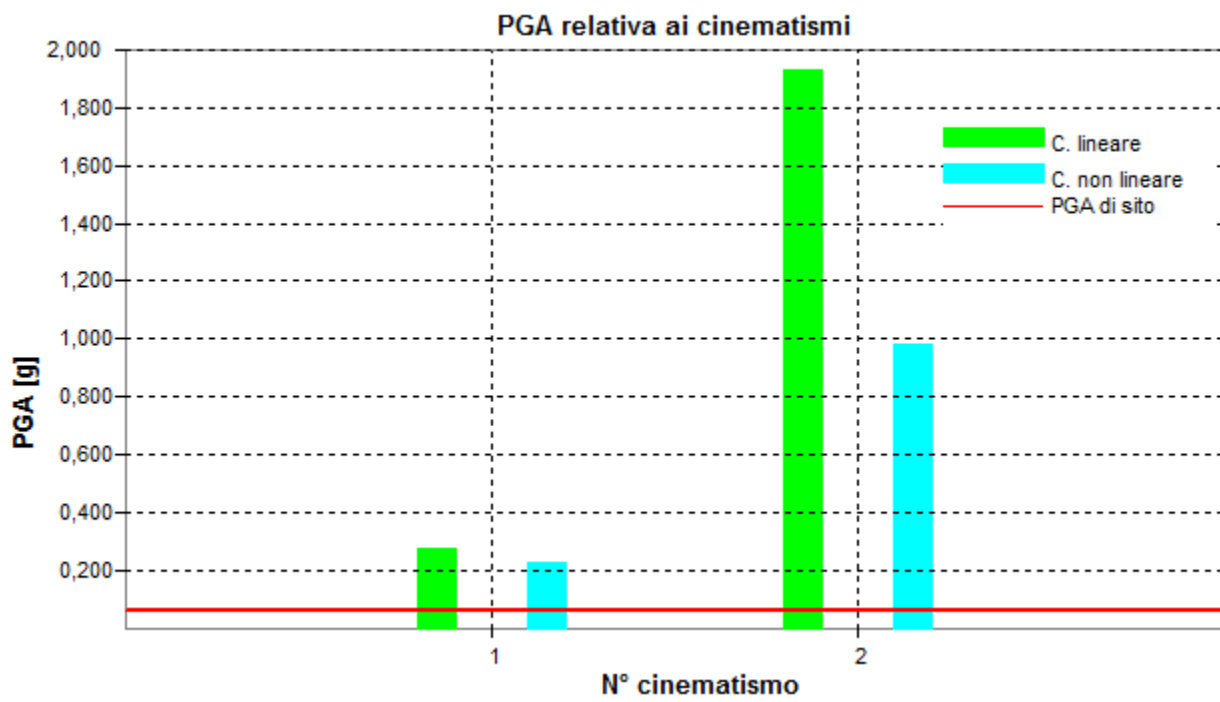
Spostamento spettrale d_u^* : 0,060[m]

Domanda di spostamento nel caso di cinematiso a quota zero $\Delta_{d, \text{ quota zero}}$: 0,002 [m]

Domanda di spostamento nel caso di cinematiso a quota maggiore di zero $\Delta_{d, \text{ quota sopraelev}}$: 0,004 [m]

Stato di verifica dell'analisi cinematica non lineare allo SLV: **Verificato**





SCHEDA DI SINTESI RISULTATI VERIFICA SISMICA SCUOLA VAUDA
VIA PONTE MASINO 1 - COMUNE DI NOLE (TO)

E' stato fatto un confronto tra i risultati otteniti dall'analisi dinamica lineare nella situazione corrispondente allo stato di fatto e con un 'accelerazione sismica pari all'1%, e l'ipotesi progettuale con un'accelerazione attesa al suolo pari al 60% al fine di ottemperare a quanto richiesto dal par. 8.4.2. per le costruzioni esistenti ad uso scolastico.

Le verifiche sismiche sono state svolte sia nei confronti di quanto richiesto dal par. 7.8.2.2. NTC 2018 (verifiche a pressoflessione nel piano e fuori dal piano, taglio e travi in muratura), sia nei confronti dei cinematismi fuori dal piano.

Vita nominale	50 anni
Classe d'uso	III
Fattore di confidenza	1,2

Le verifiche si intendono positive se < 1

Verifiche par. 7.8.2.2.	Stato di fatto (0,01 a_g)	Miglioramento sismico (0,6 a_g)
Pressoflessione nel piano	137,55	0,86
Pressoflessione fuori dal piano	70,30	0,99
Taglio	5,65	0,78
Taglio per travi in muratura	2,20	0,99
Momento per travi in muratura	0,58	0,18

Tabella di sintesi risultati verifiche cinematismi fuori dal piano (le verifiche si intendono positive se < 1)

PARETE	CINEMATISMI	PARETI	$\alpha = a_0^* / a_{g \text{ rif SLV}}$ STATO DI FATTO	$\alpha = a_0^* / a_{g \text{ rif SLV}}$ MIGLIORAMENTO
Nord - Est	Flessione verticale singola	1	17,25	18,31
	Ribaltamento multiplo	2, 3	0,00	NON ATTIVABILE
	Ribaltamento singolo	3	0,00	NON ATTIVABILE
	Flessione verticale multipla	2, 3	NON ATTIVABILE	1,4
Nord - Ovest	Flessione verticale singola	1	51,69	53,82
	Ribaltamento multiplo	2, 3	0,00	NON ATTIVABILE
	Ribaltamento singolo	3	0,00	NON ATTIVABILE
	Flessione verticale multipla	2, 3	NON ATTIVABILE	2,36
Sud - Est	Flessione verticale singola	1	19046,69	19046,69

	Flessione verticale singola	2	293,90	1273,55
	Ribaltamento multiplo	3, 4	0,00	NON ATTIVABILE
	Flessione verticale multipla	2, 3	NON ATTIVABILE	5,11
Parete Sud – Est Vano scala	Ribaltamento multiplo	1, 2, 3, 4	0,00	NON ATTIVABILE
	Ribaltamento multiplo	2, 3, 4	0,00	NON ATTIVABILE
	Ribaltamento multiplo	3, 4	0,00	NON ATTIVABILE
	Ribaltamento singolo	4	0,19	NON ATTIVABILE
	Flessione verticale multipla	1, 2, 3, 4	NON ATTIVABILE	1,07
Parete Sud – Ovest	Flessione verticale singola	1	160,67	190,45
	Ribaltamento multiplo	2, 3	0,00	NON ATTIVABILE
	Ribaltamento singolo	3	0,00	NON ATTIVABILE
	Flessione verticale multipla	2, 3	NON ATTIVABILE	2,68
Parete Sud – Ovest Vano scala	Flessione verticale singola	1	3,92	4,23
	Ribaltamento singolo	2	0,00	NON ATTIVABILE
	Flessione verticale singola	2	NON ATTIVABILE	29,75